



Run-On and Run-Off Control Plan
OML Existing Landfill
OML Expansion Phase 1

Ottumwa-Midland Landfill

Prepared for:

Interstate Power and Light Company

Ottumwa-Midland Landfill
15300 130th Street
Ottumwa, Iowa 52501

Prepared by:

SCS ENGINEERS

2830 Dairy Drive
Madison, Wisconsin 53718-6751
(608) 224-2830

September 2016
File No. 25216110.00

Offices Nationwide
www.scsengineers.com

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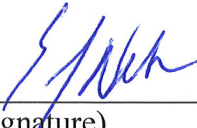
Appendix

- A Drainage Design Calculations

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PE CERTIFICATION

	I, Eric J. Nelson, hereby certify that this Run-On and Run-Off Control Plan meets the requirements of 40 CFR 257.81(c), was prepared by me or under my direct supervision, and that I am a duly licensed Professional Engineer under the laws of the State of Iowa.	
	 (signature)	<u>9/29/16</u> (date)
	<u>ERIC J. NELSON</u> (printed or typed name)	
	License number <u>23136</u>	
	My license renewal date is <u>DECEMBER 31, 2016</u> .	
Pages or sheets covered by this seal: <u>SEPTEMBER 2016 Run-On and Run-Off Control Plan</u> <u>IPL OML</u>		

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1.0 INTRODUCTION AND PROJECT SUMMARY

On behalf of Interstate Power and Light Company (IPL), SCS Engineers (SCS) has prepared this Run-on and Run-off Control Plan for the Ottumwa-Midland Landfill (OML) in accordance with 40 CFR 257.81(c) as follows.

40 CFR 257.81(c)(1). *“The owner or operator must prepare initial and periodic run-on and run-off control system plans for the CCR unit according to the timeframes specified in paragraphs (c)(3) and (4) of this section. These plans must document how the run-on and run-off control systems have been designed and constructed to meet the applicable requirement of this section. Each plan must be supported by appropriate engineering calculations. The owner or operator has completed the initial run-on and run-off control system plan when the plan has been placed in the facility’s operating record as required by section 257.105(g)(3).”*

The OML Landfill includes an active coal combustion residue (CCR) landfill, which currently consists of two existing CCR landfill units:

- OML Existing (Original) Landfill
- OML Expansion Phase 1

Five future CCR units (OML Expansion Phases 2, 3, 4, 5, and 6) are permitted with the Iowa Department of Natural Resources (IDNR), but have not been developed. When developed, the future units will be new CCR landfills, as defined by 40 CFR 257.53. Future CCR units are not addressed by this plan and are not discussed further herein.

Refer to **Figure 1** for the site location. **Figure 2** shows the run-on and run-off drainage areas.

2.0 RUN-ON AND RUN-OFF CONTROL PLAN

40 CFR 257.81(a). *“The owner or operator of an existing or new CCR landfill or any lateral expansion of a CCR landfill must design, construct, operate, and maintain:*

- (1) A run-on control system to prevent flow onto the active portion of the CCR unit during the peak discharge from a 24-hour, 25-year storm.”*

The entire facility has run-on and run-off control in place, as approved by the IDNR. Run-on is controlled by berms and swales around the perimeter of the landfill that divert storm water away from the landfill and to detention basins or natural drainage features.

- (2) “A run-off control system from the active portion of the CCR unit to collect and control at least the water volume resulting from a 24-hour, 25-year storm.”*

Run-off from the active portions of the existing OML landfill is handled as contact water and is collected by a leachate collection system, which routes the contact water to a sump, where the contact water is then pumped to a concrete-lined leachate lagoon. Run-off from the active

portions of the expansion Phase 1 is handled as contact water and is collected by a leachate collection system which routes the contact water to either the sump or to a lined contact water basin. The contact water in the leachate lagoon and contact water basin is used for ash conditioning and other applications within the CCR unit. If needed, excess water in the leachate lagoon and contact water basin is pumped into a tanker truck and taken to the Ottumwa Generating Station (OGS) Main Ash Pond. Wastewater from the OGS Main Ash Pond discharges through an outfall regulated by a National Pollutant Elimination System (NPDES) permit. Per 257.81(b), this is consistent with the surface water requirements under 40 CFR 257.3-3.

Run-off from areas of the existing CCR units with intermediate or future final cover will be diverted into perimeter drainage swales, which drain to sedimentation basins. Intermediate swales/berms, downslope flumes, and energy dissipators on the proposed final cover help minimize erosion of the intermediate cover. These features divert water to the perimeter drainage system, and ultimately to the sedimentation basins.

In addition to these controls, a rain cover has been installed to limit contact water production in Phase 1. Storm water collected on the rain cover is diverted to perimeter swales, and ultimately to a sedimentation basin. The rain cover will be removed in sections to accommodate waste placement. As the rain cover is removed, new diversion berms will be constructed to form the perimeter of a storm water containment area. The berms will prevent contact water from running onto the rain cover and will anchor or ballast the rain cover at the new limits.

2.1 DESIGN CRITERIA

The storm water features described above are designed to handle run-on and run-off from a 25-year, 24-hour storm event, as required by 40 CFR 257.81(a)(1) and (2). The precipitation depth of the 25-year, 24-hour storm event was assumed to be 5.67 inches, based on Technical Paper-40 (TP-40) precipitation data published in May 1961. The sedimentation basin outlet structures are designed to safely pass run-off from a 100-year, 24 hour storm event.

2.2 DESIGN WITH CALCULATIONS

Storm water management and contact water management design calculations (as described above) from the IDNR approved permit amendment are contained in **Appendix A**. As described in **Section 2.1**, the calculations show that the run-on and run-off control systems will control the water volume resulting from a 25-year, 24-hour storm. The calculations were performed, or overseen by, a professional engineer licensed in the State of Iowa.

2.3 CONSTRUCTION

Existing storm water management features were constructed to site specifications with construction oversight directed by a professional engineer licensed in the State of Iowa. Construction documentation reports for the storm water management features were prepared, submitted to the IDNR, and approved by the IDNR.

3.0 CERTIFICATIONS

40 CFR 257.81(c)(5). *“The owner or operator must obtain a certification from a qualified professional engineer stating that the initial and periodic run-on and run-off control system plans meet the requirements of this section.”*

Eric Nelson, PE, a licensed profession engineer in the State of Iowa, has overseen the preparation of this Run-on and Run-off Control Plan. A certification statement is provided on **page iii** of this plan.

4.0 RECORDKEEPING AND PERIOD UPDATES

40 CFR257.81(d). *“The owner or operator of the CCR unit must comply with the recordkeeping requirements specified in section 257.105(g), the notification requirements specified in section 257.106(g), and the internet requirements specified in section 257.107(g)”*

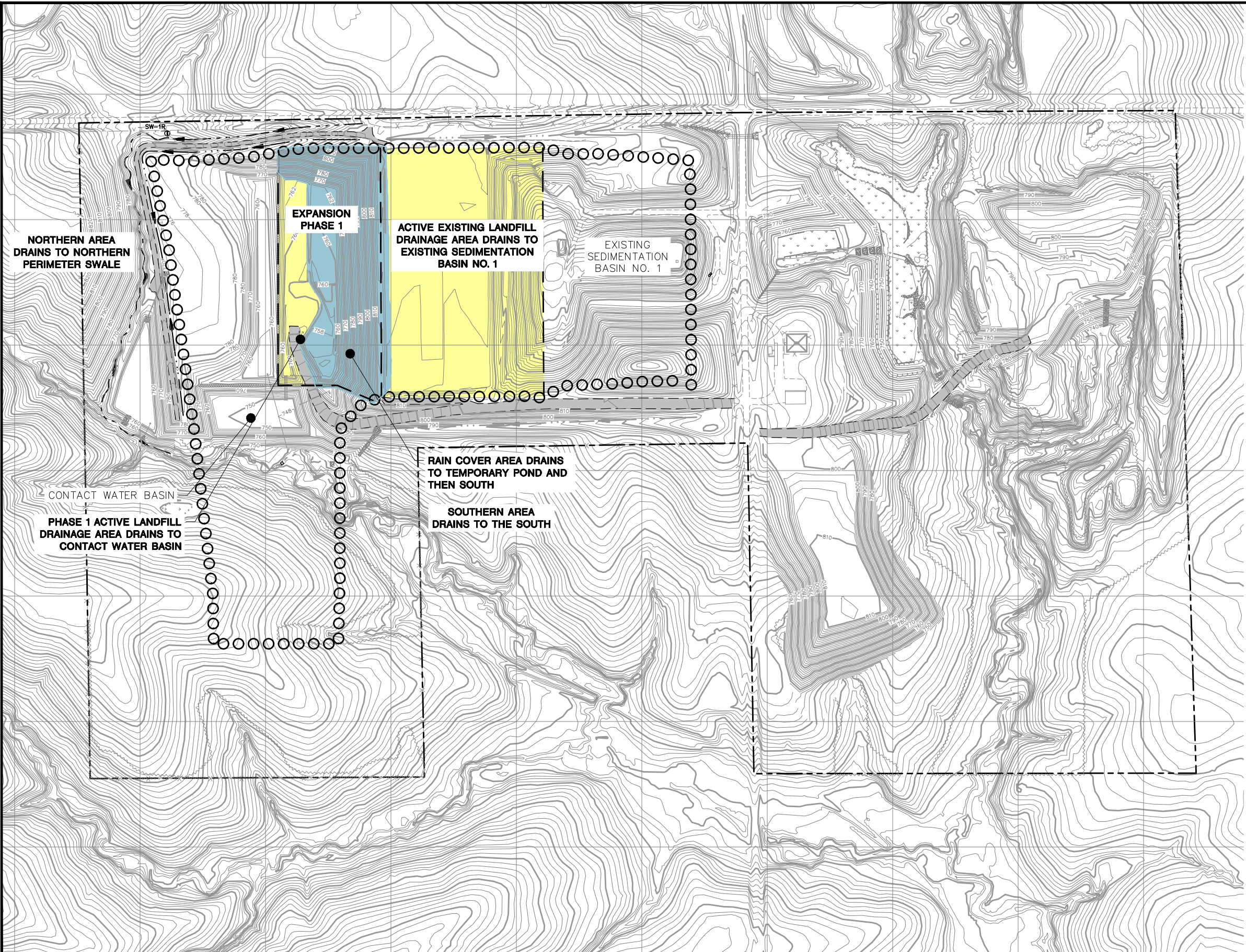
This Run-On and Run-Off Control Plan, and all periodic plans, will be placed in the facility’s operating record and on Alliant Energy’s CCR Rule Compliance Data and Information website, as will all amendments. Periodic plans will be completed every 5 years per 40 CFR 257.81(c)(4).

Notification will be provided when this Run-On and Run-Off Control Plan, and all periodic plans, are available in the facility’s operating record and on the facility’s website per 40 CFR 257.105(g), 257.106(g), and 257.107(g).

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FIGURES

- 1 Site Location Map
- 2 Run-On/Run-Off Control Plan



- LEGEND
- PROPERTY LINE
 - ○ ○ ○ ○ ○ · EXISTING LIMITS OF WASTE
 - PHASE LIMITS
 - ~~~~~ TREE/SHRUB LINE
 - 770 — EXISTING GROUND SURFACE (10' CONTOUR)
 - — — EXISTING GROUND SURFACE (2' CONTOUR)
 - X — X — X — FENCE
 - ○ ○ ○ ○ WETLAND
 - — — — — STREAM FLOW LINE
 - — — — — DITCH FLOW LINE
 - GRAVEL LIMITS
 - X — X — EXISTING CULVERT
 - ACTIVE LANDFILL DRAINAGE AREA
 - RAIN COVER DRAINAGE AREA

N



SCALE: 1" = 400'

PROJECT NO.	25216110.00	DRAWN BY:	AHB	ENGINEER SCS ENGINEERS 2830 DAIRY DRIVE MADISON, WI 53718-6751 PHONE: (608) 224-2830	CLIENT INTERSTATE POWER AND LIGHT COMPANY OTTUMWA MIDLAND LANDFILL 15300 130TH STREET OTTUMWA, IOWA 52501	SITE RUN-ON AND RUN-OFF CONTROL PLAN OTTUMWA MIDLAND LANDFILL OTTUMWA, IOWA	RUN-ON AND RUN-OFF CONTROL PLAN	FIGURE
DRAWN:	12/09/13	CHECKED BY:	JO					2
REVISED:	09/10/16	APPROVED BY:	EN 09/26/16					

APPENDIX A

Drainage Design Calculations

Job No. 25211509.03

CALC. NO.

Job: OML Expansion

REV. NO.

Client IPL

BY BLP DATE 11/26/13

Subject Contact Water Management Calculations

CHK'D. MRH DATE 11/27/13

Contact Water Management Calculations

Purpose:

To estimate the amount of contact water runoff during each phase of development and accordingly size the following contact water management features:

- Temporary contact water basins
- Temporary contact water basin culverts
- Perimeter contact water diversion berms to route the contact water runoff to the contact water basins

Approach:*Hydrograph Generation*

To properly size the contact water management features, runoff hydrographs for the 25-year, 24-hour storm event were developed. HydroCAD was used to model the storm water management system and develop the hydrographs using TR-20 methodologies. The model is designed to simulate the surface runoff response of a watershed to a precipitation event. Input parameters for the model include precipitation depth for the design storm event, contributing drainage areas, runoff curve numbers, time of concentration, and travel time.

Figures H-1 through H-6 show the drainage areas modeled for each phase of development.

Contact Water Basin Sizing

The contact water basins were sized for the 25-year, 24-hour storm event by routing the runoff hydrographs through the ponds using HydroCAD. HydroCAD utilizes the hydrographs (as determined by the Hydrograph Generation calculations) along with the input pond capacity to determine the peak water elevation in the pond.

Contact water will be stored in the ponds for CCR conditioning/dust suppression. To ensure that the contact water basins are operated properly, charts were developed to show the relationship between remaining capacities of the basins based on current water level and additional rainfall in inches. The charts are attached to this calculation and are also presented in the Operations Manual.

Contact Water Basin Culvert Sizing

The culverts routing contact water runoff from the active phase to the contact water basin were sized for the 25-year, 24-hour storm event using the HY-8 computer model developed by the US Department of Transportation, Federal Highway Administration.

Contact Water Perimeter and Interior Diversion Berm/Swale Sizing

The perimeter and interior swales were sized for the 25-year, 24-hour storm event using Manning's equation to determine the depth of flow and velocity in the swale based on the

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swale geometry and peak flow in the swale (as determined by the Hydrograph Generation calculations).

Key Assumptions:

- The runoff curve number for in-place ash was assumed to be 98, which is representative of paved areas.
- The precipitation depth for a 25-year, 24-hour storm event was assumed to be 5.67 inches, based on Bulletin 71, Rainfall Frequency Atlas of the Midwest (1992).
- The contact water basin volumes were computed based on top of leachate drainage layer and contact basin stone (i.e., no storage volume provided within these layers).
- Other assumptions are included with the attached calculations.

Results:

The proposed contact water management features are adequately sized to manage the contact water runoff resulting from a 25-year, 24-hour storm event during each phase of development, as further described below. Refer to the calculations section of this attachment for the detailed input and output.

Contact Water Basin Sizing

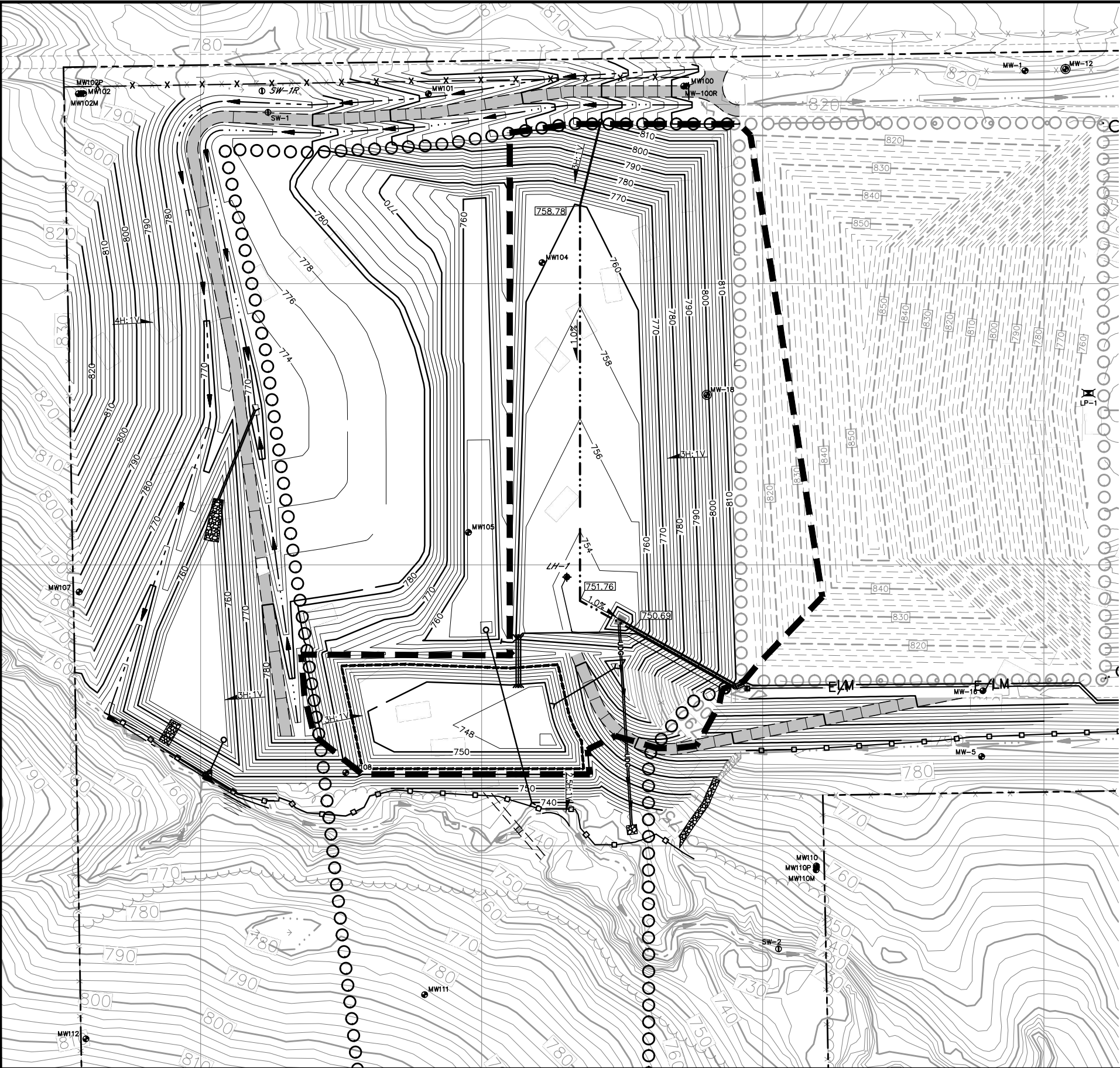
The temporary contact water basins will be lined to the elevations shown on the Expansion Permit Amendment design drawings. The liner limits shown provide a minimum 0.5 foot of freeboard for the runoff from a 25-year, 24-hour storm event.

Contact Water Basin Culvert Sizing

The temporary contact water basin culverts are adequately sized to route contact water runoff from the active phase area to the temporary contact water basin for a 25-year, 24-hour storm event without overtopping the phase delineation berm. The culvert sizes, lengths and inverts are as shown on the Expansion Permit Amendment design drawings.

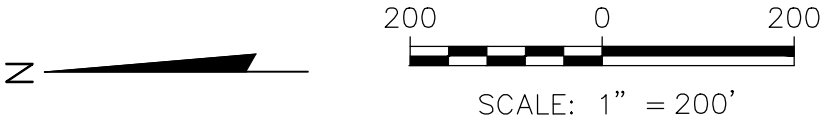
Contact Water Perimeter and Interior Diversion Berm/Swale Sizing

The perimeter and interior contact water diversion berms are adequately sized to route contact water runoff resulting from a 25-year, 24-hour storm event without overtopping the berms. The perimeter contact water diversion berm design is as shown on the Expansion Permit Amendment design drawings.

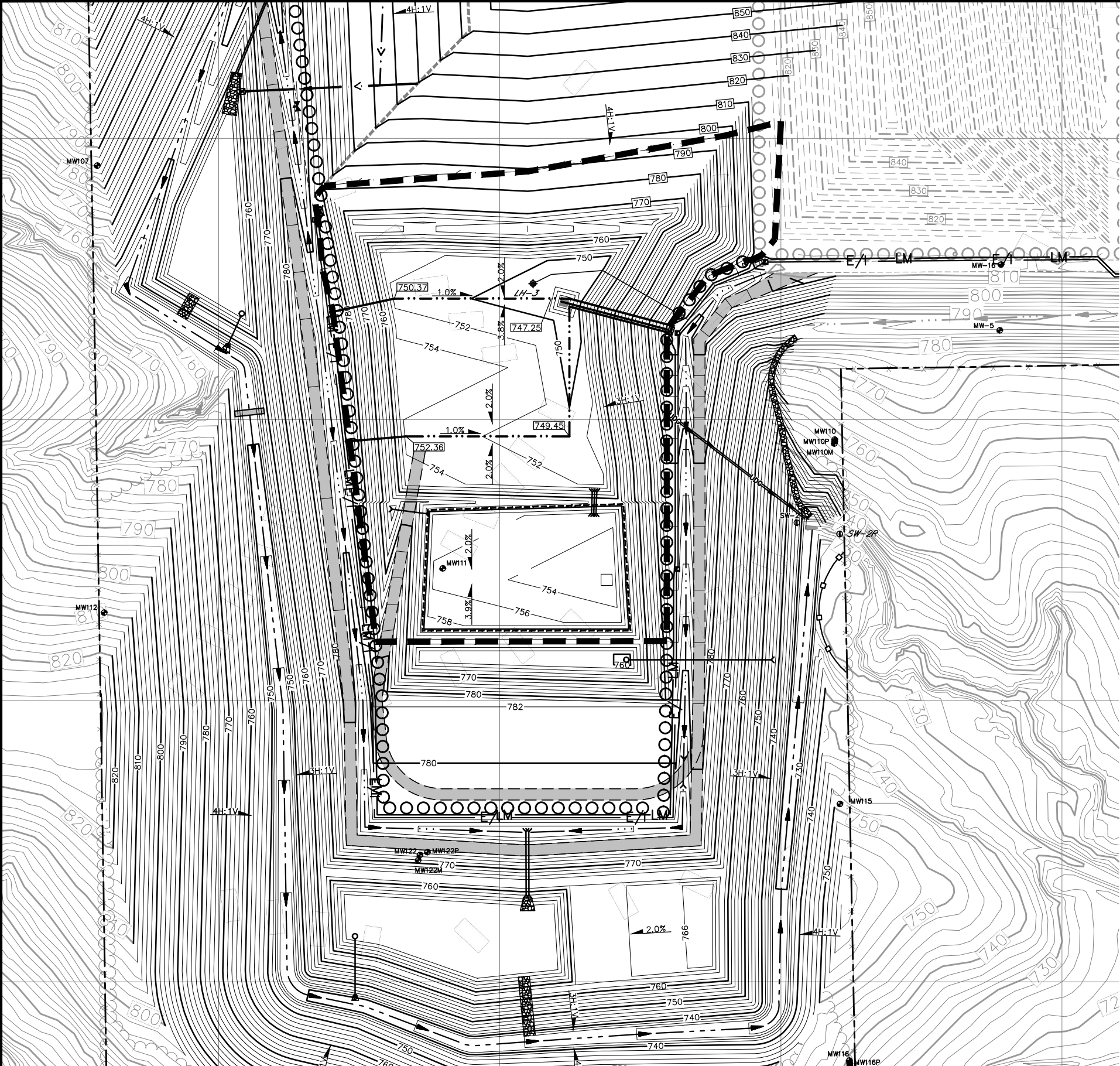


LEGEND

CONTACT WATER BASIN DRAINAGE AREA = 13.9 ACRES

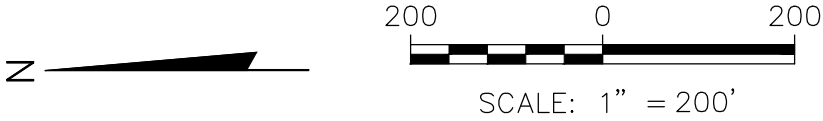


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LEGEND

--- CONTACT WATER BASIN DRAINAGE AREA = 12.2 ACRES



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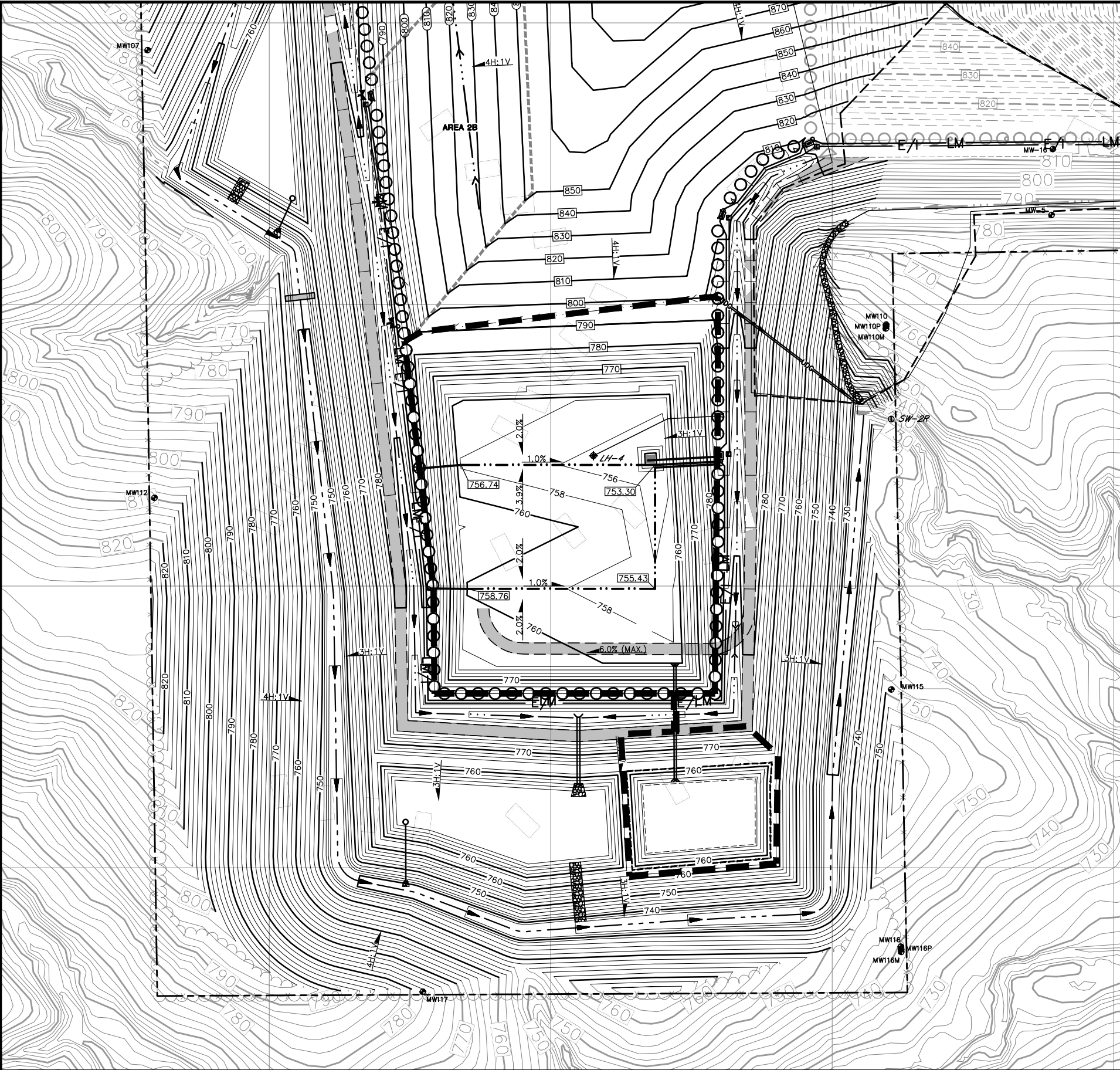
SCS ENGINEERS
2830 DAIRY DRIVE MADISON, WI 53718-6751
PHONE: (608) 224-2830

CLIENT
INTERSTATE POWER AND LIGHT COMPANY
OTTUMWA MIDLAND LANDFILL
130TH STREET
OTTUMWA, IOWA 52501

SITE
PERMIT AMENDMENT PLANS
NORTH & SOUTH EXPANSION
OTTUMWA MIDLAND LANDFILL
OTTUMWA, IOWA

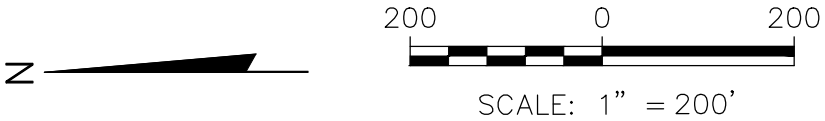
PHASE 3 CONTACT WATER BASIN
DRAINAGE AREA

FIGURE
H-3

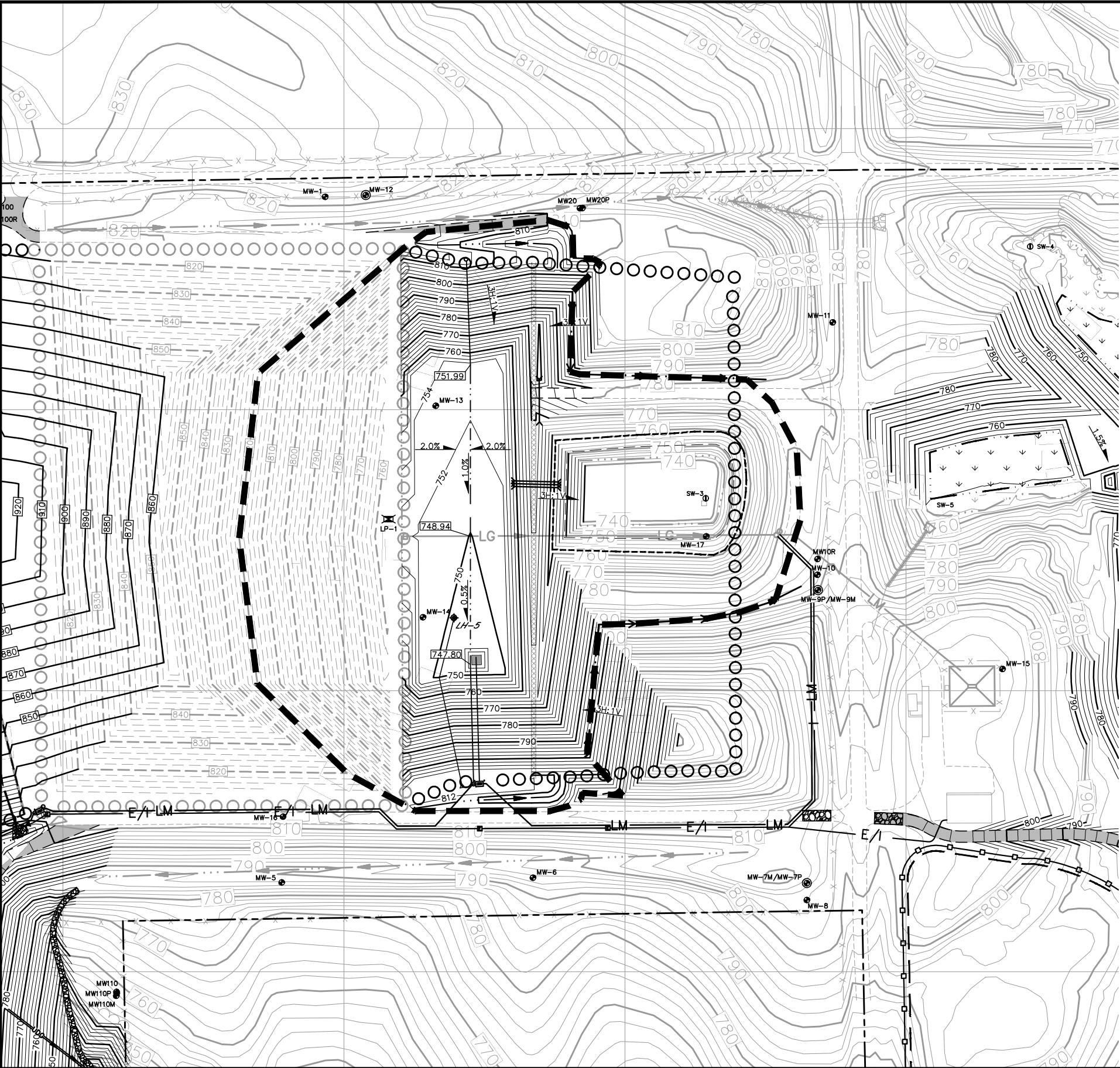


LEGEND

--- CONTACT WATER BASIN DRAINAGE AREA = 9.6 ACRES

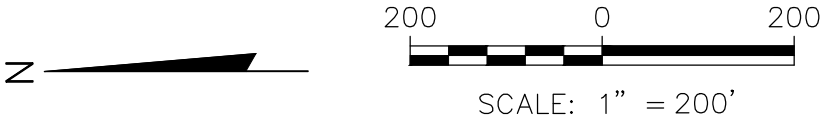


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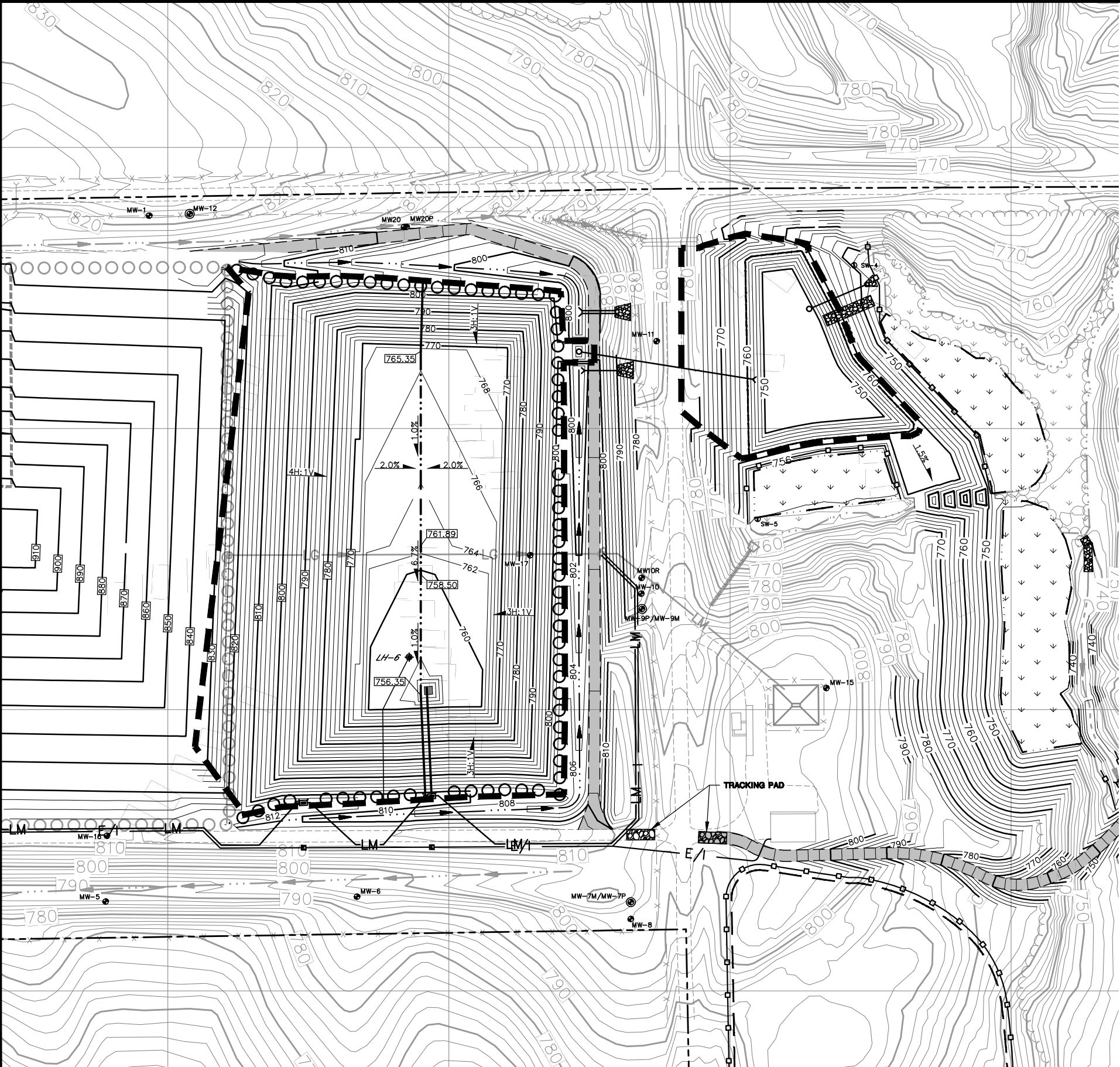


LEGEND

CONTACT WATER BASIN DRAINAGE AREA = 16.1 ACRES

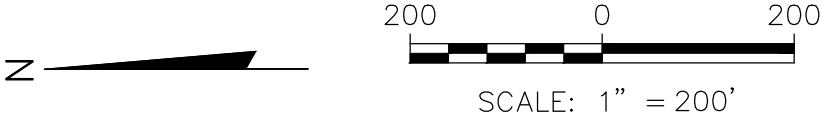


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REVISED:	11/21/13	APPROVED BY:	BP 11/27/13					



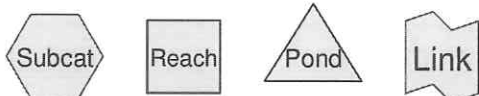
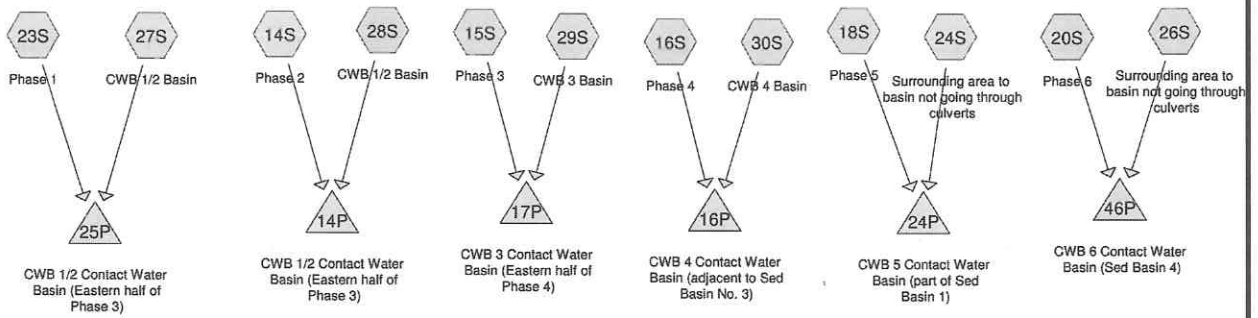
LEGEND

--- CONTACT WATER BASIN DRAINAGE AREA = 15.6 ACRES



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Contact Water Basin Sizing



Drainage Diagram for Contact Water Runoff Calcs and Basin Sizing_131126
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Contact Water Runoff Calcs and Basin Sizing_131126

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Page 2

Area Listing (selected nodes)

Area (acres)	CN	Description (subcatchment-numbers)
6.120	74	>75% Grass cover, Good, HSG C (24S,26S)
71.066	98	Ash (14S,15S,16S,18S,20S,23S)
5.900	98	Basin (27S,28S,29S,30S)
1.500	98	Basin area (26S)
1.200	98	basin area (24S)
85.786		TOTAL AREA

Contact Water Runoff Calcs and Basin Sizing_131126

Prepared by SCS Engineers

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Page 3

Soil Listing (selected nodes)

Area (acres)	Soil Group	Subcatchment Numbers
0.000	HSG A	
0.000	HSG B	
6.120	HSG C	24S, 26S
0.000	HSG D	
79.666	Other	14S, 15S, 16S, 18S, 20S, 23S, 24S, 26S, 27S, 28S, 29S, 30S
85.786		TOTAL AREA

Contact Water Runoff Calcs and Basin Sizing_ Type II 24-hr 25-year, 24-hour Rainfall=5.67"

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Page 4

Time span=0.00-30.00 hrs, dt=0.05 hrs, 601 points

Runoff by SCS TR-20 method, UH=SCS

Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 14S: Phase 2	Runoff Area=16.814 ac 100.00% Impervious Runoff Depth=5.43" Tc=3.0 min CN=98 Runoff=144.54 cfs 7.611 af
Subcatchment 15S: Phase 3	Runoff Area=10.452 ac 100.00% Impervious Runoff Depth=5.43" Tc=3.0 min CN=98 Runoff=89.85 cfs 4.731 af
Subcatchment 16S: Phase 4	Runoff Area=8.600 ac 100.00% Impervious Runoff Depth=5.43" Tc=3.0 min CN=98 Runoff=73.93 cfs 3.893 af
Subcatchment 18S: Phase 5	Runoff Area=10.400 ac 100.00% Impervious Runoff Depth=5.43" Tc=3.0 min CN=98 Runoff=89.40 cfs 4.708 af
Subcatchment 20S: Phase 6	Runoff Area=12.500 ac 100.00% Impervious Runoff Depth=5.43" Tc=3.0 min CN=98 Runoff=107.45 cfs 5.659 af
Subcatchment 23S: Phase 1	Runoff Area=12.300 ac 100.00% Impervious Runoff Depth=5.43" Tc=0.0 min CN=98 Runoff=111.67 cfs 5.568 af
Subcatchment 24S: Surrounding area to	Runoff Area=5.710 ac 21.02% Impervious Runoff Depth=3.39" Tc=3.0 min CN=79 Runoff=36.60 cfs 1.611 af
Subcatchment 26S: Surrounding area to	Runoff Area=3.110 ac 48.23% Impervious Runoff Depth=4.10" Tc=3.0 min CN=86 Runoff=23.17 cfs 1.062 af
Subcatchment 27S: CWB 1/2 Basin	Runoff Area=1.600 ac 100.00% Impervious Runoff Depth=5.43" Tc=0.0 min CN=98 Runoff=14.53 cfs 0.724 af
Subcatchment 28S: CWB 1/2 Basin	Runoff Area=1.600 ac 100.00% Impervious Runoff Depth=5.43" Tc=3.0 min CN=98 Runoff=13.75 cfs 0.724 af
Subcatchment 29S: CWB 3 Basin	Runoff Area=1.700 ac 100.00% Impervious Runoff Depth=5.43" Tc=3.0 min CN=98 Runoff=14.61 cfs 0.770 af
Subcatchment 30S: CWB 4 Basin	Runoff Area=1.000 ac 100.00% Impervious Runoff Depth=5.43" Tc=3.0 min CN=98 Runoff=8.60 cfs 0.453 af
Pond 14P: CWB 1/2 Contact Water Basin	Peak Elev=757.27' Storage=8.336 af Inflow=158.29 cfs 8.336 af Outflow=0.00 cfs 0.000 af
Pond 16P: CWB 4 Contact Water Basin	Peak Elev=760.34' Storage=4.346 af Inflow=82.52 cfs 4.346 af Outflow=0.00 cfs 0.000 af
Pond 17P: CWB 3 Contact Water Basin	Peak Elev=759.62' Storage=5.501 af Inflow=104.46 cfs 5.501 af Outflow=0.00 cfs 0.000 af
Pond 24P: CWB 5 Contact Water Basin	Peak Elev=756.27' Storage=6.319 af Inflow=125.94 cfs 6.319 af Outflow=0.00 cfs 0.000 af

Pond 25P: CWB 1/2 Contact Water Basin Peak Elev=755.69' Storage=6.292 af Inflow=126.19 cfs 6.292 af
Outflow=0.00 cfs 0.000 af

Pond 46P: CWB 6 Contact Water Basin Peak Elev=757.75' Storage=6.720 af Inflow=130.62 cfs 6.720 af
Outflow=0.00 cfs 0.000 af

Total Runoff Area = 85.786 ac Runoff Volume = 37.515 af Average Runoff Depth = 5.25"
7.13% Pervious = 6.120 ac 92.87% Impervious = 79.666 ac

Summary for Subcatchment 14S: Phase 2

[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 144.54 cfs @ 11.93 hrs, Volume= 7.611 af, Depth= 5.43"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-30.00 hrs, $dt= 0.05$ hrs
 Type II 24-hr 25-year, 24-hour Rainfall=5.67"

Area (ac)	CN	Description
* 16.814	98	Ash
16.814		Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.0					Direct Entry,

Summary for Subcatchment 15S: Phase 3

[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 89.85 cfs @ 11.93 hrs, Volume= 4.731 af, Depth= 5.43"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-30.00 hrs, $dt= 0.05$ hrs
 Type II 24-hr 25-year, 24-hour Rainfall=5.67"

Area (ac)	CN	Description
* 10.452	98	Ash
10.452		Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.0					Direct Entry,

Summary for Subcatchment 16S: Phase 4

[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 73.93 cfs @ 11.93 hrs, Volume= 3.893 af, Depth= 5.43"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-30.00 hrs, $dt= 0.05$ hrs
 Type II 24-hr 25-year, 24-hour Rainfall=5.67"

Area (ac)	CN	Description
* 8.600	98	Ash
8.600		Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.0					Direct Entry,

Summary for Subcatchment 18S: Phase 5

Area = 9.83 (phase areas to basin)

[49] Hint: Tc<2dt may require smaller dt

Runoff = 89.40 cfs @ 11.93 hrs, Volume= 4.708 af, Depth= 5.43"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
 Type II 24-hr 25-year, 24-hour Rainfall=5.67"

Area (ac)	CN	Description
* 10.400	98	Ash
10.400		Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.0					Direct Entry,

Summary for Subcatchment 20S: Phase 6

[49] Hint: Tc<2dt may require smaller dt

Runoff = 107.45 cfs @ 11.93 hrs, Volume= 5.659 af, Depth= 5.43"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
 Type II 24-hr 25-year, 24-hour Rainfall=5.67"

Area (ac)	CN	Description
* 12.500	98	Ash
12.500		Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.0					Direct Entry,

Summary for Subcatchment 23S: Phase 1

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff = 111.67 cfs @ 11.89 hrs, Volume= 5.568 af, Depth= 5.43"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
 Type II 24-hr 25-year, 24-hour Rainfall=5.67"

Area (ac)	CN	Description
* 12.300	98	Ash
12.300		Impervious Area

Summary for Subcatchment 24S: Surrounding area to basin not going through culverts

Area = 9.83 (phase areas to basin)

[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 36.60 cfs @ 11.94 hrs, Volume= 1.611 af, Depth= 3.39"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-30.00 hrs, $dt= 0.05$ hrs
 Type II 24-hr 25-year, 24-hour Rainfall=5.67"

Area (ac)	CN	Description
4.510	74	>75% Grass cover, Good, HSG C
* 1.200	98	basin area
5.710	79	Weighted Average
4.510		Pervious Area
1.200		Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.0					Direct Entry,

Summary for Subcatchment 26S: Surrounding area to basin not going through culverts

[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 23.17 cfs @ 11.93 hrs, Volume= 1.062 af, Depth= 4.10"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-30.00 hrs, $dt= 0.05$ hrs
 Type II 24-hr 25-year, 24-hour Rainfall=5.67"

Area (ac)	CN	Description
1.610	74	>75% Grass cover, Good, HSG C
* 1.500	98	Basin area
3.110	86	Weighted Average
1.610		Pervious Area
1.500		Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.0					Direct Entry,

Summary for Subcatchment 27S: CWB 1/2 Basin

[46] Hint: $T_c=0$ (Instant runoff peak depends on dt)

Runoff = 14.53 cfs @ 11.89 hrs, Volume= 0.724 af, Depth= 5.43"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
 Type II 24-hr 25-year, 24-hour Rainfall=5.67"

Area (ac)	CN	Description
* 1.600	98	Basin
1.600		Impervious Area

Summary for Subcatchment 28S: CWB 1/2 Basin

[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 13.75 cfs @ 11.93 hrs, Volume= 0.724 af, Depth= 5.43"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
 Type II 24-hr 25-year, 24-hour Rainfall=5.67"

Area (ac)	CN	Description
* 1.600	98	Basin
1.600		Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.0					Direct Entry,

Summary for Subcatchment 29S: CWB 3 Basin

[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 14.61 cfs @ 11.93 hrs, Volume= 0.770 af, Depth= 5.43"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
 Type II 24-hr 25-year, 24-hour Rainfall=5.67"

Area (ac)	CN	Description
* 1.700	98	Basin
1.700		Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.0					Direct Entry,

Summary for Subcatchment 30S: CWB 4 Basin

[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 8.60 cfs @ 11.93 hrs, Volume= 0.453 af, Depth= 5.43"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-30.00 hrs, $dt=0.05$ hrs
 Type II 24-hr 25-year, 24-hour Rainfall=5.67"

Area (ac)	CN	Description
* 1.000	98	Basin
1.000		Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.0					Direct Entry,

Summary for Pond 14P: CWB 1/2 Contact Water Basin (Eastern half of Phase 3)

Inflow Area = 18.414 ac, 100.00% Impervious, Inflow Depth = 5.43" for 25-year, 24-hour event
 Inflow = 158.29 cfs @ 11.93 hrs, Volume= 8.336 af < 10.83 af ✓
 Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, $dt=0.05$ hrs
 Peak Elev= 757.27' @ 24.20 hrs Surf.Area= 1.354 ac Storage= 8.336 af

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)
 Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert	Avail.Storage	Storage Description
#1	748.00'	12.317 af	Custom Stage Data (Prismatic) Listed below (Recalc)

Elevation (feet)	Surf.Area (acres)	Inc.Store (acre-feet)	Cum.Store (acre-feet)
748.00	0.063	0.000	0.000
750.00	0.569	0.632	0.632
752.00	0.986	1.555	2.187
754.00	1.122	2.108	4.295
756.00	1.262	2.384	6.679
758.00	1.408	2.670	9.349
760.00	1.560	2.968	12.317

← Top of Pond = 759.0 = 10.83 af w/ 1' Freeboard

Summary for Pond 16P: CWB 4 Contact Water Basin (adjacent to Sed Basin No. 3)

Inflow Area = 9.600 ac, 100.00% Impervious, Inflow Depth = 5.43" for 25-year, 24-hour event
 Inflow = 82.52 cfs @ 11.93 hrs, Volume= 4.346 af < 4.95 af ✓
 Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, $dt=0.05$ hrs

Contact Water Runoff Calcs and Basin Sizing Type II 24-hr 25-year, 24-hour Rainfall=5.67"

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Peak Elev= 760.34' @ 24.20 hrs Surf.Area= 0.849 ac Storage= 4.346 af

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no outflow)

Volume #1	Invert 754.00'	Avail.Storage 5.830 af	Storage Description Custom Stage Data (Prismatic) Listed below (Recalc)
--------------	-------------------	---------------------------	---

Elevation (feet)	Surf.Area (acres)	Inc.Store (acre-feet)	Cum.Store (acre-feet)
754.00	0.540	0.000	0.000
755.00	0.580	0.560	0.560
756.00	0.630	0.605	1.165
757.00	0.670	0.650	1.815
758.00	0.720	0.695	2.510
760.00	0.830	1.550	4.060
762.00	0.940	1.770	5.830

← Top of Basin = 761.0 = 4.95 af
w/ 1' Freeboard

Summary for Pond 17P: CWB 3 Contact Water Basin (Eastern half of Phase 4)

Inflow Area = 12.152 ac, 100.00% Impervious, Inflow Depth = 5.43" for 25-year, 24-hour event

Inflow = 104.46 cfs @ 11.93 hrs, Volume= 5.501 af < 6.13 af ✓

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

Peak Elev= 759.62' @ 24.20 hrs Surf.Area= 1.654 ac Storage= 5.501 af

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no outflow)

Volume #1	Invert 754.00'	Avail.Storage 6.127 af	Storage Description Custom Stage Data (Prismatic) Listed below (Recalc)
--------------	-------------------	---------------------------	---

Elevation (feet)	Surf.Area (acres)	Inc.Store (acre-feet)	Cum.Store (acre-feet)
754.00	0.070	0.000	0.000
755.00	0.312	0.191	0.191
756.00	0.720	0.516	0.707
757.00	1.150	0.935	1.642
758.00	1.460	1.305	2.947
759.00	1.610	1.535	4.482
760.00	1.680	1.645	6.127

← Top of Basin
w/ 1' Freeboard

Summary for Pond 24P: CWB 5 Contact Water Basin (part of Sed Basin 1)

Inflow Area = 16.110 ac, 72.00% Impervious, Inflow Depth = 4.71" for 25-year, 24-hour event

Inflow = 125.94 cfs @ 11.93 hrs, Volume= 6.319 af < 7.38 af ✓

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

Contact Water Runoff Calcs and Basin Sizing Type II 24-hr 25-year, 24-hour Rainfall=5.67"

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Peak Elev= 756.27' @ 24.20 hrs Surf.Area= 1.381 ac Storage= 6.319 af

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no outflow)

Volume #1	Invert 751.00'	Avail.Storage 8.819 af	Storage Description
Custom Stage Data (Prismatic) Listed below (Recalc)			

Elevation (feet)	Surf.Area (acres)	Inc.Store (acre-feet)	Cum.Store (acre-feet)
751.00	1.030	0.000	0.000
752.00	1.090	1.060	1.060
754.00	1.219	2.309	3.369
756.00	1.361	2.580	5.949
758.00	1.509	2.870	8.819

← Top of Basin w/ 1' Freeboard = 757.0 = 7.38 af

Summary for Pond 25P: CWB 1/2 Contact Water Basin (Eastern half of Phase 3)

Inflow Area = 13.900 ac, 100.00% Impervious, Inflow Depth = 5.43" for 25-year, 24-hour event

Inflow = 126.19 cfs @ 11.89 hrs, Volume= 6.292 af < 10.83 af ✓

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

Peak Elev= 755.69' @ 24.05 hrs Surf.Area= 1.240 ac Storage= 6.292 af

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no outflow)

Volume #1	Invert 748.00'	Avail.Storage 12.317 af	Storage Description
Custom Stage Data (Prismatic) Listed below (Recalc)			

Elevation (feet)	Surf.Area (acres)	Inc.Store (acre-feet)	Cum.Store (acre-feet)
748.00	0.063	0.000	0.000
750.00	0.569	0.632	0.632
752.00	0.986	1.555	2.187
754.00	1.122	2.108	4.295
756.00	1.262	2.384	6.679
758.00	1.408	2.670	9.349
760.00	1.560	2.968	12.317

← Top of Basin w/ 1' Freeboard = 759.0 = 10.93

Summary for Pond 46P: CWB 6 Contact Water Basin (Sed Basin 4)

Sedimentation Basin No. 4 will be lined and serve as a temporary contact water basin.

Inflow Area = 15.610 ac, 89.69% Impervious, Inflow Depth = 5.17" for 25-year, 24-hour event

Inflow = 130.62 cfs @ 11.93 hrs, Volume= 6.720 af < 8.35 af ✓

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

Contact Water Runoff Calcs and Basin Sizing Type II 24-hr 25-year, 24-hour Rainfall=5.67"

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Peak Elev= 757.75' @ 24.20 hrs Surf.Area= 1.227 ac Storage= 6.720 af

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert	Avail.Storage	Storage Description
#1	751.00'	9.673 af	Custom Stage Data (Prismatic) Listed below (Recalc)

Elevation (feet)	Surf.Area (acres)	Inc.Store (acre-feet)	Cum.Store (acre-feet)
751.00	0.779	0.000	0.000
752.00	0.840	0.810	0.810
754.00	0.967	1.807	2.617
756.00	1.102	2.069	4.686
758.00	1.245	2.347	7.033
760.00	1.395	2.640	9.673

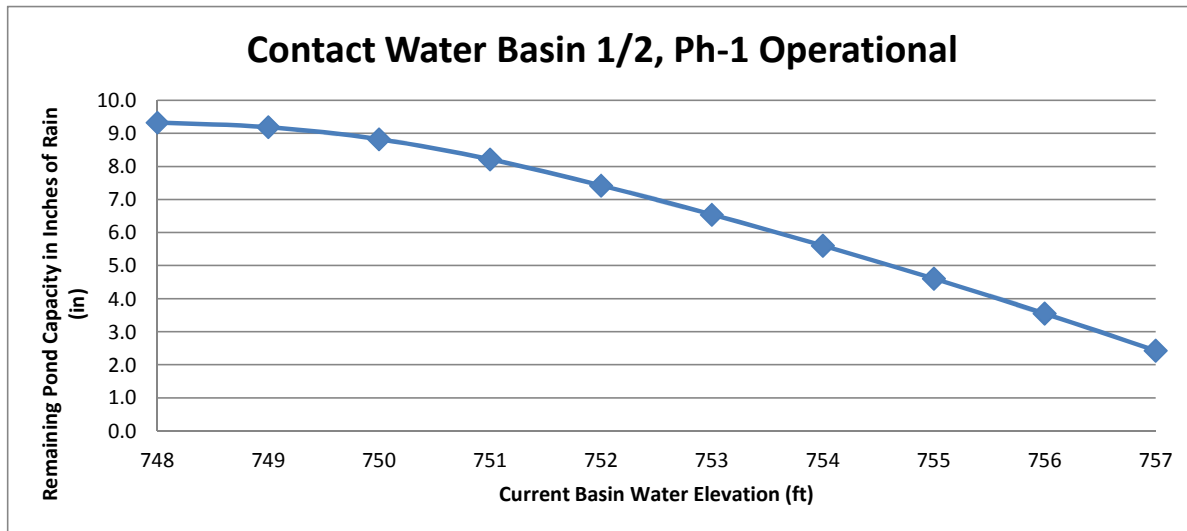
← top of Basin
w/ 1' Freeboard = 759.0' = 9.3 af

OML Expansion
Temporary Contact Water Basin 1/2, Phase 1 Operational

Starting Water Elevation in Basin	Starting Water Depth (ft)	Basin Storage Volume (cf)	Incremental Volume (cf)	Cumulative Rainfall to Reach Basin Water Elevation (in)	Remaining Pond Capacity in Inches of Rain (in)	Notes
748	0	0	N/A	0.00	9.33	Basin Bottom
749	1	7,084	7,084	0.14	9.19	
750	2	25,463	18,378	0.50	8.83	
751	3	56,131	30,668	1.11	8.22	
752	4	96,050	39,919	1.90	7.43	
753	5	140,507	44,457	2.78	6.55	
754	6	187,929	47,421	3.72	5.61	
755	7	238,317	50,388	4.72	4.61	
756	8	291,742	53,426	5.78	3.55	
757	9	348,277	56,535	6.90	2.43	
758	10	407,993	59,716	8.09	1.25	
759	11	470,963	62,970	9.33	0.00	Peak Elevation (1' Freeboard)
760	12	537,249	66,286	10.65	0.00	Top of Basin Liner

Notes:

1. Basin Volumes from AutoCAD Civil 3D surface.
2. Assumes drainage area to contact water basin = 605,524 sf, as shown on attached Figure H-1.

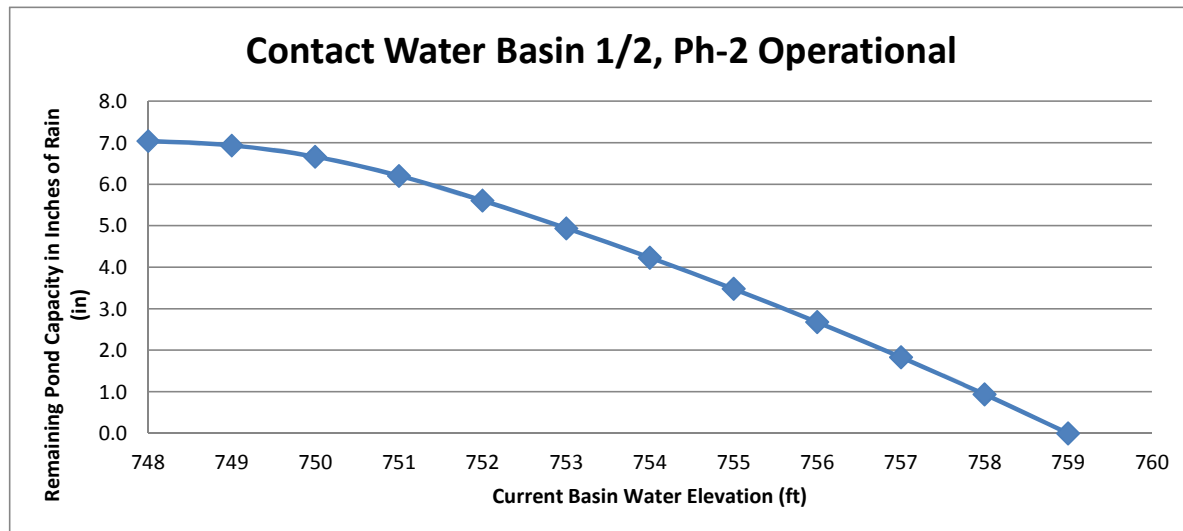


OML Expansion
Temporary Contact Water Basin 1/2, Phase 2 Operational

Starting Water Elevation in Basin	Starting Water Depth (ft)	Basin Storage Volume (cf)	Incremental Volume (cf)	Cumulative Rainfall to Reach Basin Water Elevation (in)	Remaining Pond Capacity in Inches of Rain (in)	Notes
748	0	0	N/A	0.00	7.05	Basin Bottom
749	1	7,084	7,084	0.11	6.94	
750	2	25,463	18,378	0.38	6.66	
751	3	56,131	30,668	0.84	6.21	
752	4	96,050	39,919	1.44	5.61	
753	5	140,507	44,457	2.10	4.94	
754	6	187,929	47,421	2.81	4.23	
755	7	238,317	50,388	3.57	3.48	
756	8	291,742	53,426	4.36	2.68	
757	9	348,277	56,535	5.21	1.84	
758	10	407,993	59,716	6.10	0.94	
759	11	470,963	62,970	7.05	0.00	Peak Elevation (1' Freeboard)
760	12	537,249	66,286	8.04	0.00	Top of Basin Liner

Notes:

1. Basin Volumes from AutoCAD Civil 3D surface.
2. Assumes drainage area to contact water basin = 802,117 sf, as shown on attached Figure H-2.

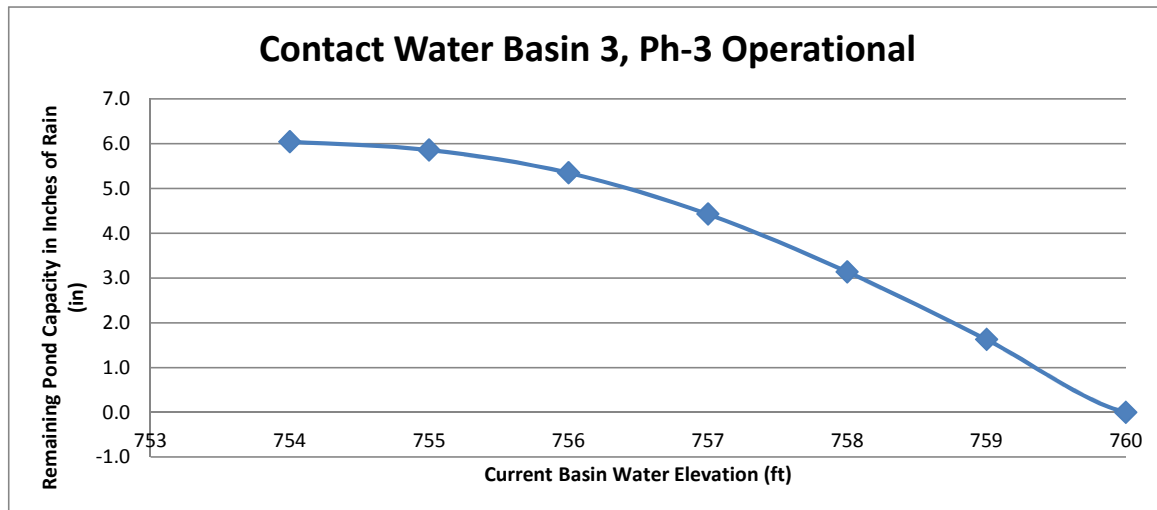


**OML Expansion
Temporary Contact Water Basin 3, Phase 3 Operational**

Starting Water Elevation in Basin	Starting Water Depth (ft)	Basin Storage Volume (cf)	Incremental Volume (cf)	Cumulative Rainfall to Reach Basin Water Elevation (in)	Remaining Pond Capacity in Inches of Rain (in)	Notes
754	0	0	N/A	0.00	6.05	Basin Bottom
755	1	8227.41	8227.41	0.19	5.86	
756	2	30703.75	22476.34	0.70	5.35	
757	3	71482.97	40779.22	1.62	4.43	
758	4	128279.82	56796.85	2.91	3.14	
759	5	194997.22	66717.4	4.42	1.63	
760	6	266705.27	71708.06	6.05	0.00	Peak Elevation (1' Freeboard)
761	7	341247.09	74541.81	7.74	0.00	Top of Basin Liner

Notes:

1. Basin Volumes from AutoCAD Civil 3D surface.
2. Assumes drainage area to contact water basin = 529,337 sf, as shown on attached Figure H-3.

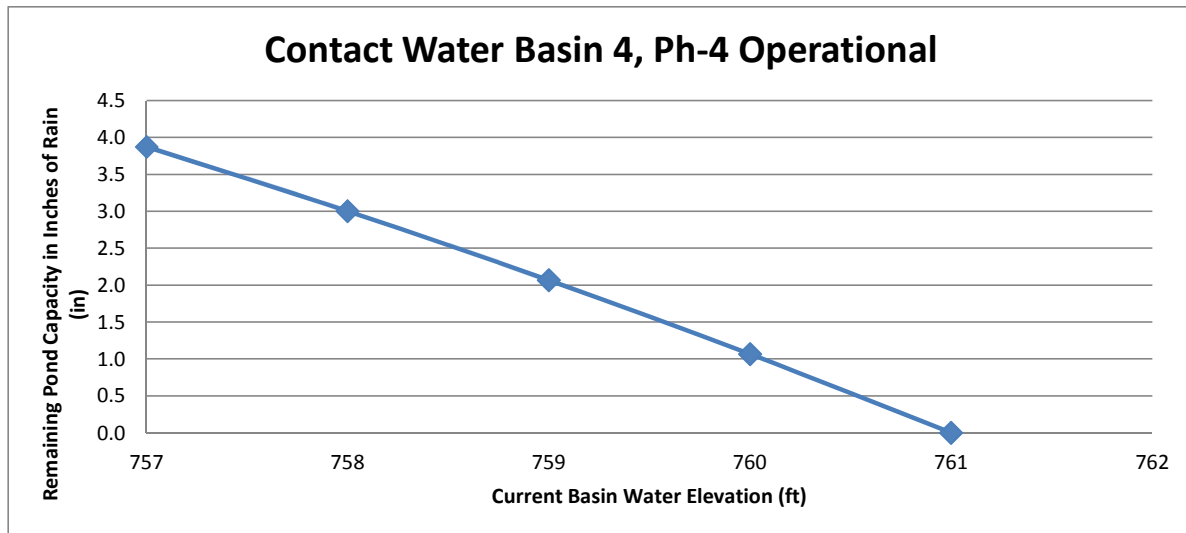


**OML Expansion
Temporary Contact Water Basin 4, Phase 4 Operational**

Starting Water Elevation in Basin	Starting Water Depth (ft)	Basin Storage Volume (cf)	Incremental Volume (cf)	Cumulative Rainfall to Reach Basin Water Elevation (in)	Remaining Pond Capacity in Inches of Rain (in)	Notes
754	0	-	N/A	0.00	6.14	Basin Bottom
755	1	24,281	24,281	0.70	5.44	
756	2	50,529	26,248	1.45	4.69	
757	3	78,818	28,289	2.26	3.88	
758	4	109,196	30,378	3.14	3.00	
759	5	141,760	32,564	4.07	2.07	
760	6	176,583	34,824	5.07	1.07	
761	7	213,739	37,156	6.14	0.00	Peak Elevation (1' Freeboard)
762	8	253,301	39,562	7.28	0.00	Top of Basin Liner

Notes:

1. Basin Volumes from AutoCAD Civil 3D surface.
2. Assumes drainage area to contact water basin = 417,711 sf, as shown on attached Figure H-4.

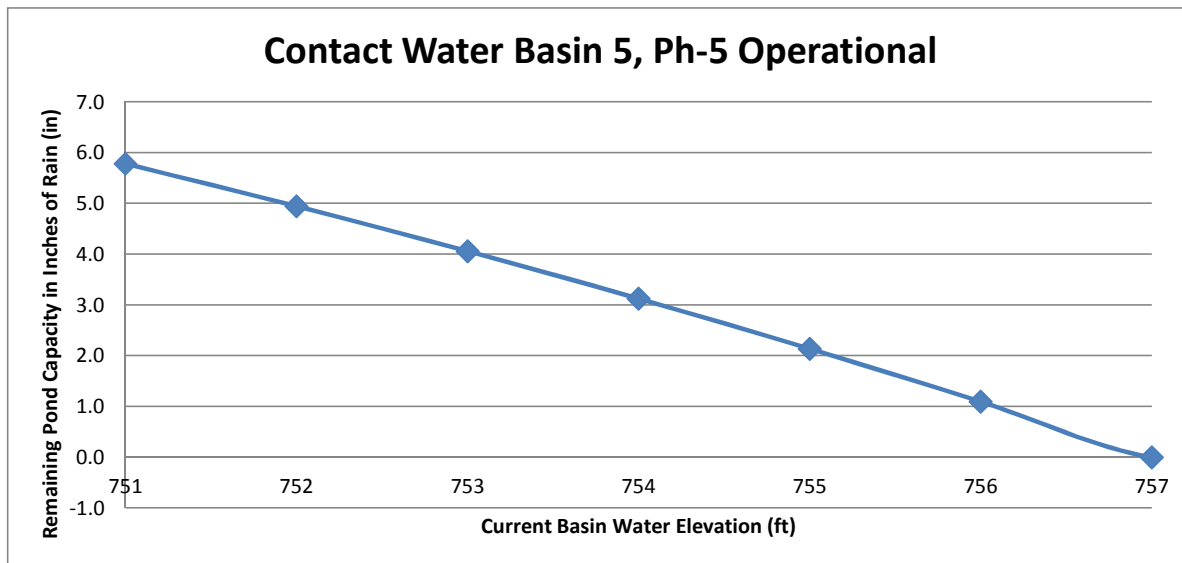


**OML Expansion
Temporary Contact Water Basin 5, Phase 5 Operational**

Starting Water Elevation in Basin	Starting Water Depth (ft)	Basin Storage Volume (cf)	Incremental Volume (cf)	Cumulative Rainfall to Reach Basin Water Elevation (in)	Remaining Pond Capacity in Inches of Rain (in)	Notes
751	0	-	N/A	0.00	5.78	Basin Bottom
752	1	48,951	48,951	0.84	4.95	
753	2	100,775	51,824	1.72	4.06	
754	3	155,474	103,650	2.66	3.12	
755	4	213,192	109,542	3.65	2.14	
756	5	274,078	164,536	4.69	1.10	
757	6	338,203	173,667	5.78	0.00	Peak Elevation (1' Freeboard)
758	7	405,640	231,973	6.94	0.00	Top of Basin Liner

Notes:

1. Basin Volumes from AutoCAD Civil 3D surface.
2. Assumes drainage area to contact water basin = 701,822 sf, as shown on attached Figure H-5.

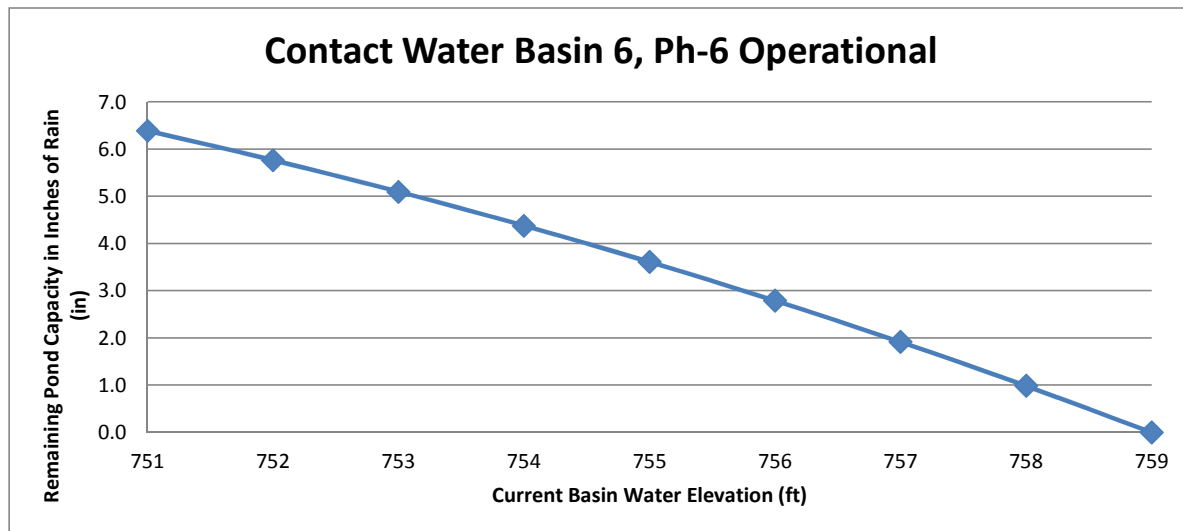


OML Expansion
Temporary Contact Water Basin 6, Phase 6 Operational

Starting Water Elevation in Basin	Starting Water Depth (ft)	Basin Storage Volume (cf)	Incremental Volume (cf)	Cumulative Rainfall to Reach Basin Water Elevation (in)	Remaining Pond Capacity in Inches of Rain (in)	Notes
751	0	-	N/A	0.00	6.39	Basin Bottom
752	1	35,250	35,250	0.62	5.77	
753	2	73,188	37,938	1.29	5.10	
754	3	113,900	40,712	2.01	4.38	
755	4	157,470	43,570	2.78	3.61	
756	5	203,982	46,513	3.60	2.79	
757	6	253,522	49,540	4.47	1.92	
758	7	306,224	52,654	5.40	0.99	
759	8	362,072	55,848	6.39	0.00	Peak Elevation (1' Freeboard)
760	9	421,196	59,124	7.43	0.00	Top of Basin Liner

Notes:

1. Basin Volumes from AutoCAD Civil 3D surface.
2. Assumes drainage area to contact water basin = 679,949 sf, as shown on attached Figure H-6.



Contact Water Basin Culvert Sizing

Phase 1 Contact Water Basin Culverts

Site Data - 3-3' dia. HDPE

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft

Inlet Elevation: 760.00 ft

Outlet Station: 82.70 ft

Outlet Elevation: 751.00 ft

Number of Barrels: 3

Culvert Data Summary - 3-3' dia. HDPE

Barrel Shape: Circular

Barrel Diameter: 3.00 ft

Barrel Material: Smooth HDPE

Embedment: 0.00 in

Barrel Manning's n: 0.0120

Culvert Type: Straight

Inlet Configuration: Thin Edge Projecting

Inlet Depression: NONE

Tailwater Channel Data - Phase 1

Tailwater Channel Option: Enter Constant Tailwater Elevation

Constant Tailwater Elevation: 755.69 ft

Roadway Data for Crossing: Phase 1

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 20.00 ft

Crest Elevation: 766.00 ft

Roadway Surface: Gravel

Roadway Top Width: 8.00 ft

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 0 cfs

Design Flow: 111.67 cfs

Maximum Flow: 111.67 cfs

Table 4 - Culvert Summary Table: 3-3' dia. HDPE

Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
	0.00	0.00	760.00	0.000	0.000	0-NF	0.000	0.000	3.000	-4.310	0.000
	11.17	11.17	760.80	0.801	0.0*	1-JS1f	0.249	0.597	3.000	-4.310	0.552
	22.33	22.33	761.16	1.158	0.0*	1-JS1f	0.342	0.854	3.000	-4.310	1.103
	33.50	33.50	761.43	1.433	0.040	1-JS1f	0.420	1.057	3.000	-4.310	1.655
	44.67	44.67	761.71	1.706	0.113	1-JS1f	0.497	1.226	3.000	-4.310	2.206
	55.84	55.84	761.97	1.971	0.206	1-JS1f	0.563	1.382	3.000	-4.310	2.758
	67.00	67.00	762.23	2.227	0.320	1-JS1f	0.610	1.520	3.000	-4.310	3.309
	78.17	78.17	762.48	2.483	0.455	1-JS1f	0.657	1.643	3.000	-4.310	3.861
	89.34	89.34	762.74	2.743	0.611	1-JS1f	0.704	1.763	3.000	-4.310	4.412
	100.50	100.50	763.01	3.014	0.787	5-JS1f	0.751	1.876	3.000	-4.310	4.964
	111.67	111.67	763.30	3.300	0.985	5-JS1f	0.798	1.980	3.000	-4.310	5.516

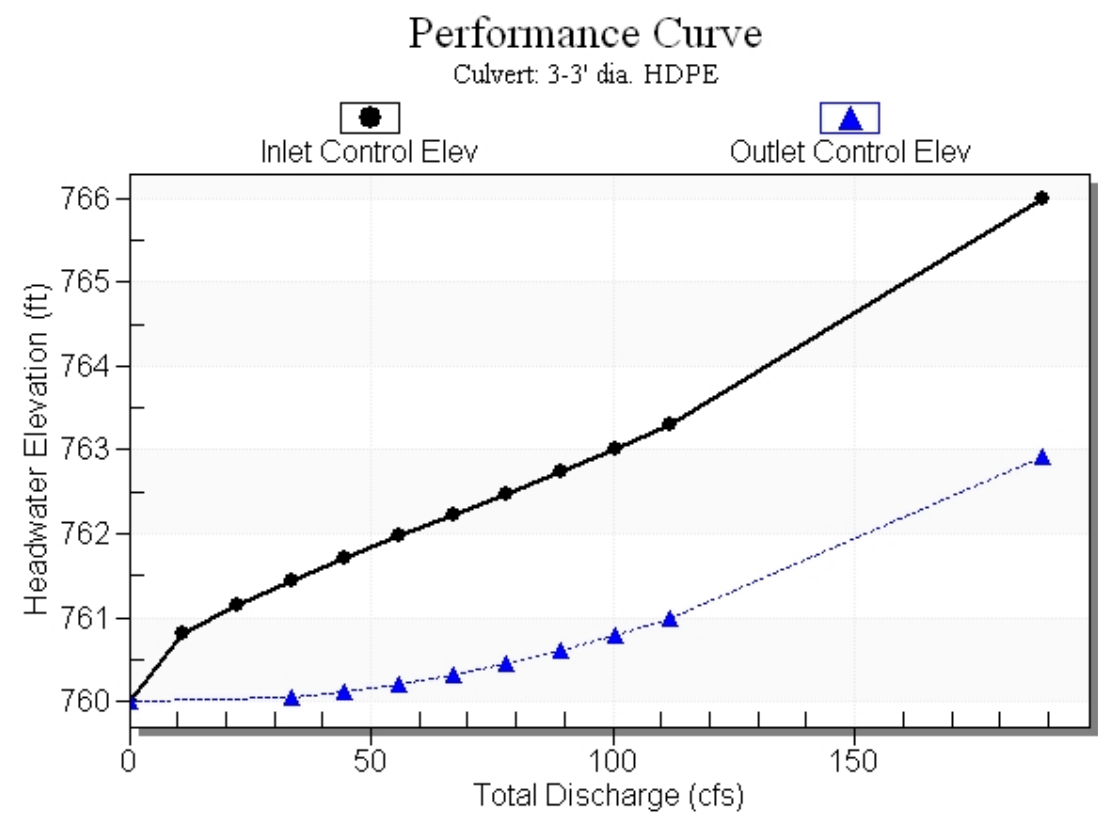
* Full Flow Headwater elevation is below inlet invert.

Straight Culvert

Inlet Elevation (invert): 760.00 ft, Outlet Elevation (invert): 751.00 ft

Culvert Length: 83.19 ft, Culvert Slope: 0.1088

Culvert Performance Curve Plot: 3-3' dia. HDPE



Water Surface Profile Plot for Culvert: 3-3' dia. HDPE

Crossing - Phase 1, Design Discharge - 111.7 cfs

Culvert - 3-3' dia. HDPE, Culvert Discharge - 111.7 cfs

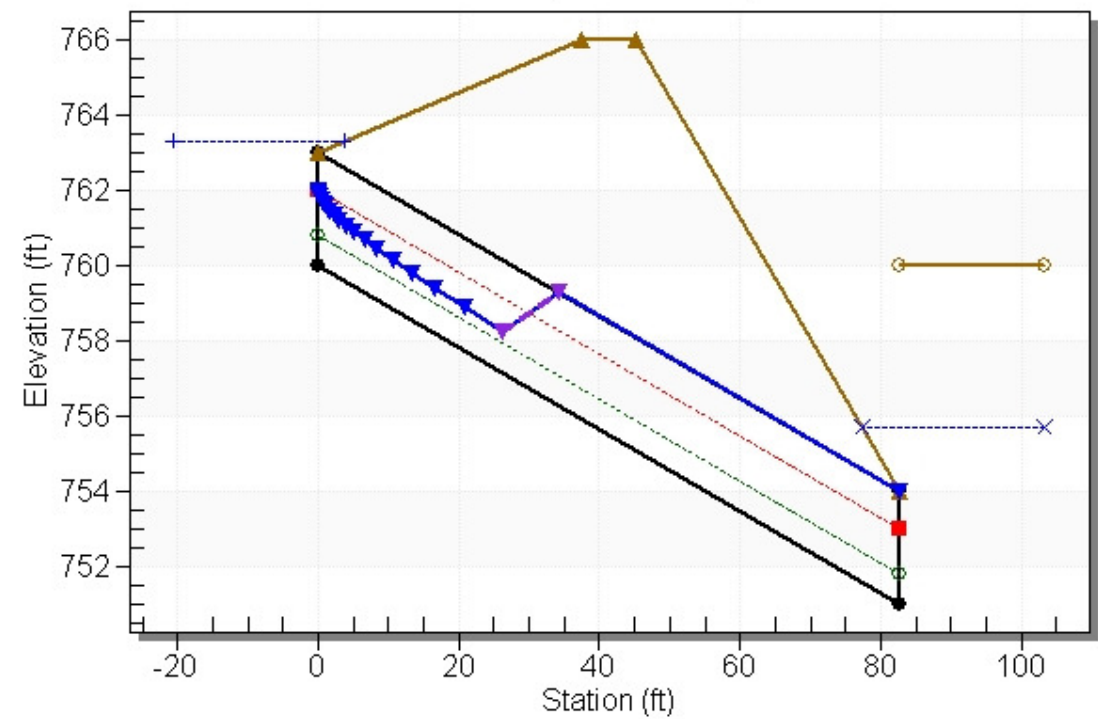


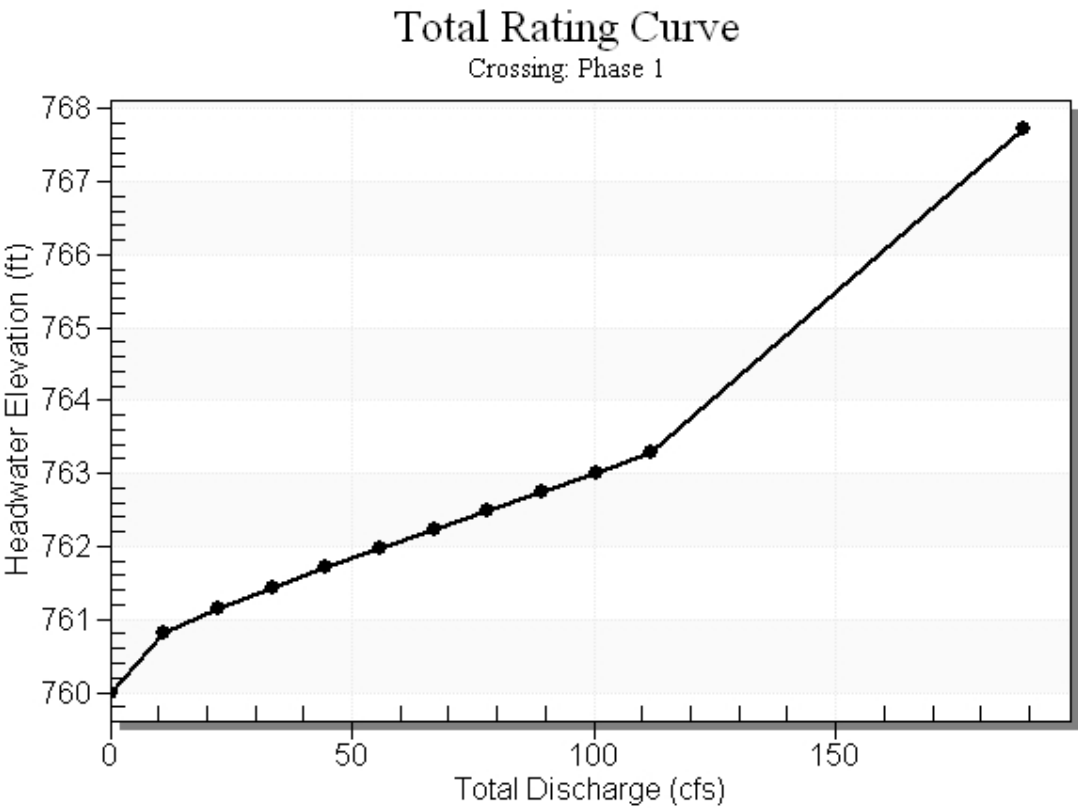
Table 5 - Downstream Channel Rating Curve (Crossing: Phase 1)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
0.00	755.69	-4.31
11.17	755.69	-4.31
22.33	755.69	-4.31
33.50	755.69	-4.31
44.67	755.69	-4.31
55.84	755.69	-4.31
67.00	755.69	-4.31
78.17	755.69	-4.31
89.34	755.69	-4.31
100.50	755.69	-4.31
111.67	755.69	-4.31

Table 6 - Summary of Culvert Flows at Crossing: Phase 1

Headwater Elevation (ft)	Total Discharge (cfs)	3-3' dia. HDPE Discharge (cfs)	Roadway Discharge (cfs)	Iterations
760.00	0.00	0.00	0.00	1
760.80	11.17	11.17	0.00	1
761.16	22.33	22.33	0.00	1
761.43	33.50	33.50	0.00	1
761.71	44.67	44.67	0.00	1
761.97	55.84	55.84	0.00	1
762.23	67.00	67.00	0.00	1
762.48	78.17	78.17	0.00	1
762.74	89.34	89.34	0.00	1
763.01	100.50	100.50	0.00	1
763.30	111.67	111.67	0.00	1
766.00	188.90	188.90	0.00	Overtopping

Rating Curve Plot for Crossing: Phase 1



Phase 2 Contact Water Basin Culverts

Site Data - 3-3' dia. HDPE

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft

Inlet Elevation: 760.50 ft

Outlet Station: 63.80 ft

Outlet Elevation: 754.00 ft

Number of Barrels: 3

Culvert Data Summary - 3-3' dia. HDPE

Barrel Shape: Circular

Barrel Diameter: 3.00 ft

Barrel Material: Smooth HDPE

Embedment: 0.00 in

Barrel Manning's n: 0.0120

Culvert Type: Straight

Inlet Configuration: Thin Edge Projecting

Inlet Depression: NONE

Tailwater Channel Data - Phase 2

Tailwater Channel Option: Enter Constant Tailwater Elevation

Constant Tailwater Elevation: 757.27 ft

Roadway Data for Crossing: Phase 2

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 100.00 ft

Crest Elevation: 766.00 ft

Roadway Surface: Gravel

Roadway Top Width: 8.00 ft

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 0 cfs

Design Flow: 144.54 cfs

Maximum Flow: 144.54 cfs

Table 1 - Culvert Summary Table: 3-3' dia. HDPE

Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
	0.00	0.00	760.50	0.000	0.000	0-NF	0.000	0.000	3.000	-3.230	0.000
	14.45	14.45	761.42	0.921	0.0*	1-JS1f	0.291	0.683	3.000	-3.230	0.714
	28.91	28.91	761.83	1.330	0.033	1-JS1f	0.395	0.978	3.000	-3.230	1.428
	43.36	43.36	762.18	1.684	0.115	1-JS1f	0.498	1.206	3.000	-3.230	2.142
	57.82	57.82	762.53	2.027	0.231	1-JS1f	0.579	1.408	3.000	-3.230	2.856
	72.27	72.27	762.86	2.358	0.380	1-JS1f	0.642	1.580	3.000	-3.230	3.570
	86.72	86.72	763.19	2.692	0.562	1-JS1f	0.705	1.736	3.000	-3.230	4.283
	101.18	101.18	763.54	3.041	0.777	5-JS1f	0.768	1.883	3.000	-3.230	4.997
	115.63	115.63	763.92	3.416	1.025	5-JS1f	0.828	2.015	3.000	-3.230	5.711
	130.09	130.09	764.33	3.827	1.306	5-JS1f	0.875	2.143	3.000	-3.230	6.425
	144.54	144.54	764.78	4.282	1.621	5-JS1f	0.923	2.257	3.000	-3.230	7.139

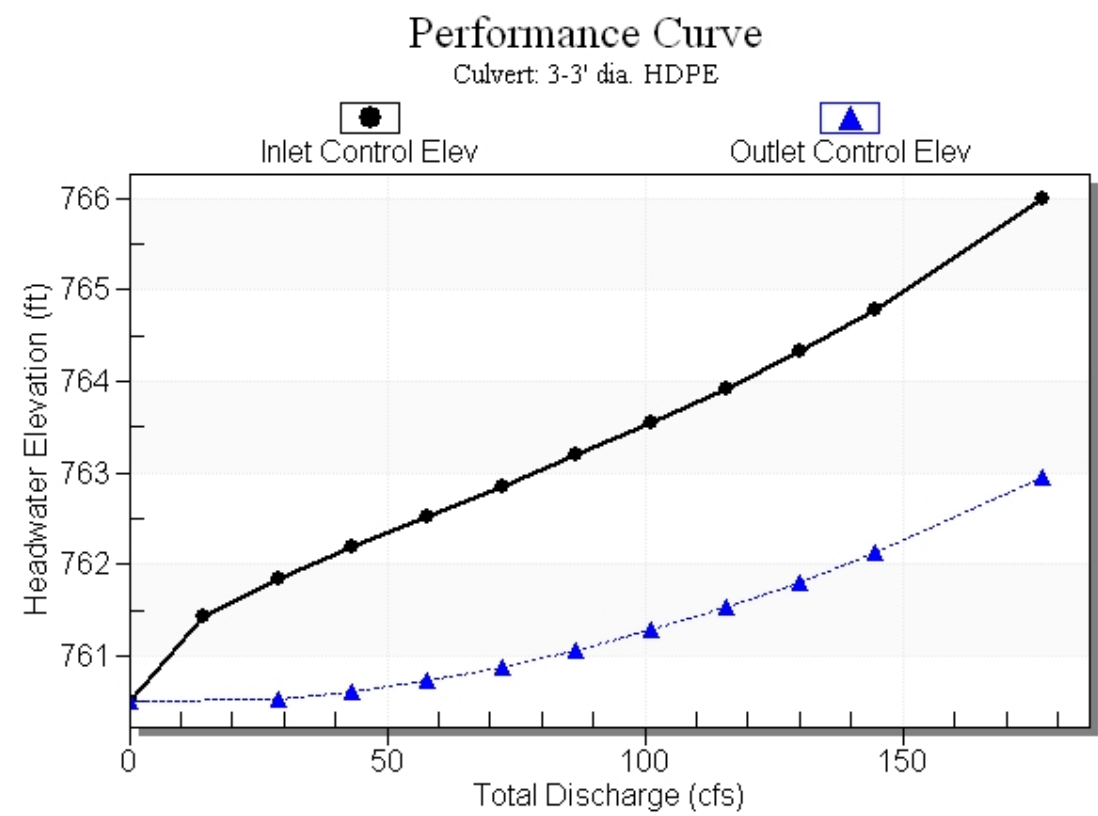
* Full Flow Headwater elevation is below inlet invert.

Straight Culvert

Inlet Elevation (invert): 760.50 ft, Outlet Elevation (invert): 754.00 ft

Culvert Length: 64.13 ft, Culvert Slope: 0.1019

Culvert Performance Curve Plot: 3-3' dia. HDPE



Water Surface Profile Plot for Culvert: 3-3' dia. HDPE

Crossing - Phase 2, Design Discharge - 144.5 cfs

Culvert - 3-3' dia. HDPE, Culvert Discharge - 144.5 cfs

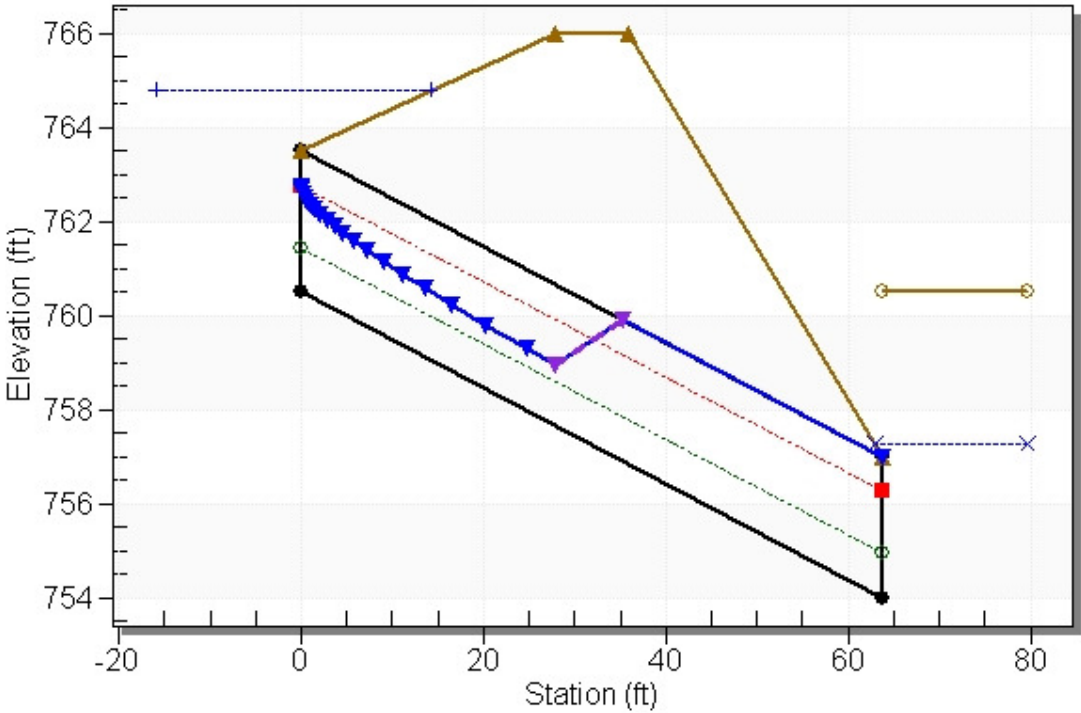


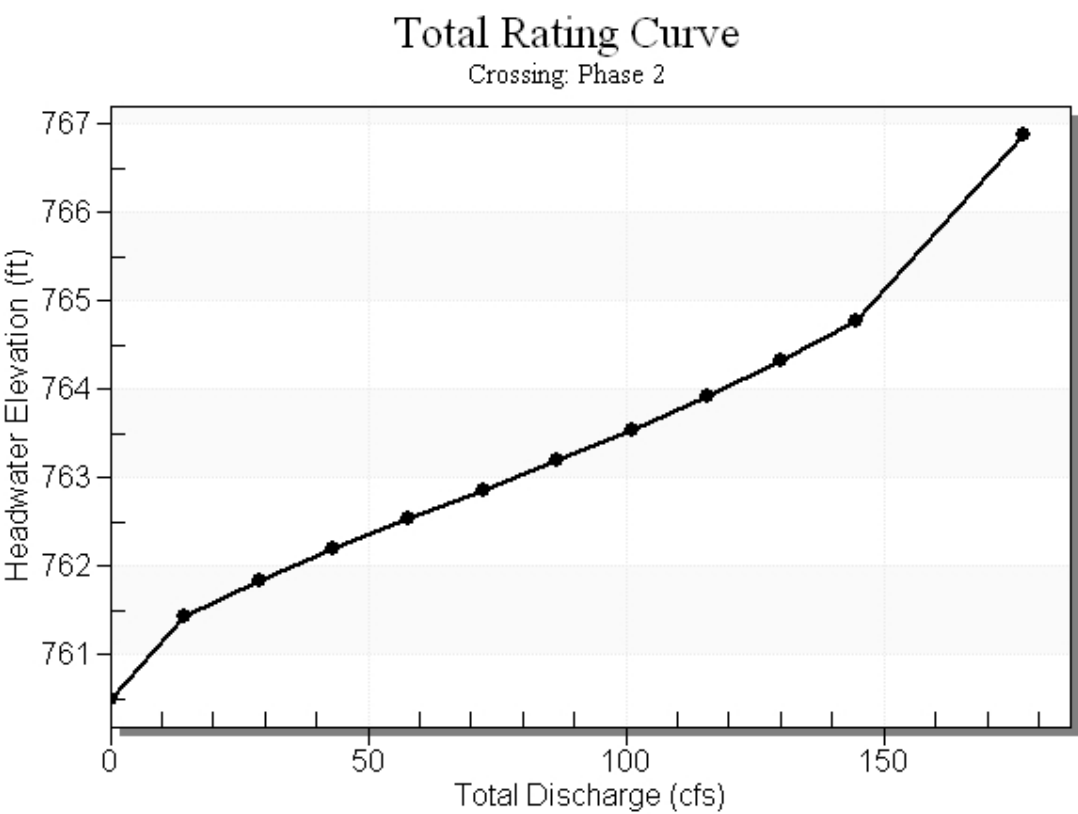
Table 2 - Downstream Channel Rating Curve (Crossing: Phase 2)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
0.00	757.27	-3.23
14.45	757.27	-3.23
28.91	757.27	-3.23
43.36	757.27	-3.23
57.82	757.27	-3.23
72.27	757.27	-3.23
86.72	757.27	-3.23
101.18	757.27	-3.23
115.63	757.27	-3.23
130.09	757.27	-3.23
144.54	757.27	-3.23

Table 3 - Summary of Culvert Flows at Crossing: Phase 2

Headwater Elevation (ft)	Total Discharge (cfs)	3-3' dia. HDPE Discharge (cfs)	Roadway Discharge (cfs)	Iterations
760.50	0.00	0.00	0.00	1
761.42	14.45	14.45	0.00	1
761.83	28.91	28.91	0.00	1
762.18	43.36	43.36	0.00	1
762.53	57.82	57.82	0.00	1
762.86	72.27	72.27	0.00	1
763.19	86.72	86.72	0.00	1
763.54	101.18	101.18	0.00	1
763.92	115.63	115.63	0.00	1
764.33	130.09	130.09	0.00	1
764.78	144.54	144.54	0.00	1
766.00	177.16	177.16	0.00	Overtopping

Rating Curve Plot for Crossing: Phase 2



Phase 3 Contact Water Basin Culverts

Site Data - 3-3' dia. HDPE

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft

Inlet Elevation: 757.50 ft

Outlet Station: 37.60 ft

Outlet Elevation: 757.00 ft

Number of Barrels: 3

Culvert Data Summary - 3-3' dia. HDPE

Barrel Shape: Circular

Barrel Diameter: 3.00 ft

Barrel Material: Smooth HDPE

Embedment: 0.00 in

Barrel Manning's n: 0.0120

Culvert Type: Straight

Inlet Configuration: Thin Edge Projecting

Inlet Depression: NONE

Tailwater Channel Data - Phase 3

Tailwater Channel Option: Enter Constant Tailwater Elevation

Constant Tailwater Elevation: 758.83 ft

Roadway Data for Crossing: Phase 3

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 20.00 ft

Crest Elevation: 761.00 ft

Roadway Surface: Gravel

Roadway Top Width: 8.00 ft

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 0 cfs

Design Flow: 89.85 cfs

Maximum Flow: 89.85 cfs

Table 7 - Culvert Summary Table: 3-3' dia. HDPE

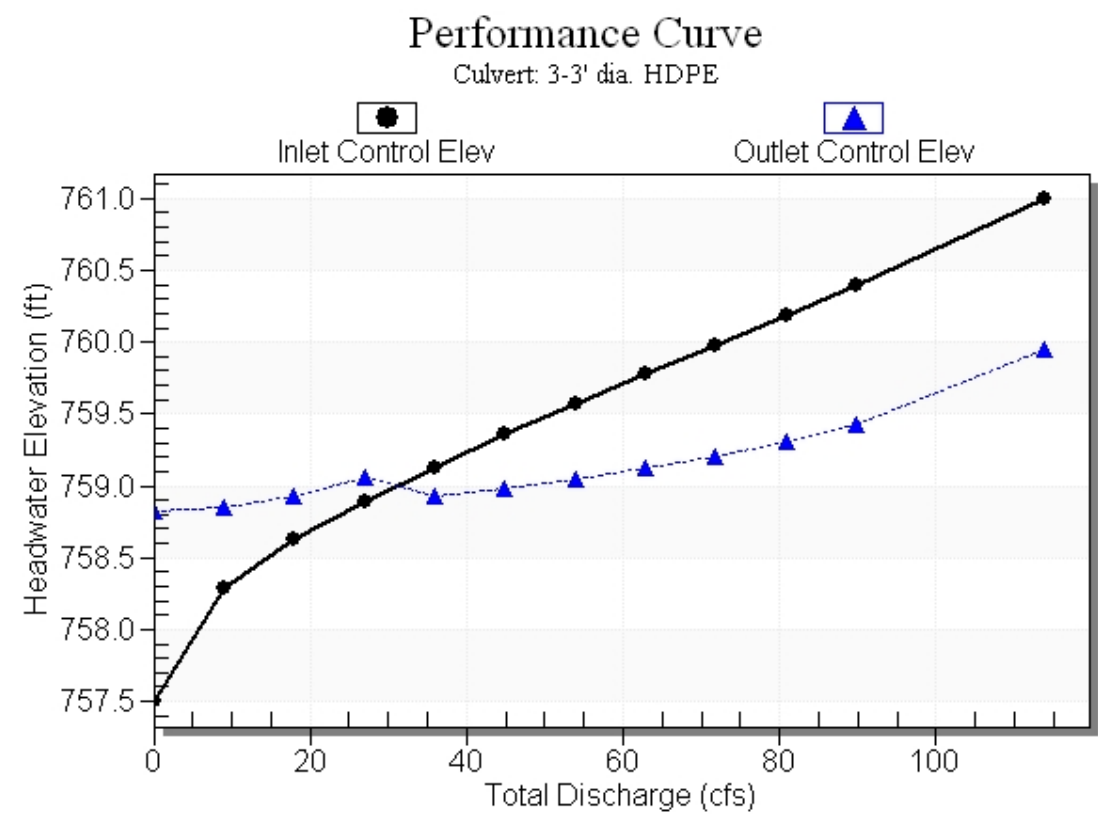
Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
	0.00	0.00	758.83	0.000	1.330	0-NF	0.000	0.000	1.830	1.330	0.000
	8.98	8.98	758.85	0.783	1.353	1-S1t	0.366	0.537	1.830	1.330	0.664
	17.97	17.97	758.92	1.122	1.425	1-S1t	0.543	0.765	1.830	1.330	1.327
	26.95	26.95	759.06	1.392	1.558	1-S1t	0.652	0.943	1.830	1.330	1.991
	35.94	35.94	759.13	1.631	1.425	1-JS1t	0.760	1.094	1.830	1.330	2.654
	44.92	44.92	759.36	1.855	1.478	1-JS1t	0.856	1.230	1.830	1.330	3.318
	53.91	53.91	759.57	2.069	1.544	1-S2n	0.938	1.357	1.039	1.330	8.254
	62.89	62.89	759.78	2.277	1.621	1-S2n	1.019	1.471	1.134	1.330	8.580
	71.88	71.88	759.98	2.482	1.710	1-S2n	1.100	1.575	1.225	1.330	8.819
	80.86	80.86	760.19	2.688	1.811	1-S2n	1.169	1.675	1.311	1.330	9.071
	89.85	89.85	760.40	2.898	1.924	1-S2n	1.238	1.768	1.394	1.330	9.312

Straight Culvert

Inlet Elevation (invert): 757.50 ft, Outlet Elevation (invert): 757.00 ft

Culvert Length: 37.60 ft, Culvert Slope: 0.0133

Culvert Performance Curve Plot: 3-3' dia. HDPE



Water Surface Profile Plot for Culvert: 3-3' dia. HDPE

Crossing - Phase 3, Design Discharge - 89.8 cfs

Culvert - 3-3' dia. HDPE, Culvert Discharge - 89.8 cfs

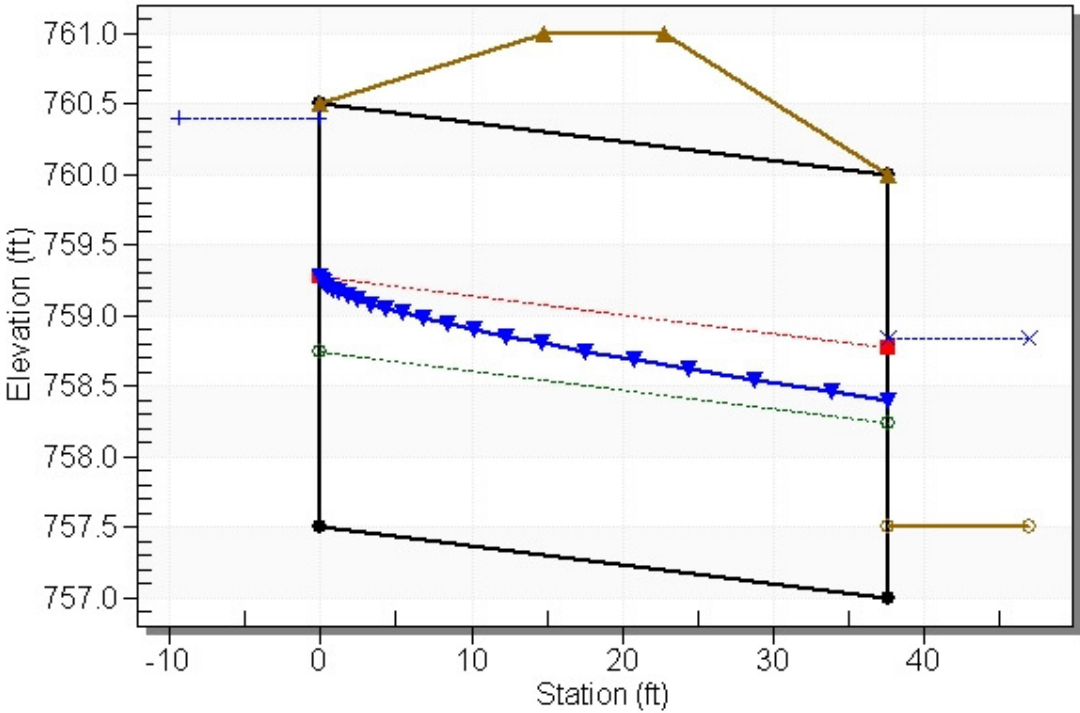


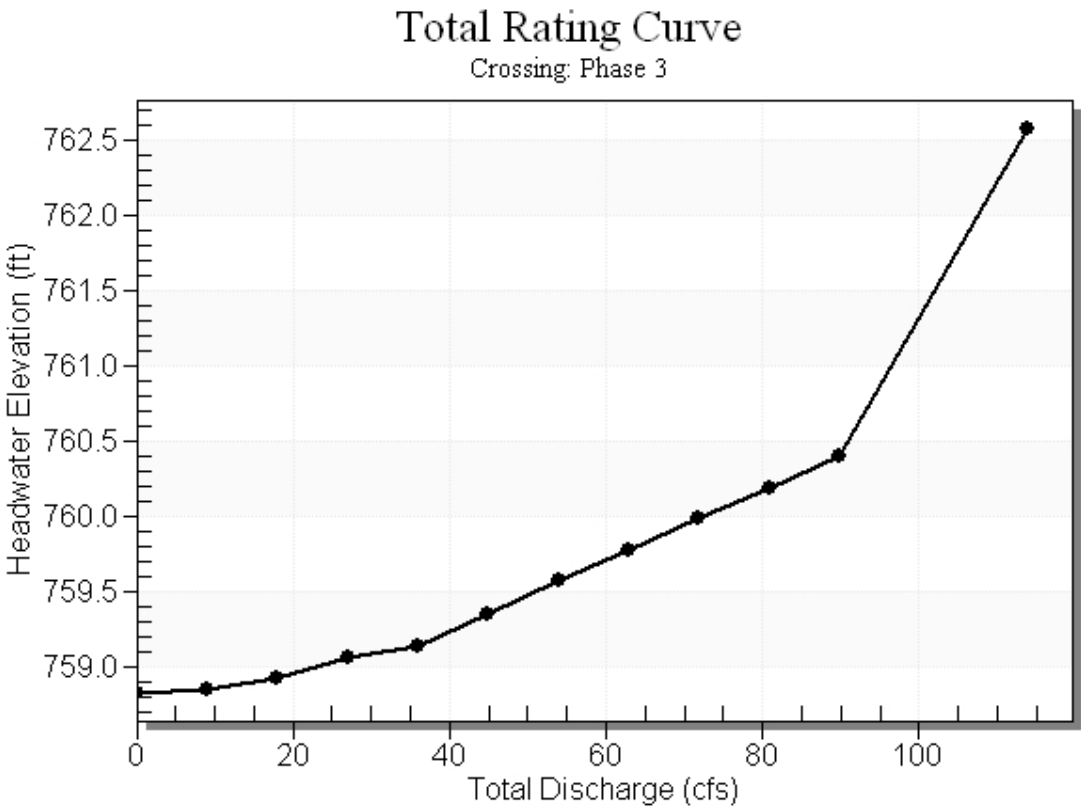
Table 8 - Downstream Channel Rating Curve (Crossing: Phase 3)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
0.00	758.83	1.33
8.98	758.83	1.33
17.97	758.83	1.33
26.95	758.83	1.33
35.94	758.83	1.33
44.92	758.83	1.33
53.91	758.83	1.33
62.89	758.83	1.33
71.88	758.83	1.33
80.86	758.83	1.33
89.85	758.83	1.33

Table 9 - Summary of Culvert Flows at Crossing: Phase 3

Headwater Elevation (ft)	Total Discharge (cfs)	3-3' dia. HDPE Discharge (cfs)	Roadway Discharge (cfs)	Iterations
758.83	0.00	0.00	0.00	1
758.85	8.98	8.98	0.00	1
758.92	17.97	17.97	0.00	1
759.06	26.95	26.95	0.00	1
759.13	35.94	35.94	0.00	1
759.36	44.92	44.92	0.00	1
759.57	53.91	53.91	0.00	1
759.78	62.89	62.89	0.00	1
759.98	71.88	71.88	0.00	1
760.19	80.86	80.86	0.00	1
760.40	89.85	89.85	0.00	1
761.00	113.80	113.80	0.00	Overtopping

Rating Curve Plot for Crossing: Phase 3



Phase 4 Contact Water Basin Culverts

Site Data - 2-3' dia. HDPE

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft

Inlet Elevation: 763.00 ft

Outlet Station: 198.50 ft

Outlet Elevation: 757.00 ft

Number of Barrels: 2

Culvert Data Summary - 2-3' dia. HDPE

Barrel Shape: Circular

Barrel Diameter: 3.00 ft

Barrel Material: Smooth HDPE

Embedment: 0.00 in

Barrel Manning's n: 0.0120

Culvert Type: Straight

Inlet Configuration: Thin Edge Projecting

Inlet Depression: NONE

Tailwater Channel Data - Phase 4

Tailwater Channel Option: Enter Constant Tailwater Elevation

Constant Tailwater Elevation: 762.35 ft

Roadway Data for Crossing: Phase 4

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 20.00 ft

Crest Elevation: 780.00 ft

Roadway Surface: Gravel

Roadway Top Width: 16.00 ft

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 0 cfs

Design Flow: 73.93 cfs

Maximum Flow: 73.93 cfs

Table 10 - Culvert Summary Table: 2-3' dia. HDPE

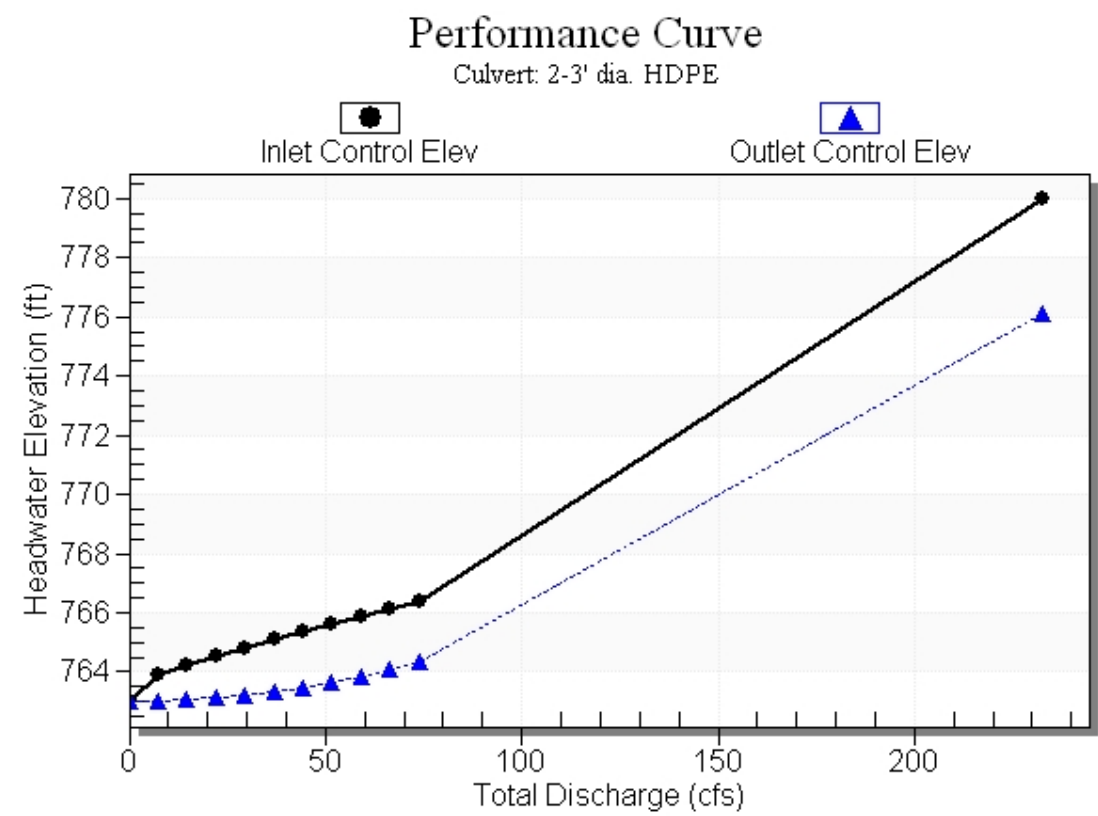
Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
	0.00	0.00	763.00	0.000	0.000	0-NF	0.000	0.000	3.000	-0.650	0.000
	7.39	7.39	763.87	0.869	0.010	1-JS1f	0.334	0.595	3.000	-0.650	0.548
	14.79	14.79	764.24	1.241	0.050	1-JS1f	0.479	0.850	3.000	-0.650	1.095
	22.18	22.18	764.54	1.536	0.116	1-JS1f	0.594	1.053	3.000	-0.650	1.643
	29.57	29.57	764.82	1.816	0.209	1-JS1f	0.682	1.221	3.000	-0.650	2.191
	36.97	36.97	765.08	2.080	0.328	1-JS1f	0.771	1.377	3.000	-0.650	2.739
	44.36	44.36	765.33	2.335	0.474	1-JS1f	0.849	1.514	3.000	-0.650	3.286
	51.75	51.75	765.59	2.588	0.646	1-JS1f	0.916	1.637	3.000	-0.650	3.834
	59.14	59.14	765.85	2.846	0.844	1-JS1f	0.983	1.756	3.000	-0.650	4.382
	66.54	66.54	766.11	3.114	1.069	5-JS1f	1.049	1.869	3.000	-0.650	4.930
	73.93	73.93	766.40	3.397	1.321	5-JS1f	1.112	1.973	3.000	-0.650	5.477

Straight Culvert

Inlet Elevation (invert): 763.00 ft, Outlet Elevation (invert): 757.00 ft

Culvert Length: 198.59 ft, Culvert Slope: 0.0302

Culvert Performance Curve Plot: 2-3' dia. HDPE



Water Surface Profile Plot for Culvert: 2-3' dia. HDPE

Crossing - Phase 4, Design Discharge - 73.9 cfs

Culvert - 2-3' dia. HDPE, Culvert Discharge - 73.9 cfs

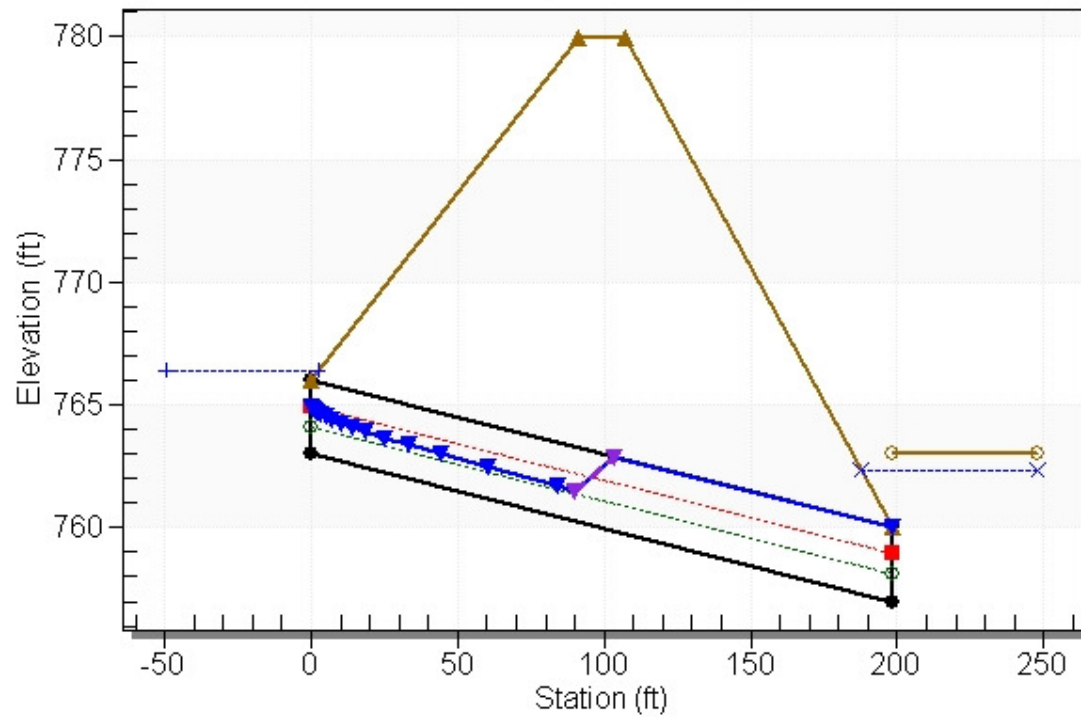


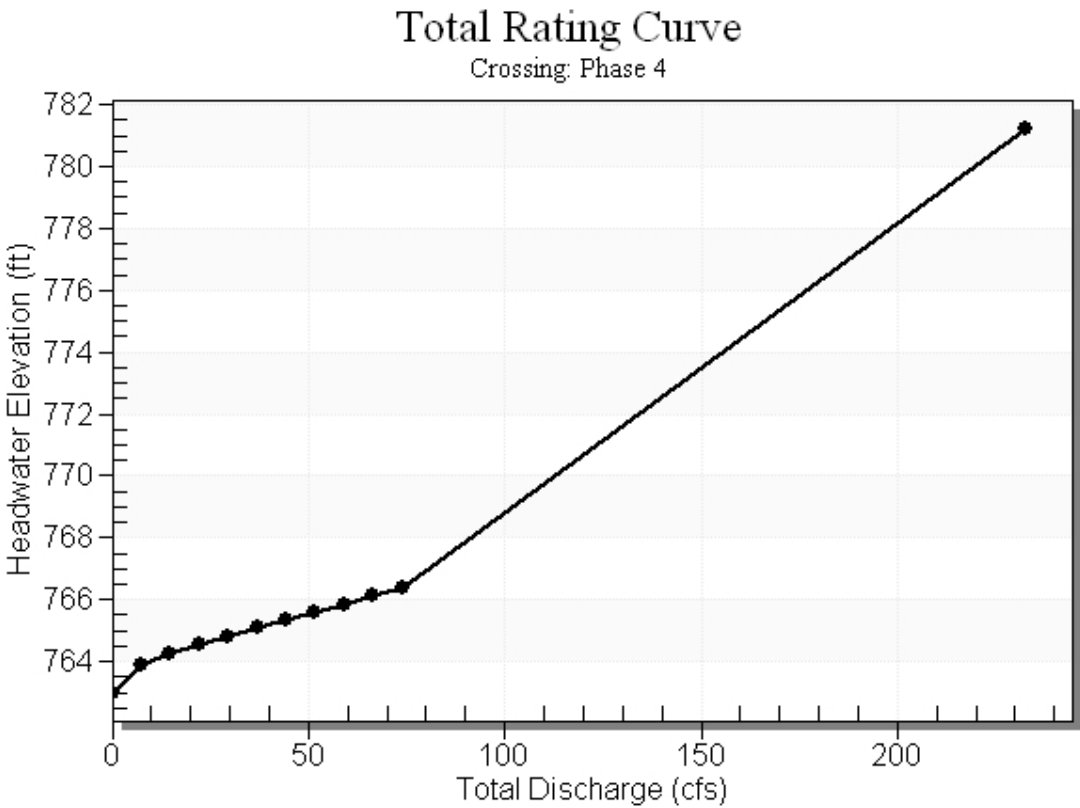
Table 11 - Downstream Channel Rating Curve (Crossing: Phase 4)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
0.00	762.35	-0.65
7.39	762.35	-0.65
14.79	762.35	-0.65
22.18	762.35	-0.65
29.57	762.35	-0.65
36.97	762.35	-0.65
44.36	762.35	-0.65
51.75	762.35	-0.65
59.14	762.35	-0.65
66.54	762.35	-0.65
73.93	762.35	-0.65

Table 12 - Summary of Culvert Flows at Crossing: Phase 4

Headwater Elevation (ft)	Total Discharge (cfs)	2-3' dia. HDPE Discharge (cfs)	Roadway Discharge (cfs)	Iterations
763.00	0.00	0.00	0.00	1
763.87	7.39	7.39	0.00	1
764.24	14.79	14.79	0.00	1
764.54	22.18	22.18	0.00	1
764.82	29.57	29.57	0.00	1
765.08	36.97	36.97	0.00	1
765.33	44.36	44.36	0.00	1
765.59	51.75	51.75	0.00	1
765.85	59.14	59.14	0.00	1
766.11	66.54	66.54	0.00	1
766.40	73.93	73.93	0.00	1
780.00	232.76	232.76	0.00	Overtopping

Rating Curve Plot for Crossing: Phase 4



Phase 5 Contact Water Basin Culverts

Site Data - 3-3' dia. HDPE

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft

Inlet Elevation: 760.00 ft

Outlet Station: 75.90 ft

Outlet Elevation: 757.00 ft

Number of Barrels: 3

Culvert Data Summary - 3-3' dia. HDPE

Barrel Shape: Circular

Barrel Diameter: 3.00 ft

Barrel Material: Smooth HDPE

Embedment: 0.00 in

Barrel Manning's n: 0.0120

Culvert Type: Straight

Inlet Configuration: Thin Edge Projecting

Inlet Depression: NONE

Tailwater Channel Data - Phase 5

Tailwater Channel Option: Enter Constant Tailwater Elevation

Constant Tailwater Elevation: 756.27 ft

Roadway Data for Crossing: Phase 5

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 110.00 ft

Crest Elevation: 764.00 ft

Roadway Surface: Gravel

Roadway Top Width: 8.00 ft

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 0 cfs

Design Flow: 89.4 cfs

Maximum Flow: 89.4 cfs

Table 13 - Culvert Summary Table: 3-3' dia. HDPE

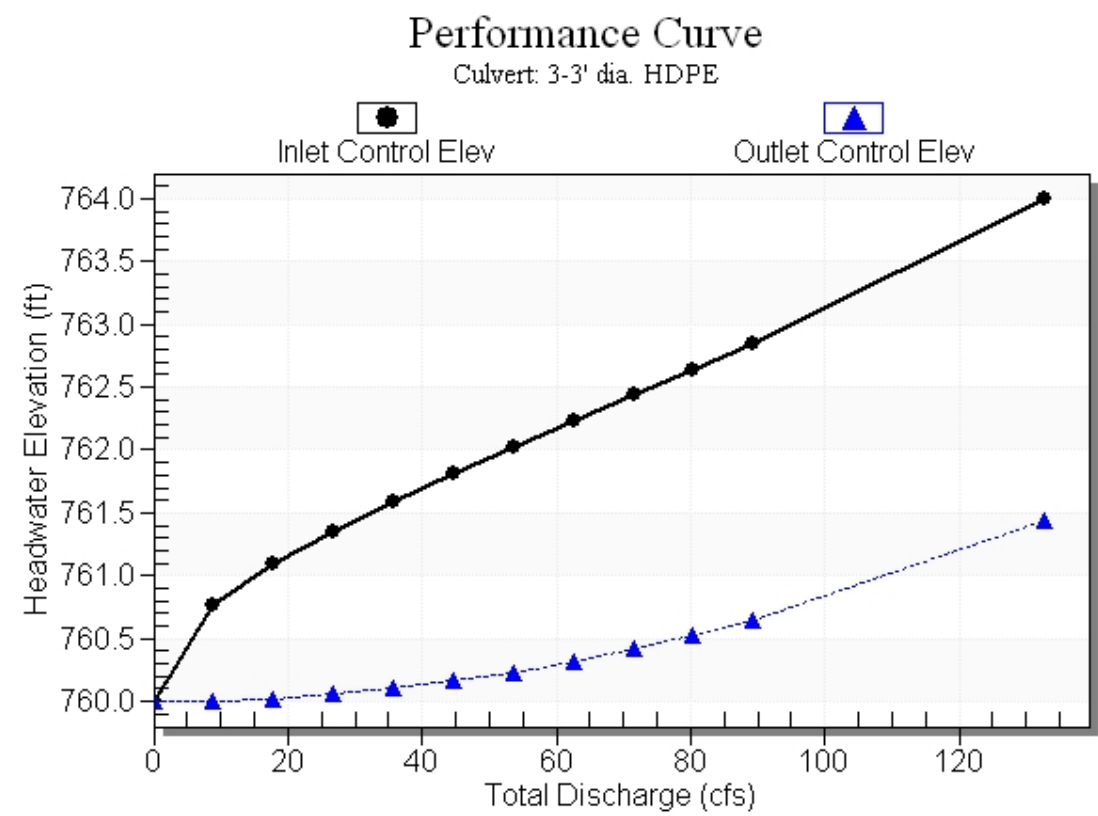
Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
	0.00	0.00	760.00	0.000	0.000	0-NF	0.000	0.000	3.000	-3.730	0.000
	8.94	8.94	760.76	0.761	0.004	1-JS1f	0.291	0.535	3.000	-3.730	0.442
	17.88	17.88	761.09	1.091	0.024	1-JS1f	0.393	0.763	3.000	-3.730	0.883
	26.82	26.82	761.35	1.353	0.056	1-JS1f	0.496	0.940	3.000	-3.730	1.325
	35.76	35.76	761.59	1.587	0.102	1-JS1f	0.578	1.091	3.000	-3.730	1.766
	44.70	44.70	761.81	1.810	0.161	1-JS1f	0.640	1.226	3.000	-3.730	2.208
	53.64	53.64	762.02	2.023	0.233	1-JS1f	0.702	1.353	3.000	-3.730	2.649
	62.58	62.58	762.23	2.230	0.318	1-JS1f	0.765	1.467	3.000	-3.730	3.091
	71.52	71.52	762.43	2.435	0.415	1-S2n	0.825	1.571	0.898	-3.730	13.352
	80.46	80.46	762.64	2.640	0.526	1-S2n	0.872	1.671	0.961	-3.730	13.690
	89.40	89.40	762.85	2.848	0.650	1-S2n	0.919	1.763	1.020	-3.730	14.033

Straight Culvert

Inlet Elevation (invert): 760.00 ft, Outlet Elevation (invert): 757.00 ft

Culvert Length: 75.96 ft, Culvert Slope: 0.0395

Culvert Performance Curve Plot: 3-3' dia. HDPE



Water Surface Profile Plot for Culvert: 3-3' dia. HDPE

Crossing - Phase 5, Design Discharge - 89.4 cfs

Culvert - 3-3' dia. HDPE, Culvert Discharge - 89.4 cfs

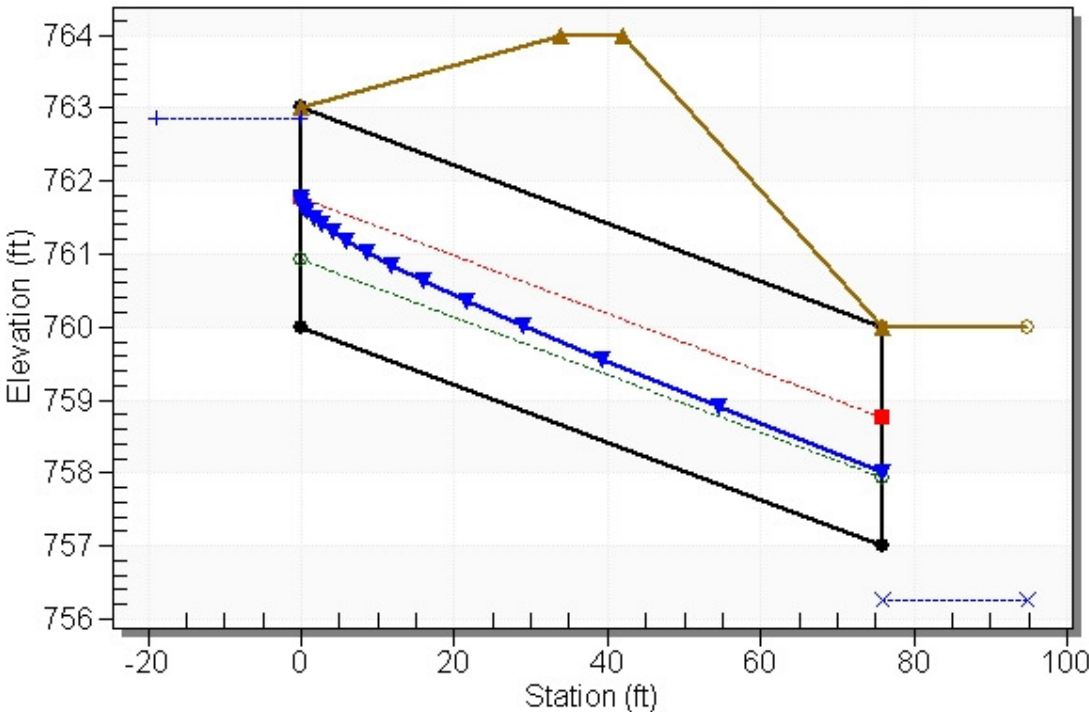


Table 14 - Downstream Channel Rating Curve (Crossing: Phase 5)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
0.00	756.27	-3.73
8.94	756.27	-3.73
17.88	756.27	-3.73
26.82	756.27	-3.73
35.76	756.27	-3.73
44.70	756.27	-3.73
53.64	756.27	-3.73
62.58	756.27	-3.73
71.52	756.27	-3.73
80.46	756.27	-3.73
89.40	756.27	-3.73

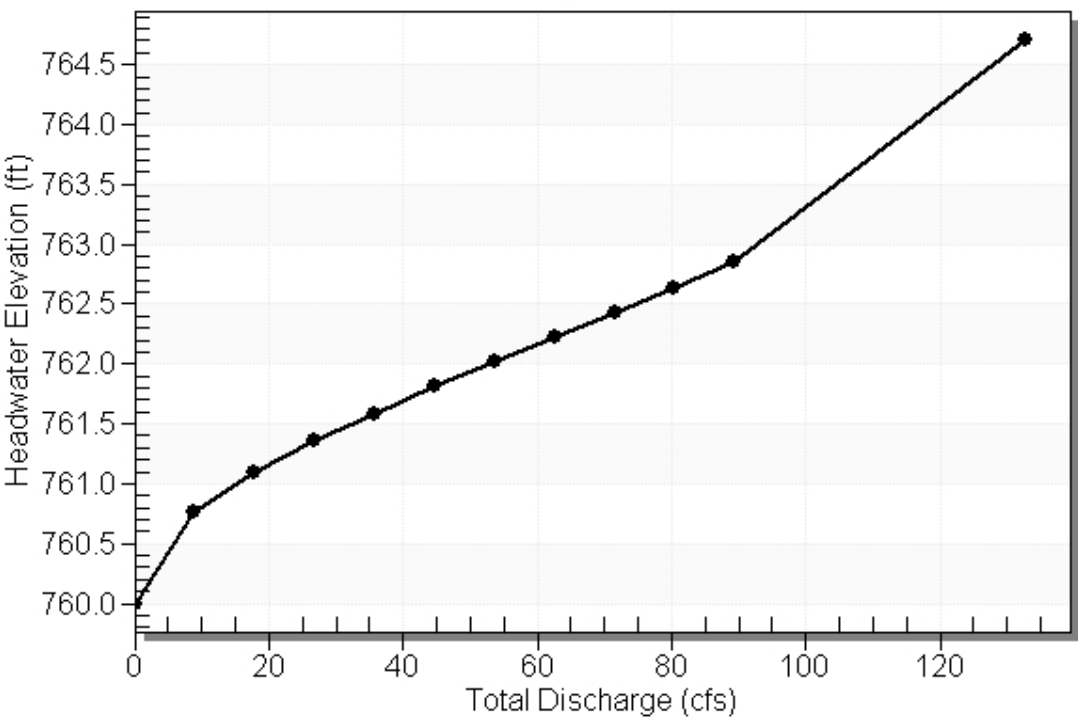
Table 15 - Summary of Culvert Flows at Crossing: Phase 5

Headwater Elevation (ft)	Total Discharge (cfs)	3-3' dia. HDPE Discharge (cfs)	Roadway Discharge (cfs)	Iterations
760.00	0.00	0.00	0.00	1
760.76	8.94	8.94	0.00	1
761.09	17.88	17.88	0.00	1
761.35	26.82	26.82	0.00	1
761.59	35.76	35.76	0.00	1
761.81	44.70	44.70	0.00	1
762.02	53.64	53.64	0.00	1
762.23	62.58	62.58	0.00	1
762.43	71.52	71.52	0.00	1
762.64	80.46	80.46	0.00	1
762.85	89.40	89.40	0.00	1
764.00	132.70	132.70	0.00	Overtopping

Rating Curve Plot for Crossing: Phase 5

Total Rating Curve

Crossing: Phase 5



Phase 6 Contact Water Basin Culverts

Site Data - 2-3' dia. HDPE

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft

Inlet Elevation: 795.00 ft

Outlet Station: 311.00 ft

Outlet Elevation: 757.00 ft

Number of Barrels: 2

Culvert Data Summary - 2-3' dia. HDPE

Barrel Shape: Circular

Barrel Diameter: 3.00 ft

Barrel Material: Smooth HDPE

Embedment: 0.00 in

Barrel Manning's n: 0.0120

Culvert Type: Straight

Inlet Configuration: Square Edge with Headwall

Inlet Depression: NONE

Tailwater Channel Data - Phase 6

Tailwater Channel Option: Enter Constant Tailwater Elevation

Constant Tailwater Elevation: 758.00 ft

Roadway Data for Crossing: Phase 6

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 35.00 ft

Crest Elevation: 800.00 ft

Roadway Surface: Paved

Roadway Top Width: 20.00 ft

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 0 cfs

Design Flow: 107 cfs

Maximum Flow: 107 cfs

Table 1 - Culvert Summary Table: 2-3' dia. HDPE

Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
	0.00	0.00	795.00	0.000	0.000	0-NF	0.000	0.000	1.000	5.000	0.000
	10.70	10.70	795.90	0.901	0.0*	1-S2n	0.293	0.722	0.293	5.000	16.820
	21.40	21.40	796.30	1.300	0.0*	1-S2n	0.398	1.034	0.398	5.000	18.605
	32.10	32.10	796.65	1.653	0.0*	1-S2n	0.502	1.277	0.502	5.000	20.333
	42.80	42.80	797.01	2.008	0.0*	1-S2n	0.583	1.487	0.583	5.000	22.424
	53.50	53.50	797.33	2.329	0.0*	1-S2n	0.647	1.669	0.647	5.000	23.644
	64.20	64.20	797.64	2.640	0.0*	1-S2n	0.710	1.835	0.710	5.000	24.862
	74.90	74.90	797.96	2.959	0.0*	1-S2n	0.774	1.986	0.774	5.000	25.812
	85.60	85.60	798.30	3.302	0.0*	5-S2n	0.833	2.129	0.833	5.000	26.773
	96.30	96.30	798.68	3.678	0.0*	5-S2n	0.881	2.257	0.881	5.000	27.721
	107.00	107.00	799.10	4.097	0.0*	5-S2n	0.929	2.374	0.953	5.000	27.617

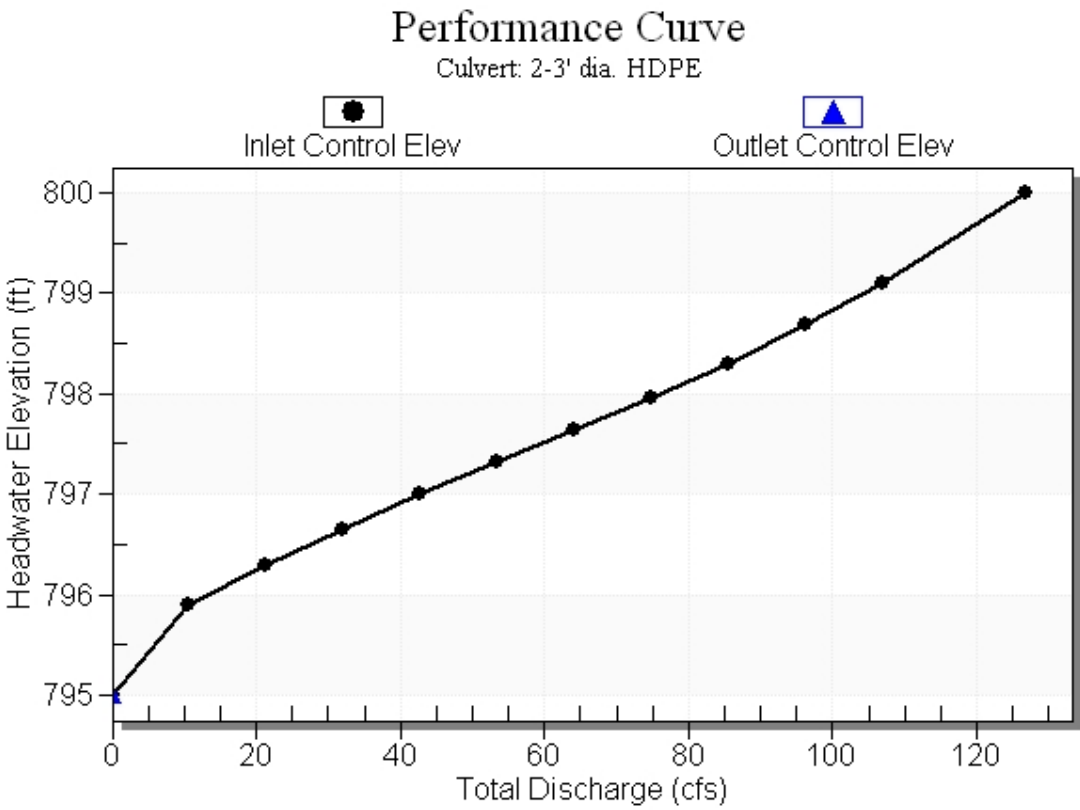
* Full Flow Headwater elevation is below inlet invert.

Straight Culvert

Inlet Elevation (invert): 795.00 ft, Outlet Elevation (invert): 757.00 ft

Culvert Length: 313.31 ft, Culvert Slope: 0.1222

Culvert Performance Curve Plot: 2-3' dia. HDPE



Water Surface Profile Plot for Culvert: 2-3' dia. HDPE

Crossing - Phase 6, Design Discharge - 107.0 cfs

Culvert - 2-3' dia. HDPE, Culvert Discharge - 107.0 cfs

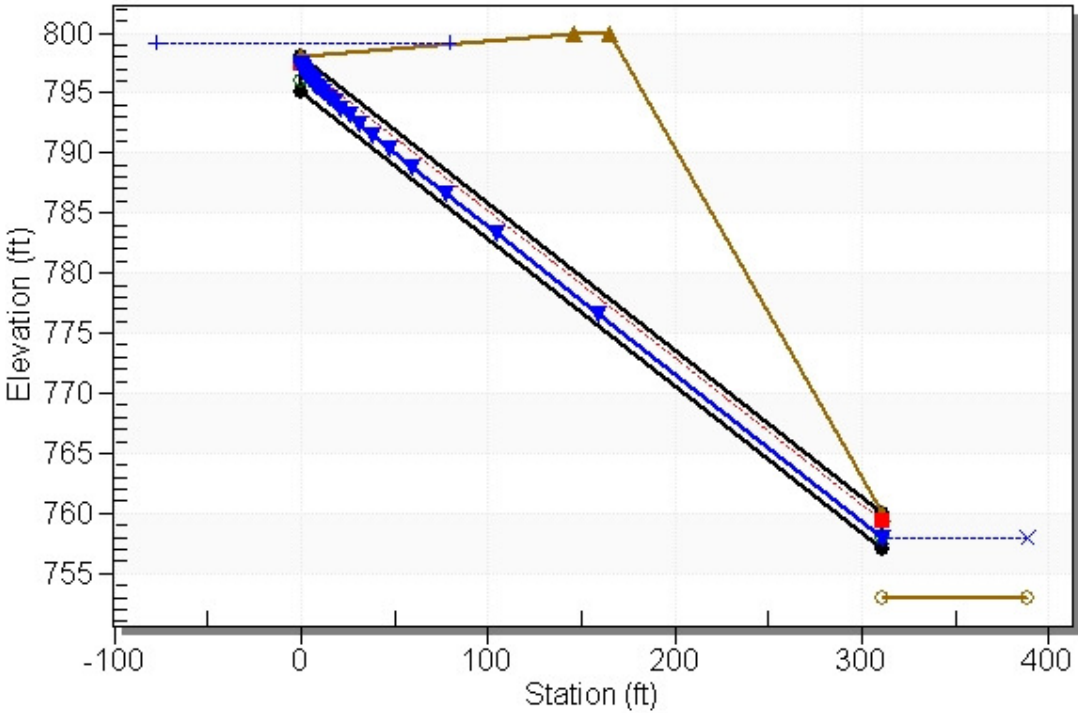


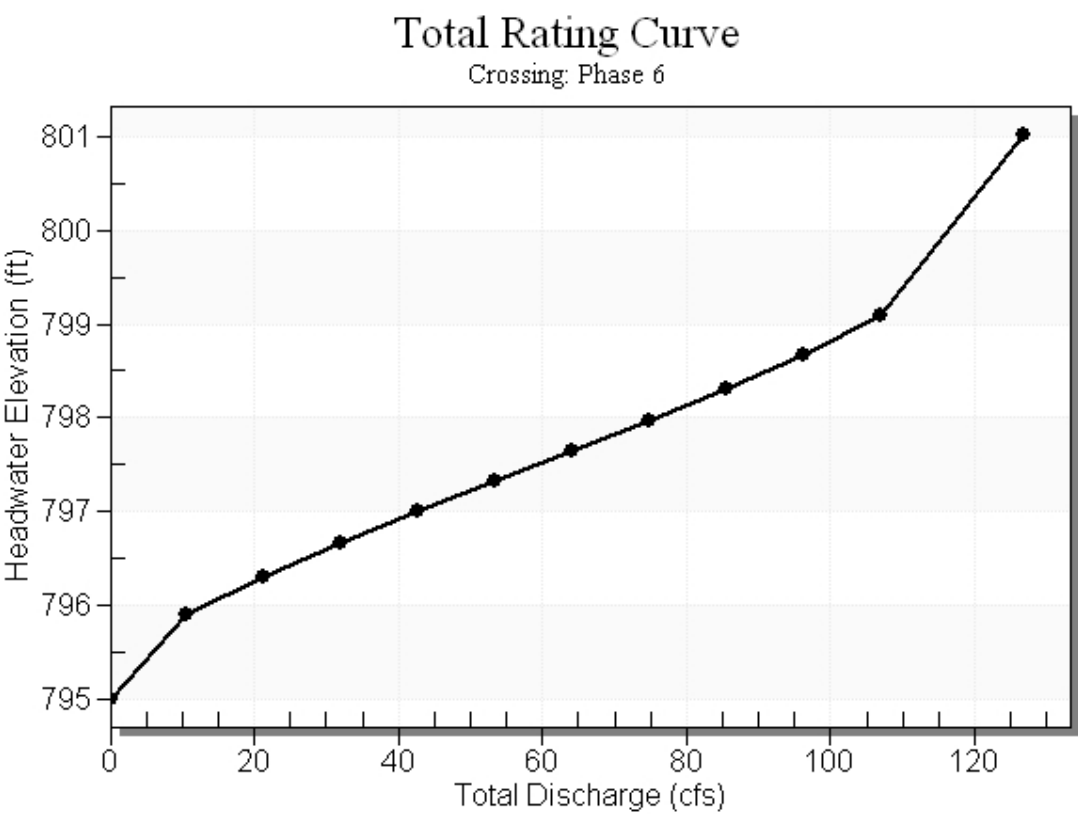
Table 2 - Downstream Channel Rating Curve (Crossing: Phase 6)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
0.00	758.00	5.00
10.70	758.00	5.00
21.40	758.00	5.00
32.10	758.00	5.00
42.80	758.00	5.00
53.50	758.00	5.00
64.20	758.00	5.00
74.90	758.00	5.00
85.60	758.00	5.00
96.30	758.00	5.00
107.00	758.00	5.00

Table 3 - Summary of Culvert Flows at Crossing: Phase 6

Headwater Elevation (ft)	Total Discharge (cfs)	2-3' dia. HDPE Discharge (cfs)	Roadway Discharge (cfs)	Iterations
795.00	0.00	0.00	0.00	1
795.90	10.70	10.70	0.00	1
796.30	21.40	21.40	0.00	1
796.65	32.10	32.10	0.00	1
797.01	42.80	42.80	0.00	1
797.33	53.50	53.50	0.00	1
797.64	64.20	64.20	0.00	1
797.96	74.90	74.90	0.00	1
798.30	85.60	85.60	0.00	1
798.68	96.30	96.30	0.00	1
799.10	107.00	107.00	0.00	1
800.00	126.83	126.83	0.00	Overtopping

Rating Curve Plot for Crossing: Phase 6



Contact Water Perimeter and Interior Diversion Berm/Swale Sizing

Job No. 25211509.3

Job: Proposed Expansion

By: BLP

Date: 11/26/13

Client: OML

Subject: Perimeter Contact Water Div Berm

Chk'd: MRH

Date: 11/27/13

Contact Water Perimeter and Interior Diversion Berm/Swale Sizing

Size the perimeter and interior swales to route the contact water runoff from the waste sideslopes to the culverts in the active phase that will then discharge to the temporary contact water basin for each phase. Sizing is based on a 25-year, 24-hour storm event

Use Manning's equation to determine flow depth in the perimeter ditch

$$\text{Manning's Equation: } Q = (1.49/n) \times A \times R^{2/3} \times S^{1/2}$$

where: Q = Flow rate, cfs (from HydroCAD model for 25-year, 24-hour storm)

n = Manning's roughness coefficient (assumed smooth surface, 0.013)

A = Flow area, sf

R = Hydraulic radius, ft

S = Channel slope, ft/ft

Vary the flow depth input value below until the flow rate estimated by HydroCAD is achieved.

From HydroCAD modeling for hydrograph generation, the peak runoff rate from the phase area to a temporary contact water basin is 144.5 cfs (Phase 2).

Phase 1 flow from phase area to perimeter diversion berm, Q = 112 cfs

Inputs for Trapezoidal Channel		Calculations/Output	
Depth of flow, y =	1.72 ft	Cross-sectional area, A =	4.4 sf
Channel side slope, H/V =	1 :1	Wetted perimeter, P =	6.3 ft
Channel side slope, H/V =	2 :1	Hydraulic radius, R =	0.7 ft
Manning's roughness, n =	0.013	Discharge, Q =	112 cfs
Channel bottom slope, s =	0.077 ft/ft	Average velocity, V =	25.24 ft/s

Phase 2 flow from phase area to perimeter diversion berm, Q = 145 cfs (Note: Minimum perimeter berm slope modeled below; majority of Phase 2 perimeter berm slope is greater than 1%; results below are worst-case and in limited area)

Inputs for Trapezoidal Channel		Calculations/Output	
Depth of flow, y =	2.78 ft	Cross-sectional area, A =	11.6 sf
Channel side slope, H/V =	1 :1	Wetted perimeter, P =	10.1 ft
Channel side slope, H/V =	2 :1	Hydraulic radius, R =	1.1 ft
Manning's roughness, n =	0.013	Discharge, Q =	145 cfs
Channel bottom slope, s =	0.01 ft/ft	Average velocity, V =	12.53 ft/s

Phase 3 flow from phase area to perimeter diversion berm, Q = 90 cfs

Inputs for Trapezoidal Channel		Calculations/Output	
Depth of flow, y =	2.32 ft	Cross-sectional area, A =	8.1 sf
Channel side slope, H/V =	1 :1	Wetted perimeter, P =	8.5 ft
Channel side slope, H/V =	2 :1	Hydraulic radius, R =	1.0 ft
Manning's roughness, n =	0.013	Discharge, Q =	90 cfs
Channel bottom slope, s =	0.01 ft/ft	Average velocity, V =	11.10 ft/s

Contact Water Perimeter and Interior Diversion Berm/Swale Sizing

Phase 4 flow from phase area to perimeter diversion berm, $Q = 74$ cfs (Note: Minimum 1% perimeter berm slope modeled below - worst-case)

Inputs for Trapezoidal Channel	Calculations/Output
Depth of flow, $y = 2.16$ ft	Cross-sectional area, $A = 7.0$ sf
Channel side slope, $H/V = 1 : 1$	Wetted perimeter, $P = 7.9$ ft
Channel side slope, $H/V = 2 : 1$	Hydraulic radius, $R = 0.9$ ft
Manning's roughness, $n = 0.013$	Discharge, $Q = 74$ cfs
Channel bottom slope, $s = 0.01$ ft/ft	Average velocity, $V = 10.59$ ft/s

Phase 5 flow from phase area to perimeter diversion berm, $Q = 89$ cfs

Inputs for Trapezoidal Channel	Calculations/Output
Depth of flow, $y = 2.31$ ft	Cross-sectional area, $A = 8.0$ sf
Channel side slope, $H/V = 1 : 1$	Wetted perimeter, $P = 8.4$ ft
Channel side slope, $H/V = 2 : 1$	Hydraulic radius, $R = 0.9$ ft
Manning's roughness, $n = 0.013$	Discharge, $Q = 89$ cfs
Channel bottom slope, $s = 0.01$ ft/ft	Average velocity, $V = 11.07$ ft/s

Phase 6 flow from phase area to perimeter diversion berm, $Q = 107$ cfs

Inputs for Trapezoidal Channel	Calculations/Output
Depth of flow, $y = 2.48$ ft	Cross-sectional area, $A = 9.2$ sf
Channel side slope, $H/V = 1 : 1$	Wetted perimeter, $P = 9.1$ ft
Channel side slope, $H/V = 2 : 1$	Hydraulic radius, $R = 1.0$ ft
Manning's roughness, $n = 0.013$	Discharge, $Q = 107$ cfs
Channel bottom slope, $s = 0.01$ ft/ft	Average velocity, $V = 11.61$ ft/s

Phase 2 flow from phase area to interior diversion berm, $Q = 145$ cfs

Inputs for Trapezoidal Channel	Calculations/Output
Depth of flow, $y = 2.23$ ft	Cross-sectional area, $A = 12.4$ sf
Channel side slope, $H/V = 3 : 1$	Wetted perimeter, $P = 12.0$ ft
Channel side slope, $H/V = 2 : 1$	Hydraulic radius, $R = 1.0$ ft
Manning's roughness, $n = 0.013$	Discharge, $Q = 146$ cfs
Channel bottom slope, $s = 0.01$ ft/ft	Average velocity, $V = 11.71$ ft/s

Manning's roughness coefficient reference table (source: Engineering Tool Box website):

Surface Material	Manning's Roughness Coefficient - n -
Asbestos cement	0.011
Asphalt	0.016
Brass	0.011
Brickwork	0.015
Cast-iron, new	0.012
Clay tile	0.014
Concrete - steel forms	0.011
Concrete - finished	0.012
Concrete - wooden forms	0.015
Concrete - centrifugally spun	0.013
Copper	0.011
Corrugated metal	0.022
Earth	0.025
Earth channel - clean	0.022
Earth channel - gravelly	0.025
Earth channel - weedy	0.030
Earth channel - stony, cobbles	0.035

Assume Manning's of 0.013 for hardened CCR

Assume Manning's of 0.013, which is between the various concrete roughness coefficients.

Storm Water Management Calculations**Purpose:**

The purpose of the storm water runoff calculations is to demonstrate that the proposed landfill surface water management system design meets the requirements of the Iowa Administrative Code, Environmental Protection Commission [567], Chapter 113.7(8)a(2) for providing a runoff control system to collect and control peak discharge from a 25-year storm event.

Approach:Final Cover Soil Loss

The Universal Soil Loss Equation (USLE) was used to estimate soil loss along the final cover slopes. The USLE estimates the final cover soil erosion based on the erodibility of the soil, the rainfall and runoff erosivity, the slope steepness, cover management, and soil practice factors. A maximum soil loss of 3 tons per acre is considered acceptable.

Hydrograph Generation

To properly size the storm water management features, runoff hydrographs for the 25-year, 24-hour, and 100-year, 24-hour, storm events were developed. HydroCAD was used to model the storm water management system and develop the hydrographs using TR-20 methodologies. The model is designed to simulate the surface runoff response of a watershed to a precipitation event. Input parameters for the model include precipitation depth for the design storm event, contributing drainage areas, runoff curve numbers, time of concentration, and travel time.

The final cover watersheds are shown on **Figure 1**.

Perimeter Ditch and Diversion Berm Sizing

Diversion berms and perimeter ditches outside the landfill limits were sized for the 25-year, 24-hour storm event using the Manning's equation to determine the depth of flow and velocity in the berm/ditch based on the berm/ditch geometry and peak flow in the berm/ditch (as determined by the Hydrograph Generation calculations). The Iowa NRCS Rock Chute Design spreadsheet was used for steep-slope locations.

Downslope Flume and Energy Dissipator Sizing

The downslope flume inlets were sized for the 25-year, 24-hour storm event using the orifice equation. The downslope flume pipes were sized based on the peak flow conditions in the pipe using Manning's equation. Energy dissipators were sized using tables from the reference book "Hydraulic Design of Energy Dissipators for Culvert and Channels," US Department of Transportation, Federal Highway Administration, July 2006.

Culvert Sizing

The culverts were sized for the 25-year, 24-hour storm event using the HY-8 computer model developed by the US Department of Transportation, Federal Highway Administration. Culvert outlet protection was sizing using guidance from the Iowa Statewide Urban Design and Specifications (SUDAS) Design Manual, Chapter 7E-10 – Riprap.

Haul Road Culvert Sizing

Culverts were sized for the 25-year, 24-hour storm event for placement under the haul road.

Sedimentation Basin Sizing

The permanent sedimentation basin sizing process involved determining an appropriate ratio of surface area to flow rate that would allow particles to settle out during a design storm event. The sedimentation

basins were sized for the 25-year, 24-hour storm event. The sedimentation basin emergency spillways were sized for the 100-year, 24-hour storm event.

A table presented in the "Erosion and Sediment Control Handbook" (Goldman, et. Al., 1986) provides the surface area-to-discharge ratio required to achieve settlement of the desired particle sizes.

The HydroCAD model was used in conjunction with accepted formulas and engineering calculations to size the sedimentation basins.

Key Assumptions:

- Runoff curve numbers were based on tables presented in Urban Hydrology for Small Watersheds, and were assumed as follows

Cover Type	CN
Landfill final cover	74 – Pasture/grassland/range in good condition, hydrologic soil group C
Gravel access road	96 – Compacted gravel surface
Sedimentation basins	98 – Water surface

- A Type II rainfall distribution was used, based on figures presented in Urban Hydrology for Small Watersheds. The following precipitation depths were assumed.

Storm Event	Precipitation Depth (inches)
2-year, 24-hour	3.14
25-year, 24-hour	5.67
100-year, 24-hour	7.59

- Other assumptions are included with the calculations attached to this appendix.

Results:

The proposed landfill surface water management system design meets the requirements of the Iowa Administrative Code, Environmental Protection Commission [567], Chapter 113.7(8)a(2). Further details are provided below.

Soil Loss

The USLE calculations indicate a minimal soil loss rate along the 20H:1V final cover sideslopes. Therefore, the 4H:1V final cover sideslopes were used to determine appropriate diversion berm spacing. The USLE calculations indicate that a 300 ft slope length will result in a soil loss rate of 3.0 tons/acre; therefore, diversion berms have been added at a maximum spacing of 300 ft to provide protection against rill formation along the final cover, to provide outlets for the final cover intermediate drains, and to provide soil loss reduction measures during vegetation establishment. Refer to the USLE Calculations section of this appendix for the detailed calculations.

Hydrograph Generation

The hydrograph modeling results for the 25-year and 100-year, 24-hour storm events are included the Hydrograph Generation section of this appendix.

Job No. 25211509.03 Job OML Expansion

BY JMO DATE 10/25/13

Client IPL Subject Storm Water Management

CHK'D. BP DATE 11/25/13

Perimeter Ditch and Diversion Berm Sizing

The diversion berms will be constructed as shown on the plan set. The diversion berms will maintain a minimum 0.5 foot freeboard. Refer to the Diversion Berm and Ditch Sizing section of this appendix for the detailed calculations.

The perimeter ditches will be constructed as shown on the plan set. The perimeter ditches will contain the runoff from the 25-year, 24-hour storm event and maintain a minimum 0.5 foot of freeboard. Two rock-lined channels will be constructed as shown on the plan set. Refer to the Diversion Berm and Ditch Sizing section of this appendix for the detailed calculations.

Downslope Flume and Energy Dissipator Sizing

The downslope flumes will be constructed as shown on the plan set. The downslope flumes are designed to accommodate the surface water runoff from the final cover for a 25-year, 24-hour storm event. Energy dissipators at the bottom of the downslope flumes have been designed to handle the peak velocities, and additional riprap protection has been sized for the energy dissipator outlets. Refer to the Downslope Flume and Energy Dissipator Sizing section of this appendix for the detailed calculations.

Culvert Sizing

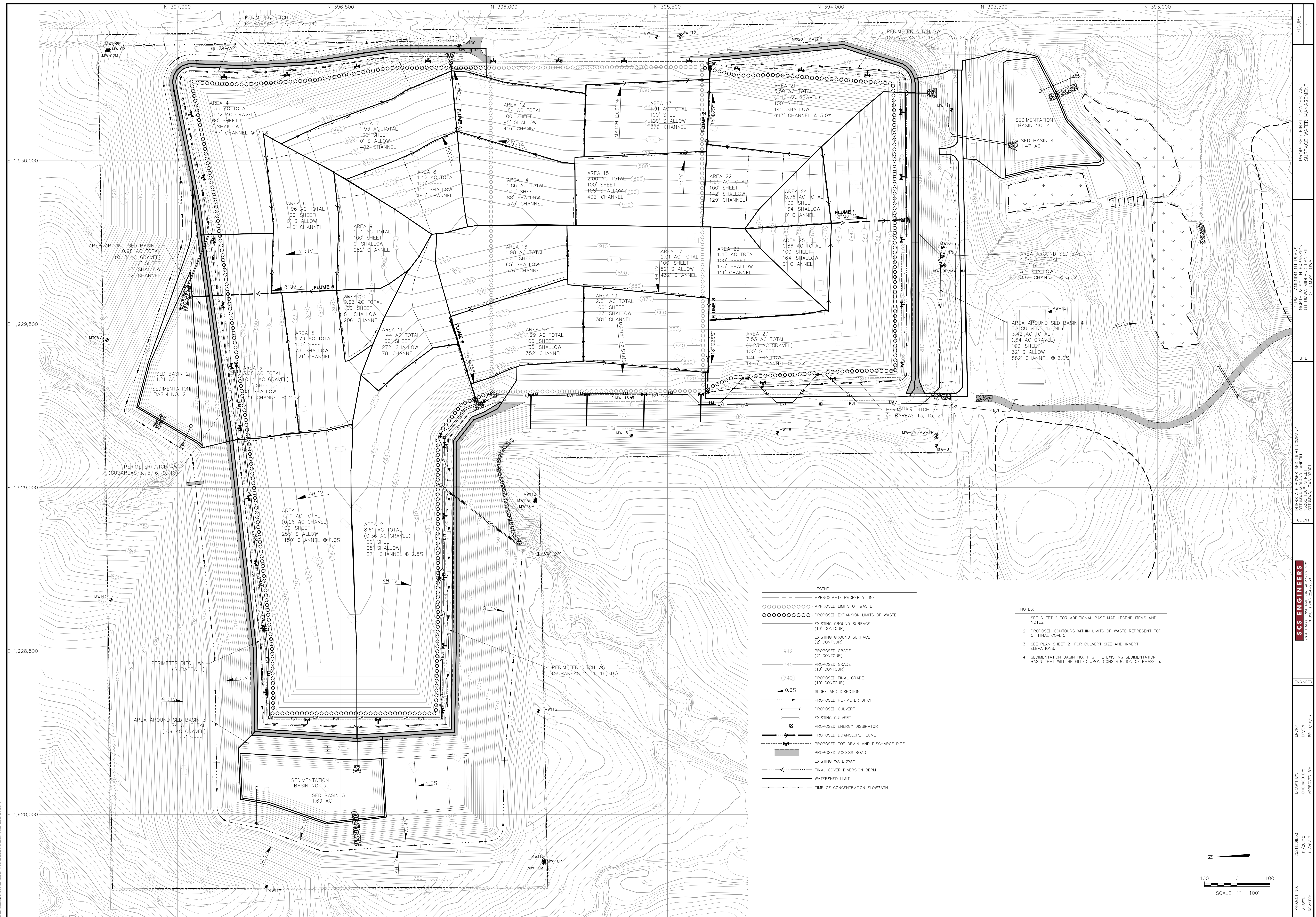
The culverts are designed to accommodate the flows from the perimeter ditches for the 25-year, 24-hour storm event. Riprap outlet protection has been sized based on the discharge rates and outlet velocities. Refer to the Culvert Sizing section of this appendix for the detailed calculations.

Haul Road Culvert Sizing

Culverts are designed to route flows from the stream for the 25-year, 24-hour storm event. Refer to the Haul Road Culvert Sizing section of this appendix for the detailed calculations. Refer to the Stream and Wetland Mitigation Plan for additional information on the stream crossing.

Sedimentation Basin Sizing

The principal outlet structures for the sedimentation basins are sized to control runoff from the 25-year, 24-hour storm event, assuming the starting water elevation is at the bottom of the lowest outlet structure opening. The sedimentation basins are designed to settle out particles 17 microns and larger in diameter. Refer to the Sedimentation Basin Sizing section of this appendix for the detailed calculations. The emergency spillways have been designed to pass the 100-year, 24-hour storm event.



USLE Calculation

Job No. 25211509.03

Job: Proposed Expansion

By: BLP

Date: 9/25/13

Client: IPL

Subject: Soil Loss Along Final Cover

Chk'd: JMO

Date: 10/14/2013

Universal Soil Loss Equation (USLE) Calculation

Use USLE to estimate soil loss along the 5% final cover slope, with the goal of maintaining ≤ 3 ton/acre of soil loss along the final cover.

USLE Equation:

$$A = R * K * LS * C * P$$

where: A = Average annual soil loss, ton/acre

R = Rainfall and runoff erosivity index

K = Soil erodibility factor, tons/acre

LS = Slope length and steepness factor

C = Cover management factor

P = Practice factor

The LS factor is a function of the slope and flow length.

$$LS = L * S$$

where: L = Slope length factor = $(l/72.6)^m$

where: l = Slope length, feet

m = Slope-length exponent (m = 0.3 for slopes of 1% to 3%)

m = 0.4 for slopes of 3.5% to 4.5%

m = 0.5 for slopes greater than 5%)

$$S = \text{Slope steepness factor} = (65.41s^2 / (s^2 + 10,000)) + (4.56s / (\text{SQRT}(s^2 + 10,000))) + 0.065$$

where: s = Slope, in percent

The soil type chosen for selecting the appropriate K factor is based on surface soil descriptions included in Table 5 of the Expansion Soil and Hydrogeologic Investigation Report (SCS, September 2013). The top layer of surface soils consists of silt loam, silty clay loam, and loam, with the majority consisting of silt loam. Silt loam with an organic matter content of 2% was assumed.

Data Entered

Slope (%), s = 5

l = 80

m = 0.5

Data Computed

S = 0.46

L = 1.0

LS = 0.5

(Note: 80 feet is the maximum slope length along the 5% slope)

Calculate Average Annual Soil Loss, A:

R = 175 *

K = 0.42 *

LS = 0.5

C = 0.004 *

P = 1.0 *

$$A = R * K * LS * C * P = 0.1 \text{ tons/acre}$$

* See attached references for R, K, C, and P factors

Soil loss along the 5% slope of the final cover results in minimal soil loss. Diversion berm spacing along the 25% final cover slope are more critical.

Job No. 25211509.03

Job: Proposed Expansion

By: BLP

Date: 9/25/13

Client: IPL

Subject: Soil Loss Along Final Cover

Chk'd: JMO

Date: 10/14/2013

Universal Soil Loss Equation (USLE) Calculation

Use USLE to estimate soil loss along the 25% final cover slope, with the goal of maintaining ≤ 3 ton/acre of soil loss along the final cover.

USLE Equation:

$$A = R * K * LS * C * P$$

where: A = Average annual soil loss, ton/acre
 R = Rainfall and runoff erosivity index
 K = Soil erodibility factor, tons/acre
 LS = Slope length and steepness factor
 C = Cover management factor
 P = Practice factor

The LS factor is a function of the slope and flow length.

$$LS = L * S$$

where: L = Slope length factor = $(l/72.6)^m$

where: l = Slope length, feet

m = Slope-length exponent (m = 0.3 for slopes of 1% to 3%
 m = 0.4 for slopes of 3.5% to 4.5%
 m = 0.5 for slopes greater than 5%)

$$S = \text{Slope steepness factor} = (65.41s^2/(s^2 + 10,000)) + (4.56s/(\text{SQRT}(s^2 + 10,000))) + 0.065$$

where: s = Slope, in percent

The soil type chosen for selecting the appropriate K factor is based on surface soil descriptions included in Table 5 of the Expansion Soil and Hydrogeologic Investigation Report (SCS, September 2013). The top layer of surface soils consists of silt loam, silty clay loam, and loam, with the majority consisting of silt loam. Silt loam with an organic matter content of 2% was assumed.

Data Entered

Slope (%), s = 25
 l = 300
 m = 0.5

Data Computed

S = 5.02
 L = 2.0
 LS = 10.2

Calculate Average Annual Soil Loss, A:

R = 175 *
 K = 0.42 *
 LS = 10.2
 C = 0.004 *
 P = 1.0 *

$$A = R * K * LS * C * P = 3.0 \text{ tons/acre}$$

* See attached references for R, K, C, and P factors

A maximum length of 300 feet should be provided between diversion berms along the 25% slope to maintain ≤ 3 ton/acre of soil loss along the final cover; this equates to maximum diversion berm spacing of 75 feet vertically.

Not only is erosion objectionable in itself but erosion can degrade the cover and seriously reduce its effectiveness.

Evaluate Erosion Potential

Step 19

The USDA universal soil loss equation (USLE) is a convenient tool for use in evaluating erosion potential. The USLE predicts average annual soil loss as the product of six quantifiable factors. The equation is:

$$A = R K L S C P$$

where A = average annual soil loss, in tons/acre

R = rainfall and runoff erosivity index

K = soil erodibility factor, tons/acre

L = slope-length factor

S = slope-steepness factor

C = cover-management factor

P = practice factor

The data necessary as input to this equation are available to the evaluator in a figure and tables included below. Note that the evaluations in Step 8 on soil composition and Steps 25-32 on vegetation all impact on the evaluation of erosion also.

Factor R in the USLE can be calculated empirically from climatological data. For average annual soil loss determinations, however, R can be obtained directly from Figure 20. Factor K, the average soil loss for a given

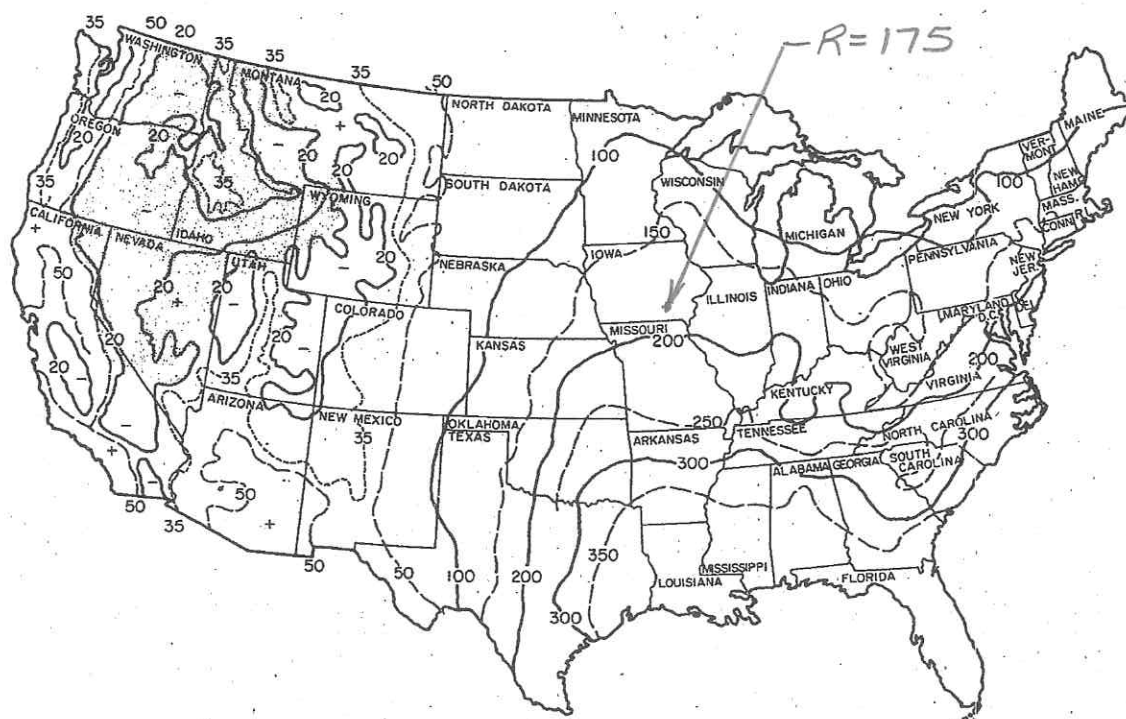


Figure 20. Average annual values of rainfall-erosivity factor R.¹¹

soil in a unit plot, pinpoints differences in erosion according to differences in soil type. Long-term plot studies under natural rainfall have produced K values generalized in Table 5 for the USDA soil types.

TABLE 5. APPROXIMATE VALUES OF FACTOR K FOR
USDA TEXTURAL CLASSES¹¹

Texture class	Organic matter content		
	<0.5%	2%	4%
	K	K	K
Sand	0.05	0.03	0.02
Fine sand	.16	.14	.10
Very fine sand	.42	.36	.28
Loamy sand	.12	.10	.08
Loamy fine sand	.24	.20	.16
Loamy very fine sand	.44	.38	.30
Sandy loam	.27	.24	.19
Fine sandy loam	.35	.30	.24
Very fine sandy loam	.47	.41	.33
Loam	.38	.34	.29
Silt loam	.48	.42	.33
Silt	.60	.52	.42
Sandy clay loam	.27	.25	.21
Clay loam	.28	.25	.21
Silty clay loam	.37	.32	.26
Sandy clay	.14	.13	.12
Silty clay	.25	.23	.19
Clay	0.13-0.29		

The values shown are estimated averages of broad ranges of specific-soil values. When a texture is near the borderline of two texture classes, use the average of the two K values.

The evaluator must next consider the shape of the slope in terms of length and inclination. The appropriate LS factor is obtained from Table 6. A nonlinear slope may have to be evaluated as a series of segments, each with uniform gradient. Two or three segments should be sufficient for most engineered landfills; provided the segments are selected so that they are also of equal length (Table 6 can be used, with certain adjustments). Enter Table 6 with the total slope length and read LS values corresponding to the percent slope of each segment. For three segments, multiply the chart LS values for the upper, middle, and lower segments by 0.58, 1.06, and 1.37, respectively. The average of the three products is a good estimate of the

TABLE 7. GENERALIZED VALUES OF FACTOR C FOR STATES
EAST OF THE ROCKY MOUNTAINS¹¹

Crop, rotation, and management	Productivity level	
	High	Mod.
	C value	
Base value: continuous fallow, tilled up and down slope	1.00	1.00
CORN		
C, RdR, fall TP, conv	0.54	0.62
C, RdR, spring TP, conv	.50	.59
C, RdL, fall TP, conv	.42	.52
C, RdR, wc seeding, spring TP, conv	.40	.49
C, RdL, standing, spring TP, conv	.38	.48
C-W-M-M, RdL, TP for C, disk for W	.039	.074
C-W-M-M-M, RdL, TP for C, disk for W	.032	.061
C, no-till pl in c-k sod, 95-80% rc	.017	.053
COTTON		
Cot, conv (Western Plains)	0.42	0.49
Cot, conv (South)	.34	.40
MEADOW		
Grass & Legume mix	0.004	0.01
Alfalfa, lespedeza or Sericia	.020	
Sweet clover	.025	
SORGHUM, GRAIN (Western Plains)		
RdL, spring TP, conv	0.43	0.53
No-till pl in shredded 70-50% rc	.11	.18
SOYBEANS		
B, RdL, spring TP, conv	0.48	0.54
C-B, TP annually, conv	.43	.51
B, no-till pl	.22	.28
C-B, no-till pl, fall shred C stalks	.18	.22
WHEAT		
W-F, fall TP after W	0.38	
W-F, stubble mulch, 500 lbs rc	.32	
W-F, stubble mulch, 1000 lbs rc	.21	

Abbreviations defined:

B - soybeans
C - corn
c-k - chemically killed
conv - conventional
cot - cotton

F - fallow
M - grass & legume hay
pl - plant
W - wheat
wc - winter cover

lbs rc - pounds of crop residue per acre remaining on surface after new crop seeding
% rc - percentage of soil surface covered by residue mulch after new crop seeding
70-50% rc - 70% cover for C values in first column; 50% for second column
RdR - residues (corn stover, straw, etc.) removed or burned
RdL - all residues left on field (on surface or incorporated)
TP - turn plowed (upper 5 or more inches of soil inverted, covering residues)

are listed in Table 8. These values are based on rather limited field data, but P has a narrower range of possible values than the other five factors.

TABLE 8. VALUES OF FACTOR P¹¹

Practice	Land slope (percent)				
	1.1-2	2.1-7	7.1-12	12.1-18	18.1-24
	(Factor P)				
Contouring (P _c)	0.60	0.50	0.60	0.80	0.90
Contour strip cropping (P _{sc})					
R-R-M-M ¹	0.30	0.25	0.30	0.40	0.45
R-W-M-M	0.30	0.25	0.30	0.40	0.45
R-R-W-M	0.45	0.38	0.45	0.60	0.68
R-W	0.52	0.44	0.52	0.70	0.90
R-O	0.60	0.50	0.60	0.80	0.90
Contour listing or ridge planting (P _{cl})	0.30	0.25	0.30	0.40	0.45
Contour terracing (P _t) ²	³ 0.6/√n	0.5/√n	0.6/√n	0.8/√n	0.9/√n
No support practice	1.0	1.0	1.0	1.0	1.0

¹ R = rowcrop, W = fall-seeded grain, O = spring-seeded grain, M = meadow. The crops are grown in rotation and so arranged on the field that rowcrop strips are always separated by a meadow or winter-grain strip.

² These P_t values estimate the amount of soil eroded to the terrace channels and are used for conservation planning. For prediction of off-field sediment, the P_t values are multiplied by 0.2.

³ n = number of approximately equal-length intervals into which the field slope is divided by the terraces. Tillage operations must be parallel to the terraces.

Example: An owner/operator proposes to close one section of his small landfill with a sandy clay subsoil cover having the surface configuration shown in Figure 21. The factor R has been established as 200 for this locality. The evaluator questions anticipated erosion along the steep side and assigns the following values to the other factors in the USLE after inspecting Tables 5 through 8:

$$K = 0.14 \quad LS = 8.3 \quad C = 1.00 \quad P = 0.90$$

The rate of erosion for the steep slope of the landfill is calculated as follows:

$$A = 200 (0.14 \text{ tons/acre}) (8.3) (1.00) (0.90) \\ = 209 \text{ tons/acre}$$

This erosion not only exceeds a limit recommended by the permitting authority but also indicates a potential

Hydrograph Generation

- 25-year, 24-hour Storm Event
- 100-year, 24-hour Storm Event

25-year, 24-hour Storm

Summary for Subcatchment 72S: Sed Basin 2

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff = 10.99 cfs @ 11.89 hrs, Volume= 0.548 af, Depth> 5.43"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

Area (ac)	CN	Description
* 1.210	98	Water
1.210		Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.0					Direct Entry, Water

Summary for Subcatchment 76S: Area around Sed Basin 2

[49] Hint: Tc<2dt may require smaller dt

Runoff = 6.94 cfs @ 11.92 hrs, Volume= 0.309 af, Depth= 3.19"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

Area (ac)	CN	Description
* 0.980	74	Grass
* 0.180	96	Gravel Road
1.160	77	Weighted Average
1.160		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.4	100	0.0150	1.21		Sheet Flow, Sheet flow across access road Smooth surfaces n= 0.011 P2= 3.14"
0.2	23	0.0150	1.97		Shallow Concentrated Flow, flow across access road Unpaved Kv= 16.1 fps
0.5	172	0.0800	5.37	9.55	Trap/Vee/Rect Channel Flow, Channel down to basin Bot.W=0.00' D=0.77' Z= 3.0 '/' Top.W=4.62' n= 0.040
2.1	295	Total			

Summary for Subcatchment 77S: Subarea 3 (NW Ditch)

Runoff = 15.50 cfs @ 11.99 hrs, Volume= 0.771 af, Depth= 3.00"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

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Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

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Area (ac)	CN	Description
* 2.940	74	Final Cover
* 0.140	96	Gravel Access Road
3.080	75	Weighted Average
3.080		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
0.4	88	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
3.2	629	0.0260	3.28	17.18	Trap/Vee/Rect Channel Flow, Perimeter Ditch Bot.W=10.00' D=0.46' Z= 3.0 '/' Top.W=12.76' n= 0.040
7.2	817	Total			

Summary for Subcatchment 78S: Subarea 4 (NE Ditch)

Runoff = 27.15 cfs @ 11.98 hrs, Volume= 1.339 af, Depth= 3.00"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

Area (ac)	CN	Description
* 5.030	74	Final Cover
* 0.320	96	Gravel Access Road
5.350	75	Weighted Average
5.350		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.5	64	0.2500	0.42		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
4.4	1,173	0.0310	4.39	34.12	Trap/Vee/Rect Channel Flow, Perimeter Ditch Bot.W=10.00' D=0.65' Z= 3.0 '/' Top.W=13.90' n= 0.040
6.9	1,237	Total			

Summary for Subcatchment 80S: Subarea 5

[49] Hint: Tc<2dt may require smaller dt

Runoff = 9.11 cfs @ 11.97 hrs, Volume= 0.434 af, Depth= 2.91"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

Area (ac)	CN	Description
* 1.790	74	Final Cover
1.790		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
0.3	73	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
1.7	421	0.0200	4.20	28.59	Channel Flow, Flow in diversion berm Area= 6.8 sf Perim= 9.5' r= 0.72' n= 0.040
5.6	594	Total			

Summary for Subcatchment 81S: Subarea 6

[49] Hint: Tc<2dt may require smaller dt

Runoff = 10.15 cfs @ 11.96 hrs, Volume= 0.475 af, Depth= 2.91"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

Area (ac)	CN	Description
* 1.960	74	Final Cover
1.960		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
1.6	410	0.0200	4.20	28.59	Channel Flow, Flow in diversion berm Area= 6.8 sf Perim= 9.5' r= 0.72' n= 0.040
5.2	510	Total			

Summary for Subcatchment 82S: Subarea 7

[49] Hint: Tc<2dt may require smaller dt

Runoff = 9.82 cfs @ 11.97 hrs, Volume= 0.468 af, Depth= 2.91"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

Area (ac)	CN	Description
* 1.930	74	Final Cover
1.930		Pervious Area

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Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
0.4	83	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
1.6	399	0.0200	4.20	28.59	Channel Flow, Flow in diversion berm Area= 6.8 sf Perim= 9.5' r= 0.72' n= 0.040
5.6	582	Total			

Summary for Subcatchment 83S: Subarea 8

[49] Hint: Tc<2dt may require smaller dt

Runoff = 7.42 cfs @ 11.96 hrs, Volume= 0.344 af, Depth= 2.91"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

Area (ac)	CN	Description
* 1.420	74	Final Cover
1.420		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
0.7	151	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
0.7	183	0.0200	4.20	28.59	Channel Flow, Flow in diversion berm Area= 6.8 sf Perim= 9.5' r= 0.72' n= 0.040
5.0	434	Total			

Summary for Subcatchment 84S: Subarea 9

[49] Hint: Tc<2dt may require smaller dt

Runoff = 8.00 cfs @ 11.95 hrs, Volume= 0.366 af, Depth= 2.91"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

Area (ac)	CN	Description
* 1.510	74	Final Cover
1.510		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
1.1	282	0.0200	4.20	28.59	Channel Flow, Flow in diversion berm Area= 6.8 sf Perim= 9.5' r= 0.72' n= 0.040
4.7	382	Total			

Summary for Subcatchment 85S: Subarea 10

[49] Hint: Tc<2dt may require smaller dt

Runoff = 3.32 cfs @ 11.96 hrs, Volume= 0.153 af, Depth= 2.91"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

Area (ac)	CN	Description
* 0.630	74	Final Cover
0.630		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
0.4	81	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
0.8	206	0.0200	4.20	28.59	Channel Flow, Flow in diversion berm Area= 6.8 sf Perim= 9.5' r= 0.72' n= 0.040
4.8	387	Total			

Summary for Subcatchment 86S: Subarea 12

[49] Hint: Tc<2dt may require smaller dt

Runoff = 9.32 cfs @ 11.97 hrs, Volume= 0.446 af, Depth= 2.91"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

Area (ac)	CN	Description
* 1.840	74	Final Cover
1.840		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
0.5	95	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
1.6	416	0.0200	4.20	28.59	Channel Flow, Flow in diversion berm Area= 6.8 sf Perim= 9.5' r= 0.72' n= 0.040
5.7	611	Total			

Summary for Subcatchment 87S: Subarea 14

[49] Hint: Tc<2dt may require smaller dt

Runoff = 9.50 cfs @ 11.96 hrs, Volume= 0.451 af, Depth= 2.91"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

Area (ac)	CN	Description
* 1.860	74	Final Cover
1.860		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
0.4	88	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
1.5	373	0.0200	4.20	28.59	Channel Flow, Flow in diversion berm Area= 6.8 sf Perim= 9.5' r= 0.72' n= 0.040
5.5	561	Total			

Summary for Subcatchment 89S: Sed Basin 3

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff = 15.34 cfs @ 11.89 hrs, Volume= 0.765 af, Depth> 5.43"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

Area (ac)	CN	Description
* 1.690	98	Water
1.690		Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.0					Direct Entry, Water

Summary for Subcatchment 90S: Area around Sed Basin 3

[49] Hint: Tc<2dt may require smaller dt

Runoff = 4.66 cfs @ 11.90 hrs, Volume= 0.197 af, Depth= 3.19"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

Area (ac)	CN	Description
* 0.650	74	Grass
* 0.090	96	Gravel Road
0.740	77	Weighted Average
0.740		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.0	67	0.0150	1.12		Sheet Flow, Sheet flow across access road Smooth surfaces n= 0.011 P2= 3.14"

Summary for Subcatchment 91S: Subarea 1 (WN Ditch)

[49] Hint: Tc<2dt may require smaller dt

Runoff = 37.50 cfs @ 11.96 hrs, Volume= 1.774 af, Depth= 3.00"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

Area (ac)	CN	Description
* 6.830	74	Final Cover
* 0.260	96	Gravel Access Road
7.090	75	Weighted Average
7.090		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
1.2	255	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
0.6	1,150	1.0000	31.01	378.54	Trap/Vee/Rect Channel Flow, Perimeter Ditch Bot.W=10.00' D=0.95' Z= 3.0 '/' Top.W=15.70' n= 0.040
5.4	1,505	Total			

Summary for Subcatchment 92S: Subarea 2 (WS Ditch)

Runoff = 41.15 cfs @ 12.00 hrs, Volume= 2.155 af, Depth= 3.00"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

Area (ac)	CN	Description
* 8.250	74	Final Cover
* 0.360	96	Gravel Access Road
8.610	75	Weighted Average
8.610		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
0.5	108	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
4.6	1,271	0.0250	4.60	49.11	Trap/Vee/Rect Channel Flow, Perimeter Ditch Bot.W=10.00' D=0.85' Z= 3.0 ' / Top.W=15.10' n= 0.040
8.7	1,479	Total			

Summary for Subcatchment 93S: Subarea 11

[49] Hint: Tc<2dt may require smaller dt

Runoff = 7.46 cfs @ 11.96 hrs, Volume= 0.349 af, Depth= 2.91"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

Area (ac)	CN	Description
* 1.440	74	Final Cover
1.440		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
1.3	272	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
0.3	78	0.0200	4.20	28.59	Channel Flow, Flow in diversion berm Area= 6.8 sf Perim= 9.5' r= 0.72' n= 0.040
5.2	450	Total			

Summary for Subcatchment 94S: Subarea 16[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 10.16 cfs @ 11.96 hrs, Volume= 0.480 af, Depth= 2.91"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, $dt=0.05$ hrs
Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

Area (ac)	CN	Description
* 1.980	74	Final Cover
1.980		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short $n=0.150$ $P2=3.14"$
0.3	65	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture $K_v=7.0$ fps
1.5	376	0.0200	4.20	28.59	Channel Flow, Flow in diversion berm Area= 6.8 sf Perim= 9.5' $r=0.72'$ $n=0.040$
5.4	541	Total			

Summary for Subcatchment 95S: Subarea 18[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 10.12 cfs @ 11.97 hrs, Volume= 0.482 af, Depth= 2.91"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, $dt=0.05$ hrs
Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

Area (ac)	CN	Description
* 1.990	74	Final Cover
1.990		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short $n=0.150$ $P2=3.14"$
0.6	130	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture $K_v=7.0$ fps
1.4	352	0.0200	4.20	28.59	Channel Flow, Flow in diversion berm Area= 6.8 sf Perim= 9.5' $r=0.72'$ $n=0.040$
5.6	582	Total			

Summary for Subcatchment 97S: Sed Basin 4[46] Hint: $T_c=0$ (Instant runoff peak depends on dt)

Runoff = 13.35 cfs @ 11.89 hrs, Volume= 0.665 af, Depth> 5.43"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, $dt=0.05$ hrs
Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

Area (ac)	CN	Description
* 1.470	98	Water
1.470		Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.0					Direct Entry, Water

Summary for Subcatchment 98S: Area around Sed Basin 4[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 6.10 cfs @ 11.96 hrs, Volume= 0.289 af, Depth= 3.10"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, $dt=0.05$ hrs
Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

Area (ac)	CN	Description
* 1.030	74	Grass
* 0.090	96	Gravel Access Road
1.120	76	Weighted Average
1.120		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.4	100	0.0150	1.21		Sheet Flow, Sheet flow across access road Smooth surfaces $n=0.011$ $P2=3.14"$
0.2	32	0.2500	3.50		Shallow Concentrated Flow, Shallow flow across final cover Short Grass Pasture $K_v=7.0$ fps
3.8	882	0.0300	3.91	11.74	Trap/Vee/Rect Channel Flow, Bot.W=0.00' D=1.00' Z= 3.0 '/' Top.W=6.00' $n=0.040$
5.4	1,014	Total			

Summary for Subcatchment 99S: Subarea 13[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 9.67 cfs @ 11.97 hrs, Volume= 0.463 af, Depth= 2.91"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

Area (ac)	CN	Description
* 1.910	74	Final Cover
1.910		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
0.6	120	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
1.5	379	0.0200	4.20	28.59	Channel Flow, Flow in diversion berm Area= 6.8 sf Perim= 9.5' r= 0.72' n= 0.040
5.7	599	Total			

Summary for Subcatchment 100S: Subarea 15

[49] Hint: Tc<2dt may require smaller dt

Runoff = 10.13 cfs @ 11.97 hrs, Volume= 0.485 af, Depth= 2.91"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

Area (ac)	CN	Description
* 2.000	74	Final Cover
2.000		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
0.5	108	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
1.6	402	0.0200	4.20	28.59	Channel Flow, Flow in diversion berm Area= 6.8 sf Perim= 9.5' r= 0.72' n= 0.040
5.7	610	Total			

Summary for Subcatchment 101S: Subarea 17

[49] Hint: Tc<2dt may require smaller dt

Runoff = 10.18 cfs @ 11.97 hrs, Volume= 0.487 af, Depth= 2.91"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

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Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

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Area (ac)	CN	Description
* 2.010	74	Final Cover
2.010		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
0.4	82	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
1.7	432	0.0200	4.20	28.59	Channel Flow, Flow in diversion berm Area= 6.8 sf Perim= 9.5' r= 0.72' n= 0.040
5.7	614	Total			

Summary for Subcatchment 102S: Subarea 19

[49] Hint: Tc<2dt may require smaller dt

Runoff = 10.18 cfs @ 11.97 hrs, Volume= 0.487 af, Depth= 2.91"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

Area (ac)	CN	Description
* 2.010	74	Final Cover
2.010		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
0.6	127	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
1.5	381	0.0200	4.20	28.59	Channel Flow, Flow in diversion berm Area= 6.8 sf Perim= 9.5' r= 0.72' n= 0.040
5.7	608	Total			

Summary for Subcatchment 103S: Subarea 20 (SW Ditch)

Runoff = 32.49 cfs @ 12.04 hrs, Volume= 1.884 af, Depth= 3.00"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

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Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

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Area (ac)	CN	Description
* 7.300	74	Final Cover
* 0.230	96	Access Road Gravel
7.530	75	Weighted Average
7.530		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
0.6	119	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
7.4	1,473	0.0116	3.34	40.77	Trap/Vee/Rect Channel Flow, Perimeter Ditch Bot.W=10.00' D=0.95' Z= 3.0 '/' Top.W=15.70' n= 0.040
11.6	1,692	Total			

Summary for Subcatchment 104S: Subarea 21 (SE Ditch)

Runoff = 17.56 cfs @ 11.99 hrs, Volume= 0.876 af, Depth= 3.00"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

Area (ac)	CN	Description
* 3.340	74	Final Cover
* 0.160	96	Gravel Access Road
3.500	75	Weighted Average
3.500		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
0.7	141	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
3.0	643	0.0300	3.53	18.45	Trap/Vee/Rect Channel Flow, Perimeter Ditch Bot.W=10.00' D=0.46' Z= 3.0 '/' Top.W=12.76' n= 0.040
7.3	884	Total			

Summary for Subcatchment 105S: Subarea 22

[49] Hint: Tc<2dt may require smaller dt

Runoff = 6.59 cfs @ 11.96 hrs, Volume= 0.303 af, Depth= 2.91"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

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Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

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Area (ac)	CN	Description
* 1.250	74	Final Cover
1.250		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
0.7	142	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
0.5	129	0.0200	4.20	28.59	Channel Flow, Flow in diversion berm Area= 6.8 sf Perim= 9.5' r= 0.72' n= 0.040
4.8	371	Total			

Summary for Subcatchment 106S: Subarea 23

[49] Hint: Tc<2dt may require smaller dt

Runoff = 7.65 cfs @ 11.96 hrs, Volume= 0.352 af, Depth= 2.91"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

Area (ac)	CN	Description
* 1.450	74	Final Cover
1.450		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
0.8	173	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
0.4	111	0.0200	4.20	28.59	Channel Flow, Flow in diversion berm Area= 6.8 sf Perim= 9.5' r= 0.72' n= 0.040
4.8	384	Total			

Summary for Subcatchment 107S: Subarea 24

[49] Hint: Tc<2dt may require smaller dt

Runoff = 4.08 cfs @ 11.95 hrs, Volume= 0.184 af, Depth= 2.91"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

Area (ac)	CN	Description
* 0.760	74	Final Cover
0.760		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
0.8	164	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
4.4	264	Total			

Summary for Subcatchment 108S: Subarea 25

[49] Hint: Tc<2dt may require smaller dt

Runoff = 4.61 cfs @ 11.95 hrs, Volume= 0.209 af, Depth= 2.91"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

Area (ac)	CN	Description
* 0.860	74	Final Cover
0.860		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
0.8	164	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
4.4	264	Total			

Summary for Subcatchment 110S: Area around Sed Basin 4 to culvert 4 only

[49] Hint: Tc<2dt may require smaller dt

Runoff = 20.54 cfs @ 11.95 hrs, Volume= 0.937 af, Depth= 3.29"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

Area (ac)	CN	Description
* 2.780	74	Grass
* 0.640	96	Gravel Access Road
3.420	78	Weighted Average
3.420		Pervious Area

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Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.4	100	0.0150	1.21		Sheet Flow, Sheet flow across access road Smooth surfaces n= 0.011 P2= 3.14"
0.2	32	0.2500	3.50		Shallow Concentrated Flow, Shallow slow across final cover Short Grass Pasture Kv= 7.0 fps
2.8	882	0.0300	5.32	21.27	Channel Flow, Channel flow Area= 4.0 sf Perim= 8.2' r= 0.49' n= 0.030 Earth, grassed & winding
4.4	1,014	Total			

Summary for Subcatchment 111S: West Rock-lined Channel (vegetation established)

Runoff = 51.10 cfs @ 11.99 hrs, Volume= 2.565 af, Depth= 3.00"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

Area (ac)	CN	Description
9.570	74	>75% Grass cover, Good, HSG C
* 0.680	96	Gravel Access Road
10.250	75	Weighted Average
10.250		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.4	100	0.2500	3.74		Sheet Flow, Sheet flow across access road Smooth surfaces n= 0.011 P2= 3.14"
0.6	78	0.1000	2.21		Shallow Concentrated Flow, Shallow slow across final cover Short Grass Pasture Kv= 7.0 fps
6.5	1,177	0.0200	3.01	13.99	Trap/Vee/Rect Channel Flow, Bot.W=0.00' D=0.88' Z= 6.0 '/' Top.W=10.56' n= 0.040
7.5	1,355	Total			

Summary for Subcatchment 112S: West Rock-lined Channel (worst case)

Runoff = 72.72 cfs @ 11.98 hrs, Volume= 3.959 af, Depth= 4.63"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

Area (ac)	CN	Description
9.570	91	Fallow, bare soil, HSG C
* 0.680	96	Gravel Access Road
10.250	91	Weighted Average
10.250		Pervious Area

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Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.4	100	0.2500	3.74		Sheet Flow, Sheet flow across access road Smooth surfaces n= 0.011 P2= 3.14"
0.6	78	0.1000	2.21		Shallow Concentrated Flow, Shallow slow across final cover Short Grass Pasture Kv= 7.0 fps
6.5	1,177	0.0200	3.01	13.99	Trap/Vee/Rect Channel Flow, Bot.W=0.00' D=0.88' Z= 6.0 '/' Top.W=10.56' n= 0.040
7.5	1,355	Total			

Summary for Subcatchment 113S: Culvert 5-1 (Ph 1 Access Road)

Runoff = 3.05 cfs @ 11.98 hrs, Volume= 0.148 af, Depth= 2.91"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

Area (ac)	CN	Description
* 0.610	74	Grass
0.610		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.3	100	0.2400	0.31		Sheet Flow, Sheet flow Grass: Dense n= 0.240 P2= 3.14"
1.0	182	0.1800	2.97		Shallow Concentrated Flow, Shallow slow across final cover Short Grass Pasture Kv= 7.0 fps
6.3	282	Total			

Summary for Subcatchment 116S: Culvert 12-1 (Across LF Perimeter Road)

Runoff = 12.23 cfs @ 11.99 hrs, Volume= 0.625 af, Depth= 3.19"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

Area (sf)	CN	Description
* 88,968	74	Final Cover
* 13,311	96	Access Road Gravel
102,279	77	Weighted Average
102,279		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.6	11	0.3300	0.33		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
7.3	1,378	0.0102	3.13	38.23	Trap/Vee/Rect Channel Flow, Perimeter Ditch Bot.W=10.00' D=0.95' Z= 3.0 '/' Top.W=15.70' n= 0.040
7.9	1,389	Total			

Summary for Subcatchment 117S: Culvert 11-1 (Ph 5 Access Road)

Runoff = 7.80 cfs @ 12.06 hrs, Volume= 0.491 af, Depth= 2.91"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

Area (ac)	CN	Description
* 2.025	74	Grass
2.025		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0	100	0.0500	0.17		Sheet Flow, Sheet flow
					Grass: Dense n= 0.240 P2= 3.14"
4.1	505	0.0871	2.07		Shallow Concentrated Flow, Shallow Flow to culvert
					Short Grass Pasture Kv= 7.0 fps
14.1	605	Total			

Summary for Subcatchment 118S: Culvert 15-1 (Ph 3 Access Road)

[49] Hint: Tc<2dt may require smaller dt

Runoff = 3.03 cfs @ 11.92 hrs, Volume= 0.136 af, Depth= 3.48"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

Area (sf)	CN	Description
* 14,820	74	Grass
* 5,567	96	Access Road Gravel
20,387	80	Weighted Average
20,387		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.7	60	0.0330	1.50		Sheet Flow, Sheet flow across final cover
					Smooth surfaces n= 0.011 P2= 3.14"
1.3	293	0.0650	3.63	2.72	Trap/Vee/Rect Channel Flow, Perimeter Ditch
					Bot.W=0.00' D=0.50' Z= 3.0 '/' Top.W=3.00' n= 0.040
2.0	353	Total			

Summary for Subcatchment 119S: Discharge Pipe from PHase 2 Area under Sed Basin 3

Runoff = 26.22 cfs @ 12.18 hrs, Volume= 2.242 af, Depth= 2.91"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

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Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

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Area (ac)	CN	Description
* 9.248	74	Grass
9.248		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.4	100	0.0600	0.26		Sheet Flow, Sheet flow across access road Grass: Short n= 0.150 P2= 3.14"
18.3	983	0.0163	0.89		Shallow Concentrated Flow, Shallow slow across final cover Short Grass Pasture Kv= 7.0 fps
24.7	1,083	Total			

Summary for Subcatchment 120S: Discharge Pipe from Phase 4 Area under Access Road

Runoff = 5.28 cfs @ 12.06 hrs, Volume= 0.334 af, Depth= 2.91"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

Area (ac)	CN	Description
* 1.379	74	Grass
1.379		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
4.0	100	0.1900	0.41		Sheet Flow, Sheet flow across access road Grass: Short n= 0.150 P2= 3.14"
10.3	382	0.0078	0.62		Shallow Concentrated Flow, Shallow slow across final cover Short Grass Pasture Kv= 7.0 fps
14.3	482	Total			

Summary for Reach 104R: SW ChannelInflow Area = 5.470 ac, 0.00% Impervious, Inflow Depth = 2.91" for 25-yr, 24-hr event
Inflow = 27.96 cfs @ 11.96 hrs, Volume= 1.326 af
Outflow = 19.86 cfs @ 12.19 hrs, Volume= 1.326 af, Atten= 29%, Lag= 13.3 minRouting by Stor-Ind+Trans method, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Max. Velocity= 2.64 fps, Min. Travel Time= 9.3 min
Avg. Velocity= 0.55 fps, Avg. Travel Time= 44.8 minPeak Storage= 11,086 cf @ 12.03 hrs, Average Depth at Peak Storage= 0.63'
Bank-Full Depth= 2.00', Capacity at Bank-Full= 161.13 cfs10.00' x 2.00' deep channel, n= 0.040
Side Slope Z-value= 3.0 '/' Top Width= 22.00'
Length= 1,467.0' Slope= 0.0116 '/'
Inlet Invert= 812.00', Outlet Invert= 795.00'



Summary for Reach 105R: SE Channel

Inflow Area = 5.160 ac, 0.00% Impervious, Inflow Depth = 2.91" for 25-yr, 24-hr event
Inflow = 26.35 cfs @ 11.96 hrs, Volume= 1.251 af
Outflow = 24.51 cfs @ 12.04 hrs, Volume= 1.251 af, Atten= 7%, Lag= 4.6 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Max. Velocity= 3.88 fps, Min. Travel Time= 2.8 min
Avg. Velocity = 0.87 fps, Avg. Travel Time= 12.3 min

Peak Storage= 4,110 cf @ 11.99 hrs, Average Depth at Peak Storage= 0.55'
Bank-Full Depth= 2.00', Capacity at Bank-Full= 257.30 cfs

10.00' x 2.00' deep channel, n= 0.040
Side Slope Z-value= 3.0 '/' Top Width= 22.00'
Length= 643.0' Slope= 0.0295 '/'
Inlet Invert= 814.00', Outlet Invert= 795.00'



Summary for Reach 109R: S Channel

[65] Warning: Inlet elevation not specified

Inflow Area = 1.620 ac, 0.00% Impervious, Inflow Depth = 2.91" for 25-yr, 24-hr event
Inflow = 8.69 cfs @ 11.95 hrs, Volume= 0.393 af
Outflow = 7.73 cfs @ 12.04 hrs, Volume= 0.393 af, Atten= 11%, Lag= 5.3 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Max. Velocity= 1.93 fps, Min. Travel Time= 3.4 min
Avg. Velocity = 0.45 fps, Avg. Travel Time= 14.5 min

Peak Storage= 1,575 cf @ 11.99 hrs, Average Depth at Peak Storage= 0.37'
Bank-Full Depth= 2.00', Capacity at Bank-Full= 164.01 cfs

10.00' x 2.00' deep channel, n= 0.040
 Side Slope Z-value= 3.0 '/' Top Width= 22.00'
 Length= 389.0' Slope= 0.0120 '/'
 Inlet Invert= 0.00', Outlet Invert= -4.67'



Summary for Reach 110R: NE Channel

Inflow Area = 7.050 ac, 0.00% Impervious, Inflow Depth = 2.91" for 25-yr, 24-hr event
 Inflow = 36.04 cfs @ 11.96 hrs, Volume= 1.709 af
 Outflow = 30.05 cfs @ 12.09 hrs, Volume= 1.709 af, Atten= 17%, Lag= 7.6 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
 Max. Velocity= 4.54 fps, Min. Travel Time= 4.9 min
 Avg. Velocity = 0.99 fps, Avg. Travel Time= 22.4 min

Peak Storage= 9,100 cf @ 12.01 hrs, Average Depth at Peak Storage= 0.58'
 Bank-Full Depth= 2.00', Capacity at Bank-Full= 290.44 cfs

10.00' x 2.00' deep channel, n= 0.040
 Side Slope Z-value= 3.0 '/' Top Width= 22.00'
 Length= 1,328.0' Slope= 0.0377 '/'
 Inlet Invert= 818.00', Outlet Invert= 768.00'



Summary for Reach 111R: N Channel

[65] Warning: Inlet elevation not specified

Inflow Area = 5.890 ac, 0.00% Impervious, Inflow Depth = 2.91" for 25-yr, 24-hr event
 Inflow = 30.53 cfs @ 11.96 hrs, Volume= 1.428 af
 Outflow = 29.25 cfs @ 11.98 hrs, Volume= 1.428 af, Atten= 4%, Lag= 1.4 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
 Max. Velocity= 3.93 fps, Min. Travel Time= 0.8 min
 Avg. Velocity = 0.93 fps, Avg. Travel Time= 3.4 min

Peak Storage= 1,427 cf @ 11.97 hrs, Average Depth at Peak Storage= 0.63'

Bank-Full Depth= 2.00', Capacity at Bank-Full= 241.26 cfs

10.00' x 2.00' deep channel, n= 0.040

Side Slope Z-value= 3.0 '/' Top Width= 22.00'

Length= 189.0' Slope= 0.0260 '/'

Inlet Invert= 0.00', Outlet Invert= -4.91'



Summary for Reach 113R: WS Channel

Inflow Area = 5.410 ac, 0.00% Impervious, Inflow Depth = 2.91" for 25-yr, 24-hr event

Inflow = 27.73 cfs @ 11.96 hrs, Volume= 1.312 af

Outflow = 22.83 cfs @ 12.11 hrs, Volume= 1.312 af, Atten= 18%, Lag= 9.0 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Max. Velocity= 3.55 fps, Min. Travel Time= 6.0 min

Avg. Velocity = 0.77 fps, Avg. Travel Time= 27.4 min

Peak Storage= 8,155 cf @ 12.01 hrs, Average Depth at Peak Storage= 0.55'

Bank-Full Depth= 2.00', Capacity at Bank-Full= 235.64 cfs

10.00' x 2.00' deep channel, n= 0.040

Side Slope Z-value= 3.0 '/' Top Width= 22.00'

Length= 1,271.0' Slope= 0.0248 '/'

Inlet Invert= 804.50', Outlet Invert= 773.00'



Summary for Pond 50P: SED BASIN 2 (NORTH)

Inflow Area = 23.740 ac, 5.10% Impervious, Inflow Depth > 3.08" for 25-yr, 24-hr event

Inflow = 97.61 cfs @ 11.98 hrs, Volume= 6.103 af

Outflow = 9.89 cfs @ 12.65 hrs, Volume= 6.068 af, Atten= 90%, Lag= 40.0 min

Primary = 9.89 cfs @ 12.65 hrs, Volume= 6.068 af

Secondary = 0.00 cfs @ 1.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Post development sw calcs_131127

Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

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Starting Elev= 757.00' Surf.Area= 36,291 sf Storage= 95,928 cf

Peak Elev= 760.39' @ 12.65 hrs Surf.Area= 47,104 sf Storage= 237,002 cf (141,074 cf above start)

Plug-Flow detention time= 1,064.8 min calculated for 3.863 af (63% of inflow)

Center-of-Mass det. time= 609.2 min (1,433.4 - 824.2)

Volume	Invert	Avail.Storage	Storage Description
#1	754.00'	317,147 cf	Custom Stage Data (Prismatic) Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
754.00	27,824	0	0
756.00	33,306	61,130	61,130
758.00	39,275	72,581	133,711
760.00	45,733	85,008	218,719
762.00	52,695	98,428	317,147

Device	Routing	Invert	Outlet Devices
#1	Primary	755.00'	24.0" x 55.0' long Culvert CPP, projecting, no headwall, Ke= 0.900 Outlet Invert= 754.50' S= 0.0091 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior
#2	Device 1	760.00'	36.0" Horiz. Orifice/Grate Limited to weir flow C= 0.600
#3	Device 1	757.00'	4.0" Vert. Orifice/Grate X 3.00 C= 0.600
#4	Secondary	761.00'	20.0' long x 10.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64

Primary OutFlow Max=9.88 cfs @ 12.65 hrs HW=760.39' (Free Discharge)

1=Culvert (Passes 9.88 cfs of 25.03 cfs potential flow)
 2=Orifice/Grate (Weir Controls 7.62 cfs @ 2.05 fps)
 3=Orifice/Grate (Orifice Controls 2.26 cfs @ 8.65 fps)

Secondary OutFlow Max=0.00 cfs @ 1.00 hrs HW=757.00' (Free Discharge)

4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 88P: SED BASIN 3 (WEST)

Inflow Area = 23.540 ac, 7.18% Impervious, Inflow Depth > 3.16" for 25-yr, 24-hr event
 Inflow = 94.53 cfs @ 11.97 hrs, Volume= 6.202 af
 Outflow = 4.79 cfs @ 13.79 hrs, Volume= 6.123 af, Atten= 95%, Lag= 109.1 min
 Primary = 4.79 cfs @ 13.79 hrs, Volume= 6.123 af
 Secondary = 0.00 cfs @ 1.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Starting Elev= 754.00' Surf.Area= 47,396 sf Storage= 128,978 cf

Peak Elev= 757.19' @ 13.79 hrs Surf.Area= 57,420 sf Storage= 295,954 cf (166,977 cf above start)

Plug-Flow detention time= 1,557.2 min calculated for 3.159 af (51% of inflow)

Center-of-Mass det. time= 847.1 min (1,667.3 - 820.1)

Post development sw calcs_131127

Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

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Volume	Invert	Avail.Storage	Storage Description
#1	751.00'	611,006 cf	Custom Stage Data (Prismatic) Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
751.00	38,660	0	0
752.00	41,501	40,081	40,081
754.00	47,396	88,897	128,978
756.00	53,576	100,972	229,950
758.00	60,040	113,616	343,566
760.00	66,789	126,829	470,395
762.00	73,822	140,611	611,006

Device	Routing	Invert	Outlet Devices
#1	Primary	751.00'	24.0" x 100.0' long Culvert CPP, projecting, no headwall, Ke= 0.900 Outlet Invert= 742.00' S= 0.0900 '/ Cc= 0.900 n= 0.013 Corrugated PE, smooth interior
#2	Device 1	757.00'	36.0" Horiz. Orifice/Grate Limited to weir flow C= 0.600
#3	Device 1	754.00'	4.0" Vert. Orifice/Grate X 3.00 C= 0.600
#4	Secondary	761.00'	20.0' long x 10.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64

Primary OutFlow Max=4.73 cfs @ 13.79 hrs HW=757.19' (Free Discharge)

- 1=Culvert (Passes 4.73 cfs of 27.20 cfs potential flow)
 2=Orifice/Grate (Weir Controls 2.54 cfs @ 1.42 fps)
 3=Orifice/Grate (Orifice Controls 2.19 cfs @ 8.37 fps)

Secondary OutFlow Max=0.00 cfs @ 1.00 hrs HW=754.00' (Free Discharge)

- 4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 96P: SED BASIN 4 (SOUTH)

Inflow Area = 29.290 ac, 5.02% Impervious, Inflow Depth > 3.12" for 25-yr, 24-hr event
 Inflow = 107.74 cfs @ 12.00 hrs, Volume= 7.622 af
 Outflow = 15.90 cfs @ 12.57 hrs, Volume= 7.585 af, Atten= 85%, Lag= 34.2 min
 Primary = 15.90 cfs @ 12.57 hrs, Volume= 7.585 af
 Secondary = 0.00 cfs @ 1.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Starting Elev= 753.00' Surf.Area= 42,207 sf Storage= 114,100 cf

Peak Elev= 756.35' @ 12.57 hrs Surf.Area= 52,239 sf Storage= 272,043 cf (157,943 cf above start)

Plug-Flow detention time= 756.8 min calculated for 4.966 af (65% of inflow)

Center-of-Mass det. time= 404.2 min (1,231.0 - 826.8)

Volume	Invert	Avail.Storage	Storage Description
#1	750.00'	484,301 cf	Custom Stage Data (Prismatic) Listed below (Recalc)

Post development sw calcs_131127

Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

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Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
750.00	33,973	0	0
752.00	39,349	73,322	73,322
754.00	45,064	84,413	157,735
756.00	51,118	96,182	253,917
758.00	57,511	108,629	362,546
760.00	64,244	121,755	484,301

Device	Routing	Invert	Outlet Devices
#1	Primary	750.00'	18.0" x 105.0' long Culvert CPP, projecting, no headwall, Ke= 0.900 Outlet Invert= 748.00' S= 0.0190 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior
#2	Device 1	755.00'	36.0" Horiz. Orifice/Grate Limited to weir flow C= 0.600
#3	Device 1	753.00'	4.0" Vert. Orifice/Grate X 3.00 C= 0.600
#4	Secondary	759.00'	20.0' long x 10.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64

Primary OutFlow Max=15.90 cfs @ 12.57 hrs HW=756.35' (Free Discharge)

1=Culvert (Inlet Controls 15.90 cfs @ 9.00 fps)
 2=Orifice/Grate (Passes < 39.55 cfs potential flow)
 3=Orifice/Grate (Passes < 2.25 cfs potential flow)

Secondary OutFlow Max=0.00 cfs @ 1.00 hrs HW=753.00' (Free Discharge)

4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 111P: Sed Basin 5 (Temp)

Inflow Area = 9.248 ac, 0.00% Impervious, Inflow Depth = 2.91" for 25-yr, 24-hr event
 Inflow = 26.22 cfs @ 12.18 hrs, Volume= 2.242 af
 Outflow = 1.44 cfs @ 14.70 hrs, Volume= 1.815 af, Atten= 95%, Lag= 151.1 min
 Primary = 1.44 cfs @ 14.70 hrs, Volume= 1.815 af

Routing by Stor-Ind method, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
 Peak Elev= 759.48' @ 14.70 hrs Surf.Area= 0.859 ac Storage= 1.365 af

Plug-Flow detention time= 500.1 min calculated for 1.813 af (81% of inflow)
 Center-of-Mass det. time= 420.4 min (1,266.0 - 845.6)

Volume	Invert	Avail.Storage	Storage Description
#1	756.00'	1.857 af	Custom Stage Data (Prismatic) Listed below (Recalc)

Elevation (feet)	Surf.Area (acres)	Inc.Store (acre-feet)	Cum.Store (acre-feet)
756.00	0.009	0.000	0.000
758.00	0.416	0.425	0.425
760.00	1.016	1.432	1.857

Device	Routing	Invert	Outlet Devices
#1	Device 2	758.00'	4.0" Vert. Orifice/Grate X 3.00 C= 0.600
#2	Primary	756.00'	12.0" x 321.0' long Culvert RCP, groove end projecting, Ke= 0.200 Outlet Invert= 739.95' S= 0.0500 '/ Cc= 0.900 n= 0.013 Corrugated PE, smooth interior
#3	Device 2	761.00'	36.0" Horiz. Orifice/Grate Limited to weir flow C= 0.600

Primary OutFlow Max=1.44 cfs @ 14.70 hrs HW=759.48' (Free Discharge)

↑ **2=Culvert** (Passes 1.44 cfs of 8.08 cfs potential flow)
 ↑ **1=Orifice/Grate** (Orifice Controls 1.44 cfs @ 5.51 fps)
 ↑ **3=Orifice/Grate** (Controls 0.00 cfs)

Summary for Pond 113P: Sed Basin 6 (Temp)

Inflow Area = 1.379 ac, 0.00% Impervious, Inflow Depth = 2.91" for 25-yr, 24-hr event
 Inflow = 5.28 cfs @ 12.06 hrs, Volume= 0.334 af
 Outflow = 0.11 cfs @ 18.46 hrs, Volume= 0.093 af, Atten= 98%, Lag= 383.5 min
 Primary = 0.11 cfs @ 18.46 hrs, Volume= 0.093 af

Routing by Stor-Ind method, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
 Peak Elev= 762.12' @ 18.46 hrs Surf.Area= 0.235 ac Storage= 0.270 af

Plug-Flow detention time= 644.9 min calculated for 0.093 af (28% of inflow)
 Center-of-Mass det. time= 514.1 min (1,350.0 - 835.9)

Volume	Invert	Avail.Storage	Storage Description
#1	760.00'	1.620 af	Custom Stage Data (Prismatic) Listed below (Recalc)
Elevation (feet)	Surf.Area (acres)	Inc.Store (acre-feet)	Cum.Store (acre-feet)
760.00	0.013	0.000	0.000
762.00	0.228	0.241	0.241
764.00	0.343	0.571	0.812
766.00	0.465	0.808	1.620

Device	Routing	Invert	Outlet Devices
#1	Device 2	762.00'	4.0" Vert. Orifice/Grate X 3.00 C= 0.600
#2	Primary	760.00'	8.0" x 210.0' long Culvert RCP, groove end projecting, Ke= 0.200 Outlet Invert= 757.90' S= 0.0100 '/ Cc= 0.900 n= 0.013 Corrugated PE, smooth interior
#3	Device 2	765.00'	36.0" Horiz. Orifice/Grate Limited to weir flow C= 0.600

Primary OutFlow Max=0.11 cfs @ 18.46 hrs HW=762.12' (Free Discharge)

↑ **2=Culvert** (Passes 0.11 cfs of 1.49 cfs potential flow)
 ↑ **1=Orifice/Grate** (Orifice Controls 0.11 cfs @ 1.20 fps)
 ↑ **3=Orifice/Grate** (Controls 0.00 cfs)

Summary for Link 97L: Flume 6

Inflow Area = 5.410 ac, 0.00% Impervious, Inflow Depth = 2.91" for 25-yr, 24-hr event
Inflow = 27.73 cfs @ 11.96 hrs, Volume= 1.312 af
Primary = 27.73 cfs @ 11.96 hrs, Volume= 1.312 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Summary for Link 98L: Flume 5

Inflow Area = 5.890 ac, 0.00% Impervious, Inflow Depth = 2.91" for 25-yr, 24-hr event
Inflow = 30.53 cfs @ 11.96 hrs, Volume= 1.428 af
Primary = 30.53 cfs @ 11.96 hrs, Volume= 1.428 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Summary for Link 99L: Flume 4

Inflow Area = 7.050 ac, 0.00% Impervious, Inflow Depth = 2.91" for 25-yr, 24-hr event
Inflow = 36.04 cfs @ 11.96 hrs, Volume= 1.709 af
Primary = 36.04 cfs @ 11.96 hrs, Volume= 1.709 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Summary for Link 100L: Flume 3

Inflow Area = 5.470 ac, 0.00% Impervious, Inflow Depth = 2.91" for 25-yr, 24-hr event
Inflow = 27.96 cfs @ 11.96 hrs, Volume= 1.326 af
Primary = 27.96 cfs @ 11.96 hrs, Volume= 1.326 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Summary for Link 101L: Flume 2

Inflow Area = 5.160 ac, 0.00% Impervious, Inflow Depth = 2.91" for 25-yr, 24-hr event
Inflow = 26.35 cfs @ 11.96 hrs, Volume= 1.251 af
Primary = 26.35 cfs @ 11.96 hrs, Volume= 1.251 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Summary for Link 102L: Flume 1

Inflow Area = 1.620 ac, 0.00% Impervious, Inflow Depth = 2.91" for 25-yr, 24-hr event
Inflow = 8.69 cfs @ 11.95 hrs, Volume= 0.393 af
Primary = 8.69 cfs @ 11.95 hrs, Volume= 0.393 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Summary for Link 108L: Across South Road (Culvert 3-1 & 3-2)

Inflow Area = 23.280 ac, 0.00% Impervious, Inflow Depth = 2.95" for 25-yr, 24-hr event
Inflow = 87.60 cfs @ 12.04 hrs, Volume= 5.730 af
Primary = 87.60 cfs @ 12.04 hrs, Volume= 5.730 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Summary for Link 112L: To Sed Basin 2 (Culvert 1-1 & 1-2)

Inflow Area = 15.480 ac, 0.00% Impervious, Inflow Depth = 2.96" for 25-yr, 24-hr event
Inflow = 62.71 cfs @ 12.01 hrs, Volume= 3.819 af
Primary = 62.71 cfs @ 12.01 hrs, Volume= 3.819 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Summary for Link 114L: To Sed Basin 3 (Culvert 2-1 & 2-2)

Inflow Area = 21.110 ac, 0.00% Impervious, Inflow Depth = 2.98" for 25-yr, 24-hr event
Inflow = 87.98 cfs @ 11.99 hrs, Volume= 5.240 af
Primary = 87.98 cfs @ 11.99 hrs, Volume= 5.240 af, Atten= 0%, Lag= 0.0 min

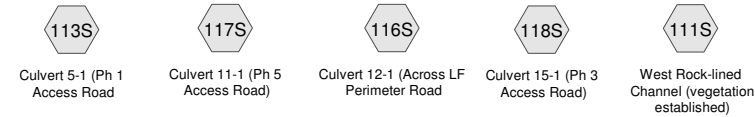
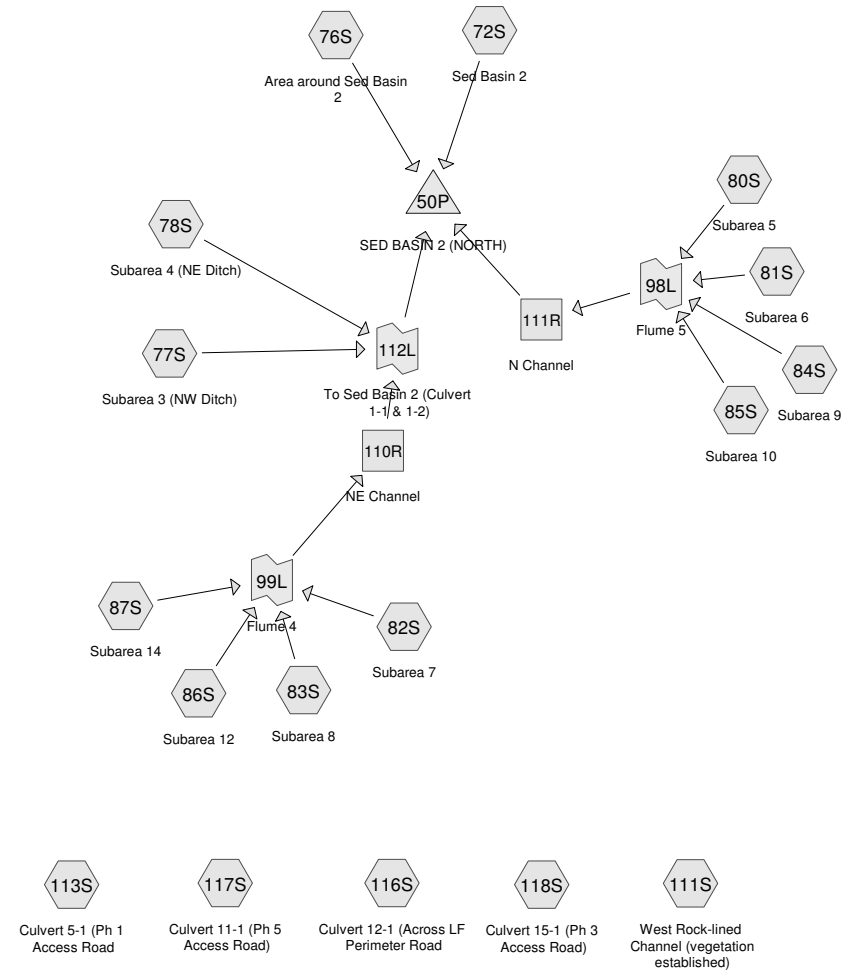
Primary outflow = Inflow, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Summary for Link 115L: To Sed Basin 4 (Culvert 4-1 & 4-2)

Inflow Area = 26.700 ac, 0.00% Impervious, Inflow Depth = 3.00" for 25-yr, 24-hr event
Inflow = 100.36 cfs @ 12.01 hrs, Volume= 6.667 af
Primary = 100.36 cfs @ 12.01 hrs, Volume= 6.667 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

100-year, 24-hour Storm



Summary for Subcatchment 72S: Sed Basin 2[46] Hint: $T_c=0$ (Instant runoff peak depends on dt)

Runoff = 14.73 cfs @ 11.89 hrs, Volume= 0.741 af, Depth> 7.34"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, $dt=0.05$ hrs
Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

Area (ac)	CN	Description
* 1.210	98	Water
1.210		Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.0					Direct Entry, Water

Summary for Subcatchment 76S: Area around Sed Basin 2[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 10.45 cfs @ 11.92 hrs, Volume= 0.474 af, Depth= 4.90"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, $dt=0.05$ hrs
Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

Area (ac)	CN	Description
* 0.980	74	Grass
* 0.180	96	Gravel Road
1.160	77	Weighted Average
1.160		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.4	100	0.0150	1.21		Sheet Flow, Sheet flow across access road Smooth surfaces $n=0.011$ $P2=3.14"$
0.2	23	0.0150	1.97		Shallow Concentrated Flow, flow across access road Unpaved $K_v=16.1$ fps
0.5	172	0.0800	5.37	9.55	Trap/Vee/Rect Channel Flow, Channel down to basin Bot.W=0.00' D=0.77' Z= 3.0 '/' Top.W=4.62' $n=0.040$
2.1	295	Total			

Summary for Subcatchment 77S: Subarea 3 (NW Ditch)

Runoff = 23.78 cfs @ 11.98 hrs, Volume= 1.199 af, Depth= 4.67"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, $dt=0.05$ hrs
Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

Area (ac)	CN	Description
* 2.940	74	Final Cover
* 0.140	96	Gravel Access Road
3.080	75	Weighted Average
3.080		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
0.4	88	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
3.2	629	0.0260	3.28	17.18	Trap/Vee/Rect Channel Flow, Perimeter Ditch Bot.W=10.00' D=0.46' Z= 3.0 '/' Top.W=12.76' n= 0.040
7.2	817	Total			

Summary for Subcatchment 78S: Subarea 4 (NE Ditch)

Runoff = 41.65 cfs @ 11.98 hrs, Volume= 2.084 af, Depth= 4.67"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

Area (ac)	CN	Description
* 5.030	74	Final Cover
* 0.320	96	Gravel Access Road
5.350	75	Weighted Average
5.350		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.5	64	0.2500	0.42		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
4.4	1,173	0.0310	4.39	34.12	Trap/Vee/Rect Channel Flow, Perimeter Ditch Bot.W=10.00' D=0.65' Z= 3.0 '/' Top.W=13.90' n= 0.040
6.9	1,237	Total			

Summary for Subcatchment 80S: Subarea 5

[49] Hint: Tc<2dt may require smaller dt

Runoff = 14.10 cfs @ 11.96 hrs, Volume= 0.680 af, Depth= 4.56"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

Area (ac)	CN	Description
* 1.790	74	Final Cover
1.790		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
0.3	73	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
1.7	421	0.0200	4.20	28.59	Channel Flow, Flow in diversion berm Area= 6.8 sf Perim= 9.5' r= 0.72' n= 0.040
5.6	594	Total			

Summary for Subcatchment 81S: Subarea 6

[49] Hint: Tc<2dt may require smaller dt

Runoff = 15.71 cfs @ 11.96 hrs, Volume= 0.745 af, Depth= 4.56"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

Area (ac)	CN	Description
* 1.960	74	Final Cover
1.960		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
1.6	410	0.0200	4.20	28.59	Channel Flow, Flow in diversion berm Area= 6.8 sf Perim= 9.5' r= 0.72' n= 0.040
5.2	510	Total			

Summary for Subcatchment 82S: Subarea 7

[49] Hint: Tc<2dt may require smaller dt

Runoff = 15.20 cfs @ 11.96 hrs, Volume= 0.734 af, Depth= 4.56"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

Area (ac)	CN	Description
* 1.930	74	Final Cover
1.930		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
0.4	83	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
1.6	399	0.0200	4.20	28.59	Channel Flow, Flow in diversion berm Area= 6.8 sf Perim= 9.5' r= 0.72' n= 0.040
5.6	582	Total			

Summary for Subcatchment 83S: Subarea 8

[49] Hint: Tc<2dt may require smaller dt

Runoff = 11.48 cfs @ 11.96 hrs, Volume= 0.540 af, Depth= 4.56"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

Area (ac)	CN	Description
* 1.420	74	Final Cover
1.420		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
0.7	151	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
0.7	183	0.0200	4.20	28.59	Channel Flow, Flow in diversion berm Area= 6.8 sf Perim= 9.5' r= 0.72' n= 0.040
5.0	434	Total			

Summary for Subcatchment 84S: Subarea 9

[49] Hint: Tc<2dt may require smaller dt

Runoff = 12.37 cfs @ 11.95 hrs, Volume= 0.574 af, Depth= 4.56"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

Area (ac)	CN	Description
* 1.510	74	Final Cover
1.510		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
1.1	282	0.0200	4.20	28.59	Channel Flow, Flow in diversion berm Area= 6.8 sf Perim= 9.5' r= 0.72' n= 0.040
4.7	382	Total			

Summary for Subcatchment 85S: Subarea 10

[49] Hint: Tc<2dt may require smaller dt

Runoff = 5.14 cfs @ 11.95 hrs, Volume= 0.239 af, Depth= 4.56"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

Area (ac)	CN	Description
* 0.630	74	Final Cover
0.630		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
0.4	81	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
0.8	206	0.0200	4.20	28.59	Channel Flow, Flow in diversion berm Area= 6.8 sf Perim= 9.5' r= 0.72' n= 0.040
4.8	387	Total			

Summary for Subcatchment 86S: Subarea 12

[49] Hint: Tc<2dt may require smaller dt

Runoff = 14.43 cfs @ 11.96 hrs, Volume= 0.699 af, Depth= 4.56"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

Area (ac)	CN	Description
* 1.840	74	Final Cover
1.840		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
0.5	95	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
1.6	416	0.0200	4.20	28.59	Channel Flow, Flow in diversion berm Area= 6.8 sf Perim= 9.5' r= 0.72' n= 0.040
5.7	611	Total			

Summary for Subcatchment 87S: Subarea 14[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 14.72 cfs @ 11.96 hrs, Volume= 0.707 af, Depth= 4.56"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

Area (ac)	CN	Description
* 1.860	74	Final Cover
1.860		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
0.4	88	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
1.5	373	0.0200	4.20	28.59	Channel Flow, Flow in diversion berm Area= 6.8 sf Perim= 9.5' r= 0.72' n= 0.040
5.5	561	Total			

Summary for Subcatchment 89S: Sed Basin 3[46] Hint: $T_c=0$ (Instant runoff peak depends on dt)

Runoff = 20.57 cfs @ 11.89 hrs, Volume= 1.034 af, Depth> 7.34"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

Area (ac)	CN	Description
* 1.690	98	Water
1.690		Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.0					Direct Entry, Water

Summary for Subcatchment 90S: Area around Sed Basin 3

[49] Hint: Tc<2dt may require smaller dt

Runoff = 7.02 cfs @ 11.90 hrs, Volume= 0.302 af, Depth= 4.90"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

Area (ac)	CN	Description
* 0.650	74	Grass
* 0.090	96	Gravel Road
0.740	77	Weighted Average
0.740		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.0	67	0.0150	1.12		Sheet Flow, Sheet flow across access road Smooth surfaces n= 0.011 P2= 3.14"

Summary for Subcatchment 91S: Subarea 1 (WN Ditch)

[49] Hint: Tc<2dt may require smaller dt

Runoff = 57.56 cfs @ 11.96 hrs, Volume= 2.761 af, Depth= 4.67"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

Area (ac)	CN	Description
* 6.830	74	Final Cover
* 0.260	96	Gravel Access Road
7.090	75	Weighted Average
7.090		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
1.2	255	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
0.6	1,150	1.0000	31.01	378.54	Trap/Vee/Rect Channel Flow, Perimeter Ditch Bot.W=10.00' D=0.95' Z= 3.0 '/' Top.W=15.70' n= 0.040
5.4	1,505	Total			

Summary for Subcatchment 92S: Subarea 2 (WS Ditch)

Runoff = 63.32 cfs @ 12.00 hrs, Volume= 3.353 af, Depth= 4.67"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

Area (ac)	CN	Description
* 8.250	74	Final Cover
* 0.360	96	Gravel Access Road
8.610	75	Weighted Average
8.610		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
0.5	108	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
4.6	1,271	0.0250	4.60	49.11	Trap/Vee/Rect Channel Flow, Perimeter Ditch Bot.W=10.00' D=0.85' Z= 3.0 ' /' Top.W=15.10' n= 0.040
8.7	1,479	Total			

Summary for Subcatchment 93S: Subarea 11

[49] Hint: Tc<2dt may require smaller dt

Runoff = 11.54 cfs @ 11.96 hrs, Volume= 0.547 af, Depth= 4.56"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

Area (ac)	CN	Description
* 1.440	74	Final Cover
1.440		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
1.3	272	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
0.3	78	0.0200	4.20	28.59	Channel Flow, Flow in diversion berm Area= 6.8 sf Perim= 9.5' r= 0.72' n= 0.040
5.2	450	Total			

Summary for Subcatchment 94S: Subarea 16[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 15.73 cfs @ 11.96 hrs, Volume= 0.753 af, Depth= 4.56"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, $dt=0.05$ hrs
Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

Area (ac)	CN	Description			
* 1.980	74	Final Cover			
1.980		Pervious Area			
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
0.3	65	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
1.5	376	0.0200	4.20	28.59	Channel Flow, Flow in diversion berm Area= 6.8 sf Perim= 9.5' r= 0.72' n= 0.040
5.4	541	Total			

Summary for Subcatchment 95S: Subarea 18[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 15.68 cfs @ 11.96 hrs, Volume= 0.756 af, Depth= 4.56"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, $dt=0.05$ hrs
Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

Area (ac)	CN	Description			
* 1.990	74	Final Cover			
1.990		Pervious Area			
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
0.6	130	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
1.4	352	0.0200	4.20	28.59	Channel Flow, Flow in diversion berm Area= 6.8 sf Perim= 9.5' r= 0.72' n= 0.040
5.6	582	Total			

Summary for Subcatchment 97S: Sed Basin 4[46] Hint: $T_c=0$ (Instant runoff peak depends on dt)

Runoff = 17.89 cfs @ 11.89 hrs, Volume= 0.900 af, Depth> 7.34"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, $dt=0.05$ hrs
Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

Area (ac)	CN	Description
* 1.470	98	Water
1.470		Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.0					Direct Entry, Water

Summary for Subcatchment 98S: Area around Sed Basin 4[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 9.28 cfs @ 11.96 hrs, Volume= 0.447 af, Depth= 4.79"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, $dt=0.05$ hrs
Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

Area (ac)	CN	Description
* 1.030	74	Grass
* 0.090	96	Gravel Access Road
1.120	76	Weighted Average
1.120		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.4	100	0.0150	1.21		Sheet Flow, Sheet flow across access road Smooth surfaces $n=0.011$ $P2=3.14"$
0.2	32	0.2500	3.50		Shallow Concentrated Flow, Shallow flow across final cover Short Grass Pasture $K_v=7.0$ fps
3.8	882	0.0300	3.91	11.74	Trap/Vee/Rect Channel Flow, Bot.W=0.00' D=1.00' Z= 3.0 '/' Top.W=6.00' $n=0.040$
5.4	1,014	Total			

Summary for Subcatchment 99S: Subarea 13[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 14.98 cfs @ 11.96 hrs, Volume= 0.726 af, Depth= 4.56"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

Area (ac)	CN	Description
* 1.910	74	Final Cover
1.910		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
0.6	120	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
1.5	379	0.0200	4.20	28.59	Channel Flow, Flow in diversion berm Area= 6.8 sf Perim= 9.5' r= 0.72' n= 0.040
5.7	599	Total			

Summary for Subcatchment 100S: Subarea 15

[49] Hint: Tc<2dt may require smaller dt

Runoff = 15.69 cfs @ 11.96 hrs, Volume= 0.760 af, Depth= 4.56"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

Area (ac)	CN	Description
* 2.000	74	Final Cover
2.000		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
0.5	108	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
1.6	402	0.0200	4.20	28.59	Channel Flow, Flow in diversion berm Area= 6.8 sf Perim= 9.5' r= 0.72' n= 0.040
5.7	610	Total			

Summary for Subcatchment 101S: Subarea 17

[49] Hint: Tc<2dt may require smaller dt

Runoff = 15.77 cfs @ 11.96 hrs, Volume= 0.764 af, Depth= 4.56"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

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Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

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Printed 11/27/2013

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Area (ac)	CN	Description
* 2.010	74	Final Cover
2.010		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
0.4	82	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
1.7	432	0.0200	4.20	28.59	Channel Flow, Flow in diversion berm Area= 6.8 sf Perim= 9.5' r= 0.72' n= 0.040
5.7	614	Total			

Summary for Subcatchment 102S: Subarea 19

[49] Hint: Tc<2dt may require smaller dt

Runoff = 15.77 cfs @ 11.96 hrs, Volume= 0.764 af, Depth= 4.56"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

Area (ac)	CN	Description
* 2.010	74	Final Cover
2.010		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
0.6	127	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
1.5	381	0.0200	4.20	28.59	Channel Flow, Flow in diversion berm Area= 6.8 sf Perim= 9.5' r= 0.72' n= 0.040
5.7	608	Total			

Summary for Subcatchment 103S: Subarea 20 (SW Ditch)

Runoff = 50.12 cfs @ 12.03 hrs, Volume= 2.932 af, Depth= 4.67"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

Area (ac)	CN	Description
* 7.300	74	Final Cover
* 0.230	96	Access Road Gravel
7.530	75	Weighted Average
7.530		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
0.6	119	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
7.4	1,473	0.0116	3.34	40.77	Trap/Vee/Rect Channel Flow, Perimeter Ditch Bot.W=10.00' D=0.95' Z= 3.0 '/' Top.W=15.70' n= 0.040
11.6	1,692	Total			

Summary for Subcatchment 104S: Subarea 21 (SE Ditch)

Runoff = 26.95 cfs @ 11.99 hrs, Volume= 1.363 af, Depth= 4.67"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

Area (ac)	CN	Description
* 3.340	74	Final Cover
* 0.160	96	Gravel Access Road
3.500	75	Weighted Average
3.500		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
0.7	141	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
3.0	643	0.0300	3.53	18.45	Trap/Vee/Rect Channel Flow, Perimeter Ditch Bot.W=10.00' D=0.46' Z= 3.0 '/' Top.W=12.76' n= 0.040
7.3	884	Total			

Summary for Subcatchment 105S: Subarea 22

[49] Hint: Tc<2dt may require smaller dt

Runoff = 10.19 cfs @ 11.95 hrs, Volume= 0.475 af, Depth= 4.56"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

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Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

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Area (ac)	CN	Description
* 1.250	74	Final Cover
1.250		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
0.7	142	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
0.5	129	0.0200	4.20	28.59	Channel Flow, Flow in diversion berm Area= 6.8 sf Perim= 9.5' r= 0.72' n= 0.040
4.8	371	Total			

Summary for Subcatchment 106S: Subarea 23

[49] Hint: Tc<2dt may require smaller dt

Runoff = 11.83 cfs @ 11.95 hrs, Volume= 0.551 af, Depth= 4.56"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

Area (ac)	CN	Description
* 1.450	74	Final Cover
1.450		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
0.8	173	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
0.4	111	0.0200	4.20	28.59	Channel Flow, Flow in diversion berm Area= 6.8 sf Perim= 9.5' r= 0.72' n= 0.040
4.8	384	Total			

Summary for Subcatchment 107S: Subarea 24

[49] Hint: Tc<2dt may require smaller dt

Runoff = 6.30 cfs @ 11.95 hrs, Volume= 0.289 af, Depth= 4.56"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

Area (ac)	CN	Description
* 0.760	74	Final Cover
0.760		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
0.8	164	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
4.4	264	Total			

Summary for Subcatchment 108S: Subarea 25

[49] Hint: Tc<2dt may require smaller dt

Runoff = 7.13 cfs @ 11.95 hrs, Volume= 0.327 af, Depth= 4.56"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

Area (ac)	CN	Description
* 0.860	74	Final Cover
0.860		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.2500	0.46		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
0.8	164	0.2500	3.50		Shallow Concentrated Flow, Final Cover Short Grass Pasture Kv= 7.0 fps
4.4	264	Total			

Summary for Subcatchment 110S: Area around Sed Basin 4 to culvert 4 only

[49] Hint: Tc<2dt may require smaller dt

Runoff = 30.72 cfs @ 11.95 hrs, Volume= 1.429 af, Depth= 5.01"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

Area (ac)	CN	Description
* 2.780	74	Grass
* 0.640	96	Gravel Access Road
3.420	78	Weighted Average
3.420		Pervious Area

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Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.4	100	0.0150	1.21		Sheet Flow, Sheet flow across access road Smooth surfaces n= 0.011 P2= 3.14"
0.2	32	0.2500	3.50		Shallow Concentrated Flow, Shallow slow across final cover Short Grass Pasture Kv= 7.0 fps
2.8	882	0.0300	5.32	21.27	Channel Flow, Channel flow Area= 4.0 sf Perim= 8.2' r= 0.49' n= 0.030 Earth, grassed & winding
4.4	1,014	Total			

Summary for Subcatchment 111S: West Rock-lined Channel (vegetation established)

Runoff = 78.46 cfs @ 11.99 hrs, Volume= 3.992 af, Depth= 4.67"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

Area (ac)	CN	Description
9.570	74	>75% Grass cover, Good, HSG C
* 0.680	96	Gravel Access Road
10.250	75	Weighted Average
10.250		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.4	100	0.2500	3.74		Sheet Flow, Sheet flow across access road Smooth surfaces n= 0.011 P2= 3.14"
0.6	78	0.1000	2.21		Shallow Concentrated Flow, Shallow slow across final cover Short Grass Pasture Kv= 7.0 fps
6.5	1,177	0.0200	3.01	13.99	Trap/Vee/Rect Channel Flow, Bot.W=0.00' D=0.88' Z= 6.0 '/' Top.W=10.56' n= 0.040
7.5	1,355	Total			

Summary for Subcatchment 112S: West Rock-lined Channel (worst case)

Runoff = 100.07 cfs @ 11.98 hrs, Volume= 5.569 af, Depth= 6.52"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

Area (ac)	CN	Description
9.570	91	Fallow, bare soil, HSG C
* 0.680	96	Gravel Access Road
10.250	91	Weighted Average
10.250		Pervious Area

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Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.4	100	0.2500	3.74		Sheet Flow, Sheet flow across access road Smooth surfaces n= 0.011 P2= 3.14"
0.6	78	0.1000	2.21		Shallow Concentrated Flow, Shallow slow across final cover Short Grass Pasture Kv= 7.0 fps
6.5	1,177	0.0200	3.01	13.99	Trap/Vee/Rect Channel Flow, Bot.W=0.00' D=0.88' Z= 6.0 '/' Top.W=10.56' n= 0.040
7.5	1,355	Total			

Summary for Subcatchment 113S: Culvert 5-1 (Ph 1 Access Road)

Runoff = 4.67 cfs @ 11.97 hrs, Volume= 0.232 af, Depth= 4.56"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

Area (ac)	CN	Description
* 0.610	74	Grass
0.610		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.3	100	0.2400	0.31		Sheet Flow, Sheet flow Grass: Dense n= 0.240 P2= 3.14"
1.0	182	0.1800	2.97		Shallow Concentrated Flow, Shallow slow across final cover Short Grass Pasture Kv= 7.0 fps
6.3	282	Total			

Summary for Subcatchment 116S: Culvert 12-1 (Across LF Perimeter Road)

Runoff = 18.49 cfs @ 11.99 hrs, Volume= 0.959 af, Depth= 4.90"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

Area (sf)	CN	Description
* 88,968	74	Final Cover
* 13,311	96	Access Road Gravel
102,279	77	Weighted Average
102,279		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.6	11	0.3300	0.33		Sheet Flow, Sheet flow across final cover Grass: Short n= 0.150 P2= 3.14"
7.3	1,378	0.0102	3.13	38.23	Trap/Vee/Rect Channel Flow, Perimeter Ditch Bot.W=10.00' D=0.95' Z= 3.0 '/' Top.W=15.70' n= 0.040
7.9	1,389	Total			

Summary for Subcatchment 117S: Culvert 11-1 (Ph 5 Access Road)

Runoff = 12.18 cfs @ 12.06 hrs, Volume= 0.770 af, Depth= 4.56"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

Area (ac)	CN	Description
* 2.025	74	Grass
2.025		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0	100	0.0500	0.17		Sheet Flow, Sheet flow
					Grass: Dense n= 0.240 P2= 3.14"
4.1	505	0.0871	2.07		Shallow Concentrated Flow, Shallow Flow to culvert
					Short Grass Pasture Kv= 7.0 fps
14.1	605	Total			

Summary for Subcatchment 118S: Culvert 15-1 (Ph 3 Access Road)

[49] Hint: Tc<2dt may require smaller dt

Runoff = 4.47 cfs @ 11.92 hrs, Volume= 0.204 af, Depth= 5.24"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

Area (sf)	CN	Description
* 14,820	74	Grass
* 5,567	96	Access Road Gravel
20,387	80	Weighted Average
20,387		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.7	60	0.0330	1.50		Sheet Flow, Sheet flow across final cover
					Smooth surfaces n= 0.011 P2= 3.14"
1.3	293	0.0650	3.63	2.72	Trap/Vee/Rect Channel Flow, Perimeter Ditch
					Bot.W=0.00' D=0.50' Z= 3.0 '/' Top.W=3.00' n= 0.040
2.0	353	Total			

Summary for Subcatchment 119S: Discharge Pipe from PHase 2 Area under Sed Basin 3

Runoff = 41.21 cfs @ 12.18 hrs, Volume= 3.515 af, Depth= 4.56"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

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Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

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Area (ac)	CN	Description
* 9.248	74	Grass
9.248		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.4	100	0.0600	0.26		Sheet Flow, Sheet flow across access road Grass: Short n= 0.150 P2= 3.14"
18.3	983	0.0163	0.89		Shallow Concentrated Flow, Shallow slow across final cover Short Grass Pasture Kv= 7.0 fps
24.7	1,083	Total			

Summary for Subcatchment 120S: Discharge Pipe from Phase 4 Area under Access Road

Runoff = 8.24 cfs @ 12.06 hrs, Volume= 0.524 af, Depth= 4.56"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

Area (ac)	CN	Description
* 1.379	74	Grass
1.379		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
4.0	100	0.1900	0.41		Sheet Flow, Sheet flow across access road Grass: Short n= 0.150 P2= 3.14"
10.3	382	0.0078	0.62		Shallow Concentrated Flow, Shallow slow across final cover Short Grass Pasture Kv= 7.0 fps
14.3	482	Total			

Summary for Reach 104R: SW ChannelInflow Area = 5.470 ac, 0.00% Impervious, Inflow Depth = 4.56" for 100-yr, 24-hr event
Inflow = 43.29 cfs @ 11.96 hrs, Volume= 2.079 af
Outflow = 32.31 cfs @ 12.15 hrs, Volume= 2.079 af, Atten= 25%, Lag= 11.6 minRouting by Stor-Ind+Trans method, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Max. Velocity= 3.11 fps, Min. Travel Time= 7.9 min
Avg. Velocity= 0.61 fps, Avg. Travel Time= 40.2 minPeak Storage= 15,558 cf @ 12.02 hrs, Average Depth at Peak Storage= 0.85'
Bank-Full Depth= 2.00', Capacity at Bank-Full= 161.13 cfs10.00' x 2.00' deep channel, n= 0.040
Side Slope Z-value= 3.0 '/' Top Width= 22.00'
Length= 1,467.0' Slope= 0.0116 '/'
Inlet Invert= 812.00', Outlet Invert= 795.00'



Summary for Reach 105R: SE Channel

Inflow Area = 5.160 ac, 0.00% Impervious, Inflow Depth = 4.56" for 100-yr, 24-hr event
Inflow = 40.80 cfs @ 11.96 hrs, Volume= 1.961 af
Outflow = 37.70 cfs @ 12.03 hrs, Volume= 1.961 af, Atten= 8%, Lag= 4.1 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Max. Velocity= 4.50 fps, Min. Travel Time= 2.4 min
Avg. Velocity = 0.98 fps, Avg. Travel Time= 10.9 min

Peak Storage= 5,544 cf @ 11.99 hrs, Average Depth at Peak Storage= 0.71'
Bank-Full Depth= 2.00', Capacity at Bank-Full= 257.30 cfs

10.00' x 2.00' deep channel, n= 0.040
Side Slope Z-value= 3.0 '/' Top Width= 22.00'
Length= 643.0' Slope= 0.0295 '/'
Inlet Invert= 814.00', Outlet Invert= 795.00'



Summary for Reach 109R: S Channel

[65] Warning: Inlet elevation not specified

Inflow Area = 1.620 ac, 0.00% Impervious, Inflow Depth = 4.56" for 100-yr, 24-hr event
Inflow = 13.43 cfs @ 11.95 hrs, Volume= 0.616 af
Outflow = 12.25 cfs @ 12.03 hrs, Volume= 0.616 af, Atten= 9%, Lag= 4.7 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Max. Velocity= 2.25 fps, Min. Travel Time= 2.9 min
Avg. Velocity = 0.50 fps, Avg. Travel Time= 13.0 min

Peak Storage= 2,115 cf @ 11.98 hrs, Average Depth at Peak Storage= 0.48'
Bank-Full Depth= 2.00', Capacity at Bank-Full= 164.01 cfs

10.00' x 2.00' deep channel, n= 0.040
 Side Slope Z-value= 3.0 '/' Top Width= 22.00'
 Length= 389.0' Slope= 0.0120 '/'
 Inlet Invert= 0.00', Outlet Invert= -4.67'



Summary for Reach 110R: NE Channel

Inflow Area = 7.050 ac, 0.00% Impervious, Inflow Depth = 4.56" for 100-yr, 24-hr event
 Inflow = 55.80 cfs @ 11.96 hrs, Volume= 2.679 af
 Outflow = 47.72 cfs @ 12.07 hrs, Volume= 2.679 af, Atten= 14%, Lag= 6.5 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
 Max. Velocity= 5.31 fps, Min. Travel Time= 4.2 min
 Avg. Velocity = 1.11 fps, Avg. Travel Time= 20.0 min

Peak Storage= 12,442 cf @ 12.00 hrs, Average Depth at Peak Storage= 0.76'
 Bank-Full Depth= 2.00', Capacity at Bank-Full= 290.44 cfs

10.00' x 2.00' deep channel, n= 0.040
 Side Slope Z-value= 3.0 '/' Top Width= 22.00'
 Length= 1,328.0' Slope= 0.0377 '/'
 Inlet Invert= 818.00', Outlet Invert= 768.00'



Summary for Reach 111R: N Channel

[65] Warning: Inlet elevation not specified

Inflow Area = 5.890 ac, 0.00% Impervious, Inflow Depth = 4.56" for 100-yr, 24-hr event
 Inflow = 47.26 cfs @ 11.96 hrs, Volume= 2.239 af
 Outflow = 45.42 cfs @ 11.98 hrs, Volume= 2.239 af, Atten= 4%, Lag= 1.3 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
 Max. Velocity= 4.56 fps, Min. Travel Time= 0.7 min
 Avg. Velocity = 1.05 fps, Avg. Travel Time= 3.0 min

Peak Storage= 1,916 cf @ 11.97 hrs, Average Depth at Peak Storage= 0.81'

Bank-Full Depth= 2.00', Capacity at Bank-Full= 241.26 cfs

10.00' x 2.00' deep channel, n= 0.040

Side Slope Z-value= 3.0 '/' Top Width= 22.00'

Length= 189.0' Slope= 0.0260 '/'

Inlet Invert= 0.00', Outlet Invert= -4.91'



Summary for Reach 113R: WS Channel

Inflow Area = 5.410 ac, 0.00% Impervious, Inflow Depth = 4.56" for 100-yr, 24-hr event

Inflow = 42.94 cfs @ 11.96 hrs, Volume= 2.056 af

Outflow = 35.76 cfs @ 12.09 hrs, Volume= 2.056 af, Atten= 17%, Lag= 7.9 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Max. Velocity= 4.18 fps, Min. Travel Time= 5.1 min

Avg. Velocity = 0.86 fps, Avg. Travel Time= 24.5 min

Peak Storage= 11,208 cf @ 12.01 hrs, Average Depth at Peak Storage= 0.72'

Bank-Full Depth= 2.00', Capacity at Bank-Full= 235.64 cfs

10.00' x 2.00' deep channel, n= 0.040

Side Slope Z-value= 3.0 '/' Top Width= 22.00'

Length= 1,271.0' Slope= 0.0248 '/'

Inlet Invert= 804.50', Outlet Invert= 773.00'



Summary for Pond 50P: SED BASIN 2 (NORTH)

Inflow Area = 23.740 ac, 5.10% Impervious, Inflow Depth > 4.76" for 100-yr, 24-hr event

Inflow = 155.71 cfs @ 11.98 hrs, Volume= 9.415 af

Outflow = 40.36 cfs @ 12.22 hrs, Volume= 9.378 af, Atten= 74%, Lag= 14.4 min

Primary = 27.73 cfs @ 12.22 hrs, Volume= 9.052 af

Secondary = 12.63 cfs @ 12.22 hrs, Volume= 0.326 af

Routing by Stor-Ind method, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

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Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

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Starting Elev= 757.00' Surf.Area= 36,291 sf Storage= 95,928 cf

Peak Elev= 761.39' @ 12.22 hrs Surf.Area= 50,579 sf Storage= 285,761 cf (189,833 cf above start)

Plug-Flow detention time= 686.9 min calculated for 7.176 af (76% of inflow)

Center-of-Mass det. time= 436.7 min (1,249.2 - 812.5)

Volume	Invert	Avail.Storage	Storage Description
#1	754.00'	317,147 cf	Custom Stage Data (Prismatic) Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
754.00	27,824	0	0
756.00	33,306	61,130	61,130
758.00	39,275	72,581	133,711
760.00	45,733	85,008	218,719
762.00	52,695	98,428	317,147

Device	Routing	Invert	Outlet Devices
#1	Primary	755.00'	24.0" x 55.0' long Culvert CPP, projecting, no headwall, Ke= 0.900 Outlet Invert= 754.50' S= 0.0091 '/ Cc= 0.900 n= 0.013 Corrugated PE, smooth interior
#2	Device 1	760.00'	36.0" Horiz. Orifice/Grate Limited to weir flow C= 0.600
#3	Device 1	757.00'	4.0" Vert. Orifice/Grate X 3.00 C= 0.600
#4	Secondary	761.00'	20.0' long x 10.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64

Primary OutFlow Max=27.71 cfs @ 12.22 hrs HW=761.39' (Free Discharge)

- 1=Culvert (Inlet Controls 27.71 cfs @ 8.82 fps)
 2=Orifice/Grate (Passes < 40.06 cfs potential flow)
 3=Orifice/Grate (Passes < 2.59 cfs potential flow)

Secondary OutFlow Max=12.22 cfs @ 12.22 hrs HW=761.39' (Free Discharge)

- 4=Broad-Crested Rectangular Weir (Weir Controls 12.22 cfs @ 1.59 fps)

Summary for Pond 88P: SED BASIN 3 (WEST)

Inflow Area = 23.540 ac, 7.18% Impervious, Inflow Depth > 4.85" for 100-yr, 24-hr event
 Inflow = 149.19 cfs @ 11.97 hrs, Volume= 9.507 af
 Outflow = 28.18 cfs @ 12.32 hrs, Volume= 9.423 af, Atten= 81%, Lag= 20.8 min
 Primary = 28.18 cfs @ 12.32 hrs, Volume= 9.423 af
 Secondary = 0.00 cfs @ 1.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Starting Elev= 754.00' Surf.Area= 47,396 sf Storage= 128,978 cf

Peak Elev= 757.90' @ 12.32 hrs Surf.Area= 59,729 sf Storage= 337,808 cf (208,830 cf above start)

Plug-Flow detention time= 1,004.6 min calculated for 6.462 af (68% of inflow)

Center-of-Mass det. time= 602.4 min (1,411.6 - 809.2)

Volume	Invert	Avail.Storage	Storage Description
#1	751.00'	611,006 cf	Custom Stage Data (Prismatic) Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
751.00	38,660	0	0
752.00	41,501	40,081	40,081
754.00	47,396	88,897	128,978
756.00	53,576	100,972	229,950
758.00	60,040	113,616	343,566
760.00	66,789	126,829	470,395
762.00	73,822	140,611	611,006

Device	Routing	Invert	Outlet Devices
#1	Primary	751.00'	24.0" x 100.0' long Culvert CPP, projecting, no headwall, Ke= 0.900 Outlet Invert= 742.00' S= 0.0900 '/ Cc= 0.900 n= 0.013 Corrugated PE, smooth interior
#2	Device 1	757.00'	36.0" Horiz. Orifice/Grate Limited to weir flow C= 0.600
#3	Device 1	754.00'	4.0" Vert. Orifice/Grate X 3.00 C= 0.600
#4	Secondary	761.00'	20.0' long x 10.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64

Primary OutFlow Max=28.83 cfs @ 12.32 hrs HW=757.90' (Free Discharge)

- ↑ **1=Culvert** (Passes 28.83 cfs of 29.01 cfs potential flow)
- ↑ **2=Orifice/Grate** (Weir Controls 26.40 cfs @ 3.11 fps)
- ↑ **3=Orifice/Grate** (Orifice Controls 2.44 cfs @ 9.31 fps)

Secondary OutFlow Max=0.00 cfs @ 1.00 hrs HW=754.00' (Free Discharge)

- ↑ **4=Broad-Crested Rectangular Weir** (Controls 0.00 cfs)

Summary for Pond 96P: SED BASIN 4 (SOUTH)

Inflow Area = 29.290 ac, 5.02% Impervious, Inflow Depth > 4.80" for 100-yr, 24-hr event
 Inflow = 172.35 cfs @ 12.00 hrs, Volume= 11.727 af
 Outflow = 18.39 cfs @ 12.69 hrs, Volume= 11.689 af, Atten= 89%, Lag= 41.6 min
 Primary = 18.39 cfs @ 12.69 hrs, Volume= 11.689 af
 Secondary = 0.00 cfs @ 1.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Starting Elev= 753.00' Surf.Area= 42,207 sf Storage= 114,100 cf

Peak Elev= 758.24' @ 12.69 hrs Surf.Area= 58,334 sf Storage= 376,711 cf (262,611 cf above start)

Plug-Flow detention time= 527.9 min calculated for 9.070 af (77% of inflow)

Center-of-Mass det. time= 326.3 min (1,141.1 - 814.8)

Volume	Invert	Avail.Storage	Storage Description
#1	750.00'	484,301 cf	Custom Stage Data (Prismatic) Listed below (Recalc)

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Type II 24-hr 100-yr, 24-hr Rainfall=7.59"

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Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
750.00	33,973	0	0
752.00	39,349	73,322	73,322
754.00	45,064	84,413	157,735
756.00	51,118	96,182	253,917
758.00	57,511	108,629	362,546
760.00	64,244	121,755	484,301

Device	Routing	Invert	Outlet Devices
#1	Primary	750.00'	18.0" x 105.0' long Culvert CPP, projecting, no headwall, Ke= 0.900 Outlet Invert= 748.00' S= 0.0190 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior
#2	Device 1	755.00'	36.0" Horiz. Orifice/Grate Limited to weir flow C= 0.600
#3	Device 1	753.00'	4.0" Vert. Orifice/Grate X 3.00 C= 0.600
#4	Secondary	759.00'	20.0' long x 10.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64

Primary OutFlow Max=18.39 cfs @ 12.69 hrs HW=758.24' (Free Discharge)

↑ **1=Culvert** (Inlet Controls 18.39 cfs @ 10.41 fps)
 ↑ **2=Orifice/Grate** (Passes < 61.30 cfs potential flow)
 ↑ **3=Orifice/Grate** (Passes < 2.84 cfs potential flow)

Secondary OutFlow Max=0.00 cfs @ 1.00 hrs HW=753.00' (Free Discharge)↑ **4=Broad-Crested Rectangular Weir** (Controls 0.00 cfs)**Summary for Pond 111P: Sed Basin 5 (Temp)**

[93] Warning: Storage range exceeded by 53.90'

[85] Warning: Oscillations may require Finer Routing>1

Inflow Area = 9.248 ac, 0.00% Impervious, Inflow Depth = 4.56" for 100-yr, 24-hr event
 Inflow = 41.21 cfs @ 12.18 hrs, Volume= 3.515 af
 Outflow = 16.20 cfs @ 12.61 hrs, Volume= 3.090 af, Atten= 61%, Lag= 25.6 min
 Primary = 16.20 cfs @ 12.61 hrs, Volume= 3.090 af

Routing by Stor-Ind method, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
 Peak Elev= 813.90' @ 12.60 hrs Surf.Area= 1.016 ac Storage= 1.857 af

Plug-Flow detention time= 495.8 min calculated for 3.090 af (88% of inflow)
 Center-of-Mass det. time= 436.6 min (1,269.3 - 832.8)

Volume	Invert	Avail.Storage	Storage Description
#1	756.00'	1.857 af	Custom Stage Data (Prismatic) Listed below (Recalc)

Elevation (feet)	Surf.Area (acres)	Inc.Store (acre-feet)	Cum.Store (acre-feet)
756.00	0.009	0.000	0.000
758.00	0.416	0.425	0.425
760.00	1.016	1.432	1.857

Device	Routing	Invert	Outlet Devices
#1	Device 2	758.00'	4.0" Vert. Orifice/Grate X 3.00 C= 0.600
#2	Primary	756.00'	12.0" x 321.0' long Culvert RCP, groove end projecting, Ke= 0.200 Outlet Invert= 739.95' S= 0.0500 '/ Cc= 0.900 n= 0.013 Corrugated PE, smooth interior
#3	Device 2	761.00'	36.0" Horiz. Orifice/Grate Limited to weir flow C= 0.600

Primary OutFlow Max=15.31 cfs @ 12.61 hrs HW=807.51' (Free Discharge)

↑ **2=Culvert** (Barrel Controls 15.31 cfs @ 19.49 fps)
 ↑ **1=Orifice/Grate** (Passes < 8.85 cfs potential flow)
 ↑ **3=Orifice/Grate** (Passes < 232.11 cfs potential flow)

Summary for Pond 113P: Sed Basin 6 (Temp)

Inflow Area = 1.379 ac, 0.00% Impervious, Inflow Depth = 4.56" for 100-yr, 24-hr event
 Inflow = 8.24 cfs @ 12.06 hrs, Volume= 0.524 af
 Outflow = 0.51 cfs @ 13.36 hrs, Volume= 0.283 af, Atten= 94%, Lag= 77.7 min
 Primary = 0.51 cfs @ 13.36 hrs, Volume= 0.283 af

Routing by Stor-Ind method, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
 Peak Elev= 762.33' @ 13.36 hrs Surf.Area= 0.247 ac Storage= 0.319 af

Plug-Flow detention time= 371.2 min calculated for 0.283 af (54% of inflow)
 Center-of-Mass det. time= 257.0 min (1,080.2 - 823.1)

Volume	Invert	Avail.Storage	Storage Description
#1	760.00'	1.620 af	Custom Stage Data (Prismatic) Listed below (Recalc)

Elevation (feet)	Surf.Area (acres)	Inc.Store (acre-feet)	Cum.Store (acre-feet)
760.00	0.013	0.000	0.000
762.00	0.228	0.241	0.241
764.00	0.343	0.571	0.812
766.00	0.465	0.808	1.620

Device	Routing	Invert	Outlet Devices
#1	Device 2	762.00'	4.0" Vert. Orifice/Grate X 3.00 C= 0.600
#2	Primary	760.00'	8.0" x 210.0' long Culvert RCP, groove end projecting, Ke= 0.200 Outlet Invert= 757.90' S= 0.0100 '/ Cc= 0.900 n= 0.013 Corrugated PE, smooth interior
#3	Device 2	765.00'	36.0" Horiz. Orifice/Grate Limited to weir flow C= 0.600

Primary OutFlow Max=0.51 cfs @ 13.36 hrs HW=762.33' (Free Discharge)

↑ **2=Culvert** (Passes 0.51 cfs of 1.54 cfs potential flow)

↑ **1=Orifice/Grate** (Orifice Controls 0.51 cfs @ 1.96 fps)

↑ **3=Orifice/Grate** (Controls 0.00 cfs)

Summary for Link 97L: Flume 6

Inflow Area = 5.410 ac, 0.00% Impervious, Inflow Depth = 4.56" for 100-yr, 24-hr event
Inflow = 42.94 cfs @ 11.96 hrs, Volume= 2.056 af
Primary = 42.94 cfs @ 11.96 hrs, Volume= 2.056 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Summary for Link 98L: Flume 5

Inflow Area = 5.890 ac, 0.00% Impervious, Inflow Depth = 4.56" for 100-yr, 24-hr event
Inflow = 47.26 cfs @ 11.96 hrs, Volume= 2.239 af
Primary = 47.26 cfs @ 11.96 hrs, Volume= 2.239 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Summary for Link 99L: Flume 4

Inflow Area = 7.050 ac, 0.00% Impervious, Inflow Depth = 4.56" for 100-yr, 24-hr event
Inflow = 55.80 cfs @ 11.96 hrs, Volume= 2.679 af
Primary = 55.80 cfs @ 11.96 hrs, Volume= 2.679 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Summary for Link 100L: Flume 3

Inflow Area = 5.470 ac, 0.00% Impervious, Inflow Depth = 4.56" for 100-yr, 24-hr event
Inflow = 43.29 cfs @ 11.96 hrs, Volume= 2.079 af
Primary = 43.29 cfs @ 11.96 hrs, Volume= 2.079 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Summary for Link 101L: Flume 2

Inflow Area = 5.160 ac, 0.00% Impervious, Inflow Depth = 4.56" for 100-yr, 24-hr event
Inflow = 40.80 cfs @ 11.96 hrs, Volume= 1.961 af
Primary = 40.80 cfs @ 11.96 hrs, Volume= 1.961 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Summary for Link 102L: Flume 1

Inflow Area = 1.620 ac, 0.00% Impervious, Inflow Depth = 4.56" for 100-yr, 24-hr event
Inflow = 13.43 cfs @ 11.95 hrs, Volume= 0.616 af
Primary = 13.43 cfs @ 11.95 hrs, Volume= 0.616 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Summary for Link 108L: Across South Road (Culvert 3-1 & 3-2)

Inflow Area = 23.280 ac, 0.00% Impervious, Inflow Depth = 4.61" for 100-yr, 24-hr event
Inflow = 141.13 cfs @ 12.03 hrs, Volume= 8.951 af
Primary = 141.13 cfs @ 12.03 hrs, Volume= 8.951 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Summary for Link 112L: To Sed Basin 2 (Culvert 1-1 & 1-2)

Inflow Area = 15.480 ac, 0.00% Impervious, Inflow Depth = 4.62" for 100-yr, 24-hr event
Inflow = 102.06 cfs @ 12.01 hrs, Volume= 5.962 af
Primary = 102.06 cfs @ 12.01 hrs, Volume= 5.962 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Summary for Link 114L: To Sed Basin 3 (Culvert 2-1 & 2-2)

Inflow Area = 21.110 ac, 0.00% Impervious, Inflow Depth = 4.64" for 100-yr, 24-hr event
Inflow = 140.27 cfs @ 11.99 hrs, Volume= 8.170 af
Primary = 140.27 cfs @ 11.99 hrs, Volume= 8.170 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Summary for Link 115L: To Sed Basin 4 (Culvert 4-1 & 4-2)

Inflow Area = 26.700 ac, 0.00% Impervious, Inflow Depth = 4.67" for 100-yr, 24-hr event
Inflow = 161.24 cfs @ 12.01 hrs, Volume= 10.380 af
Primary = 161.24 cfs @ 12.01 hrs, Volume= 10.380 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Perimeter Ditch and Diversion Berm Sizing

- Perimeter Ditch and Diversion Berm Sizing
- Rock-lined Channel Sizing

Perimeter Ditch and Diversion Berm Sizing

Perimeter Ditch and Diversion Berm Sizing Flow Summary

This calculation sums the flows from the contributing drainage subareas to each perimeter ditch for the 25-year, 24-hour storm event. By summing the flows, this approach is considered conservative. This calculation also considers the worst-case diversion berm flow for the 25-year, 24-hour storm event.

Perimeter Ditch Flows

Swale	Subarea	Flow Rate (cfs)
NE	4	27.15
	7	9.82
	8	7.42
	12	9.32
	14	9.50
		63.21

Swale	Subarea	Flow Rate (cfs)
NW	3	15.50
	5	9.11
	6	10.15
	9	8.00
	10	3.32
		46.08

Swale	Subarea	Flow Rate (cfs)
WN	1	37.50
		37.50

Swale	Subarea	Flow Rate (cfs)
WS	2	41.15
	11	7.46
	16	10.16
	18	10.12
		68.89

Notes:

1. Refer to Storm Water Management Plan Sheet for swale locations
2. Subarea flow rates from HydroCAD model output for 25-yr, 24-hr storm event

I:\25211509\Reports\Permit Amendment\Appendices\Storm Water Management\Calcs - final\Perimeter Ditch and Diversion Berm Sizing_131127.xls]Ditch Flows 1

Perimeter Ditch Flows (continued)

Swale	Subarea	Flow Rate (cfs)
SW	17	10.18
	19	10.18
	20	32.49
	23	7.65
	24	4.08
	25	4.61
	Total:	69.19

Swale	Subarea	Flow Rate (cfs)
SE	13	9.67
	15	10.13
	21	17.56
	22	6.59
	Total:	43.95

Worst-Case Diversion Berm Flow

Diversion Berm	Flow Rate (cfs)
Subareas 17, 19	10.18

Notes:

1. Refer to Storm Water Management Plan Sheet for swale locations
2. Subarea flow rates from HydroCAD model output for 25-yr, 24-hr storm event

I:\25211509\Reports\Permit Amendment\Appendices\Storm Water Management\Calcs - final\Perimeter Ditch and Diversion Berm Sizing_131127.xls]Ditch Flows 2

1 Lining Type: Vegetation

2	Project ID: 25211509.03
3	Location: Ottuma Iowa
4	Designer/Checker: JMO/
5	Date: 10/25/13

6							
7	DITCH/DIVERSION BERM	NE	NW	WN	WS	SW	SE
8							Diversion Berm
9							Subareas 17, 19
10	Channel/Ditch Geometry						
11	Channel Slope, S_o (ft/ft)	0.031	0.026	0.010	0.025	0.012	0.030
12	Channel Bottom Width, B (ft)	10	10	10	10	10	10
13	Channel Side Slope, z_1	3	3	3	3	3	3
14	Channel Side Slope, z_2	3	3	3	3	3	3
15	Flow Depth, d (ft) Solve iteratively	0.81	0.75	1.02	0.92	1.27	0.70
16	Safety Factor, SF	1.5	1.5	1.5	1.5	1.5	1.5
17	Vegetation/Soil Parameters						
18	Vegetation Retardance Class	D	D	D	D	D	D
19	Vegetation Condition	good	good	good	good	good	good
20	Vegetation Growth Form	turf	turf	turf	turf	turf	turf
21	Soil Type	cohesive	cohesive	cohesive	cohesive	cohesive	cohesive
22	D_{75} (in) (Set at 0.00 for cohesive soils)						
23	ASTM Soil Class	ML	ML	ML	ML	ML	ML
24	Plasticity Index, PI	16	16	16	16	16	16
25	Results Summary						
26	Design Q (ft ³ /s)	63.21	46.08	37.50	68.89	69.19	43.95
27	Calculated Q (ft ³ /s)	63.3	46.1	37.6	69.1	69.4	44.1
28	Difference Between Design & Calc. Flow (%)	0.2%	0.1%	0.3%	0.3%	0.3%	0.4%
29	Stable (Yes or No)	YES	YES	YES	YES	YES	YES
30	Channel Parameters						
31	Vegetation Height, h (ft)	0.33	0.33	0.33	0.33	0.33	0.33
32	Grass Roughness Coefficient, C_n	0.165	0.165	0.165	0.165	0.165	0.165
33	Cover Factor, C_f	0.90	0.90	0.90	0.90	0.90	0.90
34	Noncohesive Soil						
35	Soil Grain Roughness, n_s	0.016	0.016	0.016	0.016	0.016	0.016
36	Permissible Soil Shear Stress, τ_p (lb/ft ²)	N/A	N/A	N/A	N/A	N/A	N/A
37	Cohesive Soil						
38	Porosity, e	0.33	0.33	0.33	0.33	0.33	0.33
39	Soil Coefficient 1, c_1	1.0700	1.0700	1.0700	1.0700	1.0700	1.0700
40	Soil Coefficient 2, c_2	7.15	7.15	7.15	7.15	7.15	7.15
41	Soil Coefficient 3, c_3	11.900	11.900	11.900	11.900	11.900	11.900
42	Soil Coefficient 4, c_4	1.48	1.48	1.48	1.48	1.48	1.48
43	Soil Coefficient 5, c_5	-0.57	-0.57	-0.57	-0.57	-0.57	-0.57
44	Soil Coefficient 6, c_6	0.00010	0.00010	0.00010	0.00010	0.00010	0.00010
45	Permissible Soil Shear Stress, τ_p (lb/ft ²)	0.067	0.067	0.067	0.067	0.067	0.067
46	Total Permissible Shear Stress, τ_p (lb/ft ²)	0.067	0.067	0.067	0.067	0.067	0.067
47	Cross Sectional Area, A (ft ²)	10.113	9.202	13.353	11.786	17.592	8.399
48	Wetted Perimeter, P (ft)	15.14	14.75	16.46	15.84	18.05	14.40
49	Hydraulic Radius, R (ft)	0.668	0.624	0.811	0.744	0.975	0.583
50	Top Width, T (ft)						
51	Hydraulic Depth, D (ft)	#VALUE!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
52	Froude Number (Q design)	#VALUE!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
53	Channel Shear Stress, τ_o (lb/ft ²)	1.29	1.01	0.51	1.16	0.71	1.07
54	Actual Shear Stress, τ_d (lb/ft ²)	1.57	1.22	0.64	1.44	0.92	1.28
55	Mannings n	0.032	0.035	0.046	0.033	0.040	0.034
56	Average Velocity, V (ft/s)	6.25	5.01	2.81	5.85	3.93	5.23
57	Calculated Flow, Q (ft ³ /s)	63.3	46.1	37.6	69.1	69.4	44.1
58	Difference Between Design & Calc. Flow (%)	0.2%	0.1%	0.3%	0.3%	0.3%	0.4%
59	Effective Shear on Soil Surface, τ_e (lb/ft ²)	0.039	0.025	0.008	0.034	0.015	0.028
60	Total Permissible Shear on Veg., $\tau_{p,veg}$ (lb/ft ²)	2.67	3.20	5.52	2.84	4.17	3.02
61	Stable (Y or N)	YES	YES	YES	YES	YES	YES

Rock-lined Channel Sizing

Rock Chute Design Data

(Version 4.01 - 04/23/03, Based on Design of Rock Chutes by Robinson, Rice, Kadavy, ASAE, 1998)

Project: OML Expansion

Designer: JMO

Date: 11/27/2013

County: Wapello

Checked by: BP

Date: 11/27/13

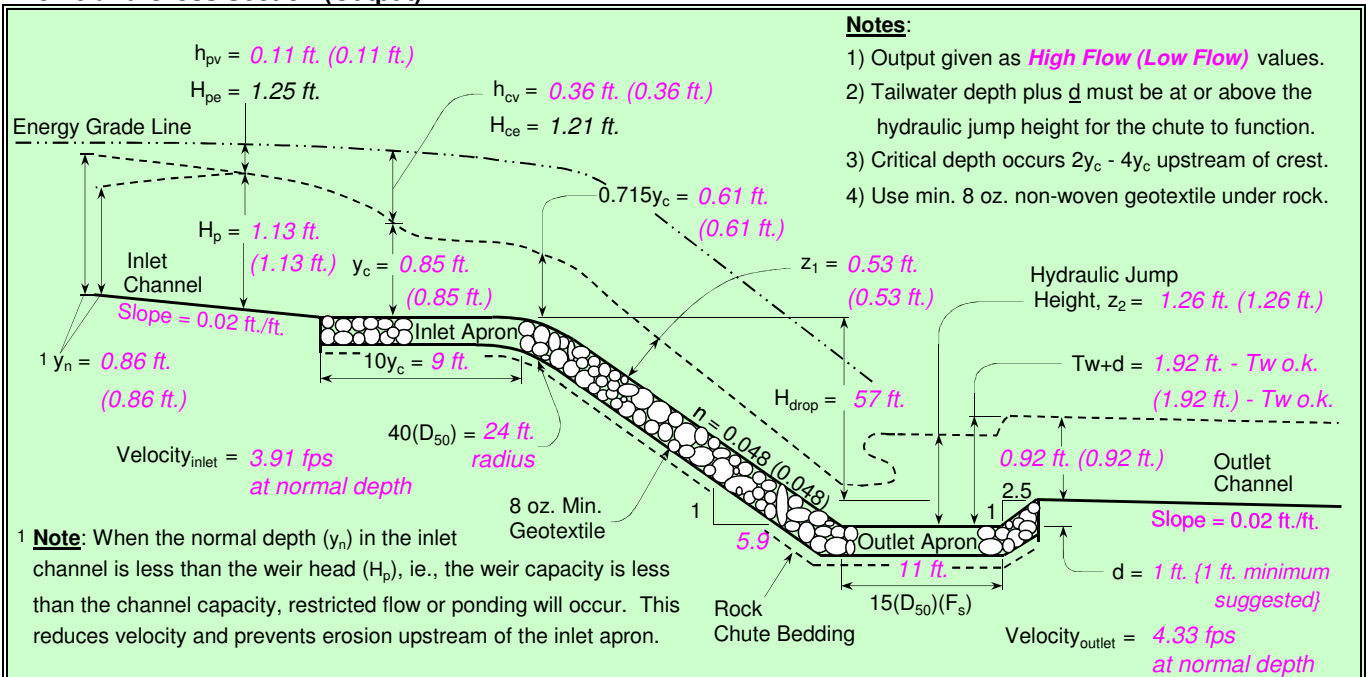
Input Channel Geometry

Inlet Channel	Chute	Outlet Channel
Bw = 10.0 ft.	Bw = 10.0 ft.	Bw = 10.0 ft.
Side slopes = 6.0 (m:1)	Factor of safety = 1.20 (F_s)	Side slopes = 3.0 (m:1)
n-value = 0.040	Side slopes = 3.0 (m:1) → 2.0:1 max.	n-value = 0.040
Bed slope = 0.0200 ft./ft.	Bed slope (5.9:1) = 0.170 ft./ft. → 2.5:1 max.	Bed slope = 0.0200 ft./ft.
Freeboard = 0.5 ft.	Outlet apron depth, d = 1.0 ft.	Base flow = 0.0 cfs

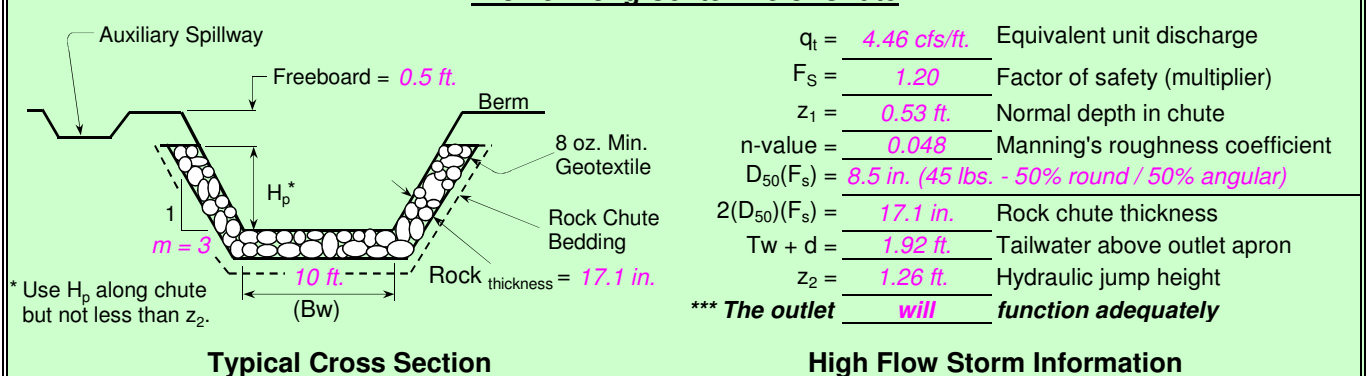
Design Storm Data (Table 2, NHCP, NRCS Grade Stabilization Structure No. 410)

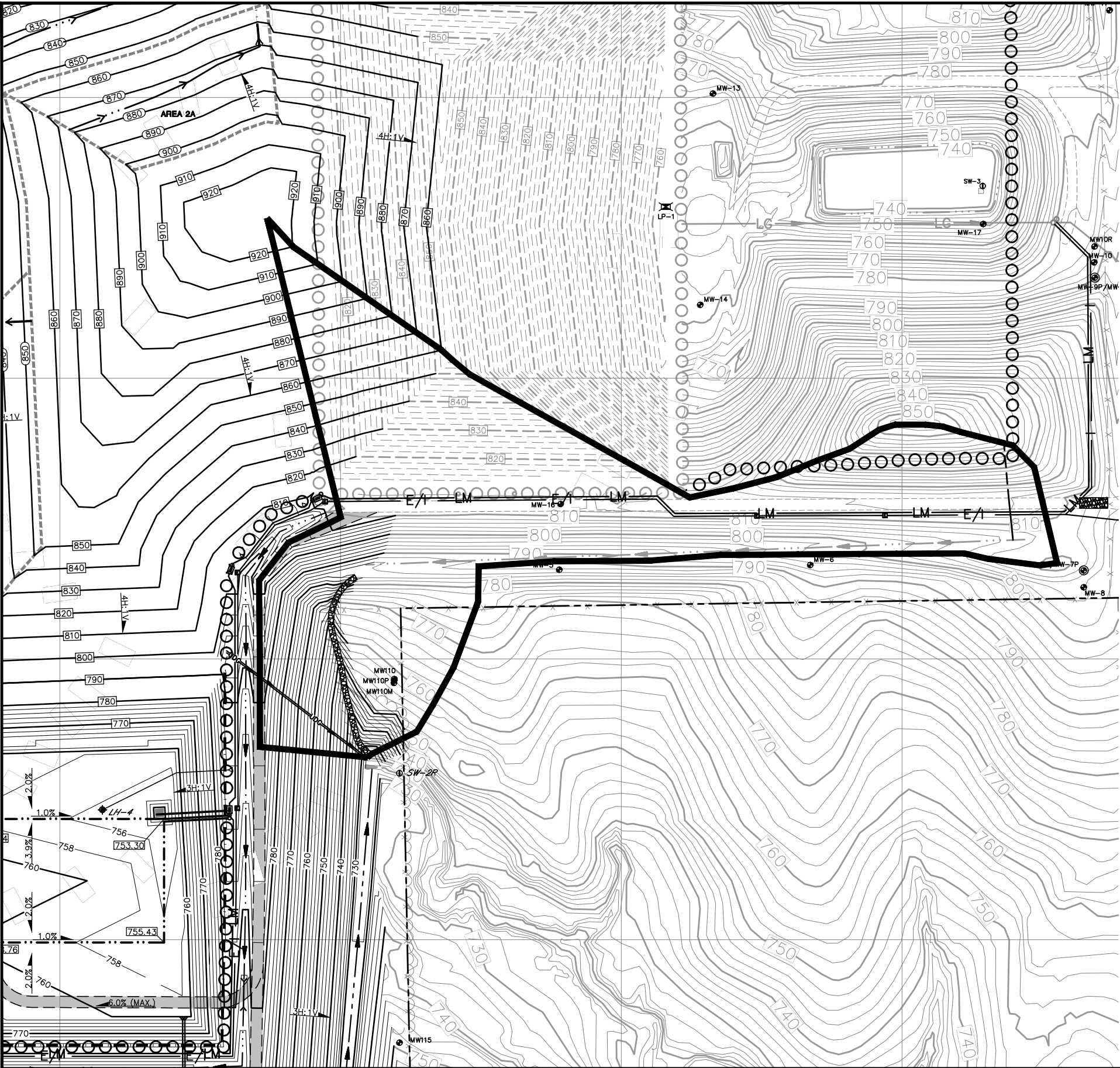
Drainage area =	acres	Rainfall = ☐ 0 - 3 in. ☐ 3 - 5 in. ☒ 5+ in.	Note: The total required capacity is routed through the chute (principal spillway) or in combination with an auxiliary spillway.
Apron elev. --- Inlet =	784.0 ft. --- Outlet =	726.0 ft. --- ($H_{drop} = 57$ ft.)	Input tailwater (T_w):
Chute capacity =	Q25-year	Minimum capacity (based on a 5-year, 24-hour storm with a 5+ inch rainfall)	
Total capacity =	Q100-year		
$Q_{high} =$	51.1 cfs	High flow storm through chute	T_w (ft.) = Program 0.17
$Q_{low} =$	51.1 cfs	Low flow storm through chute	T_w (ft.) = Program

Profile and Cross Section (Output)



Profile Along Centerline of Chute





- LEGEND
- ROCK CHUTE DRAINAGE AREA = 10.25 ACRES
 - SHEET FLOW = 100 FT
 - SHALLOW FLOW = 78 FT
 - CHANNEL FLOW = 1177 FT

N



SCALE: 1" = 200'

PROJECT NO.	25211509.03	DRAWN BY:	BJM	ENGINEER SCS ENGINEERS 2830 DAIRY DRIVE MADISON, WI 53718-6751 PHONE: (608) 224-2830	CLIENT INTERSTATE POWER AND LIGHT COMPANY OTTUMWA MIDLAND LANDFILL 130TH STREET OTTUMWA, IOWA 52501	SITE PERMIT AMENDMENT PLANS NORTH & SOUTH EXPANSION OTTUMWA MIDLAND LANDFILL OTTUMWA, IOWA	ROCK CHUTE DRAINAGE AREA	FIGURE
DRAWN:	10/25/13	CHECKED BY:	BP					2
REVISED:	11/27/13	APPROVED BY:	BP 11/27/13					

Downslope Flume and Energy Dissipator Sizing

Job No. 25211509.03

Job: OML Expansion

By: JMO

Date: 10/25/13

Client: IPL

Subject: Downslope Flume Sizing

Chk'd: BP

Date: 11/25/13

Purpose: To size the downslope flume pipes to accommodate the flows expected from a 25-year, 24-hour storm event.

Approach: Use the orifice equation to size the downslope pipe inlet and Manning's equation to size the downslope pipes.

Calculations:

For the diversion berm swales, the maximum flow from the 25-year, 24-hour storm is 10.18 cfs (see Subareas 17 and 19 in Hydrograph Generation section of appendix).

Flume inlet sizing:

$$\text{Orifice Equation: } Q = C \times A \times (2 \times g \times h)^{0.5}$$

Q = flow rate (cfs)

C = orifice coefficient = 0.63

A = area of orifice = 1.8 sf for 18" dia. pipe

g = acceleration due to gravity = 32.2 ft/sec²

h = orifice head acting on centerline = 1.25 ft for 18" dia. pipe

$$Q_{18" \text{ pipe}} = 0.63 \times 1.8 \times (2 \times 32.2 \times 1.25)^{0.5} = 10.2 \text{ cfs} \quad \text{ok}$$

Downslope pipe sizing:

The downslope flume pipe diameter will be at least as big as the inlet pipe diameter. The capacity of an 18" dia. flume at the following slopes is as follows (see attached Sheets 2 and 3):

Flume Size	Flow Capacity of Pipe
	25% slope
18" dia.	68 cfs

The peak flows from a 25-year, 24-hour storm to each flume are as follows:

Flume Number	Subareas Contributing Flow	Flow Rate (cfs)
Flume 1	24, 25	9
Flume 2	13, 15, 22	26
Flume 3	17, 19, 23	28
Flume 4	7, 8, 12, 14	36
Flume 5	5, 6, 9, 10	31
Flume 6	11, 16, 18	28

The 18" dia. Downslope flume pipes have sufficient capacity to accommodate the incoming flows.

Results:

18" dia. flume inlets will accommodate flows along diversion berms resulting from a 25-year, 24 hour storm.

18" dia. downslope flume pipes will accommodate flows resulting from a 25-year, 24-hour storm event.

I:\25211509\Reports\Permit Amendment\Appendices\Storm Water Management\Calcs - final\[Downslope Flume Sizing_131127.xls]Sizing Calc

Job No. 25211509.03

Job: OML

By: JMO

Date: 10/25/2013

Client: IPL

Subject: Downslope Flume Sizing

Chk'd: BP

Date: 11/27/2013

Pipe Capacity - 18" dia.

Use the Manning Formula to determine max flow in a pipe flowing full

$$\text{Manning's Equation: } Q = (1.49/n) \times A \times R^{2/3} \times S^{1/2}$$

where: Q = Flow Rate, cfs

n = Manning's Roughness Coefficient

A = Flow Area, sf

R = Hydraulic Radius, ft (= A/P)

S = Pipe Slope, ft/ft

Design Criteria

Pipe Diameter (in) = D = 18

Pipe Slope (ft/ft) = S = 0.25

Manning's Roughness Coefficient = n = 0.010

Water Level (in) = 18

Cross Sectional Area Calculation

Pipe Radius (ft) = 0.75

Circle Segment Height (ft) = 0.0

Central Angle (rad) = 0.00

Wetted Perimeter (ft) = P = 4.71

Flow Area (sf) = A = 1.77

Hydraulic Radius (ft) = A/P = R = 0.38

Flow Velocity Calculation

$$\text{Flow Velocity (fps)} = V = (1.49/n) \times R^{2/3} \times S^{1/2} = 38.63$$

Flow Rate Calculation

$$\text{Flow Rate (cfs)} = Q = V \times A = 68.27$$

I:\25211509\Reports\Permit Amendment\Appendices\Storm Water Management\Calcs - final\[Downslope Flume Sizing_131127.xls]18" capacity

Job No. 25211509.03

Job: OML Expansion

By: JMO

Date: 10/25/13

Client: IPL

Subject: Energy Dissipator Design

Chk'd: BP

Date: 11/25/13

Energy Dissipator Design**Pipe/Culvert: Flume 1**

* Peak flow in this flume from 25-year, 24-hour event is 9 cfs.

Compute Flow Area:

$$A = Q/V$$

where: A = Flow Area

$$Q = \text{Maximum flow rate} = 9.0 \text{ cfs}$$

$$V = \text{Outlet velocity} = 27 \text{ ft/sec (from Manning's equation, see Sheet 4)}$$

$$A = 0.3 \text{ sf}$$

Compute Equivalent Depth of Flow Entering Dissipator:

$$Y_e = (A/2)^{1/2}$$

where: Y_e = Equivalent depth

A = Area (from above)

$$Y_e = 0.4 \text{ ft}$$

Compute Froude Number:

$$Fr = V/[(g*Y_e)^{1/2}]$$

where: Fr = Froude Number

V = Velocity (from above)

g = Gravity constant (32.2 ft/sec)

 Y_e = Equivalent depth (from above)

$$Fr = 7.4$$

Compute Energy at End of Pipe:

$$H_o = Y_e + V^2/2g$$

where: H_o = Energy Y_e = Equivalent depth (from above)

V = Velocity (from above)

g = Gravity constant (32.2 ft/sec)

$$H_o = 11.5 \text{ ft}$$

Determine Width of Dissipator:

Use Froude Number computed above and Figure 9.14 from "Hydraulic Design of Energy Dissipators for Culverts and Channels" to obtain value for H_o/W . Given H_o above, compute W (width of dissipator).

$$\text{From Figure 9.14, } H_o/W_B = 3.1 \text{ (interpolated)}$$

$$W_B = 3.7 \text{ ft}$$

Determine Remaining Dimensions of the Dissipator:

Based on W determined above, use Table 9.2 (CU) to determine the remaining dissipator dimensions. Round the value of W_B to the nearest entry in the table (interpolation is not necessary).

Job No. 25211509.03

Job: OML

By: JMO

Date: 10/25/13

Client: IPL

Subject: Energy Dissipator Sizing

Chk'd: BP

Date: 11/25/13

Flume 1

Use the Manning Formula to determine flow in a pipe

$$\text{Manning's Equation: } Q = (1.49/n) \times A \times R^{2/3} \times S^{1/2}$$

where: Q = Flow Rate, cfs n = Manning's Roughness Coefficient A = Flow Area, sf R = Hydraulic Radius, ft (= A/P) S = Pipe Slope, ft/ft**Design Criteria**Pipe Diameter (in) = D = 18Pipe Slope (ft/ft) = S = 0.25Manning's Roughness Coefficient = n = 0.010

Water Level (in) = 4.413

Cross Sectional Area Calculation

Pipe Radius (ft) = 0.75

Circle Segment Height (ft) = 0.4

Central Angle (rad) = 2.07

Wetted Perimeter (ft) = P = 1.55Flow Area (sf) = A = 0.34Hydraulic Radius (ft) = A/P = R = 0.22**Flow Velocity Calculation**

$$\text{Flow Velocity (fps)} = V = (1.49/n) \times R^{2/3} \times S^{1/2} = 26.77$$

Flow Rate Calculation

$$\text{Flow Rate (cfs)} = Q = V \times A = 9.00$$

Job No. 25211509.03

Job: OML Expansion

By: JMO

Date: 10/25/13

Client: IPL

Subject: Energy Dissipator Design

Chk'd: BP

Date: 11/25/13

Energy Dissipator Design**Pipe/Culvert: Flumes 2, 3, 4, 5, 6**

* Peak flow in these flumes from 25-year, 24-hour event ranges from 26-36 cfs. Design for 36 cfs.

Compute Flow Area:

$$A = Q/V$$

where: A = Flow Area

$$Q = \text{Maximum flow rate} = 36.0 \text{ cfs}$$

$$V = \text{Outlet velocity} = 39 \text{ ft/sec (from Manning's equation, see Sheet 8)}$$

$$A = 0.9 \text{ sf}$$

Compute Equivalent Depth of Flow Entering Dissipator:

$$Y_e = (A/2)^{1/2}$$

where: Y_e = Equivalent depth

A = Area (from above)

$$Y_e = 0.7 \text{ ft}$$

Compute Froude Number:

$$Fr = V/[(g*Y_e)^{1/2}]$$

where: Fr = Froude Number

V = Velocity (from above)

g = Gravity constant (32.2 ft/sec)

 Y_e = Equivalent depth (from above)

$$Fr = 8.4$$

Compute Energy at End of Pipe:

$$H_o = Y_e + V^2/2g$$

where: H_o = Energy Y_e = Equivalent depth (from above)

V = Velocity (from above)

g = Gravity constant (32.2 ft/sec)

$$H_o = 24.5 \text{ ft}$$

Determine Width of Dissipator:

Use Froude Number computed above and Figure 9.14 from "Hydraulic Design of Energy Dissipators for Culverts and Channels" to obtain value for H_o/W . Given H_o above, compute W (width of dissipator).

$$\text{From Figure 9.14, } H_o/W_b = 4.2 \text{ (interpolated)}$$

$$W_b = 5.8 \text{ ft}$$

Determine Remaining Dimensions of the Dissipator:

Based on W determined above, use Table 9.2 (CU) to determine the remaining dissipator dimensions. Round the value of W_b to the nearest entry in the table (interpolation is not necessary).

Job No. 25211509.03

Job: OML

By: JMO

Date: 10/25/13

Client: IPL

Subject: Energy Dissipator Sizing

Chk'd: BP

Date: 11/25/13

Flumes 2, 3, 4, 5, 6

Use the Manning Formula to determine flow in a pipe

$$\text{Manning's Equation: } Q = (1.49/n) \times A \times R^{2/3} \times S^{1/2}$$

where: Q = Flow Rate, cfs

n = Manning's Roughness Coefficient

A = Flow Area, sf

R = Hydraulic Radius, ft (= A/P)

S = Pipe Slope, ft/ft

Design Criteria

Pipe Diameter (in) = D = 18

Pipe Slope (ft/ft) = S = 0.25

Manning's Roughness Coefficient = n = 0.010

Water Level (in) = 9.288

Cross Sectional Area Calculation

Pipe Radius (ft) = 0.75

Circle Segment Height (ft) = 0.7

Central Angle (rad) = 3.08

Wetted Perimeter (ft) = P = 2.40

Flow Area (sf) = A = 0.92

Hydraulic Radius (ft) = A/P = R = 0.38

Flow Velocity Calculation

$$\text{Flow Velocity (fps)} = V = (1.49/n) \times R^{2/3} \times S^{1/2} = 39.15$$

Flow Rate Calculation

$$\text{Flow Rate (cfs)} = Q = V \times A = 36.00$$

shows the relationship of the Froude number to the ratio of the energy entering the dissipator to the width of dissipator required. The Los Angeles tests indicate that limited extrapolation of this curve is permissible.

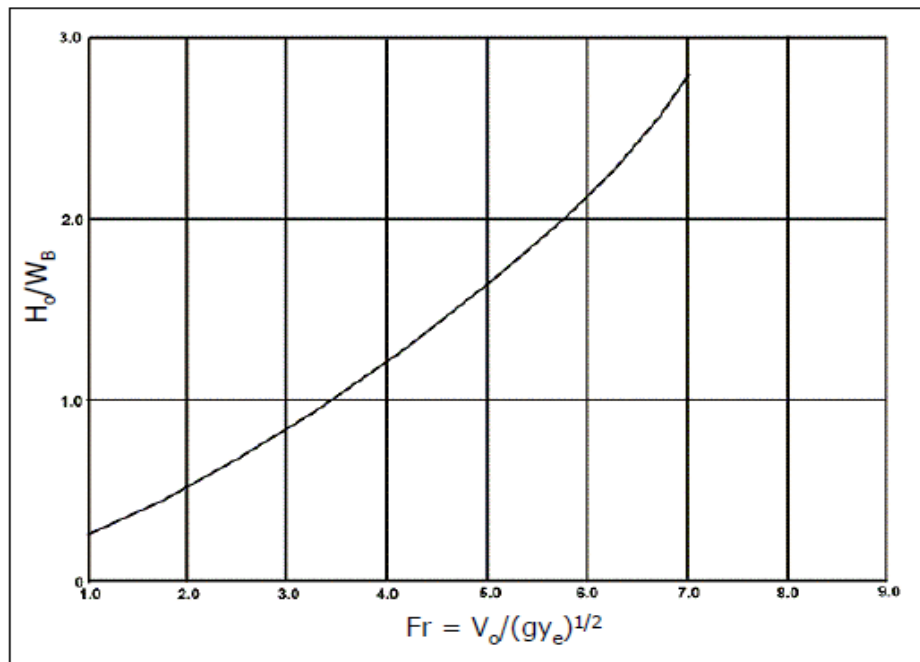


Figure 9.14. Design Curve for USBR Type VI Impact Basin

Once the basin width, W_B , has been determined, many of the other dimensions shown in Figure 9.13 follow according to Table 9.2. To use Table 9.2, round the value of W_B to the nearest entry in the table to determine the other dimensions. Interpolation is not necessary.

In calculating the energy and the Froude number, the equivalent depth of flow, $y_e = (A/2)^{1/2}$, entering the dissipator from a pipe or irregular-shaped conduit must be computed. In other words, the cross section flow area in the pipe is converted into an equivalent rectangular cross section in which the width is twice the depth of flow. The conduit preceding the dissipator can be open, closed, or of any cross section.

The effectiveness of the basin is best illustrated by comparing the energy losses within the structure to those in a natural hydraulic jump, Figure 9.15. The energy loss was computed based on depth and velocity measurements made in the approach pipe and also in the downstream channel with no tailwater. Compared with the natural hydraulic jump, the USBR Type VI impact basin shows a greater capacity for dissipating energy.

Job No. 25211509.03

Job: Ottumwa Midland Landfill Expansion

By: BJM

Date: 10/11/13

Client: Interstate Power and Light

Subject: Riprap Sizing at Dissipators

Chk'd: JMO

Date: 10/25/2013

Purpose:

To size the riprap at the outfall of the energy dissipators.

Approach:

Determine the exit velocity from the dissipator as described in Section 9.4 (USBR Type VI Impact Basin) in the "Hydraulic Design of Energy Dissipators for Culverts and Channels", Hydraulic Engineering Circular Number 14, Third Edition, Federal Highway Administration (HEC 14, FHA). The method uses an energy balance between the culvert exit and basin exit using the following equation:

$$H_b = Q/(W_b V_b) + V_b^2/(2g) = H_o(1 - H_L/H_o)$$

where: H_b = Energy at end of basin

Q = Flow rate

W_b = Width of basin

V_b = Exit velocity from basin

g = Gravitational acceleration constant

H_o = Energy at end of pipe

H_L = Total head loss

Using the equation, determine the exit velocity by trial and error. The equation yields 3 solutions, two positive and one negative. The negative solution is discarded, and the two positive results yield a subcritical and supercritical solution. Where low or no tailwater exists, the supercritical solution is used.

Once the exit velocity has been determined, use the method described in Section 10.3 (Riprap Aprons After Energy Dissipators) from the HEC 14 FHA reference to size the riprap downstream of the energy dissipator.

$$D_{50} = (0.692/S-1)(V^2/2g)$$

where: D_{50} = Median rock size

V = Exit velocity from dissipator

g = Gravitational acceleration constant

S = Riprap specific gravity

Assumptions:

The energy dissipator sizes and culvert discharge velocity into the dissipators is as presented in the Downslope Flume and Energy Dissipator Sizing section of this appendix.

The riprap specific gravity is 2.65, based on a typical value as presented in HEC 14, FHA.

Results:

Below is a summary of the D_{50} for riprap at the end of each dissipator. Refer to Sheet 9 for detailed calculations.

	Flume 1	Flumes 2, 3, 4, 5, 6
D50 (inches)	12	18

Calculations:

Value	Units	Flume 1	Flumes 2, 3, 4, 5, 6	Comment
Calculate Exit Velocity				
Q	cfs	9	36	direct input from Downslope Flume and Energy Dissipator Sizing
W_B	ft	4	6	direct input from Downslope Flume and Energy Dissipator Sizing
V_B (supercritical)	fps	12.30	15.07	vary this number to achieve H_B below; one positive solution to equation (supercritical)
V_B (subcritical)	fps	0.90	1.55	vary this number to achieve H_B below; second positive solution to equation (subcritical)
g	ft/sec ²	32.2	32.2	direct input
Fr	--	7.4	8.4	direct input from Downslope Flume and Energy Dissipator Sizing
H_L/H_O	ft/ft	0.78	0.84	direct input from Figure 9.15 from HEC 14, FHA (see Sheet 10)
H_O	ft	11.5	24.5	direct input from Downslope Flume and Energy Dissipator Sizing
H_B (supercritical)	ft	2.53	3.92	computed from $Q/(W_B V_B) + V_B^2/(2g)$ equation, varying V_B above to equal below computed H_B
H_B (subcritical)	ft	2.53	3.92	computed from $Q/(W_B V_B) + V_B^2/(2g)$ equation, varying V_B above to equal below computed H_B
H_B	ft	2.53	3.92	computed from $H_O(1-H_L/H_O)$ equation
V_O	fps	27	39	direct input from Downslope Flume and Energy Dissipator Sizing
V_B (supercritical)	fps	12.3	15.1	as determined above, assume supercritical, no tailwater
Reduction in velocity	percent	54%	61%	$(V_O - V_B)/V_O \times 100\%$
Calculate Riprap Size				
S		2.65	2.65	direct input
V	fps	12.3	15.07	from above calculations, supercritical
g	ft/sec ²	32.2	32.2	direct input
D_{50}	ft	1.0	1.5	computed
D_{50}	in	12	18	computed
Calculate Riprap Apron Dimensions				
D	ft	0.18	0.40	depth of water exiting flume
L	ft	15	25	length of riprap apron, from SUDAS Design Manual Figure 7E-10.03
B_1	ft	6.2	9.3	width of apron at flume
B_2	ft	19	31	computed

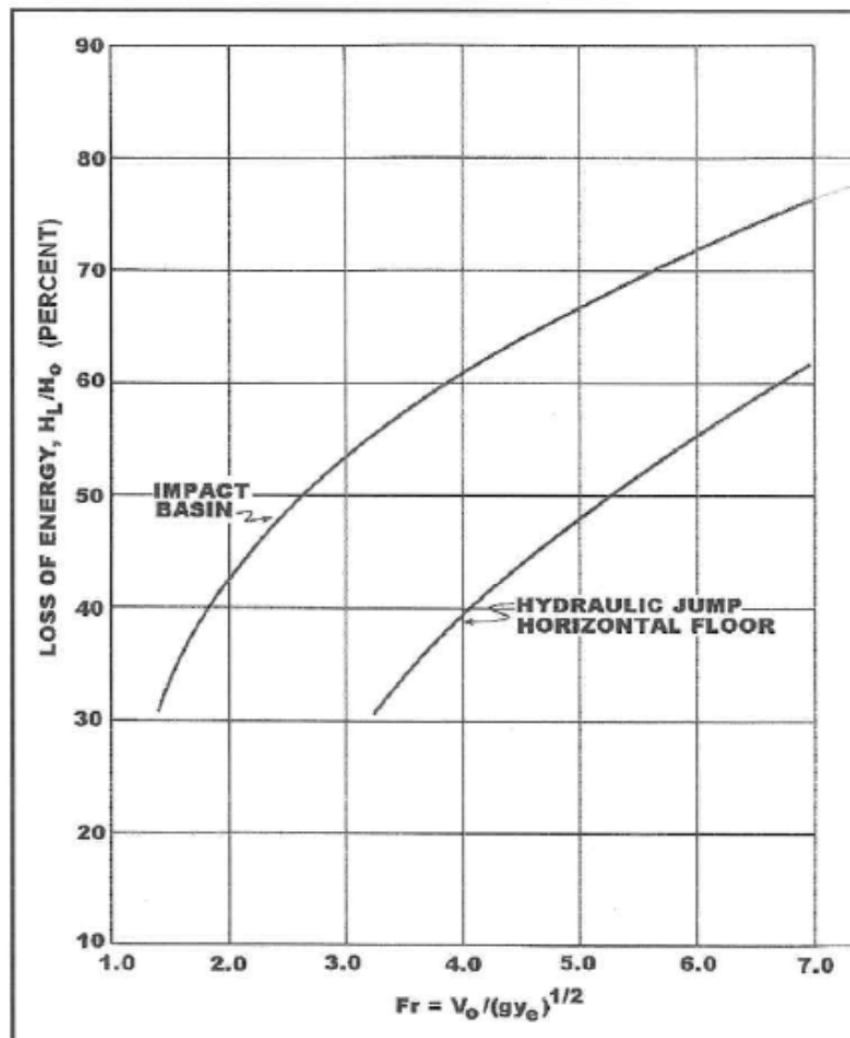


Figure 9.15. Energy Loss of USBR Type VI Impact Basin versus Hydraulic Jump

Source: HEC 14, FHA

Culvert Sizing

Culvert Sizing Flow Summary

This summary sheet provides design flows from the contributing drainage areas to each culvert for the 25-year, 24-hour storm event.

Culvert Flows

Culvert	HydroCAD Node	Flow Rate (cfs)	Culvert Diameter (ft)
1-1 & 1-2 (To Sed Basin 2)	112L	62.71	2 - 30" Barrels
2-1 & 2-2 (To Sed Basin 3)	114L	87.98	2 - 30" Barrels
3-1 & 3-2 (Across LF Perimeter Rd)	108L	87.60	2 - 36" Barrels
4-1 & 4-2 (To Sed Basin 4)	115L	100.36	2 - 36" Barrels
5-1 (Ph 1 Access Rd)	113S	3.05	1 - 12" Barrel
11-1 (Ph 5 Access Rd)	117S	7.80	1 - 18" Barrel
12-1 (Across LF Perimeter Rd)	116S	12.23	1 - 18" Barrel
14-1 & 14-2 (Across Haul Rd)	See Haul Road Culvert section of this appendix		2 - 48" Barrel
15-1 (Ph 3 Access Rd)	118S	3.03	1 - 12" Barrel

Purpose:

To size riprap aprons at the outlet of culverts.

Approach:

Size riprap D50 and size riprap apron dimensions using the Iowa Statewide Urban Design and Specifications (SUDAS) Design Manual, Chapter 7E-10 - Riprap.

Source: USDA NRCS, 2004

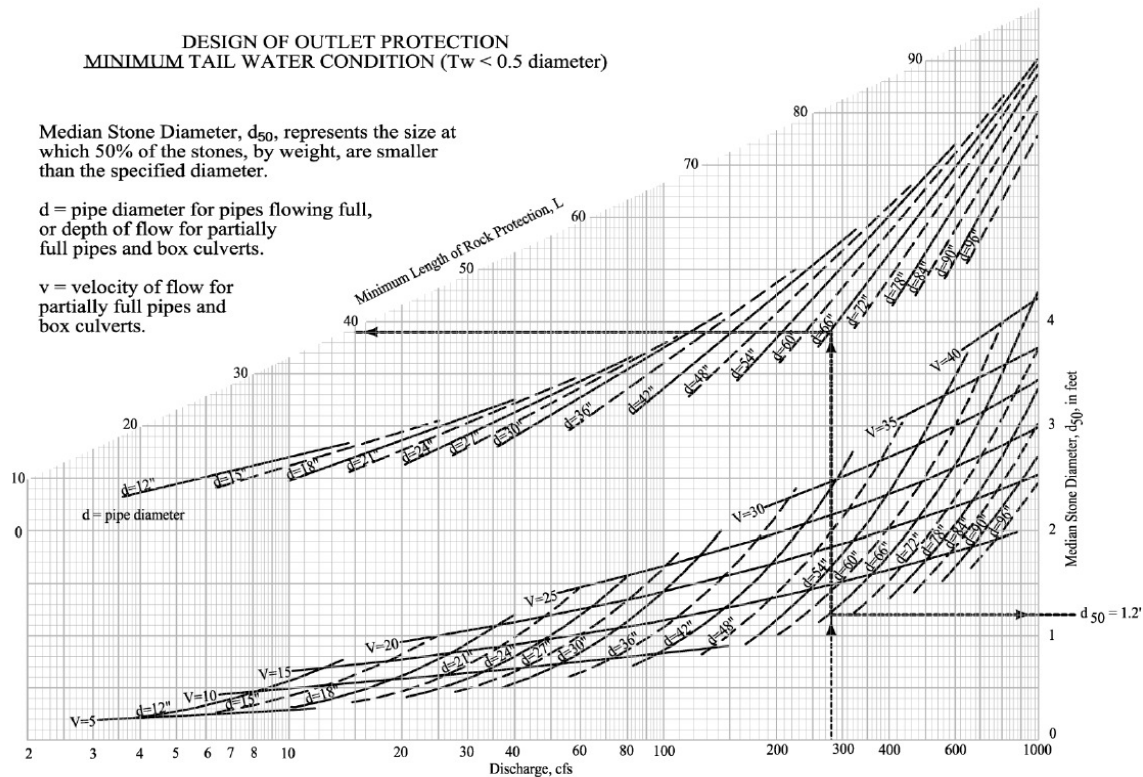


Figure 7E-10.03: Design of Outlet Protection, Minimum Tailwater Condition

Assumptions:

The riprap specific gravity is 2.65, based on a typical value as presented in SUDAS Chapter 7E-10.

Results:

The following sheets show the design D50 and apron dimensions for riprap at the end of each culvert outlet.

I:\25211509\Reports\Permit Amendment\Appendices\Storm Water Management\Calcs - final\[Culvert Outlet Riprap Sizing Calc_131127.xls]Culvert Summary

Calculations:**Riprap D50 Sizing**

<u>Culvert Outlet</u>	<u>Design Q (cfs)</u>	<u>Culvert Diameter (ft)</u>	<u>Design D50 (ft)</u>	<u>Design Stone</u>
1-1 & 1-2	31.36 ea.	2.5	1.0	Iowa DOT Section 4130.02 Class E Revetment
2-1 & 2-2	43.99 ea.	2.5	1.5	Iowa DOT Section 4130.02 Class B Revetment
3-1 & 3-2	43.80 ea.	3.0	1.0	Iowa DOT Section 4130.02 Class E Revetment
4-1 & 4-2	50.18 ea.	3.0	1.0	Iowa DOT Section 4130.02 Class E Revetment
Sed Basin 2 Outlet	9.88	2.0	0.5	Iowa DOT Section 4130.04 Erosion Stone
Sed Basin 3 Outlet	4.73	2.0	0.5	Iowa DOT Section 4130.04 Erosion Stone
Sed Basin 4 Outlet	12.72	1.5	1.0	Iowa DOT Section 4130.02 Class E Revetment

*No riprap anticipated at culverts 5, 11, 12, & 15.

**Refer to Wetland and Stream Mitigation Plan for Culvert 14-1 & 14-2 outlet protection.

Calculations:

Riprap Apron Dimension Sizing

<u>Culvert Outlet</u>	<u>Culvert Diameter (ft)</u>	<u>D50 (ft)</u>	<u>Apron Width @ Culvert (ft)</u>	<u>Apron Length (ft)</u>	<u>Apron Width @ End (ft)</u>	<u>Apron Depth (ft)</u>
1-1 & 1-2	2.5	1.0	17.1	23.0	26.0	2.1
2-1 & 2-2	2.5	1.5	14.9	23.0	26.0	3.0
3-1 & 3-2	3.0	1.0	17.1	28.0	31.0	2.1
4-1 & 4-2	3.0	1.0	17.1	28.0	31.0	2.1
Sed Basin 2 Outlet	2.0	.5	6.0	15.0	17.0	1.2
Sed Basin 3 Outlet	2.0	.5	6.0	10.0	12.0	1.2
Sed Basin 4 Outlet	1.5	1.0	4.5	20.0	22.0	2.1

*No riprap anticipated at culverts 5, 11, 12, & 15.

**Refer to Wetland and Stream Mitigation Plan for Culvert 14-1 & 14-2 outlet protection.

HY-8 Culvert Analysis Report (Culverts 1-1 & 1-2)

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 0 cfs

Design Flow: 62.71 cfs

Maximum Flow: 62.71 cfs

Table 1 - Summary of Culvert Flows at Crossing: To Sed Basin 2 (Culverts 1-1 & 1-2)

Headwater Elevation (ft)	Total Discharge (cfs)	Sed Basin 2 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
768.20	0.00	0.00	0.00	1
769.08	6.27	6.27	0.00	1
769.47	12.54	12.54	0.00	1
769.78	18.81	18.81	0.00	1
770.04	25.08	25.08	0.00	1
770.29	31.36	31.36	0.00	1
770.54	37.63	37.63	0.00	1
770.82	43.90	43.90	0.00	1
771.13	50.17	50.17	0.00	1
771.48	56.44	56.44	0.00	1
771.87	62.71	62.71	0.00	1
772.50	71.47	71.47	0.00	Overtopping

Tailwater Channel Data - To Sed Basin 2 (Culverts 1-1 & 1-2)

Tailwater Channel Option: Enter Constant Tailwater Elevation

Constant Tailwater Elevation: 757.00 ft

Roadway Data for Crossing: To Sed Basin 2 (Culverts 1-1 & 1-2)

Roadway Profile Shape: Constant Roadway Elevation

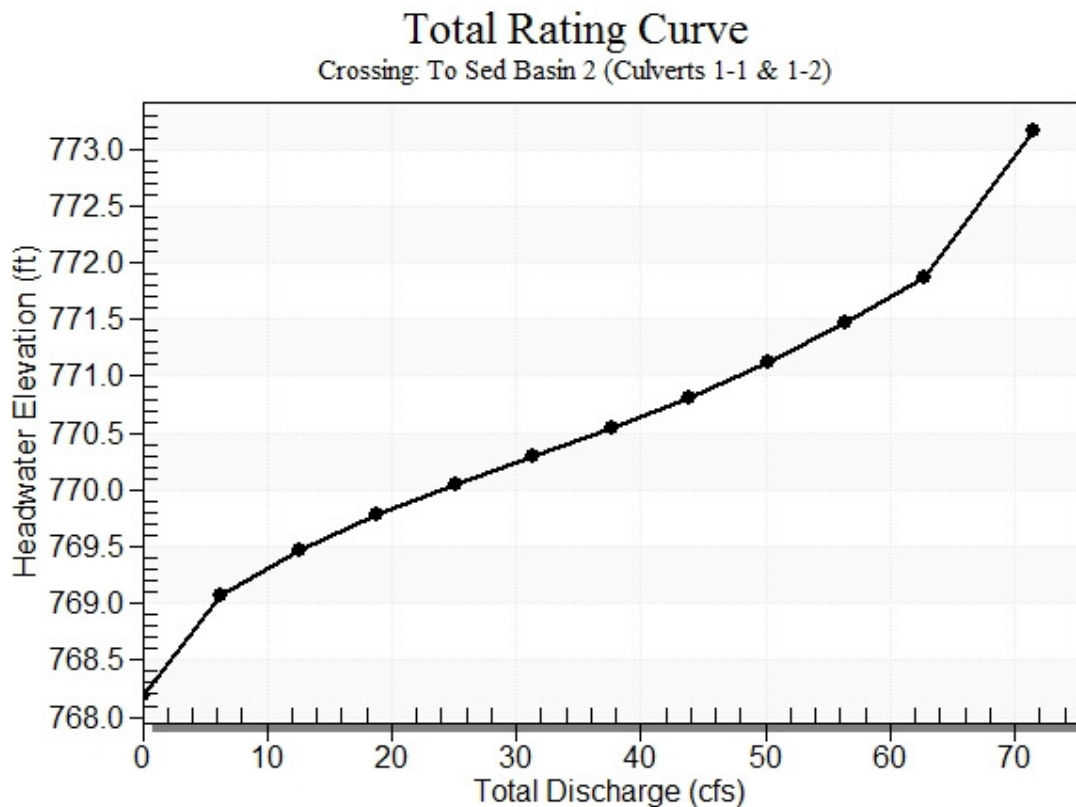
Crest Length: 100.00 ft

Crest Elevation: 772.50 ft

Roadway Surface: Gravel

Roadway Top Width: 18.00 ft

Rating Curve Plot for Crossing: To Sed Basin 2 (Culverts 1-1 & 1-2)



Site Data - Sed Basin 2

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft

Inlet Elevation: 768.20 ft

Outlet Station: 156.00 ft

Outlet Elevation: 760.00 ft

Number of Barrels: 2

Culvert Data Summary - Sed Basin 2

Barrel Shape: Circular

Barrel Diameter: 2.50 ft

Barrel Material: Smooth HDPE

Embedment: 0.00 in

Barrel Manning's n: 0.0120

Culvert Type: Straight

Inlet Configuration: Mitered to Conform to Slope

Inlet Depression: NONE

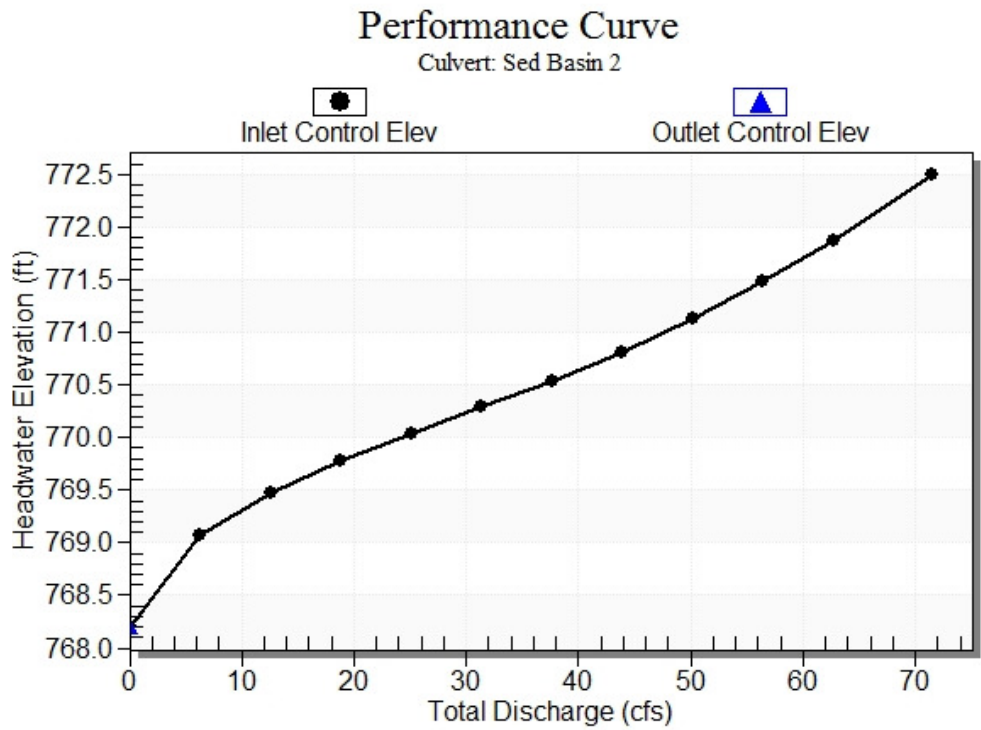
Table 2 - Culvert Summary Table: Sed Basin 2

Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
0.00	0.00	768.20	0.000	0.000	0-NF	0.000	0.000	0.000	3.000	0.000	0.000
6.27	6.27	769.08	0.876	0.0*	1-S2n	0.284	0.577	0.284	3.000	9.860	0.000
12.54	12.54	769.47	1.271	0.0*	1-S2n	0.410	0.826	0.410	3.000	11.740	0.000
18.81	18.81	769.78	1.579	0.0*	1-S2n	0.505	1.020	0.505	3.000	13.164	0.000
25.08	25.08	770.04	1.841	0.0*	1-S2n	0.582	1.189	0.582	3.000	14.321	0.000
31.36	31.36	770.29	2.088	0.0*	1-S2n	0.659	1.334	0.659	3.000	15.119	0.000
37.63	37.63	770.54	2.340	0.0*	1-S2n	0.723	1.466	0.749	3.000	15.155	0.000
43.90	43.90	770.82	2.616	0.0*	5-S2n	0.781	1.590	0.805	3.000	16.022	0.000
50.17	50.17	771.13	2.926	0.0*	5-S2n	0.839	1.702	0.866	3.000	16.587	0.000
56.44	56.44	771.48	3.278	0.0*	5-S2n	0.898	1.809	0.926	3.000	17.077	0.000
62.71	62.71	771.87	3.674	0.0*	5-S2n	0.949	1.905	0.987	3.000	17.381	0.000

* Full Flow Headwater elevation is below inlet invert.

Straight Culvert
Inlet Elevation (invert): 768.20 ft, Outlet Elevation (invert): 760.00 ft
Culvert Length: 156.22 ft, Culvert Slope: 0.0526

Culvert Performance Curve Plot: Sed Basin 2



Water Surface Profile Plot for Culvert: Sed Basin 2

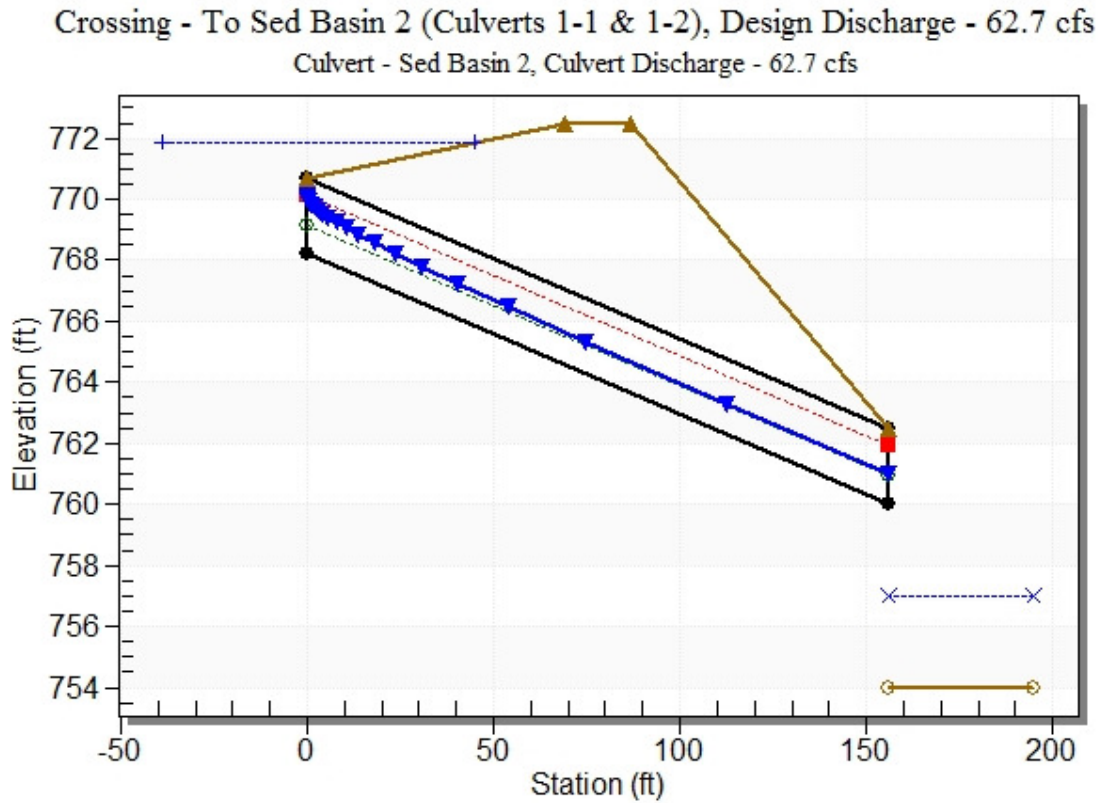


Table 3 - Downstream Channel Rating Curve (Crossing: To Sed Basin 2 (Culverts 1-1 & 1-2))

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
0.00	757.00	3.00
6.27	757.00	3.00
12.54	757.00	3.00
18.81	757.00	3.00
25.08	757.00	3.00
31.36	757.00	3.00
37.63	757.00	3.00
43.90	757.00	3.00
50.17	757.00	3.00
56.44	757.00	3.00
62.71	757.00	3.00

HY-8 Culvert Analysis Report (Culverts 2-1 & 2-2)

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 0 cfs

Design Flow: 87.98 cfs

Maximum Flow: 87.98 cfs

Table 1 - Summary of Culvert Flows at Crossing: To Sed Basin 3 (Culverts 2-1 & 2-2)

Headwater Elevation (ft)	Total Discharge (cfs)	Sed Basin 3 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
772.20	0.00	0.00	0.00	1
773.06	8.80	8.80	0.00	1
773.44	17.60	17.60	0.00	1
773.84	26.39	26.39	0.00	1
774.19	35.19	35.19	0.00	1
774.52	43.99	43.99	0.00	1
774.88	52.79	52.79	0.00	1
775.29	61.59	61.59	0.00	1
775.75	70.38	70.38	0.00	1
776.28	79.18	79.18	0.00	1
776.89	87.98	87.98	0.00	1
778.00	102.09	102.09	0.00	Overtopping

Tailwater Channel Data - To Sed Basin 3 (Culverts 2-1 & 2-2)

Tailwater Channel Option: Enter Constant Tailwater Elevation

Constant Tailwater Elevation: 755.00 ft

Roadway Data for Crossing: To Sed Basin 3 (Culverts 2-1 & 2-2)

Roadway Profile Shape: Constant Roadway Elevation

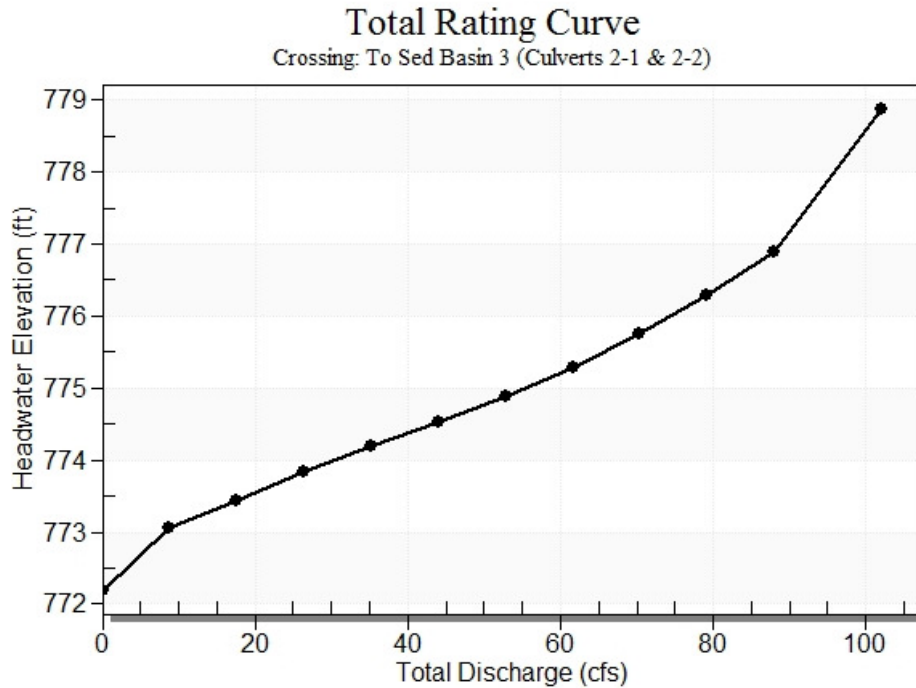
Crest Length: 100.00 ft

Crest Elevation: 778.00 ft

Roadway Surface: Gravel

Roadway Top Width: 18.00 ft

Rating Curve Plot for Crossing: To Sed Basin 3 (Culverts 2-1 & 2-2)



Site Data - Sed Basin 3

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft

Inlet Elevation: 772.20 ft

Outlet Station: 113.00 ft

Outlet Elevation: 758.00 ft

Number of Barrels: 2

Culvert Data Summary - Sed Basin 3

Barrel Shape: Circular

Barrel Diameter: 2.50 ft

Barrel Material: Smooth HDPE

Embedment: 0.00 in

Barrel Manning's n: 0.0120

Culvert Type: Straight

Inlet Configuration: Square Edge with Headwall

Inlet Depression: NONE

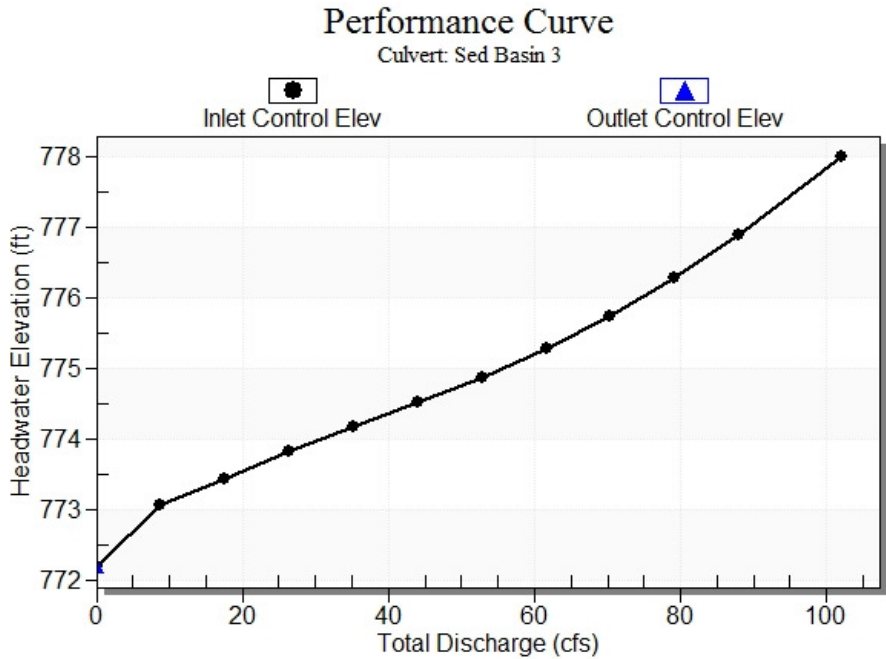
Table 2 - Culvert Summary Table: Sed Basin 3

Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
0.00	0.00	772.20	0.000	0.000	0-NF	0.000	0.000	0.000	3.000	0.000	0.000
8.80	8.80	773.06	0.860	0.0*	1-S2n	0.272	0.685	0.283	3.000	13.901	0.000
17.60	17.60	773.44	1.242	0.0*	1-S2n	0.387	0.983	0.425	3.000	15.747	0.000
26.39	26.39	773.84	1.638	0.0*	1-S2n	0.483	1.221	0.514	3.000	17.986	0.000
35.19	35.19	774.19	1.986	0.0*	1-S2n	0.553	1.417	0.575	3.000	20.406	0.000
43.99	43.99	774.52	2.323	0.0*	1-S2n	0.623	1.592	0.649	3.000	21.649	0.000
52.79	52.79	774.88	2.683	0.0*	5-S2n	0.691	1.746	0.726	3.000	22.445	0.000
61.59	61.59	775.29	3.087	0.0*	5-S2n	0.743	1.889	0.786	3.000	23.195	0.000
70.38	70.38	775.75	3.551	0.0*	5-S2n	0.796	2.012	0.851	3.000	23.796	0.000
79.18	79.18	776.28	4.083	0.0*	5-S2n	0.849	2.119	0.911	3.000	24.496	0.000
87.98	87.98	776.89	4.686	0.0*	5-S2n	0.902	2.208	0.967	3.000	25.069	0.000

* Full Flow Headwater elevation is below inlet invert.

Straight Culvert
Inlet Elevation (invert): 772.20 ft, Outlet Elevation (invert): 758.00 ft
Culvert Length: 113.89 ft, Culvert Slope: 0.1257

Culvert Performance Curve Plot: Sed Basin 3



Water Surface Profile Plot for Culvert: Sed Basin 3

Crossing - To Sed Basin 3 (Culverts 2-1 & 2-2), Design Discharge - 88.0 cfs
Culvert - Sed Basin 3, Culvert Discharge - 88.0 cfs

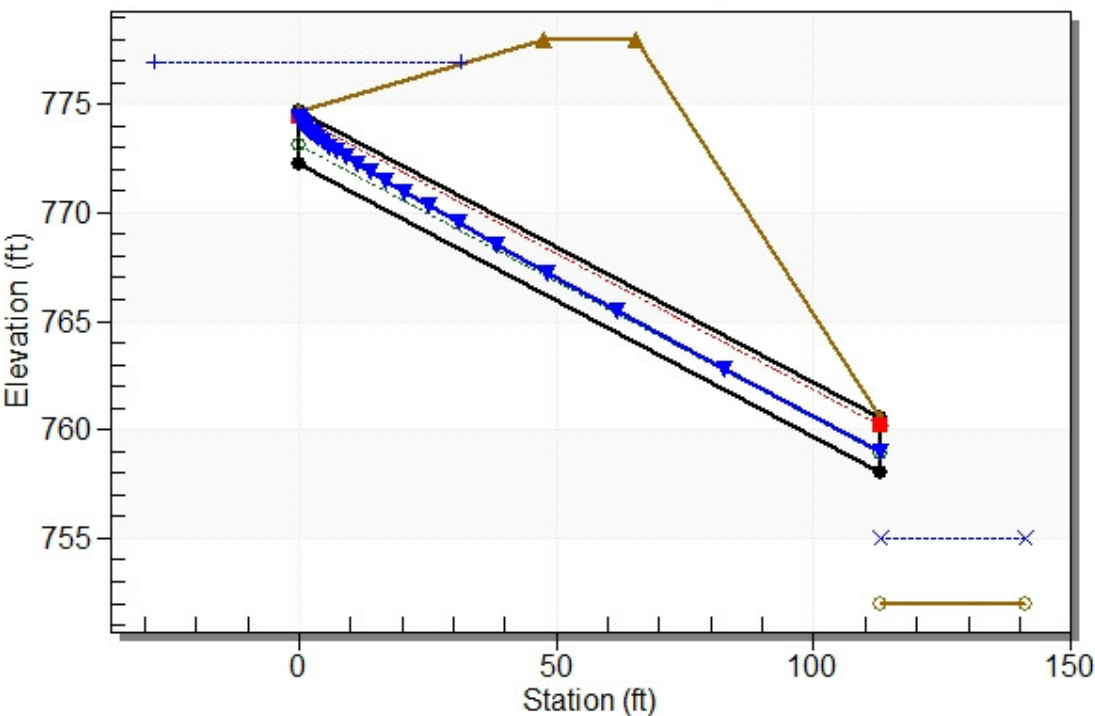


Table 3 - Downstream Channel Rating Curve (Crossing: To Sed Basin 3 (Culverts 2-1 & 2-2))

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
0.00	755.00	3.00
8.80	755.00	3.00
17.60	755.00	3.00
26.39	755.00	3.00
35.19	755.00	3.00
43.99	755.00	3.00
52.79	755.00	3.00
61.59	755.00	3.00
70.38	755.00	3.00
79.18	755.00	3.00
87.98	755.00	3.00

HY-8 Culvert Analysis Report (Culverts 3-1 & 3-2)

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 0 cfs

Design Flow: 87.6 cfs

Maximum Flow: 87.6 cfs

Table 1 - Summary of Culvert Flows at Crossing: Across South Road (Culvert 3-1 & 3-2)

Headwater Elevation (ft)	Total Discharge (cfs)	Across South Road Discharge (cfs)	Roadway Discharge (cfs)	Iterations
795.70	0.00	0.00	0.00	1
796.57	8.76	8.76	0.00	1
796.96	17.52	17.52	0.00	1
797.28	26.28	26.28	0.00	1
797.60	35.04	35.04	0.00	1
797.88	43.80	43.80	0.00	1
798.14	52.56	52.56	0.00	1
798.40	61.32	61.32	0.00	1
798.65	70.08	70.08	0.00	1
798.92	78.84	78.84	0.00	1
799.21	87.60	87.60	0.00	1
800.00	108.50	108.50	0.00	Overtopping

Tailwater Channel Data - Across South Road (Culvert 3-1 & 3-2)

Tailwater Channel Option: Enter Constant Tailwater Elevation

Constant Tailwater Elevation: 779.00 ft

Roadway Data for Crossing: Across South Road (Culvert 3-1 & 3-2)

Roadway Profile Shape: Constant Roadway Elevation

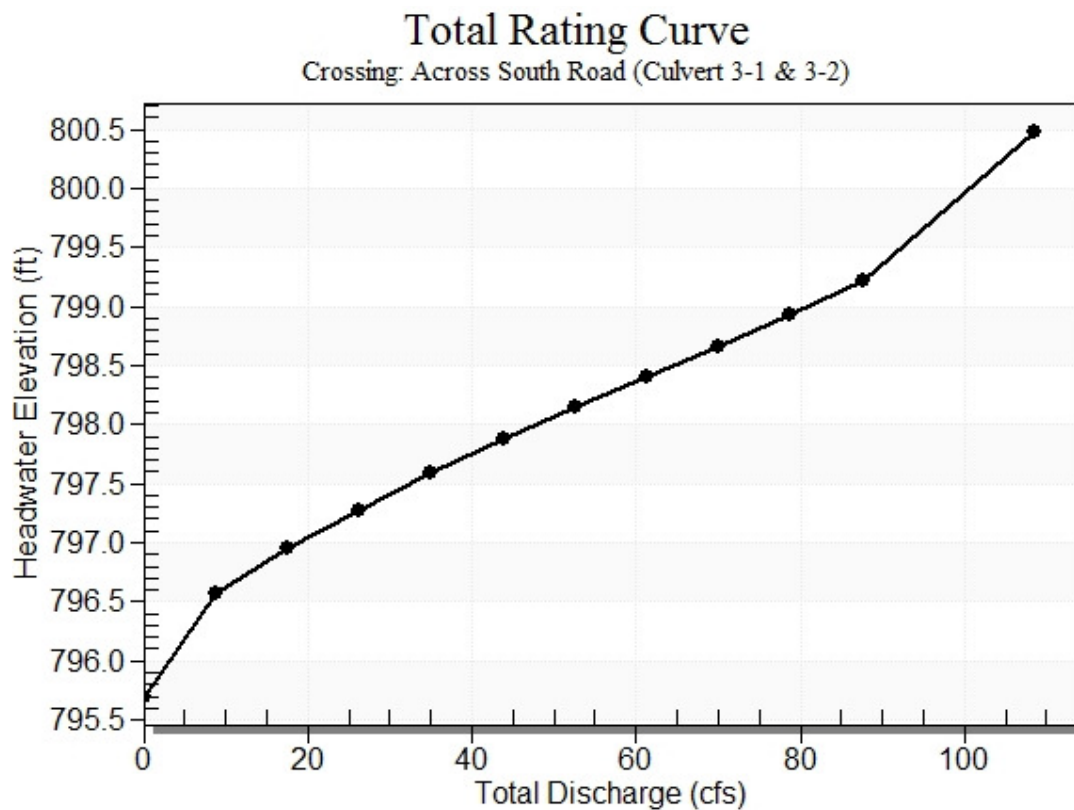
Crest Length: 333.00 ft

Crest Elevation: 800.00 ft

Roadway Surface: Gravel

Roadway Top Width: 18.00 ft

Rating Curve Plot for Crossing: Across South Road (Culvert 3-1 & 3-2)



Site Data - Across South Road

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft

Inlet Elevation: 795.70 ft

Outlet Station: 60.00 ft

Outlet Elevation: 794.00 ft

Number of Barrels: 2

Culvert Data Summary - Across South Road

Barrel Shape: Circular

Barrel Diameter: 3.00 ft

Barrel Material: Smooth HDPE

Embedment: 0.00 in

Barrel Manning's n: 0.0120

Culvert Type: Straight

Inlet Configuration: Square Edge with Headwall

Inlet Depression: NONE

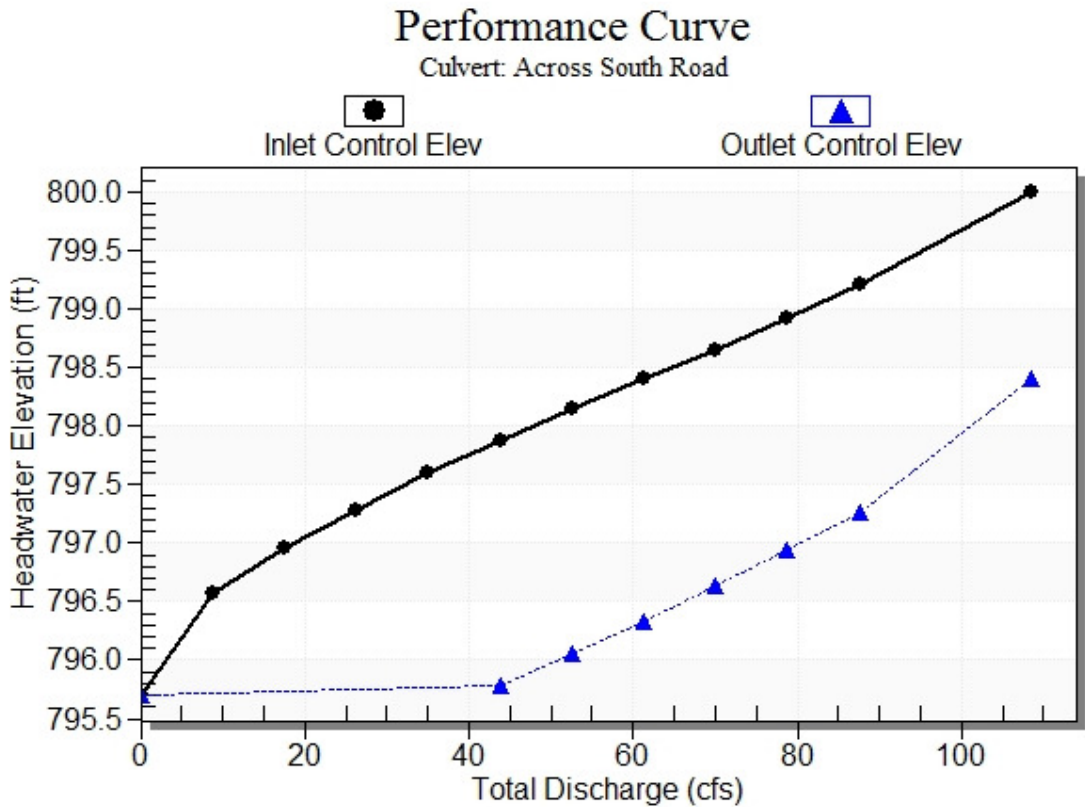
Table 2 - Culvert Summary Table: Across South Road

Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
0.00	0.00	795.70	0.000	0.000	0-NF	0.000	0.000	0.000	3.000	0.000	0.000
8.76	8.76	796.57	0.870	0.0*	1-S2n	0.366	0.650	0.398	3.000	7.608	0.000
17.52	17.52	796.96	1.255	0.0*	1-S2n	0.544	0.930	0.568	3.000	9.490	0.000
26.28	26.28	797.28	1.577	0.0*	1-S2n	0.653	1.149	0.711	3.000	10.155	0.000
35.04	35.04	797.60	1.896	0.0*	1-S2n	0.761	1.339	0.835	3.000	10.923	0.000
43.80	43.80	797.88	2.180	0.083	1-S2n	0.857	1.505	0.949	3.000	11.361	0.000
52.56	52.56	798.14	2.443	0.351	1-S2n	0.939	1.650	1.055	3.000	11.827	0.000
61.32	61.32	798.40	2.697	0.635	1-S2n	1.021	1.789	1.158	3.000	12.173	0.000
70.08	70.08	798.65	2.954	0.933	1-S2n	1.101	1.920	1.254	3.000	12.506	0.000
78.84	78.84	798.92	3.223	1.240	5-S2n	1.170	2.038	1.345	3.000	12.843	0.000
87.60	87.60	799.21	3.510	1.567	5-S2n	1.239	2.153	1.435	3.000	13.116	0.000

* Full Flow Headwater elevation is below inlet invert.

Straight Culvert
Inlet Elevation (invert): 795.70 ft, Outlet Elevation (invert): 794.00 ft
Culvert Length: 60.02 ft, Culvert Slope: 0.0283

Culvert Performance Curve Plot: Across South Road



Water Surface Profile Plot for Culvert: Across South Road

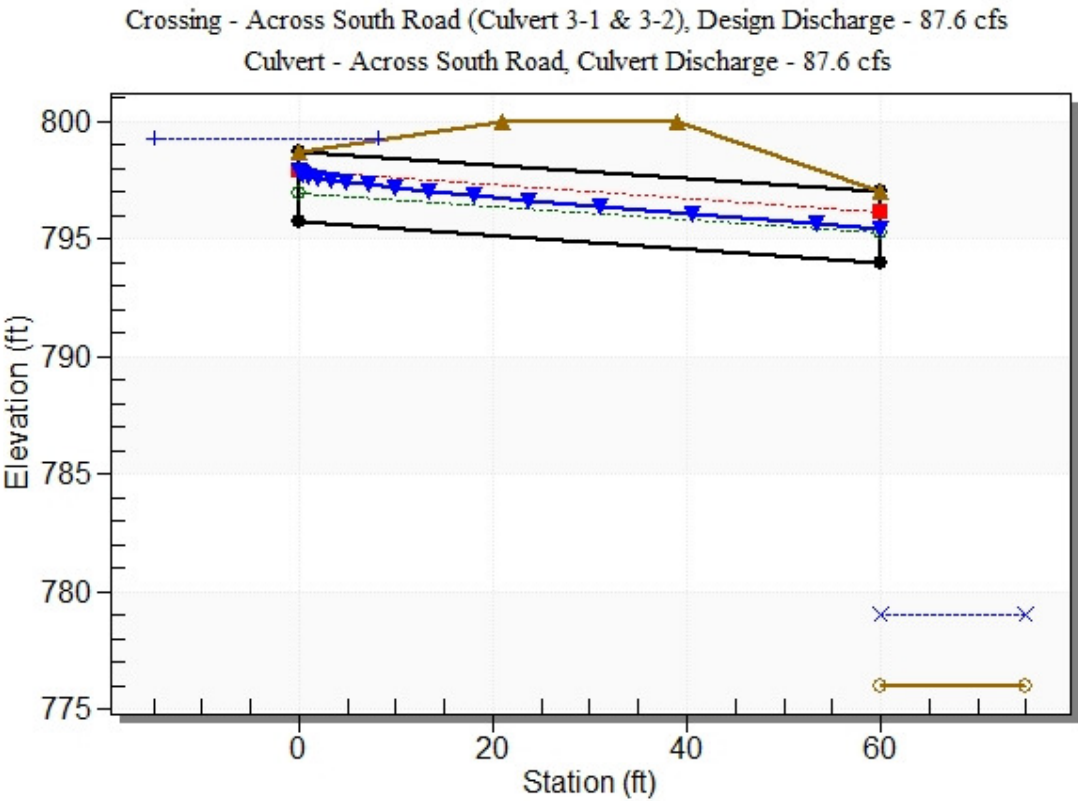


Table 3 - Downstream Channel Rating Curve (Crossing: Across South Road (Culvert 3-1 & 3-2))

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
0.00	779.00	3.00
8.76	779.00	3.00
17.52	779.00	3.00
26.28	779.00	3.00
35.04	779.00	3.00
43.80	779.00	3.00
52.56	779.00	3.00
61.32	779.00	3.00
70.08	779.00	3.00
78.84	779.00	3.00
87.60	779.00	3.00

HY-8 Culvert Analysis Report (Culverts 4-1 & 4-2)

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 0 cfs

Design Flow: 100.36 cfs

Maximum Flow: 100.36 cfs

Table 1 - Summary of Culvert Flows at Crossing: To Sed Basin 4 (Culvert 4-1 & 4-2)

Headwater Elevation (ft)	Total Discharge (cfs)	To Sed Basin 4 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
776.00	0.00	0.00	0.00	1
776.93	10.04	10.04	0.00	1
777.34	20.07	20.07	0.00	1
777.71	30.11	30.11	0.00	1
778.05	40.14	40.14	0.00	1
778.36	50.18	50.18	0.00	1
778.65	60.22	60.22	0.00	1
778.95	70.25	70.25	0.00	1
779.26	80.29	80.29	0.00	1
779.59	90.32	90.32	0.00	1
779.96	100.36	100.36	0.00	1
782.00	143.10	143.10	0.00	Overtopping

Tailwater Channel Data - To Sed Basin 4 (Culvert 4-1 & 4-2)

Tailwater Channel Option: Enter Constant Tailwater Elevation

Constant Tailwater Elevation: 753.00 ft

Roadway Data for Crossing: To Sed Basin 4 (Culvert 4-1 & 4-2)

Roadway Profile Shape: Constant Roadway Elevation

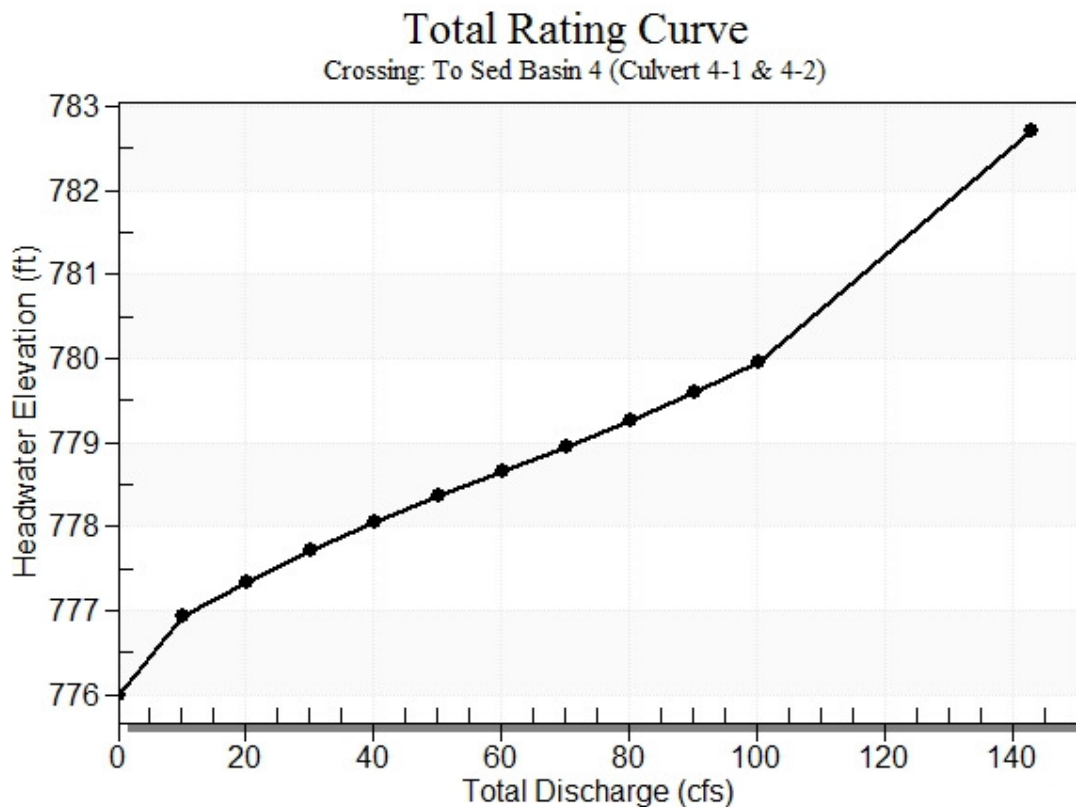
Crest Length: 333.00 ft

Crest Elevation: 782.00 ft

Roadway Surface: Gravel

Roadway Top Width: 18.00 ft

Rating Curve Plot for Crossing: To Sed Basin 4 (Culvert 4-1 & 4-2)



Site Data - To Sed Basin 4

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft

Inlet Elevation: 776.00 ft

Outlet Station: 110.00 ft

Outlet Elevation: 772.00 ft

Number of Barrels: 2

Culvert Data Summary - To Sed Basin 4

Barrel Shape: Circular

Barrel Diameter: 3.00 ft

Barrel Material: Smooth HDPE

Embedment: 0.00 in

Barrel Manning's n: 0.0120

Culvert Type: Straight

Inlet Configuration: Square Edge with Headwall

Inlet Depression: NONE

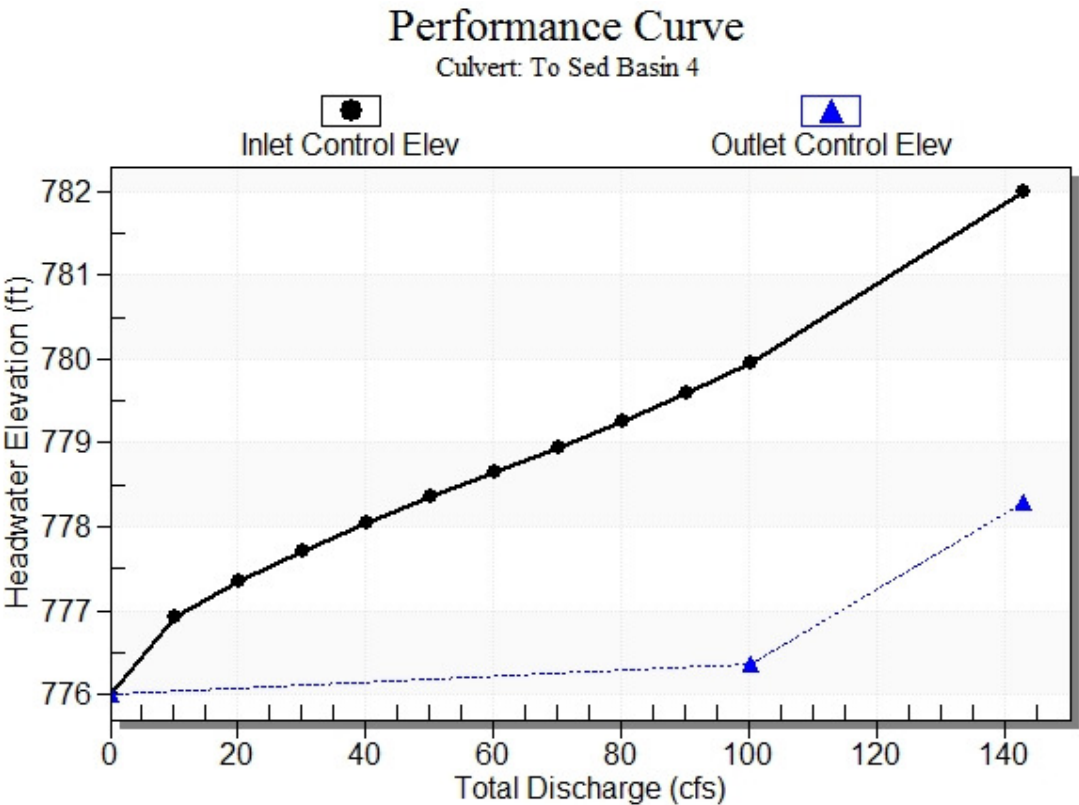
Table 2 - Culvert Summary Table: To Sed Basin 4

Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
0.00	0.00	776.00	0.000	0.000	0-NF	0.000	0.000	0.000	3.000	0.000	0.000
10.04	10.04	776.93	0.928	0.0*	1-S2n	0.368	0.698	0.368	3.000	9.744	0.000
20.07	20.07	777.34	1.341	0.0*	1-S2n	0.547	0.999	0.547	3.000	11.390	0.000
30.11	30.11	777.71	1.710	0.0*	1-S2n	0.657	1.233	0.657	3.000	13.016	0.000
40.14	40.14	778.05	2.053	0.0*	1-S2n	0.766	1.438	0.805	3.000	13.139	0.000
50.18	50.18	778.36	2.360	0.0*	1-S2n	0.862	1.612	0.909	3.000	13.817	0.000
60.22	60.22	778.65	2.653	0.0*	1-S2n	0.944	1.773	1.010	3.000	14.353	0.000
70.25	70.25	778.95	2.947	0.0*	1-S2n	1.027	1.922	1.104	3.000	14.889	0.000
80.29	80.29	779.26	3.257	0.0*	5-S2n	1.107	2.061	1.194	3.000	15.290	0.000
90.32	90.32	779.59	3.592	0.0*	5-S2n	1.177	2.187	1.279	3.000	15.696	0.000
100.36	100.36	779.96	3.960	0.353	5-S2n	1.247	2.302	1.363	3.000	16.056	0.000

* Full Flow Headwater elevation is below inlet invert.

Straight Culvert
Inlet Elevation (invert): 776.00 ft, Outlet Elevation (invert): 772.00 ft
Culvert Length: 110.07 ft, Culvert Slope: 0.0364

Culvert Performance Curve Plot: To Sed Basin 4



Water Surface Profile Plot for Culvert: To Sed Basin 4

Crossing - To Sed Basin 4 (Culvert 4-1 & 4-2), Design Discharge - 100.4 cfs
Culvert - To Sed Basin 4, Culvert Discharge - 100.4 cfs

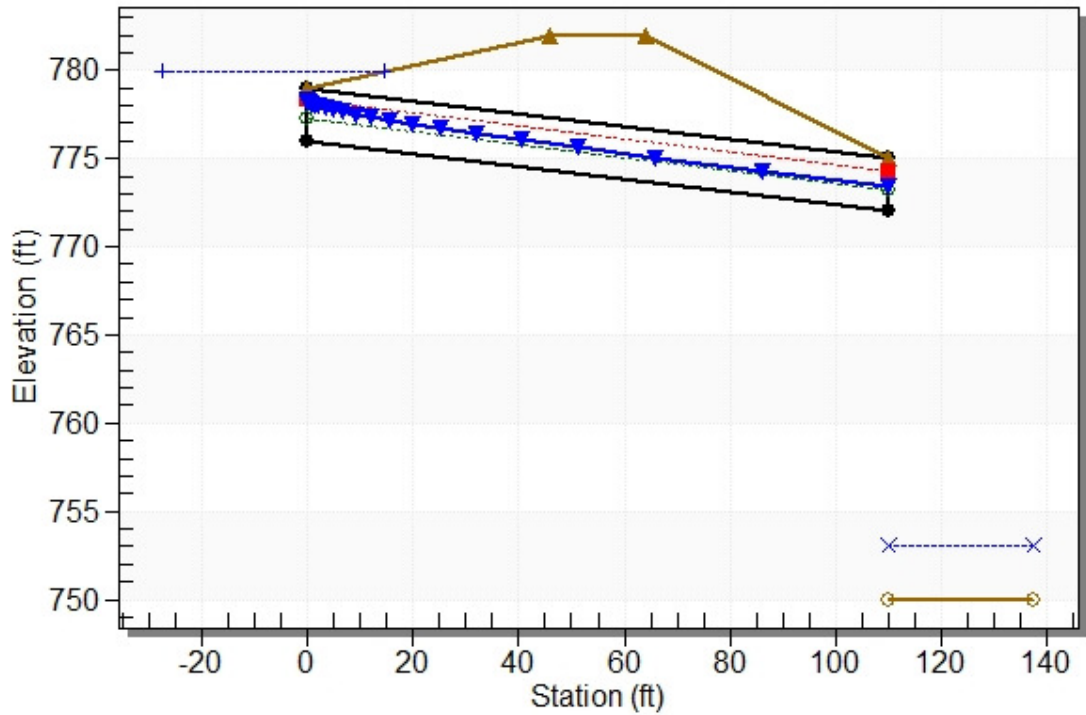


Table 3 - Downstream Channel Rating Curve (Crossing: To Sed Basin 4 (Culvert 4-1 & 4-2))

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
0.00	753.00	3.00
10.04	753.00	3.00
20.07	753.00	3.00
30.11	753.00	3.00
40.14	753.00	3.00
50.18	753.00	3.00
60.22	753.00	3.00
70.25	753.00	3.00
80.29	753.00	3.00
90.32	753.00	3.00
100.36	753.00	3.00

HY-8 Culvert Analysis Report (Culvert 5-1)

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 0 cfs

Design Flow: 3.05 cfs

Maximum Flow: 3.05 cfs

Table 1 - Summary of Culvert Flows at Crossing: 5-1 (Ph 1 Access Rd)

Headwater Elevation (ft)	Total Discharge (cfs)	5-1 (Ph 1 Access Rd) Discharge (cfs)	Roadway Discharge (cfs)	Iterations
758.00	0.00	0.00	0.00	1
758.31	0.30	0.30	0.00	1
758.44	0.61	0.61	0.00	1
758.55	0.92	0.92	0.00	1
758.66	1.22	1.22	0.00	1
758.76	1.52	1.52	0.00	1
758.85	1.83	1.83	0.00	1
758.95	2.13	2.13	0.00	1
759.04	2.44	2.44	0.00	1
759.14	2.75	2.75	0.00	1
759.25	3.05	3.05	0.00	1
772.50	12.18	12.18	0.00	Overtopping

Tailwater Channel Data - 5-1 (Ph 1 Access Rd)

Tailwater Channel Option: Enter Constant Tailwater Elevation

Constant Tailwater Elevation: 749.00 ft

Roadway Data for Crossing: 5-1 (Ph 1 Access Rd)

Roadway Profile Shape: Constant Roadway Elevation

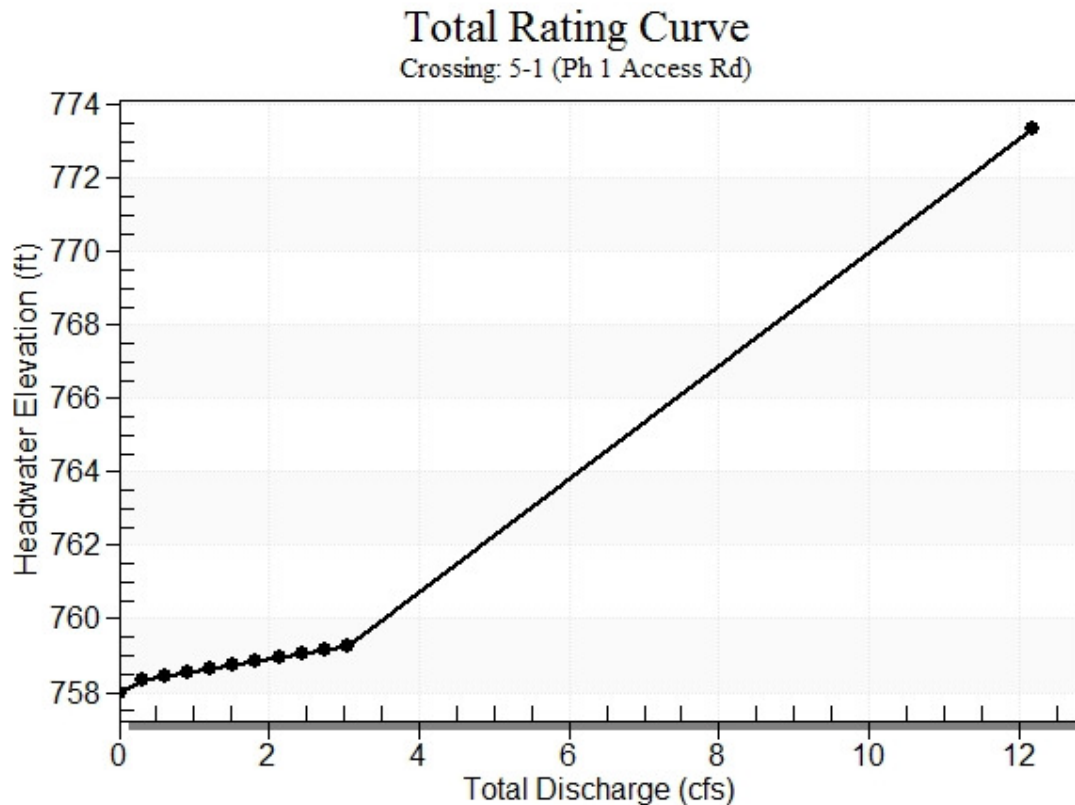
Crest Length: 100.00 ft

Crest Elevation: 772.50 ft

Roadway Surface: Gravel

Roadway Top Width: 20.00 ft

Rating Curve Plot for Crossing: 5-1 (Ph 1 Access Rd)



Site Data - 5-1 (Ph 1 Access Rd)

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft

Inlet Elevation: 758.00 ft

Outlet Station: 125.00 ft

Outlet Elevation: 753.50 ft

Number of Barrels: 1

Culvert Data Summary - 5-1 (Ph 1 Access Rd)

Barrel Shape: Circular

Barrel Diameter: 1.00 ft

Barrel Material: Smooth HDPE

Embedment: 0.00 in

Barrel Manning's n: 0.0120

Culvert Type: Straight

Inlet Configuration: Square Edge with Headwall

Inlet Depression: NONE

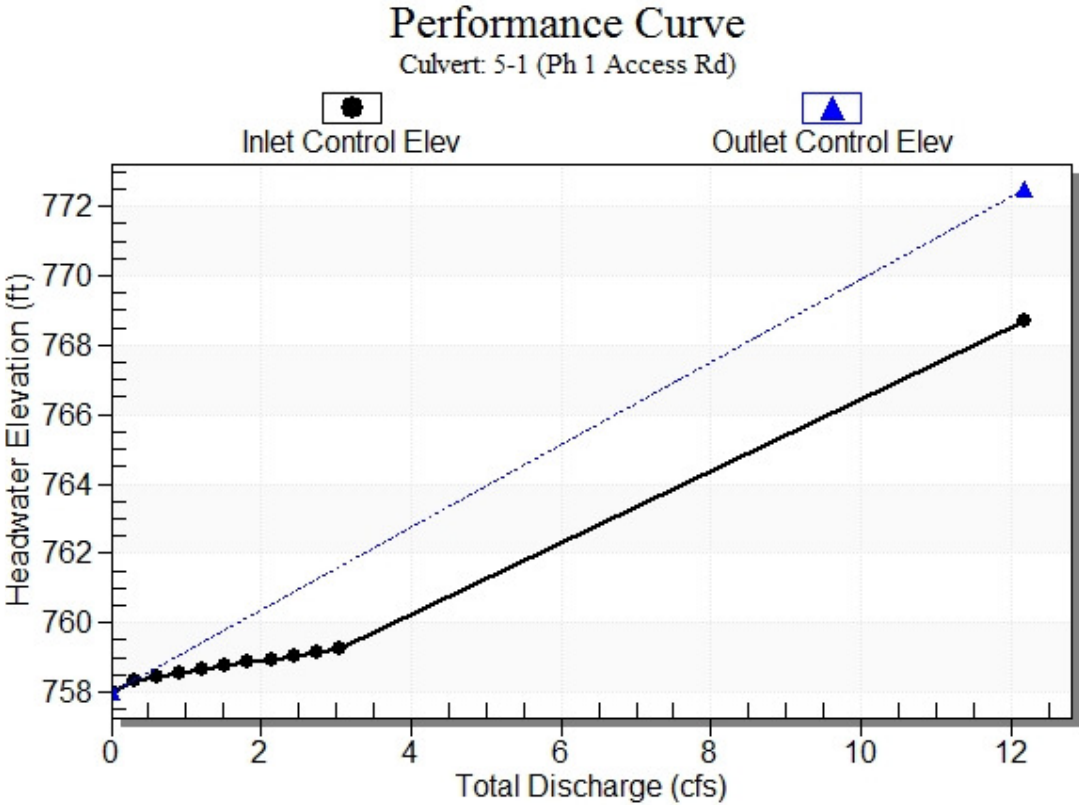
Table 2 - Culvert Summary Table: 5-1 (Ph 1 Access Rd)

Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
0.00	0.00	758.00	0.000	0.000	0-NF	0.000	0.000	0.000	1.000	0.000	0.000
0.30	0.30	758.31	0.309	0.0*	1-S2n	0.131	0.224	0.131	1.000	10.698	0.000
0.61	0.61	758.44	0.439	0.0*	1-S2n	0.193	0.322	0.193	1.000	5.806	0.000
0.92	0.92	758.55	0.551	0.0*	1-S2n	0.235	0.399	0.235	1.000	6.459	0.000
1.22	1.22	758.66	0.662	0.0*	1-S2n	0.275	0.466	0.275	1.000	6.939	0.000
1.52	1.52	758.76	0.761	0.0*	1-S2n	0.307	0.523	0.307	1.000	7.544	0.000
1.83	1.83	758.85	0.854	0.0*	1-S2n	0.339	0.573	0.339	1.000	7.797	0.000
2.13	2.13	758.95	0.946	0.0*	1-S2n	0.369	0.622	0.369	1.000	8.115	0.000
2.44	2.44	759.04	1.042	0.0*	5-S2n	0.396	0.664	0.396	1.000	8.474	0.000
2.75	2.75	759.14	1.143	0.0*	5-S2n	0.422	0.708	0.422	1.000	8.692	0.000
3.05	3.05	759.25	1.254	0.0*	5-S2n	0.449	0.746	0.449	1.000	8.917	0.000

* Full Flow Headwater elevation is below inlet invert.

Straight Culvert
Inlet Elevation (invert): 758.00 ft, Outlet Elevation (invert): 753.50 ft
Culvert Length: 125.08 ft, Culvert Slope: 0.0360

Culvert Performance Curve Plot: 5-1 (Ph 1 Access Rd)



Water Surface Profile Plot for Culvert: 5-1 (Ph 1 Access Rd)

Crossing - 5-1 (Ph 1 Access Rd), Design Discharge - 3.0 cfs
Culvert - 5-1 (Ph 1 Access Rd), Culvert Discharge - 3.0 cfs

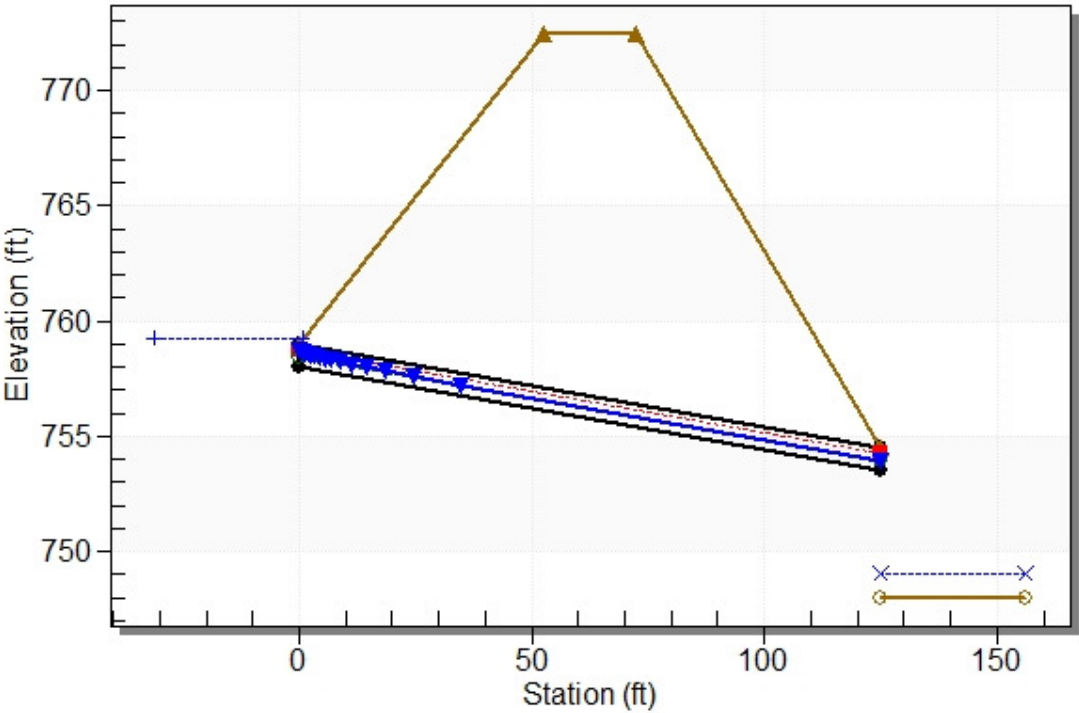


Table 3 - Downstream Channel Rating Curve (Crossing: 5-1 (Ph 1 Access Rd))

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
0.00	749.00	1.00
0.30	749.00	1.00
0.61	749.00	1.00
0.92	749.00	1.00
1.22	749.00	1.00
1.52	749.00	1.00
1.83	749.00	1.00
2.13	749.00	1.00
2.44	749.00	1.00
2.75	749.00	1.00
3.05	749.00	1.00

HY-8 Culvert Analysis Report (Culvert 11-1)

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 0 cfs

Design Flow: 7.8 cfs

Maximum Flow: 7.8 cfs

Table 1 - Summary of Culvert Flows at Crossing: Culvert 11-1 (Ph 5 Access Rd)

Headwater Elevation (ft)	Total Discharge (cfs)	Culvert 11-1 (Ph 5 Access Rd) Discharge (cfs)	Roadway Discharge (cfs)	Iterations
770.00	0.00	0.00	0.00	1
770.44	0.78	0.78	0.00	1
770.63	1.56	1.56	0.00	1
770.79	2.34	2.34	0.00	1
770.95	3.12	3.12	0.00	1
771.10	3.90	3.90	0.00	1
771.23	4.68	4.68	0.00	1
771.36	5.46	5.46	0.00	1
771.49	6.24	6.24	0.00	1
771.62	7.02	7.02	0.00	1
771.77	7.80	7.80	0.00	1
774.00	15.40	15.40	0.00	Overtopping

Tailwater Channel Data - Culvert 11-1 (Ph 5 Access Rd)

Tailwater Channel Option: Triangular Channel

Side Slope (H:V): 3.00 (_:1)

Channel Slope: 0.3300

Channel Manning's n: 0.0200

Channel Invert Elevation: 768.00 ft

Roadway Data for Crossing: Culvert 11-1 (Ph 5 Access Rd)

Roadway Profile Shape: Constant Roadway Elevation

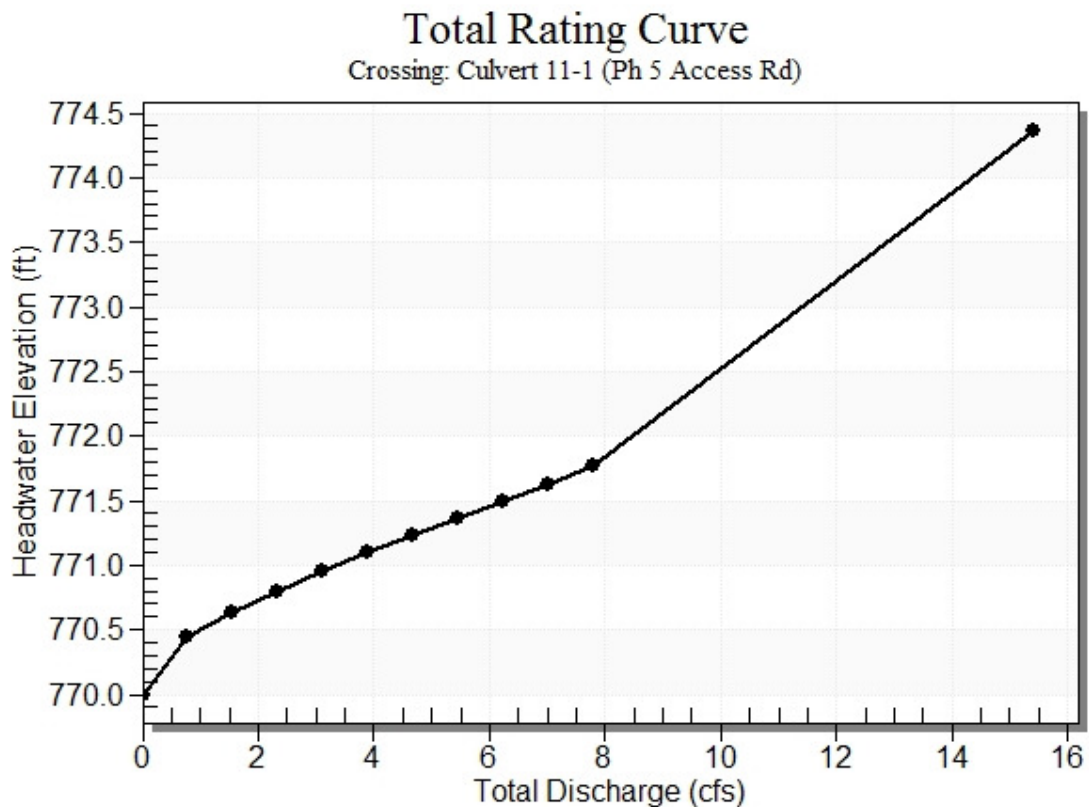
Crest Length: 100.00 ft

Crest Elevation: 774.00 ft

Roadway Surface: Gravel

Roadway Top Width: 18.00 ft

Rating Curve Plot for Crossing: Culvert 11-1 (Ph 5 Access Rd)



Site Data - Culvert 11-1 (Ph 5 Access Rd)

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft

Inlet Elevation: 770.00 ft

Outlet Station: 75.00 ft

Outlet Elevation: 768.00 ft

Number of Barrels: 1

Culvert Data Summary - Culvert 11-1 (Ph 5 Access Rd)

Barrel Shape: Circular

Barrel Diameter: 1.50 ft

Barrel Material: Smooth HDPE

Embedment: 0.00 in

Barrel Manning's n: 0.0120

Culvert Type: Straight

Inlet Configuration: Square Edge with Headwall

Inlet Depression: NONE

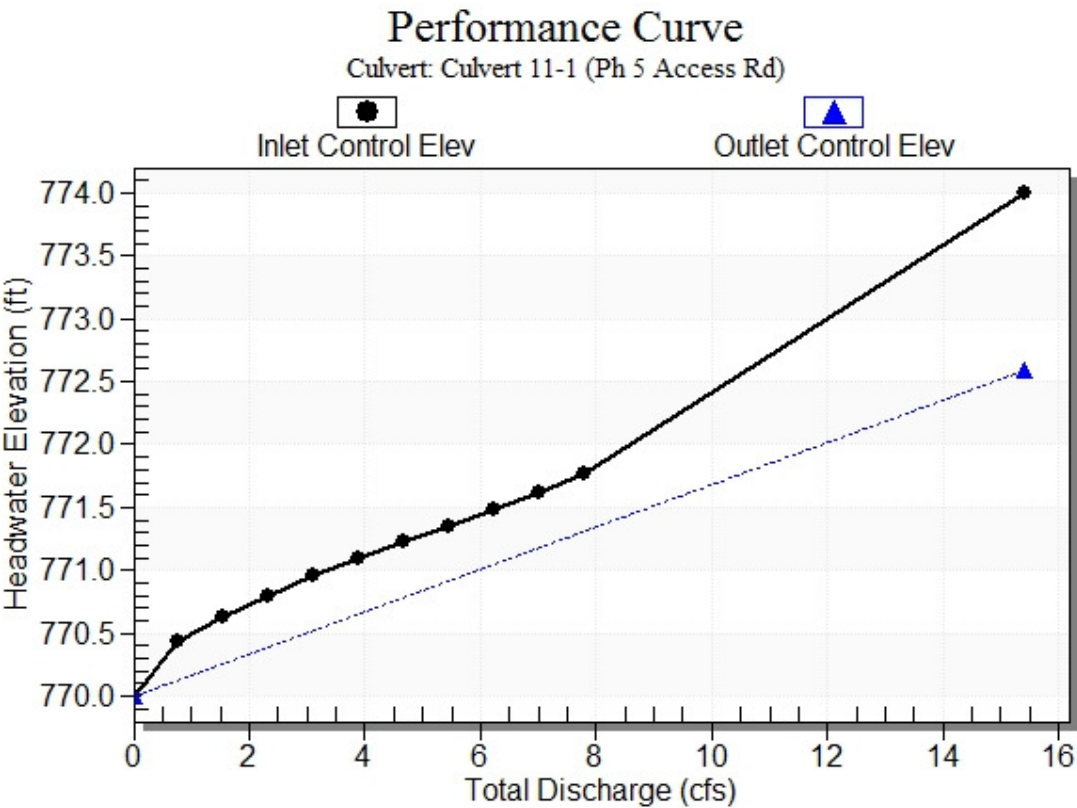
Table 2 - Culvert Summary Table: Culvert 11-1 (Ph 5 Access Rd)

Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
0.00	0.00	770.00	0.000	0.000	0-NF	0.000	0.000	0.000	0.000	0.000	0.000
0.78	0.78	770.44	0.437	0.0*	1-S2n	0.198	0.323	0.211	0.178	4.977	8.212
1.56	1.56	770.63	0.631	0.0*	1-S2n	0.290	0.464	0.290	0.231	6.572	9.766
2.34	2.34	770.79	0.794	0.0*	1-S2n	0.353	0.574	0.359	0.269	7.131	10.808
3.12	3.12	770.95	0.954	0.0*	1-S2n	0.415	0.672	0.415	0.299	7.850	11.614
3.90	3.90	771.10	1.096	0.0*	1-S2n	0.462	0.755	0.474	0.325	8.113	12.280
4.68	4.68	771.23	1.228	0.0*	1-S2n	0.510	0.828	0.520	0.348	8.592	12.853
5.46	5.46	771.36	1.356	0.0*	1-S2n	0.556	0.898	0.568	0.369	8.915	13.358
6.24	6.24	771.49	1.486	0.0*	1-S2n	0.596	0.960	0.612	0.388	9.189	13.812
7.02	7.02	771.62	1.622	0.0*	5-S2n	0.637	1.023	0.655	0.406	9.453	14.224
7.80	7.80	771.77	1.767	0.0*	5-S2n	0.677	1.078	0.695	0.422	9.737	14.604

* Full Flow Headwater elevation is below inlet invert.

Straight Culvert
Inlet Elevation (invert): 770.00 ft, Outlet Elevation (invert): 768.00 ft
Culvert Length: 75.03 ft, Culvert Slope: 0.0267

Culvert Performance Curve Plot: Culvert 11-1 (Ph 5 Access Rd)



Water Surface Profile Plot for Culvert: Culvert 11-1 (Ph 5 Access Rd)

Crossing - Culvert 11-1 (Ph 5 Access Rd), Design Discharge - 7.8 cfs

Culvert - Culvert 11-1 (Ph 5 Access Rd), Culvert Discharge - 7.8 cfs

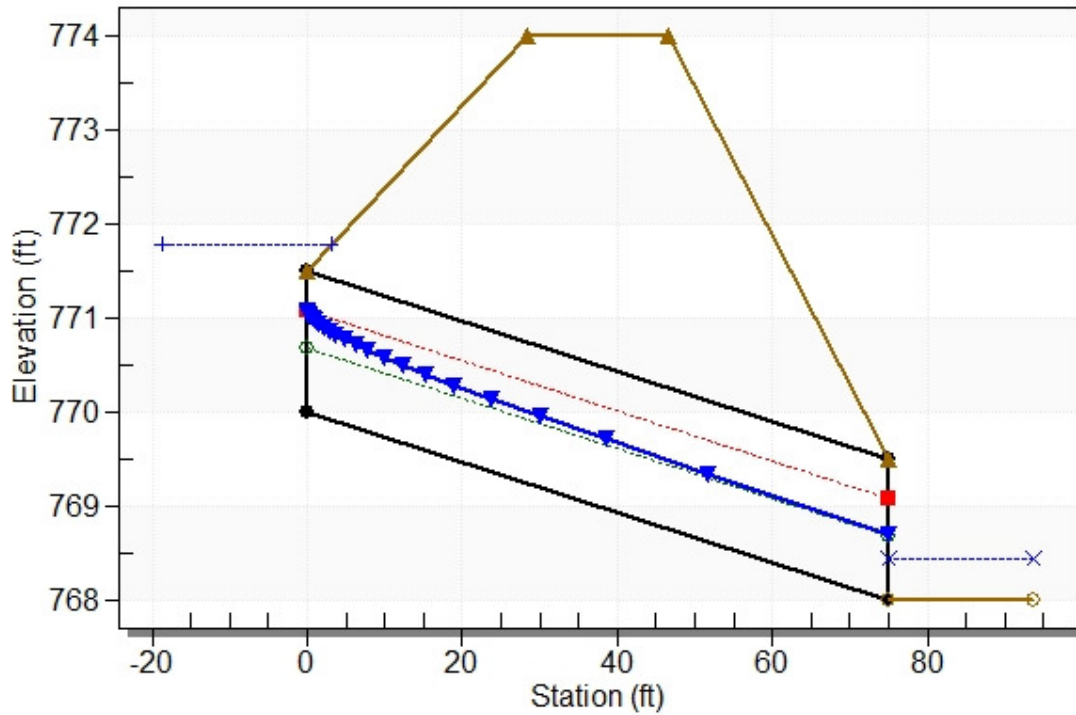


Table 3 - Downstream Channel Rating Curve (Crossing: Culvert 11-1 (Ph 5 Access Rd))

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)	Velocity (ft/s)	Shear (psf)	Froude Number
0.00	768.00	0.00	0.00	0.00	0.00
0.78	768.18	0.18	8.21	3.66	4.85
1.56	768.23	0.23	9.77	4.75	5.07
2.34	768.27	0.27	10.81	5.53	5.20
3.12	768.30	0.30	11.61	6.16	5.29
3.90	768.33	0.33	12.28	6.70	5.37
4.68	768.35	0.35	12.85	7.17	5.43
5.46	768.37	0.37	13.36	7.60	5.48
6.24	768.39	0.39	13.81	7.99	5.53
7.02	768.41	0.41	14.22	8.35	5.57
7.80	768.42	0.42	14.60	8.69	5.60

HY-8 Culvert Analysis Report (Culvert 12-1)

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 0 cfs

Design Flow: 12.23 cfs

Maximum Flow: 12.23 cfs

Table 1 - Summary of Culvert Flows at Crossing: Culvert 12-1 (Across LF Perimeter Road)

Headwater Elevation (ft)	Total Discharge (cfs)	Culvert 12-1 (Across LF Perimeter Road) Discharge (cfs)	Roadway Discharge (cfs)	Iterations
796.30	0.00	0.00	0.00	1
796.82	1.22	1.22	0.00	1
797.06	2.45	2.45	0.00	1
797.30	3.67	3.67	0.00	1
797.50	4.89	4.89	0.00	1
797.71	6.12	6.12	0.00	1
797.92	7.34	7.34	0.00	1
798.16	8.56	8.56	0.00	1
798.44	9.78	9.78	0.00	1
798.76	11.01	11.01	0.00	1
799.12	12.23	12.23	0.00	1
800.00	14.78	14.78	0.00	Overtopping

Tailwater Channel Data - Culvert 12-1 (Across LF Perimeter Road)

Tailwater Channel Option: Enter Constant Tailwater Elevation

Constant Tailwater Elevation: 777.00 ft

Roadway Data for Crossing: Culvert 12-1 (Across LF Perimeter Road)

Roadway Profile Shape: Constant Roadway Elevation

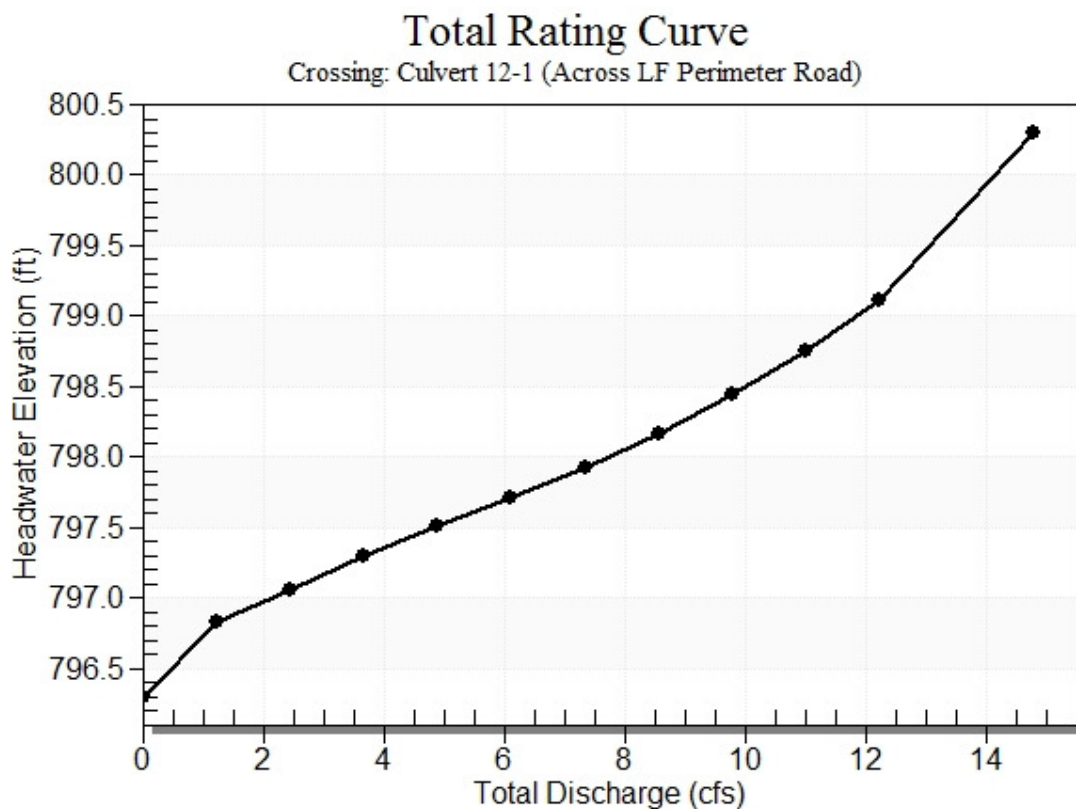
Crest Length: 100.00 ft

Crest Elevation: 800.00 ft

Roadway Surface: Gravel

Roadway Top Width: 18.00 ft

Rating Curve Plot for Crossing: Culvert 12-1 (Across LF Perimeter Road)



Site Data - Culvert 12-1 (Across LF Perimeter Road)

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft

Inlet Elevation: 796.30 ft

Outlet Station: 70.00 ft

Outlet Elevation: 789.00 ft

Number of Barrels: 1

Culvert Data Summary - Culvert 12-1 (Across LF Perimeter Road)

Barrel Shape: Circular

Barrel Diameter: 1.50 ft

Barrel Material: Smooth HDPE

Embedment: 0.00 in

Barrel Manning's n: 0.0120

Culvert Type: Straight

Inlet Configuration: Square Edge with Headwall

Inlet Depression: NONE

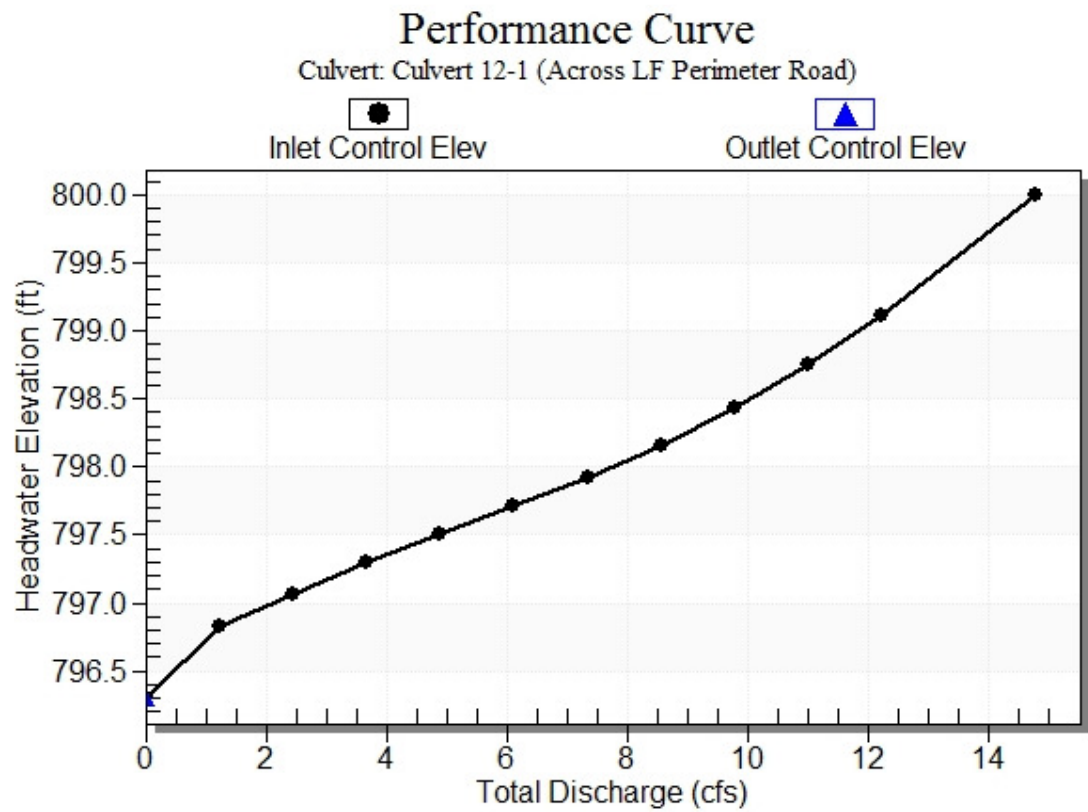
Table 2 - Culvert Summary Table: Culvert 12-1 (Across LF Perimeter Road)

Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
0.00	0.00	796.30	0.000	0.000	0-NF	0.000	0.000	0.000	3.000	0.000	0.000
1.22	1.22	796.82	0.523	0.0*	1-S2n	0.176	0.411	0.176	3.000	16.733	0.000
2.45	2.45	797.06	0.758	0.0*	1-S2n	0.259	0.589	0.259	3.000	11.934	0.000
3.67	3.67	797.30	0.997	0.0*	1-S2n	0.314	0.732	0.314	3.000	14.012	0.000
4.89	4.89	797.50	1.205	0.0*	1-S2n	0.364	0.846	0.364	3.000	14.640	0.000
6.12	6.12	797.71	1.407	0.0*	1-S2n	0.413	0.951	0.438	3.000	14.329	0.000
7.34	7.34	797.92	1.622	0.0*	5-S2n	0.451	1.046	0.479	3.000	15.035	0.000
8.56	8.56	798.16	1.863	0.0*	5-S2n	0.489	1.129	0.522	3.000	15.627	0.000
9.78	9.78	798.44	2.139	0.0*	5-S2n	0.526	1.206	0.526	3.000	17.662	0.000
11.01	11.01	798.76	2.456	0.0*	5-S2n	0.561	1.270	0.596	3.000	16.813	0.000
12.23	12.23	799.12	2.816	0.0*	5-S2n	0.593	1.322	0.626	3.000	17.492	0.000

* Full Flow Headwater elevation is below inlet invert.

Straight Culvert
Inlet Elevation (invert): 796.30 ft, Outlet Elevation (invert): 789.00 ft
Culvert Length: 70.38 ft, Culvert Slope: 0.1043

Culvert Performance Curve Plot: Culvert 12-1 (Across LF Perimeter Road)



Water Surface Profile Plot for Culvert: Culvert 12-1 (Across LF Perimeter Road)

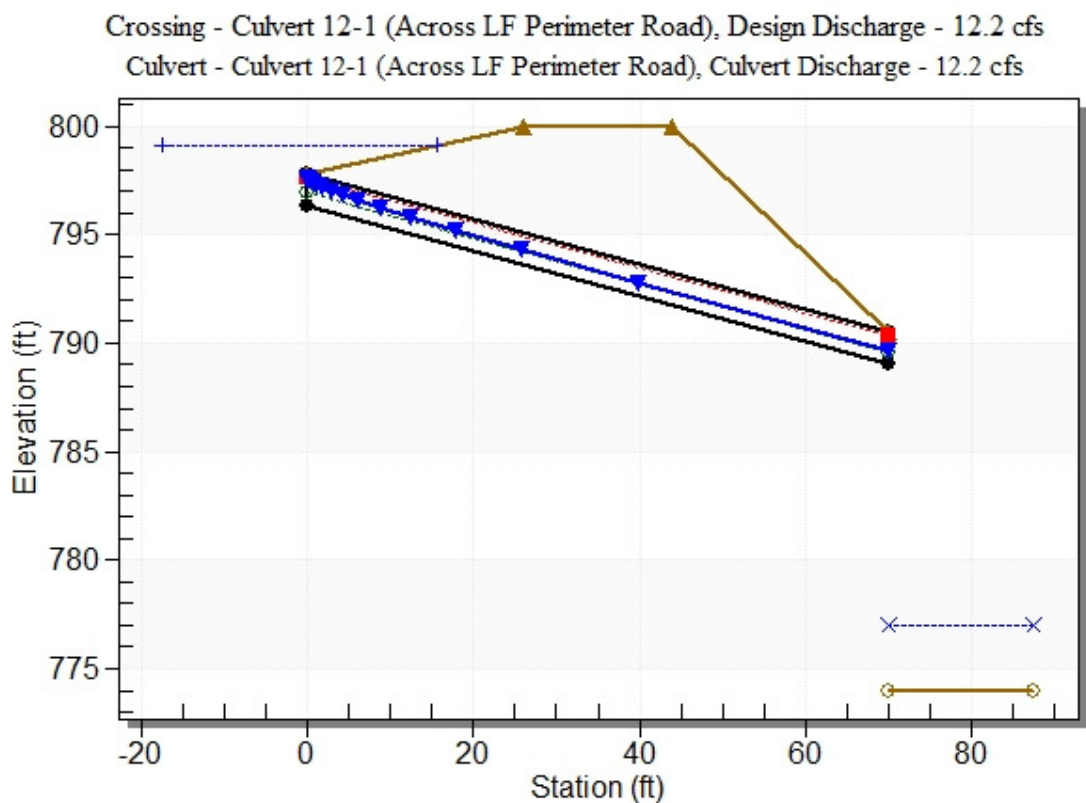


Table 3 - Downstream Channel Rating Curve (Crossing: Culvert 12-1 (Across LF Perimeter Road))

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
0.00	777.00	3.00
1.22	777.00	3.00
2.45	777.00	3.00
3.67	777.00	3.00
4.89	777.00	3.00
6.12	777.00	3.00
7.34	777.00	3.00
8.56	777.00	3.00
9.78	777.00	3.00
11.01	777.00	3.00
12.23	777.00	3.00

HY-8 Culvert Analysis Report (Culvert 15-1)

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 0 cfs

Design Flow: 3.03 cfs

Maximum Flow: 3.03 cfs

Table 1 - Summary of Culvert Flows at Crossing: Culvert 15-1 (Ph 3 Access Rd)

Headwater Elevation (ft)	Total Discharge (cfs)	Culvert 15-1 (Ph 3 Access Rd) Discharge (cfs)	Roadway Discharge (cfs)	Iterations
764.00	0.00	0.00	0.00	1
764.30	0.30	0.30	0.00	1
764.43	0.61	0.61	0.00	1
764.54	0.91	0.91	0.00	1
764.65	1.21	1.21	0.00	1
764.75	1.51	1.51	0.00	1
764.84	1.82	1.82	0.00	1
764.93	2.12	2.12	0.00	1
765.03	2.42	2.42	0.00	1
765.13	2.73	2.73	0.00	1
765.24	3.03	3.03	0.00	1
769.00	8.12	8.12	0.00	Overtopping

Tailwater Channel Data - Culvert 15-1 (Ph 3 Access Rd)

Tailwater Channel Option: Enter Constant Tailwater Elevation

Constant Tailwater Elevation: 756.00 ft

Roadway Data for Crossing: Culvert 15-1 (Ph 3 Access Rd)

Roadway Profile Shape: Constant Roadway Elevation

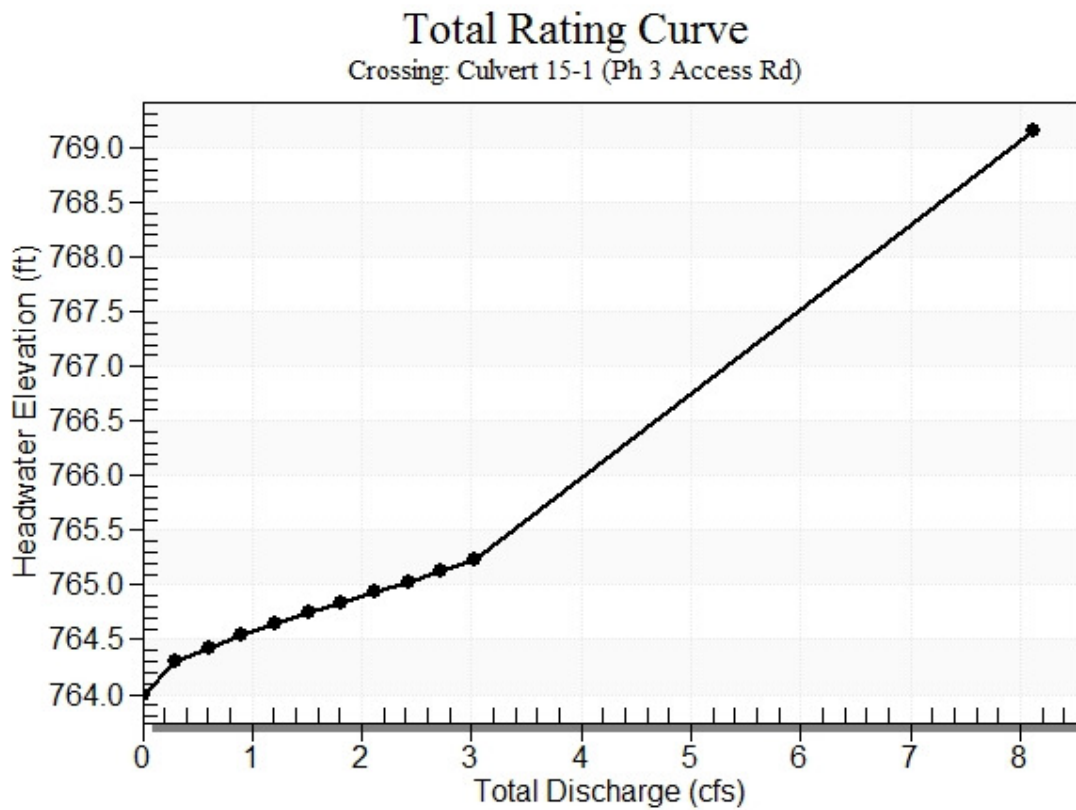
Crest Length: 100.00 ft

Crest Elevation: 769.00 ft

Roadway Surface: Gravel

Roadway Top Width: 18.00 ft

Rating Curve Plot for Crossing: Culvert 15-1 (Ph 3 Access Rd)



Site Data - Culvert 15-1 (Ph 3 Access Rd)

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft

Inlet Elevation: 764.00 ft

Outlet Station: 70.00 ft

Outlet Elevation: 760.00 ft

Number of Barrels: 1

Culvert Data Summary - Culvert 15-1 (Ph 3 Access Rd)

Barrel Shape: Circular

Barrel Diameter: 1.00 ft

Barrel Material: Smooth HDPE

Embedment: 0.00 in

Barrel Manning's n: 0.0120

Culvert Type: Straight

Inlet Configuration: Square Edge with Headwall

Inlet Depression: NONE

Table 2 - Culvert Summary Table: Culvert 15-1 (Ph 3 Access Rd)

Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
0.00	0.00	764.00	0.000	0.000	0-NF	0.000	0.000	0.000	2.000	0.000	0.000
0.30	0.30	764.30	0.302	0.0*	1-S2n	0.117	0.223	0.117	2.000	9.281	0.000
0.61	0.61	764.43	0.430	0.0*	1-S2n	0.171	0.321	0.171	2.000	6.726	0.000
0.91	0.91	764.54	0.538	0.0*	1-S2n	0.208	0.398	0.216	2.000	7.506	0.000
1.21	1.21	764.65	0.648	0.0*	1-S2n	0.241	0.464	0.241	2.000	8.243	0.000
1.51	1.51	764.75	0.747	0.0*	1-S2n	0.274	0.521	0.274	2.000	8.692	0.000
1.82	1.82	764.84	0.840	0.0*	1-S2n	0.299	0.571	0.299	2.000	9.319	0.000
2.12	2.12	764.93	0.931	0.0*	1-S2n	0.323	0.619	0.323	2.000	9.614	0.000
2.42	2.42	765.03	1.026	0.0*	5-S2n	0.348	0.662	0.348	2.000	9.946	0.000
2.73	2.73	765.13	1.127	0.0*	5-S2n	0.372	0.706	0.375	2.000	10.157	0.000
3.03	3.03	765.24	1.236	0.0*	5-S2n	0.393	0.743	0.393	2.000	10.629	0.000

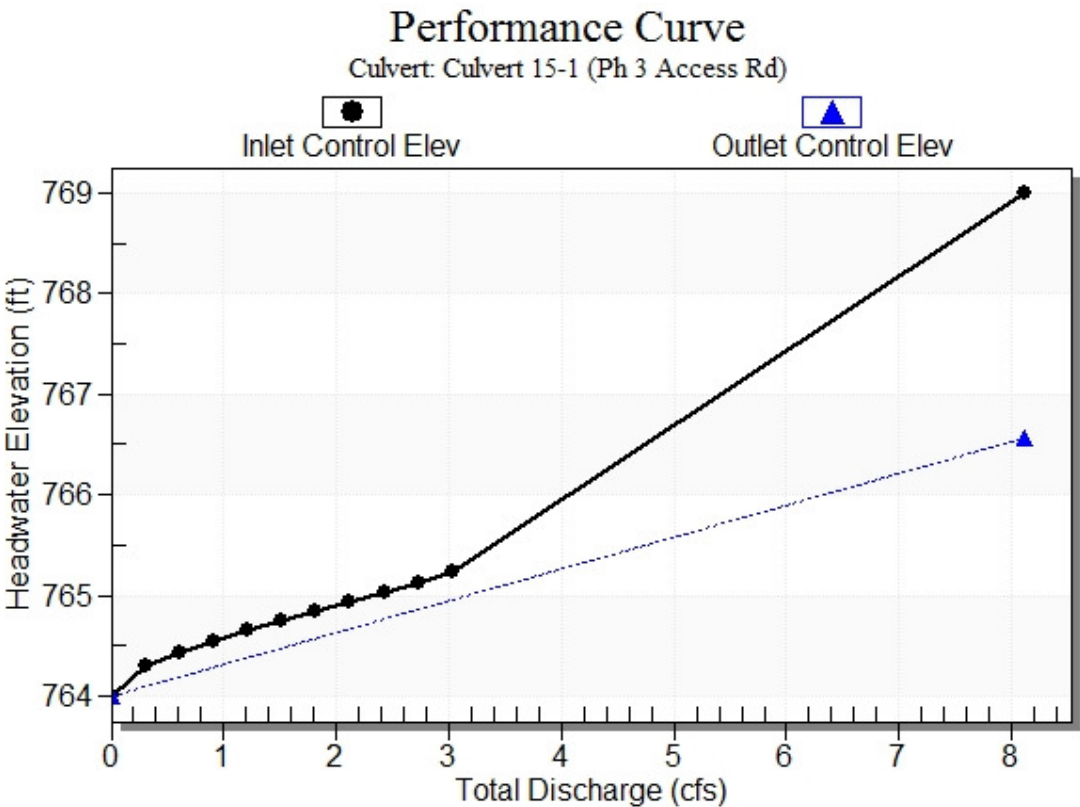
* Full Flow Headwater elevation is below inlet invert.

Straight Culvert

Inlet Elevation (invert): 764.00 ft, Outlet Elevation (invert): 760.00 ft

Culvert Length: 70.11 ft, Culvert Slope: 0.0571

Culvert Performance Curve Plot: Culvert 15-1 (Ph 3 Access Rd)



Water Surface Profile Plot for Culvert: Culvert 15-1 (Ph 3 Access Rd)

Crossing - Culvert 15-1 (Ph 3 Access Rd), Design Discharge - 3.0 cfs

Culvert - Culvert 15-1 (Ph 3 Access Rd), Culvert Discharge - 3.0 cfs

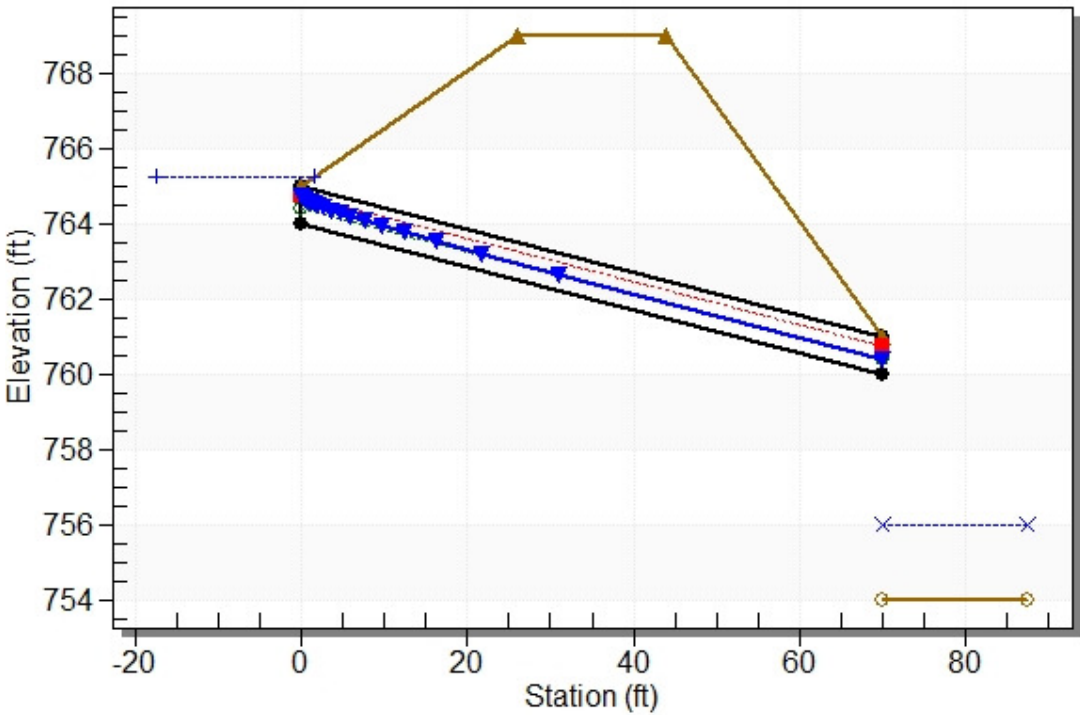


Table 3 - Downstream Channel Rating Curve (Crossing: Culvert 15-1 (Ph 3 Access Rd))

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
0.00	756.00	2.00
0.30	756.00	2.00
0.61	756.00	2.00
0.91	756.00	2.00
1.21	756.00	2.00
1.51	756.00	2.00
1.82	756.00	2.00
2.12	756.00	2.00
2.42	756.00	2.00
2.73	756.00	2.00
3.03	756.00	2.00

Haul Road Culvert Sizing

Haul Road Culvert Sizing

Determine size of culvert required for haul road to stockpile area.

Use HydroCAD to estimate peak runoff to culvert for the 25-year, 24-hour storm event. See attached figure for drainage area and Tc flow paths. Use HY-8 to size culverts.

Drainage area to culvert = 189.5 ac

Tc Flow

Sheet flow = 100 ft at 0.5 % slope

Shallow concentrated flow = 1373 ft at 2.3% slope, short grass

Channel flow = 3225 ft at 2% slope in a trapazoidal channel, n = 0.035 earth, dense weeds.

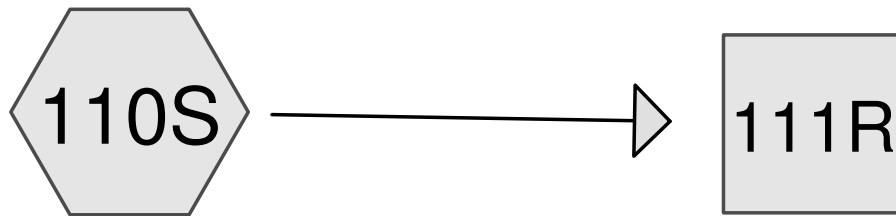
The wetland area is modeled as a reach of 734 ft in length and a slope of 0.14%

See sheets 2 - 8 for HydroCAD model of watershed and runoff calculations.

25-yr storm peak discharge rate to culverts = 304 cfs

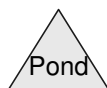
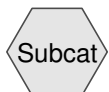
The invert elevations, length of culverts, and height of access road over culvert are as shown on the Expansion Permit Amendment drawings.

Based on the results of the HY-8 analysis, 2-48" diameter culverts will accommodate the peak flows resulting from the 25-year, 24-hour storm event without overtopping the haul road.



Haul Road Culvert

Wetland



Haul Road Culvert2

Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

Prepared by SCS Engineers

Printed 11/27/2013

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Summary for Subcatchment 110S: Haul Road Culvert

Runoff = 374.75 cfs @ 12.43 hrs, Volume= 47.419 af, Depth= 3.00"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs
Type II 24-hr 25-yr, 24-hr Rainfall=5.67"

Area (ac)	CN	Description
* 189.500	75	Grass
189.500		Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
17.2	100	0.0050	0.10		Sheet Flow, Sheet flow across access road Grass: Short n= 0.150 P2= 3.14"
21.6	1,373	0.0230	1.06		Shallow Concentrated Flow, Shallow slow across final cover Short Grass Pasture Kv= 7.0 fps
5.8	3,225	0.0200	9.34	478.90	Trap/Vee/Rect Channel Flow, Bot.W=15.00' D=2.55' Z= 2.0 ' /' Top.W=25.20' n= 0.035 Earth, dense weeds
44.6	4,698	Total			

Summary for Reach 111R: Wetland

[91] Warning: Storage range exceeded by 4.64'

[55] Hint: Peak inflow is 818% of Manning's capacity

Inflow Area = 189.500 ac, 0.00% Impervious, Inflow Depth = 3.00" for 25-yr, 24-hr event
 Inflow = 374.75 cfs @ 12.43 hrs, Volume= 47.419 af
 Outflow = 304.16 cfs @ 12.92 hrs, Volume= 47.419 af, Atten= 19%, Lag= 29.3 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-72.00 hrs, dt= 0.05 hrs

Max. Velocity= 0.75 fps, Min. Travel Time= 16.3 min

Avg. Velocity = 0.13 fps, Avg. Travel Time= 92.0 min

Peak Storage= 298,452 cf @ 12.65 hrs, Average Depth at Peak Storage= 6.14'

Bank-Full Depth= 1.50', Capacity at Bank-Full= 45.83 cfs

40.00' x 1.50' deep channel, n= 0.110
 Side Slope Z-value= 10.0 ' /' Top Width= 70.00'
 Length= 734.0' Slope= 0.0014 ' /'
 Inlet Invert= 746.00', Outlet Invert= 745.00'



‡

Haul Road Culvert Sizing

Site Data - Box Culvert

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft

Inlet Elevation: 772.20 ft

Outlet Station: 100.00 ft

Outlet Elevation: 770.20 ft

Number of Barrels: 1

Culvert Data Summary - Box Culvert

Barrel Shape: Concrete Box

Barrel Span: 20.00 ft

Barrel Rise: 6.00 ft

Barrel Material: Concrete

Embedment: 0.00 in

Barrel Manning's n: 0.0120

Culvert Type: Straight

Inlet Configuration: Square Edge (90°) Headwall

Inlet Depression: NONE

Tailwater Channel Data - Haul Road Box Culvert

Tailwater Channel Option: Trapezoidal Channel

Bottom Width: 15.00 ft

Side Slope (H:V): 2.00 (2:1)

Channel Slope: 0.0200

Channel Manning's n: 0.0350

Channel Invert Elevation: 772.20 ft

Roadway Data for Crossing: Haul Road Box Culvert

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 100.00 ft

Crest Elevation: 780.00 ft

Roadway Surface: Gravel

Roadway Top Width: 18.00 ft

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 0 cfs

Design Flow: 685 cfs

Maximum Flow: 685 cfs

Table 1 - Culvert Summary Table: Box Culvert

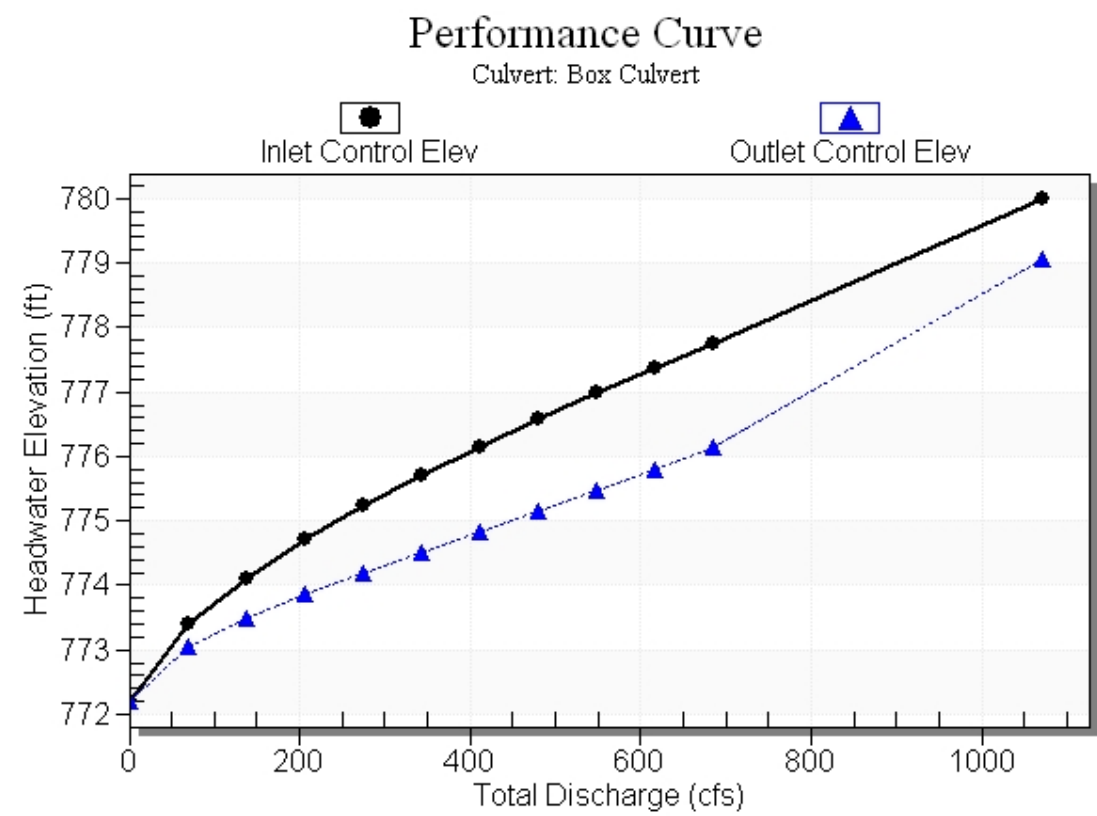
Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
	0.00	0.00	772.20	0.000	0.000	0-NF	0.000	0.000	2.000	0.000	0.000
	68.50	68.50	773.40	1.202	0.843	1-JS1t	0.303	0.714	2.835	0.835	1.208
	137.00	137.00	774.11	1.908	1.284	1-JS1t	0.575	1.134	3.251	1.251	2.107
	205.50	205.50	774.70	2.500	1.656	1-JS1t	0.721	1.486	3.581	1.581	2.869
	274.00	274.00	775.23	3.029	1.996	1-JS1t	0.867	1.800	3.863	1.863	3.546
	342.50	342.50	775.70	3.505	2.321	1-JS1t	1.014	2.088	4.114	2.114	4.163
	411.00	411.00	776.15	3.950	2.640	1-JS1t	1.142	2.358	4.342	2.342	4.733
	479.50	479.50	776.57	4.372	2.958	1-JS1t	1.252	2.613	4.552	2.552	5.267
	548.00	548.00	776.98	4.776	3.277	1-S2n	1.361	2.857	1.732	2.747	15.817
	616.50	616.50	777.37	5.168	3.602	1-S2n	1.470	3.090	1.897	2.931	16.252
	685.00	685.00	777.75	5.553	3.933	1-S2n	1.579	3.315	2.058	3.105	16.642

Straight Culvert

Inlet Elevation (invert): 772.20 ft, Outlet Elevation (invert): 770.20 ft

Culvert Length: 100.02 ft, Culvert Slope: 0.0200

Culvert Performance Curve Plot: Box Culvert



Water Surface Profile Plot for Culvert: Box Culvert

Crossing - Haul Road Box Culvert, Design Discharge - 685.0 cfs

Culvert - Box Culvert, Culvert Discharge - 685.0 cfs

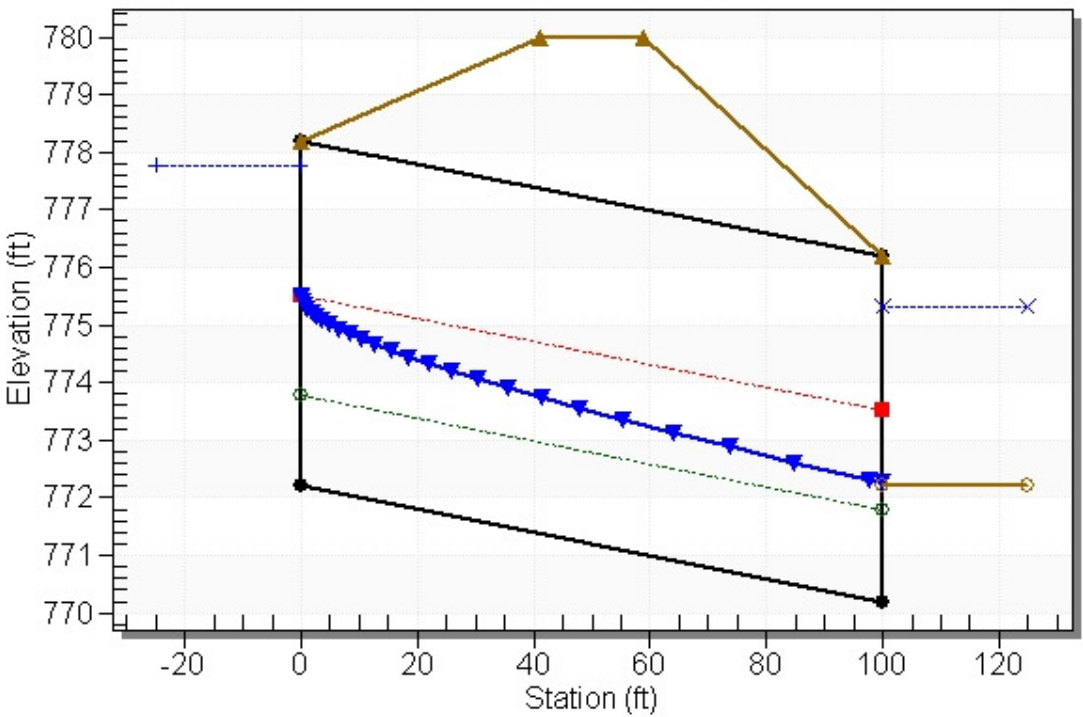


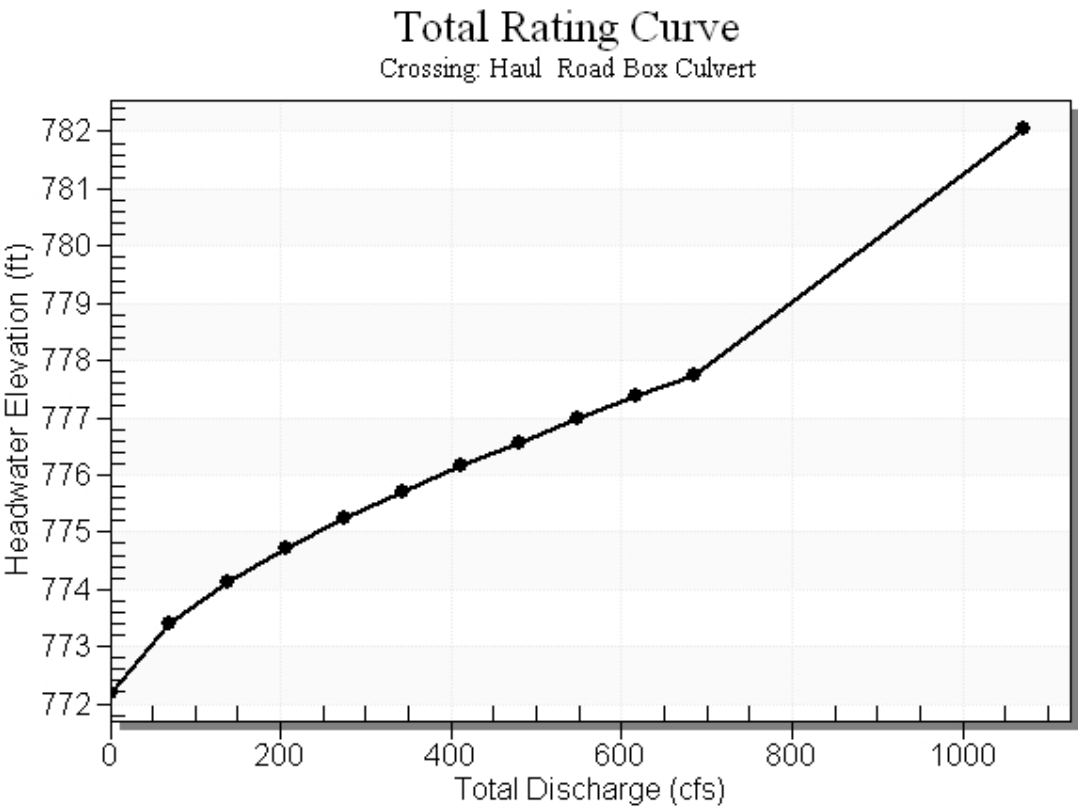
Table 2 - Downstream Channel Rating Curve (Crossing: Haul Road Box Culvert)

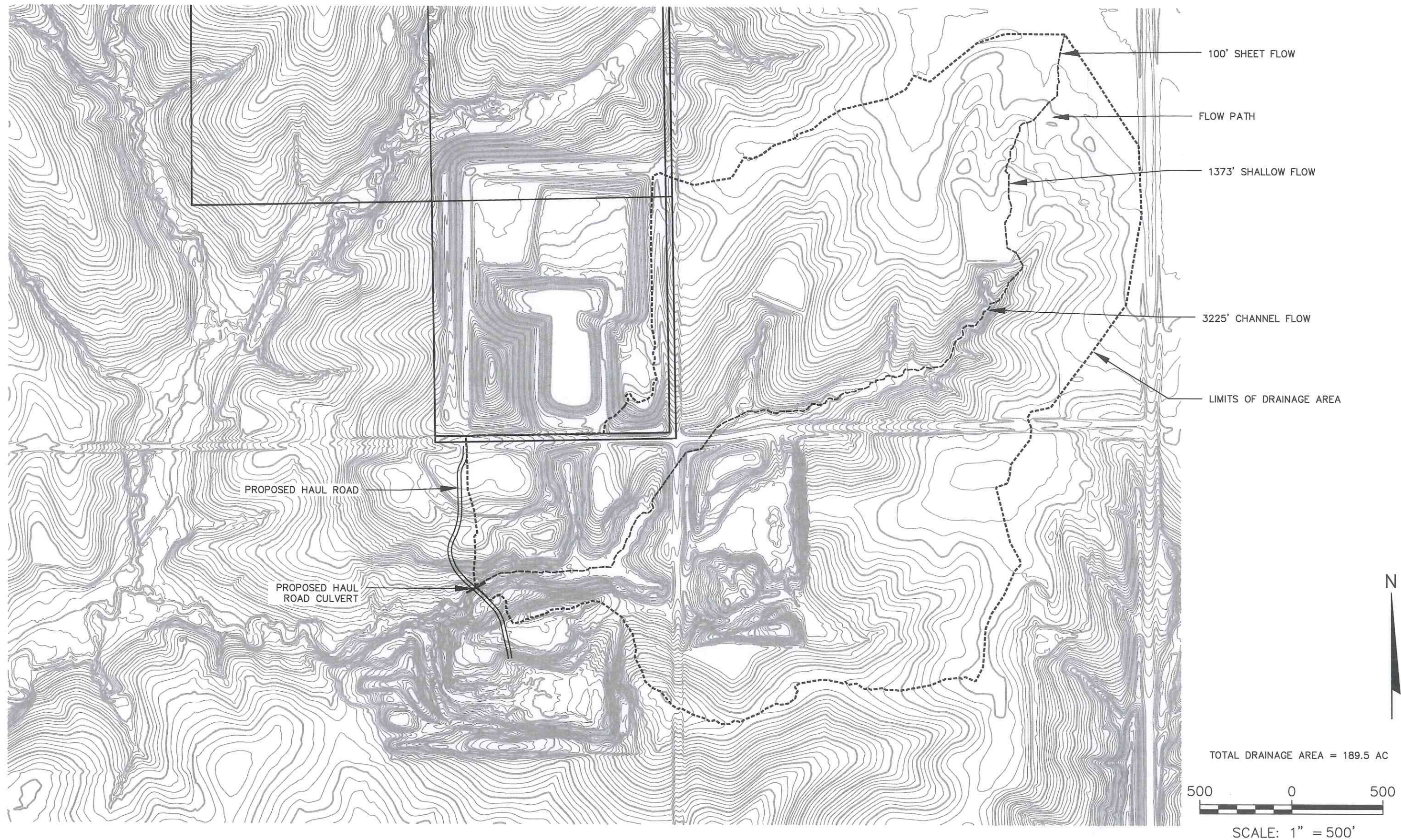
Flow (cfs)	Water Surface Elev (ft)	Depth (ft)	Velocity (ft/s)	Shear (psf)	Froude Number
0.00	772.20	0.00	0.00	0.00	0.00
68.50	773.03	0.83	4.92	1.04	1.00
137.00	773.45	1.25	6.26	1.56	1.05
205.50	773.78	1.58	7.16	1.97	1.09
274.00	774.06	1.86	7.85	2.33	1.11
342.50	774.31	2.11	8.43	2.64	1.13
411.00	774.54	2.34	8.92	2.92	1.14
479.50	774.75	2.55	9.35	3.18	1.15
548.00	774.95	2.75	9.73	3.43	1.17
616.50	775.13	2.93	10.08	3.66	1.17
685.00	775.31	3.11	10.40	3.88	1.18

Table 3 - Summary of Culvert Flows at Crossing: Haul Road Box Culvert

Headwater Elevation (ft)	Total Discharge (cfs)	Box Culvert Discharge (cfs)	Roadway Discharge (cfs)	Iterations
772.20	0.00	0.00	0.00	1
773.40	68.50	68.50	0.00	1
774.11	137.00	137.00	0.00	1
774.70	205.50	205.50	0.00	1
775.23	274.00	274.00	0.00	1
775.70	342.50	342.50	0.00	1
776.15	411.00	411.00	0.00	1
776.57	479.50	479.50	0.00	1
776.98	548.00	548.00	0.00	1
777.37	616.50	616.50	0.00	1
777.75	685.00	685.00	0.00	1
780.00	1072.05	1072.05	0.00	Overtopping

Rating Curve Plot for Crossing: Haul Road Box Culvert





PROJECT NO.	25211509.03	DRAWN BY:	BJM	SCS ENGINEERS 2830 DAIRY DRIVE MADISON, WI 53718-6751 PHONE: (608) 224-2830	CLIENT INTERSTATE POWER AND LIGHT COMPANY OTTUMWA MIDLAND LANDFILL 15300 130TH STREET OTTUMWA, IOWA 52501	SITE PERMIT AMENDMENT PLAN NORTH & SOUTH EXPANSION OTTUMWA MIDLAND LANDFILL OTTUMWA, IOWA	HAUL ROAD CULVERT	FIGURE
DRAWN:	10/15/13	CHECKED BY:	BP					X OF X
REVISED:	10/18/13	APPROVED BY:						

Sedimentation Basin Sizing

Sedimentation Basin Sizing**Performance Criteria:**

- Sedimentation basins have been designed to settle out particles 15 microns and greater for storms up to the 25-year, 24-hour storm event.
- Principle spillways have been designed to pass a 25-year, 24-hour storm event.
- Emergency spillways have been designed to pass a 100-year, 24-hour storm event.

Use the table presented in the Erosion and Sediment Control Handbook (Goldman, *et al.*, 1986) that provides the surface area-to-discharge ratios required to achieve settlement of the desired particle sizes. The table is included below. From the table, use the surface area to flow ratio for the sedimentation basins to determine the maximum particle size settled.

The table below summarizes the surface area to flow ratios for the sedimentation basins. It also summarizes the freeboard in the basins for a 100-year, 24-hour storm event. The information is based on the HydroCAD model output included with this appendix.

Spillway Sizing:

- Spillways will be sized with a 20' wide bottom width.

Use outputs from the HydroCAD Modeling to determine the water velocity over the spillway and provide appropriate riprap size.

TABLE 8.1 Surface Area Requirements of Sediment Traps and Basins

Particle size, mm	Settling velocity, ft/sec (m/sec)	Surface area requirements, ft ² per ft ³ /sec (m ² per m ³ /sec discharge discharge)	
		ft ² per ft ³ /sec discharge	(m ² per m ³ /sec discharge)
0.5 (coarse sand)	0.19 (0.058)	6.3	(20.7)
0.2 (medium sand)	0.067 (0.020)	17.9	(58.7)
0.1 (fine sand)	0.023 (0.0070)	52.2	(171.0)
0.05 (coarse silt)	0.0062 (0.0019)	193.6	(635.0)
0.02 (medium silt)	0.00096 (0.00029)	1,250.0	(4,101.0)
0.01 (fine silt)	0.00024 (0.000073)	5,000.0	(16,404.0)
0.005 (clay)	0.00006 (0.000018)	20,000.0	(65,617.0)

Sedimentation Basin Performance Summary

Feature	25-yr, 24-hr Storm			Surface Area at Peak Water Surface Elevation, SA (sf)	SA/Q Ratio	Maximum Particle Size Settled (mm)	100-yr, 24-hr Storm Peak Water Surface Elevation	Top of Berm Elevation (Freeboard)	Basin Freeboard for 100-yr Storm (feet)
	Peak Inflow (cfs)	Peak Discharge, Q (cfs)	Peak Water Surface Elevation						
Sedimentation Basin No. 2	97.61	9.89	760.39	47,104	4,762	.010	761.40	762.0	0.60
Sedimentation Basin No. 3	94.53	4.79	757.19	57,420	11,987	.006	757.90	762.0	4.10
Sedimentation Basin No. 4	107.74	15.90	756.35	52,239	3,285	.015	758.24	760.0	1.76

**Velocity Over Riprap Spillways
OML Expansion**

100-year, 24-hour Storm

Basin	Width of Spillway, ft	Flow Rate, cfs	Depth of Flow, ft	Cross- sectional flow area, sq. ft.	Velocity, fps	Riprap D50, ft
Sed Basin 2	20	12.52	0.4	8.10	1.5	0.5
Sed Basin 3	20	0.0	--	--	--	0.5
Sed Basin 4	20	0.0	--	--	--	0.5

Notes:

1. The peak water levels from the 25-year, 24-hour storm events do not overtop the emergency spillways.
2. The peak water levels from the 100-year, 24-hour storm events do not overtop the emergency spillway at sed basin 3 and sed basin 4.
3. Flow rate and spillway configuration based on HydroCAD modeling.