

**VIA EMAIL**

October 30, 2020

Mr. Jeffrey Maxted
Alliant Energy – Environmental Services Manager
4902 North Biltmore Lane
Madison, WI 53718-2148

Re: Unstable Areas Determination CCR Surface Impoundments - §257.64
Interstate Power and Light Company (IPL)
Lansing Generating Station
Lansing, Iowa

Mr. Jeffrey Maxted,

This Unstable Areas Determination has been prepared in accordance with the requirements of the United States Environmental Protection Agency (USEPA) published Final Rule for Hazardous and Solid Waste Management System – Disposal of Coal Combustion Residual (CCR) from Electric Utilities (40 CFR Parts 257 and 261, also known as the CCR Rule) published on April 17, 2015 (effective October 19, 2015) and subsequent amendments. This letter assesses the factors of one CCR unit at Interstate Power and Light Company (IPL), Lansing Generating Station (LAN) in Lansing, Iowa in accordance with the CCR Rule §257.64 Unstable Areas. For purposes of this Report, “CCR unit” refers to an existing or inactive CCR surface impoundment.

Background Information

In accordance with the requirements set forth in §257.64 of the CCR Rule a CCR unit must not be located in an unstable area. The owner or operator must consider all the following factors:

- On-site or local soil conditions that may result in significant differential settling,
- On-site or local geologic or geomorphologic features; and,
- On-site or local human-made features or events (both surface and subsurface).

Facility Specific Information

LAN is located at 2320 Power Plant Drive, Lansing, Iowa. Figure 1 provides both a topographic map and an aerial of the LAN facility location, with the approximate property boundary of the facility identified. LAN has one existing CCR surface impoundment (Figure 2), which is the LAN Upper Ash Pond.

Differential Settling

The LAN Upper Ash Pond was constructed in 1974 in a valley directly south of the LAN generating station. The construction took place within the valley with the east and south side of the Upper Ash Pond being constructed against naturally occurring ground surface. The north and west sides of the impoundment were constructed of dredge spoil medium to fine sand from Mississippi River maintenance dredging.

To allow construction of the impoundment, the Unnamed Creek #1 was rerouted to run along the west side of the valley between the impoundment and a County Road on the east side slope of the valley, Figure 1. Soil investigations completed at the time of construction indicate the valley is underlain by a medium dense deposit of sand and gravel over the full valley floor with loose to very loose river silt laying on top of the sand and gravel at the north end of the planned Upper Ash Pond. Only organic topsoil was removed prior to constructing the two embankment sides of the LAN Upper Ash Pond and the river silt remains in the foundation at the northern end of the LAN Upper Ash Pond. The details of the LAN Upper Ash Pond construction are shown in drawings prepared by Sargent & Lundy in 1974, Exhibit A.

The LAN Upper Ash Pond was constructed on foundation soils that are medium dense sand and gravel in the southern part of the Pond and are suitable foundation soils. In the northern end of the pond the sand and gravels have an overlying river silt deposit that is loose to very loose and is saturated due to the Mississippi River. The original construction of the LAN Upper Ash Pond was completed over the top of the river silt which has no clay-like properties (Exhibit B) and supported the embankment without substantial settlement after construction.

In 2015, a subsurface soil investigation was undertaken to collect soil samples and determine the in-situ density of the north and west embankments and the underlying foundation soil. The soil borings were undertaken with hollow stem augers and sampling was completed with a standard split spoon (Figure 2). The density information along with soil test results for water content, grain size, and Atterberg limits (Exhibit B) indicate the current conditions of the embankments as they were constructed in 1974.

The test results indicate that the embankment is constructed of uniform, fine to medium sand (SP). The sand was compacted to medium dense to dense consistency as shown by the SPT results. Below the embankment, the two northern borings SB-1 and SB-7 (Figure 2) show that a very loose to loose silt is present under the embankment overlying a medium dense gravel. In borings SB-3 and SB-5 (Figure 2) the silt is thin and overlies the same gravel. The silt deposit in the two northern borings is from backwater deposition by the Mississippi River prior to the installation of the LAN Upper Ash Pond and the thin silt layer to the south is natural deposition from flooding of the Unnamed Stream #1.

The silt layer under the northern embankment of the LAN would have compressed under the load from installing the embankment in 1974. Annual inspections of the embankment and topographic surveys completed in 2015 show the northern embankment was built to its design elevation and has not settled since the embankment was installed. The loose silt is susceptible to liquefaction

settlement from an earthquake. However, the LAN site is not in an area of strong ground motion to induce liquefaction.

The Iowa Bedrock Survey Map (Exhibit C), available from the Iowa Geology and Water Survey, July 2013 indicates that bedrock is at an approximate elevation of 560 feet (depth of 90 feet below top of embankment) in the northern part of the LAN Upper Ash Pond and rises in elevation moving south up the valley of the Unnamed Stream #1.

Based on the known geotechnical information, LAN impoundments are not susceptible to significant differential settlement from liquefaction of the silt layer. Additionally, annual inspections of the embankments for the last 4 years have indicated no observable areas of differential settlement on the embankments.

Geologic and Geomorphologic Features

The Bedrock Geologic Map of Iowa (Exhibit C) shows that the site contains up to five types of bedrock formations: Prairie du Chien Group, St. Peter Sandstone, Jordan Sandstone, St. Lawrence, and Lone Rock Formations. The formations are comprised of dolomite and siltstone. The Iowa Bedrock Survey Map available from the Iowa Geology and Water Survey, July 2013 indicates that bedrock is at an approximate elevation of 560 feet (depth of 90 feet below top of embankment) in the northern part of the LAN Upper Ash Pond and rises in elevation moving south up the valley of the Unnamed Stream #1.

Karst formations in Iowa are predominately in the northeast part of the state, see Exhibit D, which is where LAN is located. An Iowa Department of Natural Resources map of known and potential karst terrain and/or paleosinks (sinkholes) near LAN has also been included in Exhibit D. This map shows that the LAN is located inside an area potentially susceptible to karst formations. A sinkhole has been identified approximately 2,000 feet east of the LAN Upper Ash Pond. The mapped location of the sinkhole is approximately 300 feet higher than the impoundment. As presented within the SCS Engineers Unstable Areas Compliance Demonstration¹ for the onsite landfill, The Galena Group, which consists of limestone and dolostone, has identified paleosinks within Allamakee County and is stratigraphically above the weathered sandstone unit observed in many borings installed throughout the LAN Upper Ash Pond and the landfill site. As a result, it is unlikely that karst conditions are present below the impoundment.

Several figures and tables have been included in Exhibit E which have been provided by SCS Engineers. These figures show that the local shallow groundwater direction descends from the bluffs as well as generally moving northward to the Mississippi River. The measurement of occasional downward gradient in the nested wells likely results from the silt layer discussed above acting as an aquitard separating the upper ground water in the valley from the deeper ground water of the Mississippi River elevation. Additionally, water recharging the valley groundwater from operations at LAN is at or above a pH of 7. As a result, there is no risk for the formation of paleosinks.

¹ Unstable Areas Demonstration Lansing Landfill, SCS Engineers, October 2018

Human-made Features or Events

Generally, man-made risks to the stability of CCR impoundments can include such events as: large dam failure, failure due to improper cut and fill during construction, excessive drawdown of groundwater, extreme fluctuations in flooding from human-made changes, or failure due to underground mining. Based on the information provided herein, the LAN Upper Ash Pond are is not susceptible to anthropogenic activities.

Unstable Areas Determination

After review of the reasonably and readily available documentation, we determine that the LAN Upper Ash Pond is not located in unstable area.

Qualified Professional Engineer Certification

The owner or operator of the CCR unit must obtain a certification from a qualified professional engineer attesting that the documentation as to whether a CCR unit meets the requirements 40 CFR 257.64(b).

To meet the requirements of 40 CFR 257.64(c), I Mark W. Loerop hereby certify that I am a licensed Professional Engineer in the State of Iowa; and that, to the best of my knowledge, all information contained in this document is correct and the document was prepared in compliance with all applicable requirements in 40 CFR 257.64.



By:

Name:

Date:

cc: Tony Morse, Alliant Energy
Robert Solak, Hard Hat Services

att: Figure 1 – Site Location
Figure 2 – Soil Boring Locations
Exhibit A – 1974 Drawings
Exhibit B – 2015 Investigation
Exhibit C – Iowa Bedrock Map
Exhibit D – Iowa Karst Maps
Exhibit E – Groundwater Info from SCS Engineers

MWL/tjh/MWL

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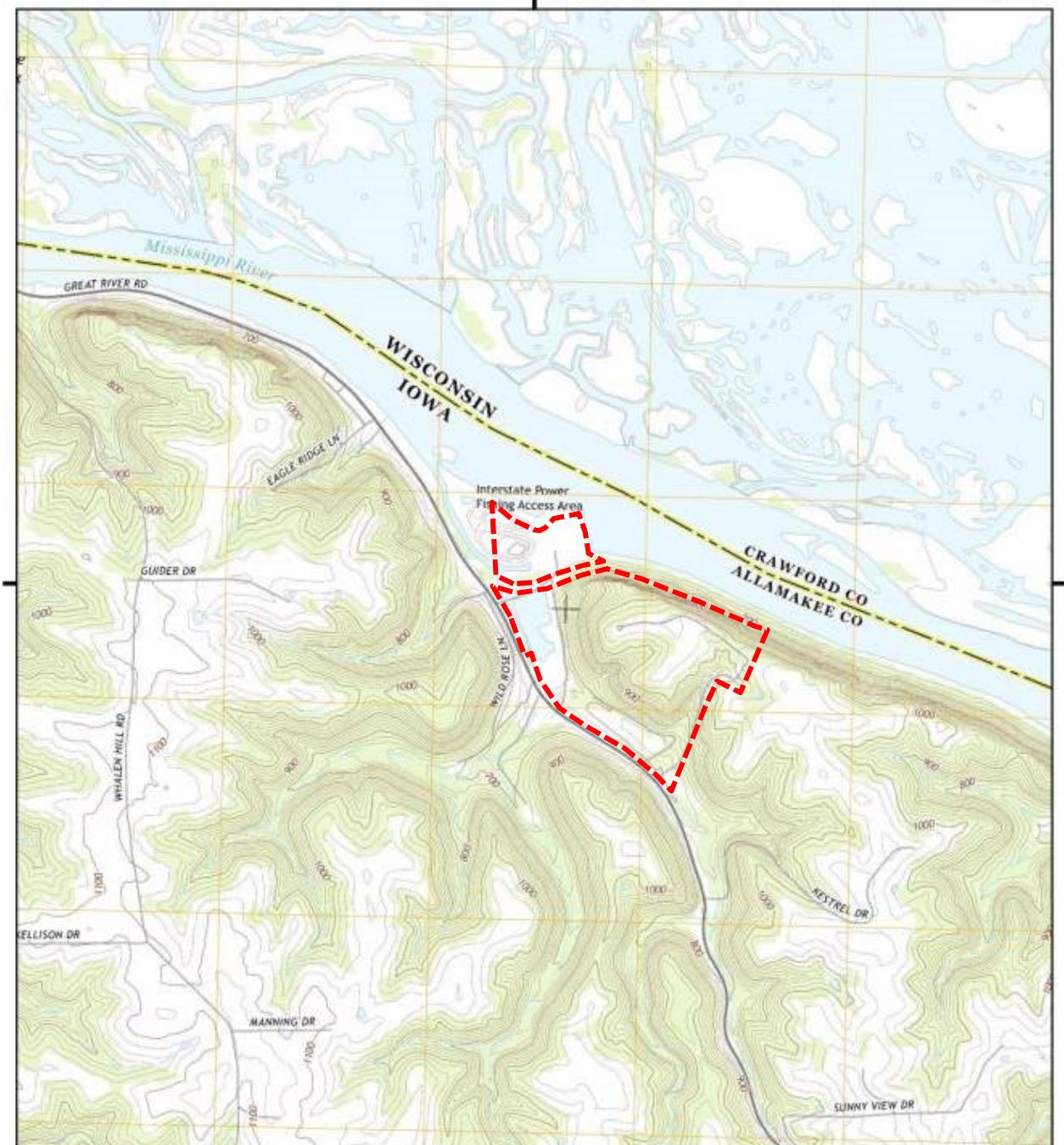
FIGURES

Alliant Energy
Interstate Power and Light Company
Lansing Generating Station
Lansing, Iowa

Unstable Area Determination
Figure 1 – Site Location
Figure 2 – Soil Boring Locations

Historical Topo Map

2013

**Historical Aerial Photo**

----- Approximate Property Boundary



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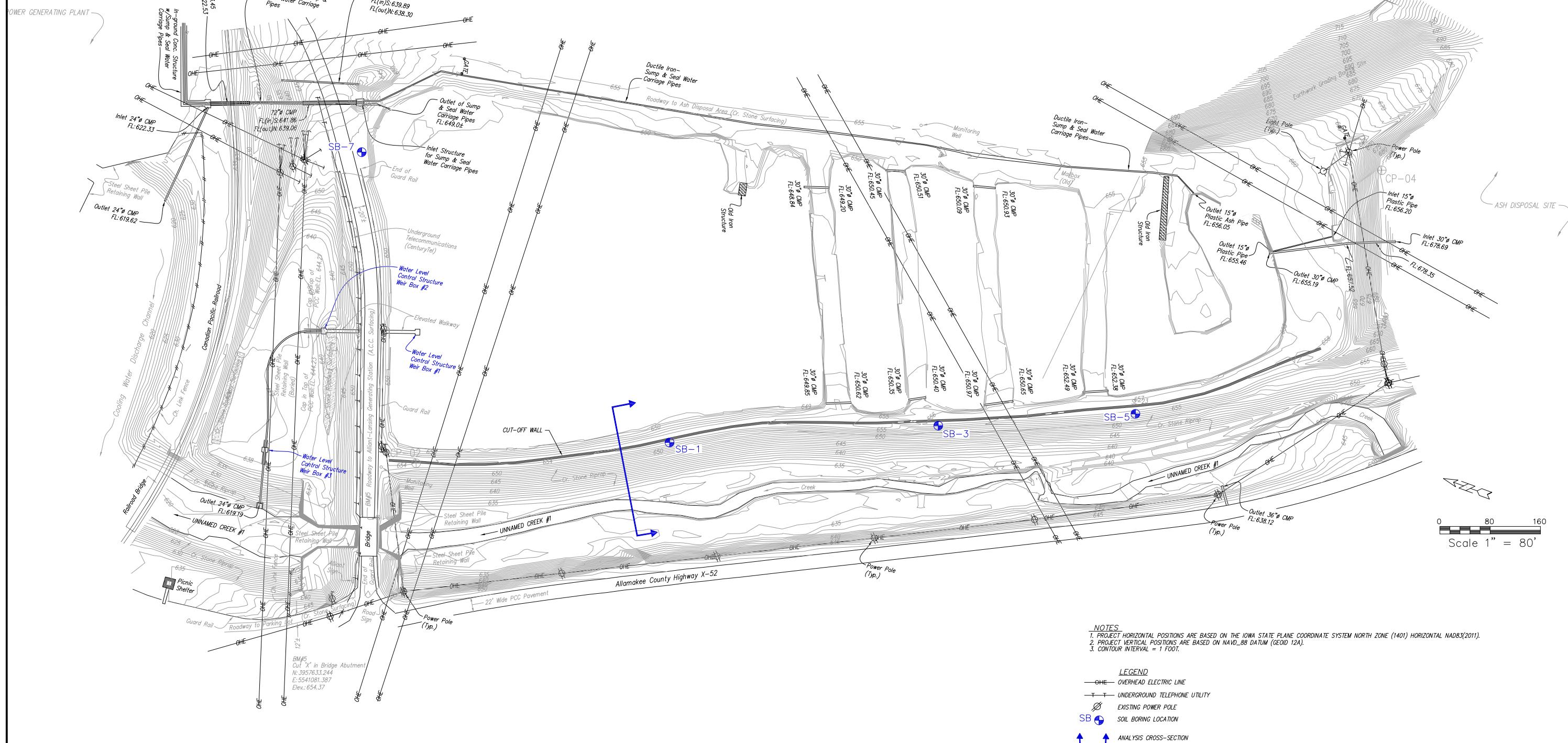
Site Location
Lansing Generating Station
Intersate Power and Light Company

Drawing
Figure 1
Date
6/7/2016

UPPER AND LOWER CCR POND TOPOGRAPHIC SURVEY AND LOWER CCR POND BATHYMETRY

at
ALLIANT LANSING POWER GENERATING STATION

for

INTERSTATE POWER & LIGHT COMPANY - ALLIANT ENERGY
BEING IN PART OF SECTION 2, TOWNSHIP 98 NORTH, RANGE 3 WEST OF THE FIFTH PRINCIPAL MERIDIAN, ALLAMAKEE COUNTY, IOWA.

- NOTE:**
1. SURVEY INFORMATION PROVIDED ABOVE WAS COMPILED BY MOHN SURVEYING, INC.
1890 GREAT RIVER ROAD LANSING, IOWA 52151, APRIL 2015.
 2. ALLIANT ENERGY REQUIRES 20 FEET OVERHEAD SEPARATION DISTANCE FOR EQUIPMENT OPERATING UNDER POWERLINES.

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OF HARD HAT SERVICES AND IS
NOT TO BE REPRODUCED,
CHANGED, OR COPIED IN ANY FORM
OR MANNER WITHOUT PRIOR
WRITTEN PERMISSION. ALL RIGHTS
RESERVED.



REV

DATE

BY

APP

DESCRIPTION

SCALE: AS SHOWN DATE: 5-19-16
DRAWN BY: JFD CHECKED BY: CTS APPROVED BY: MWL
HARD HAT SERVICES™
Engineering, Construction and Management Solutions

CLIENT / LOCATION
INTERSTATE POWER AND LIGHT (IPL)
LANSING GENERATING STATION PROJECT
2320 POWER PLANT DR
LANSING, IA 52151


DRAWING DESCRIPTION
SOIL BORING AND
SLOPE STABILITY CROSS-SECTION LOCATION

JOB 154.018.012.002
SHT. FIGURE 2
DWG. 154.018.012.002-D2

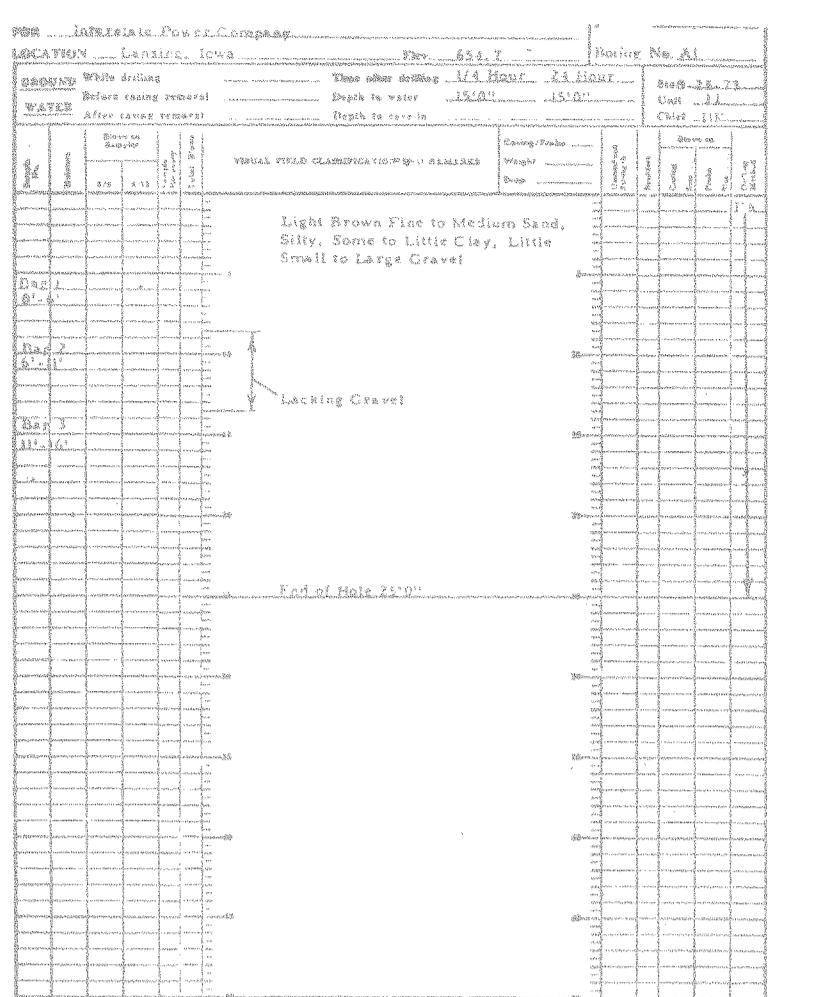
EXHIBIT A – 1974 Drawings

Alliant Energy
Interstate Power and Light Company
Lansing Generating Station
Lansing, Iowa

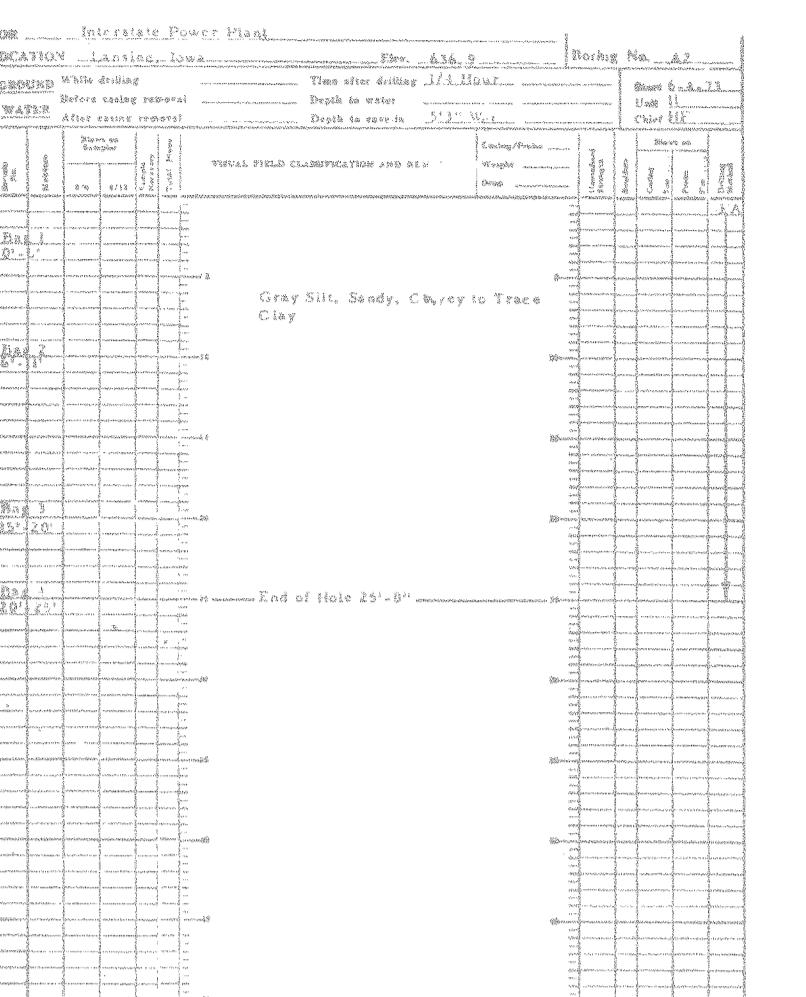
Unstable Area Determination



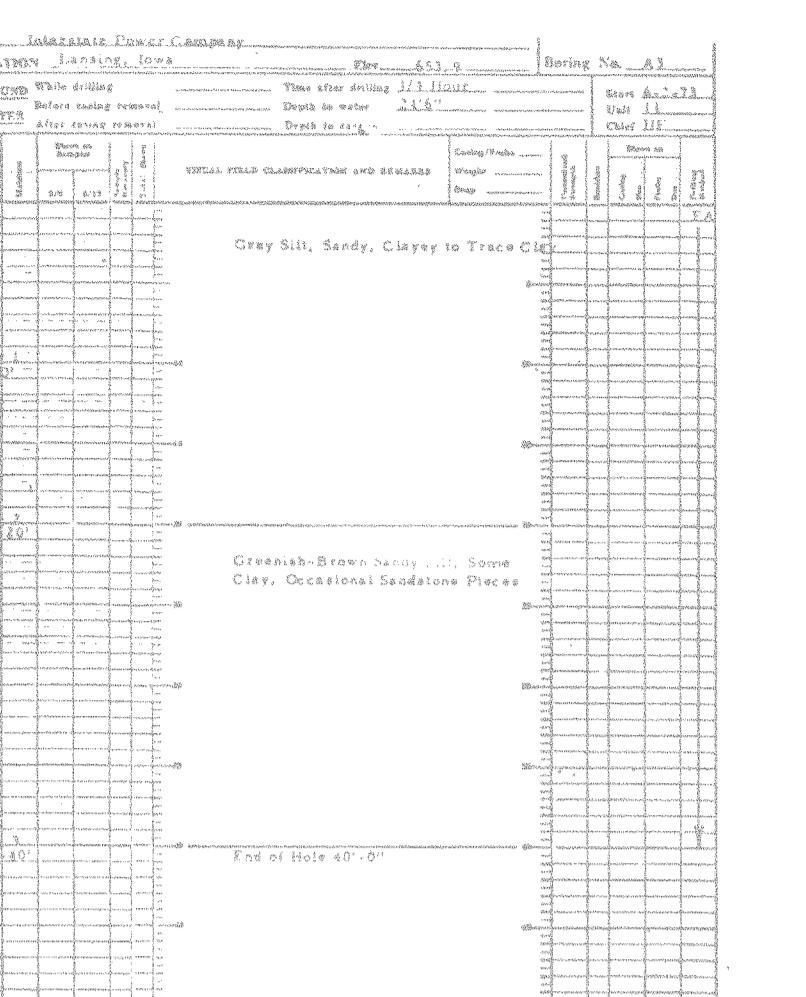
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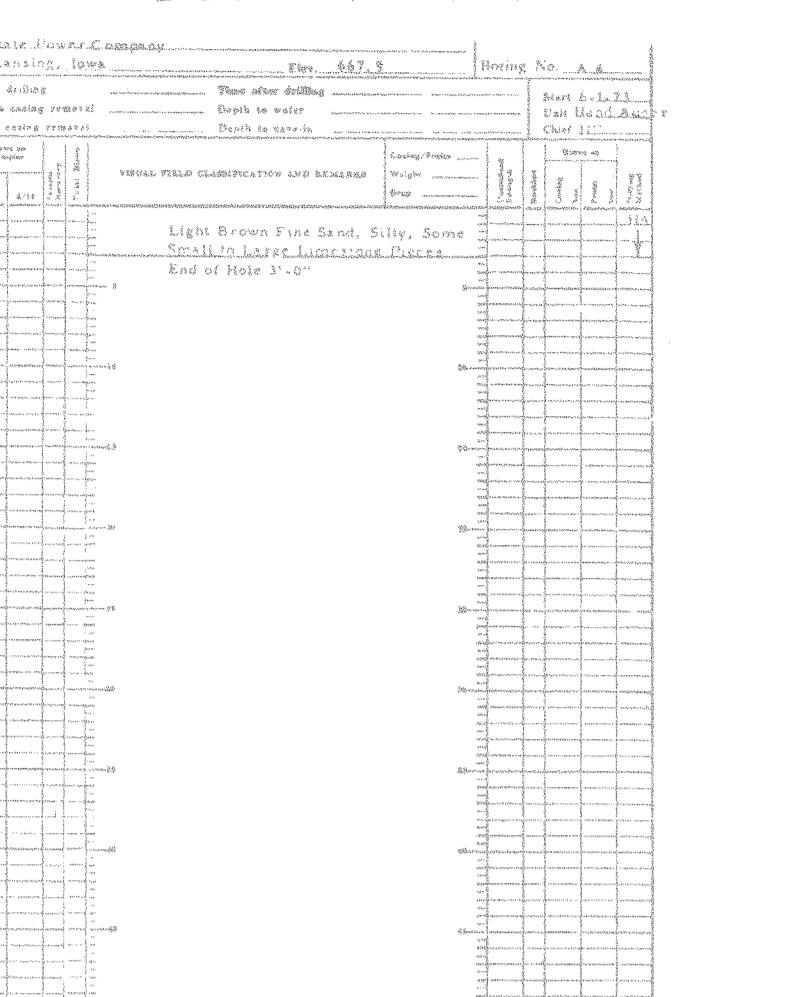
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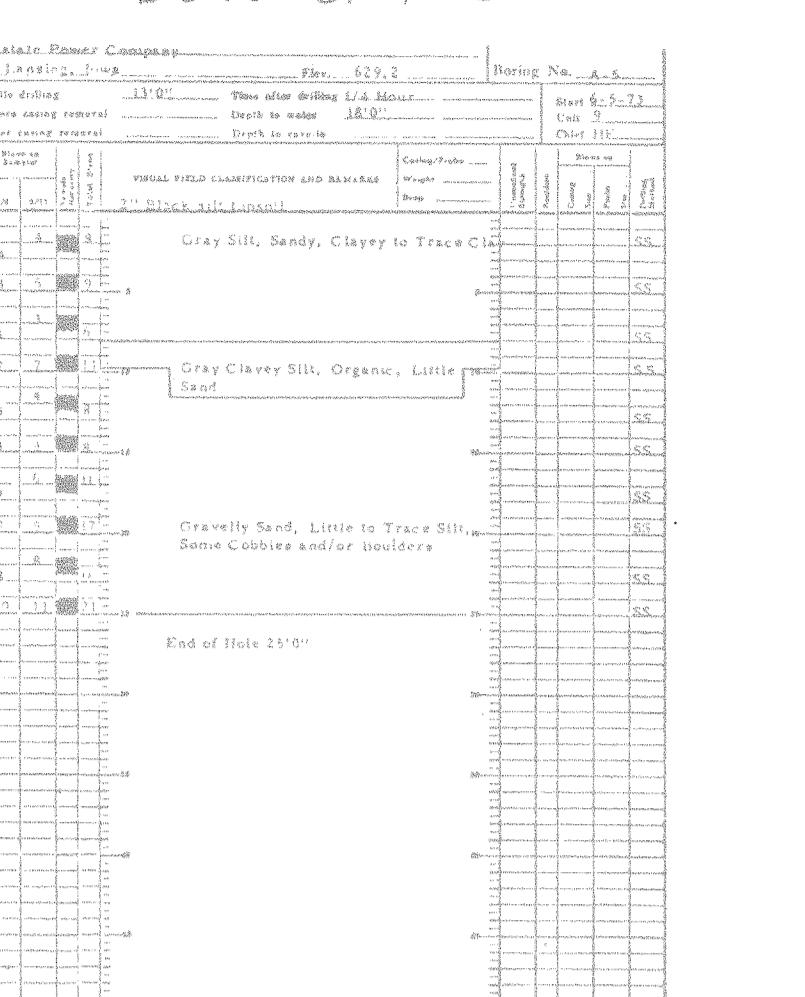
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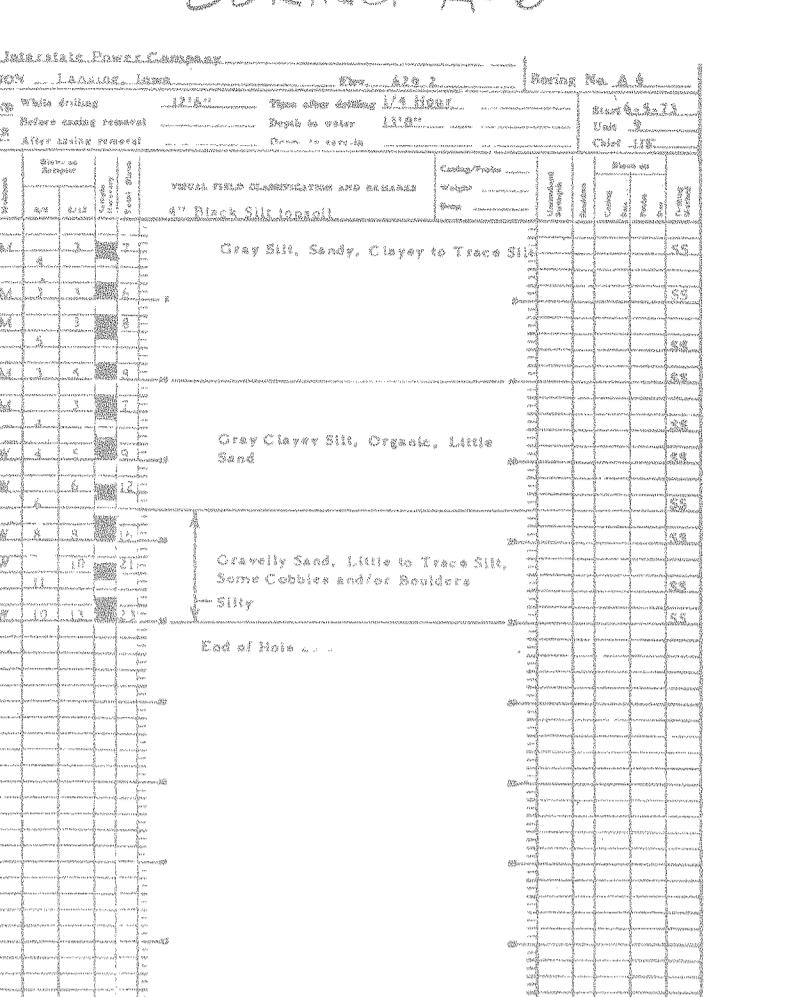
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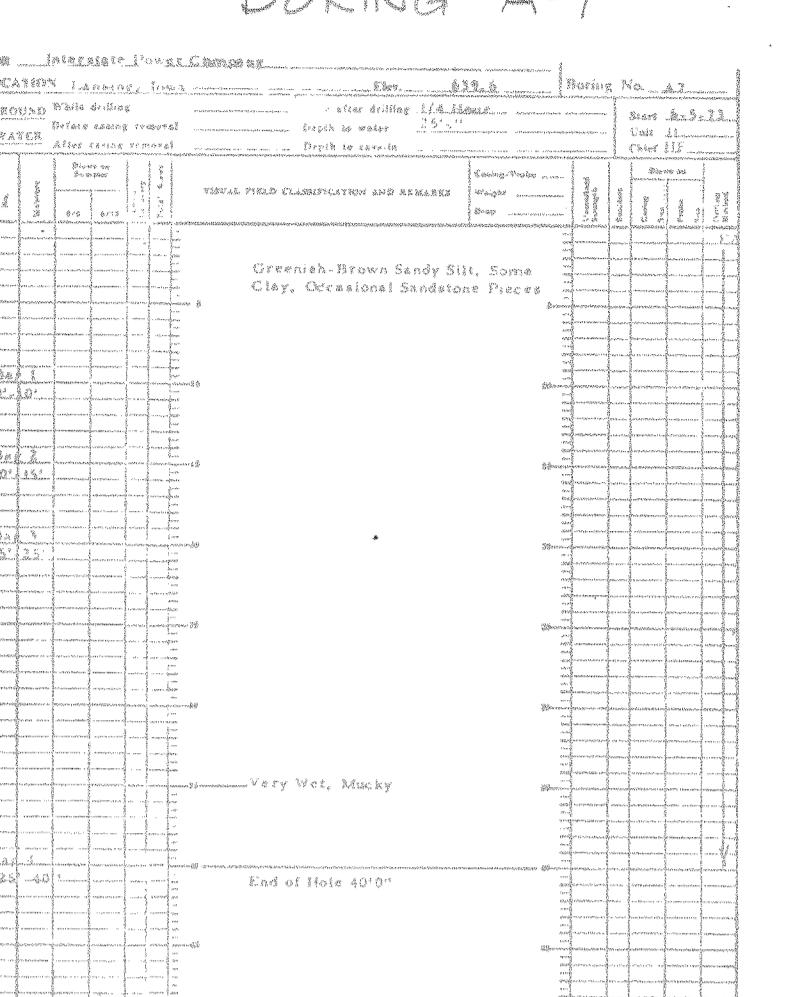
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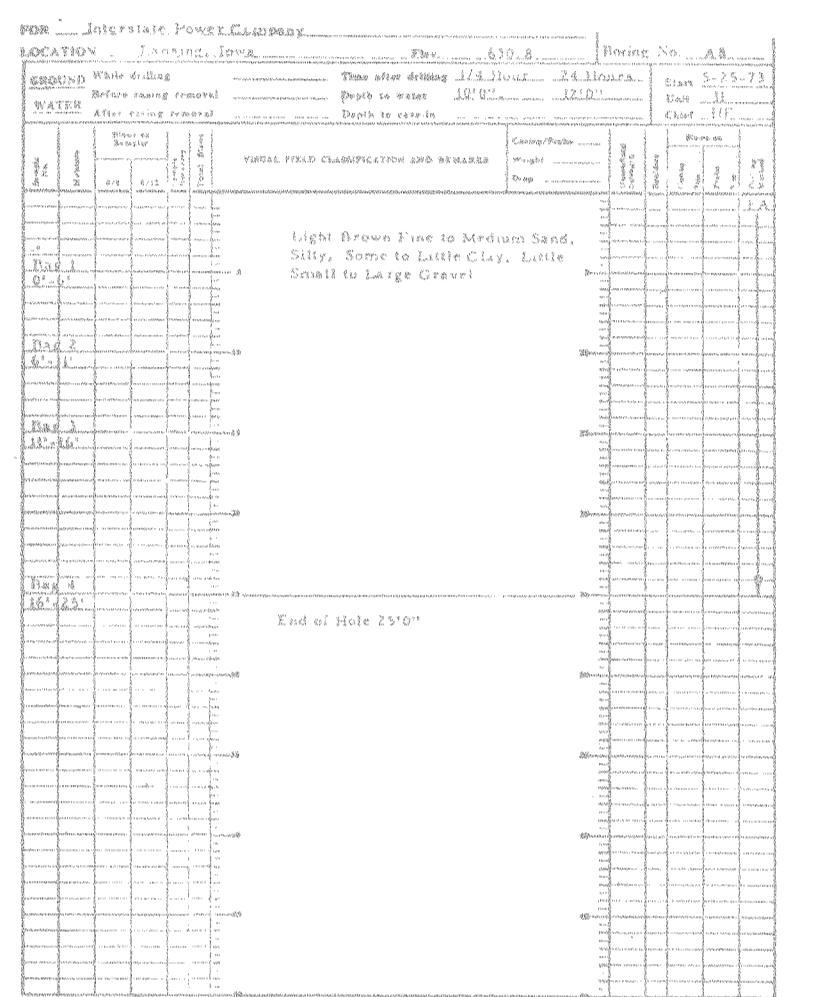
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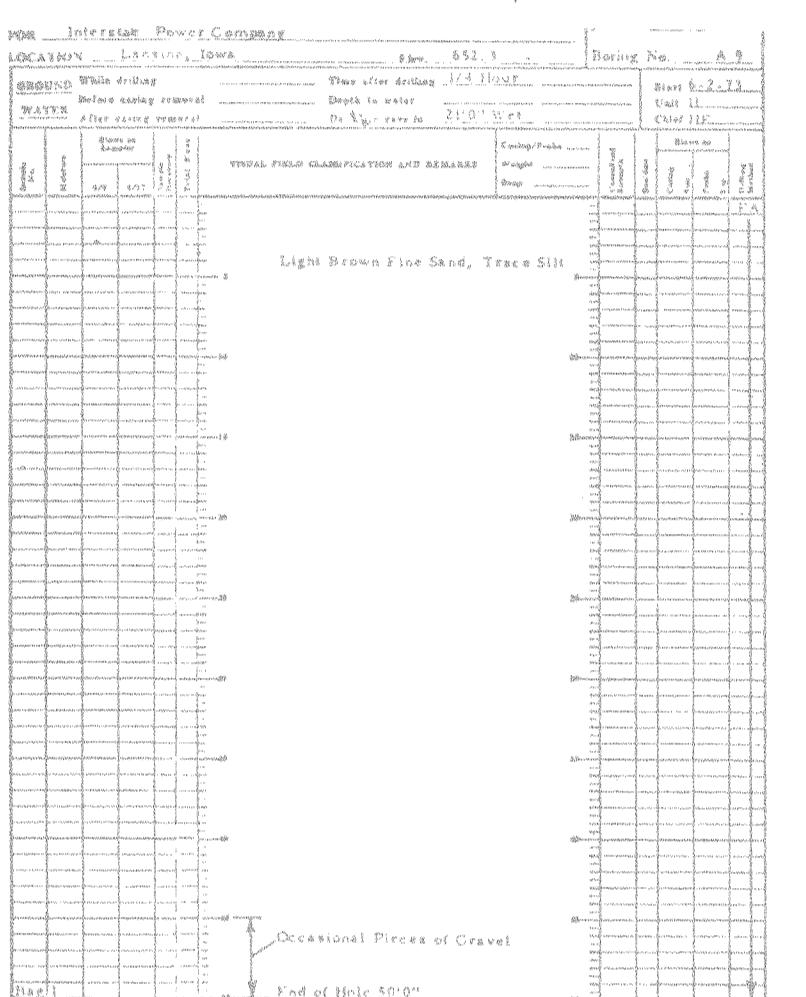
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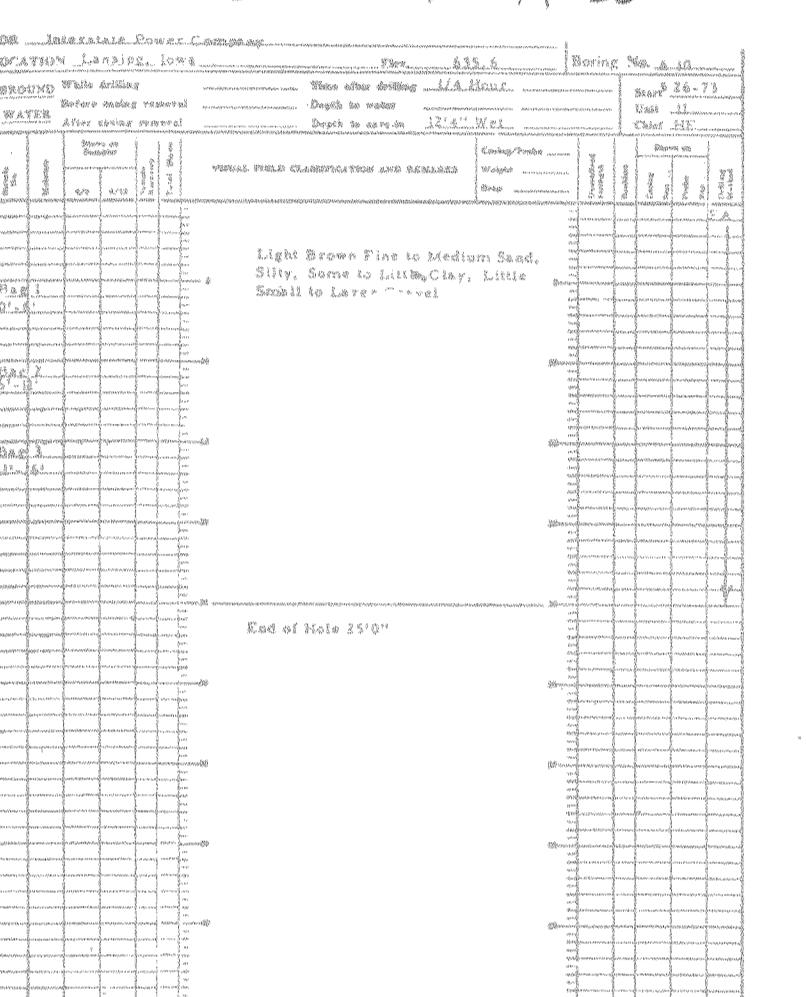
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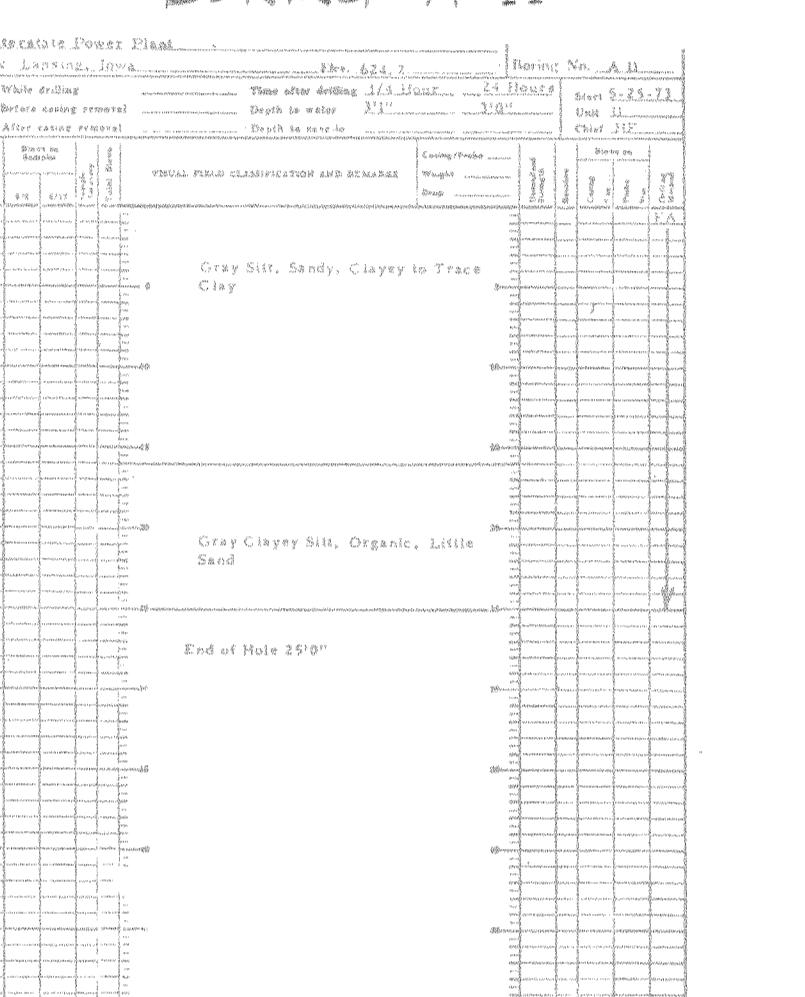
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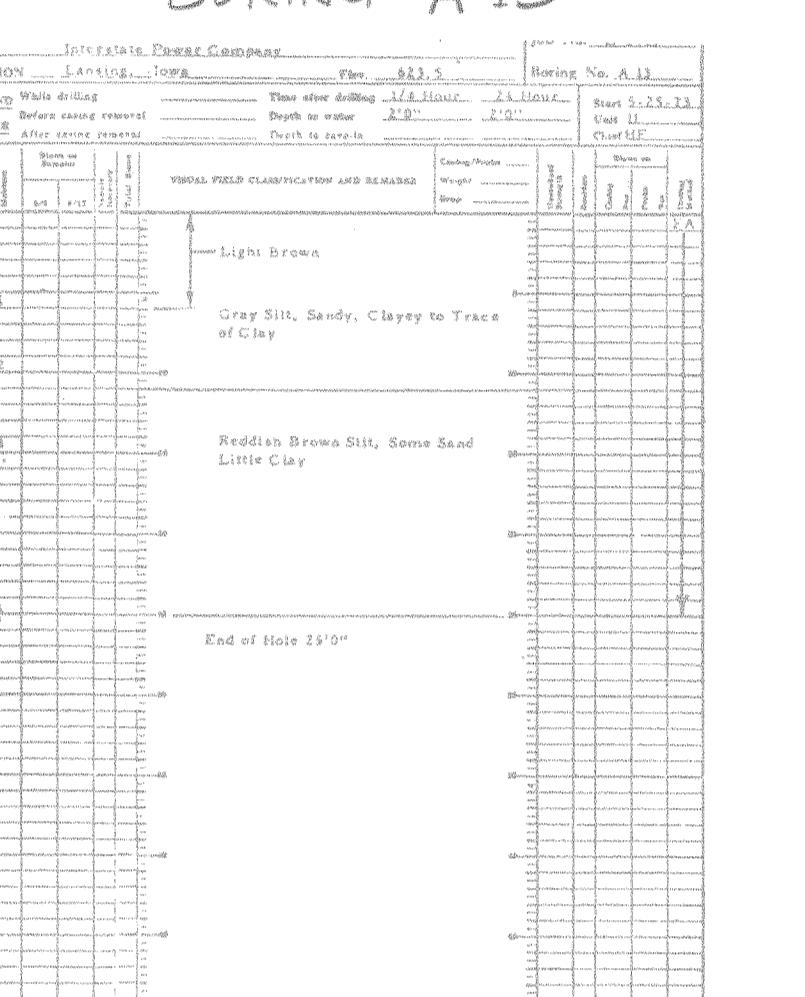
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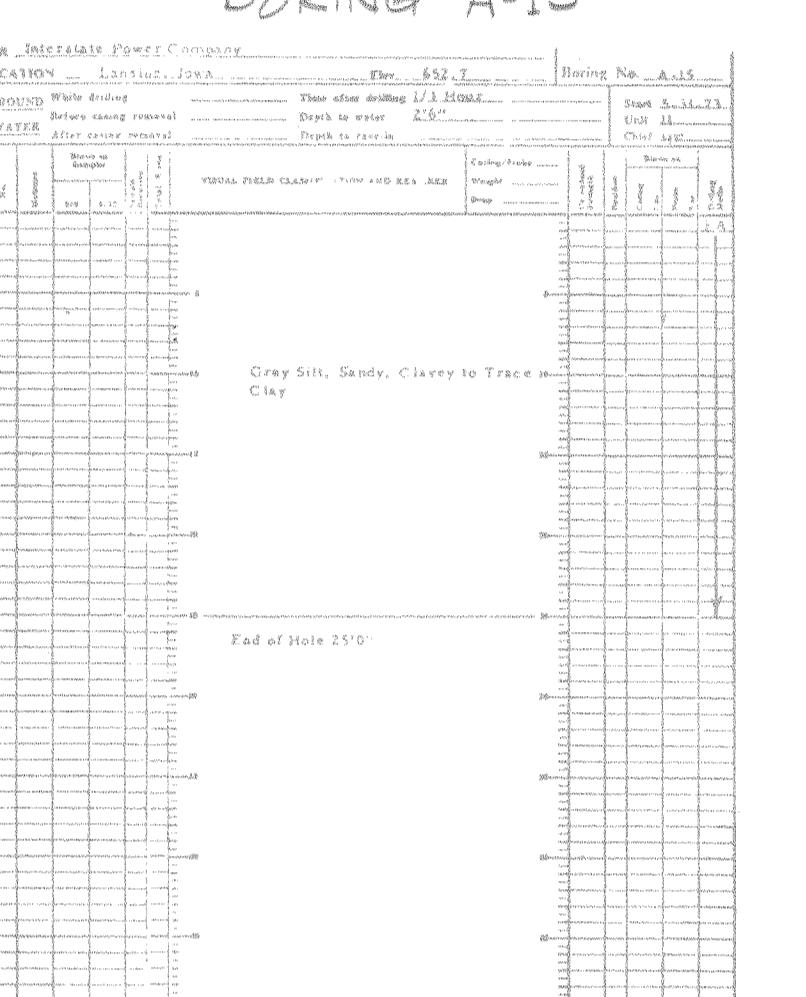
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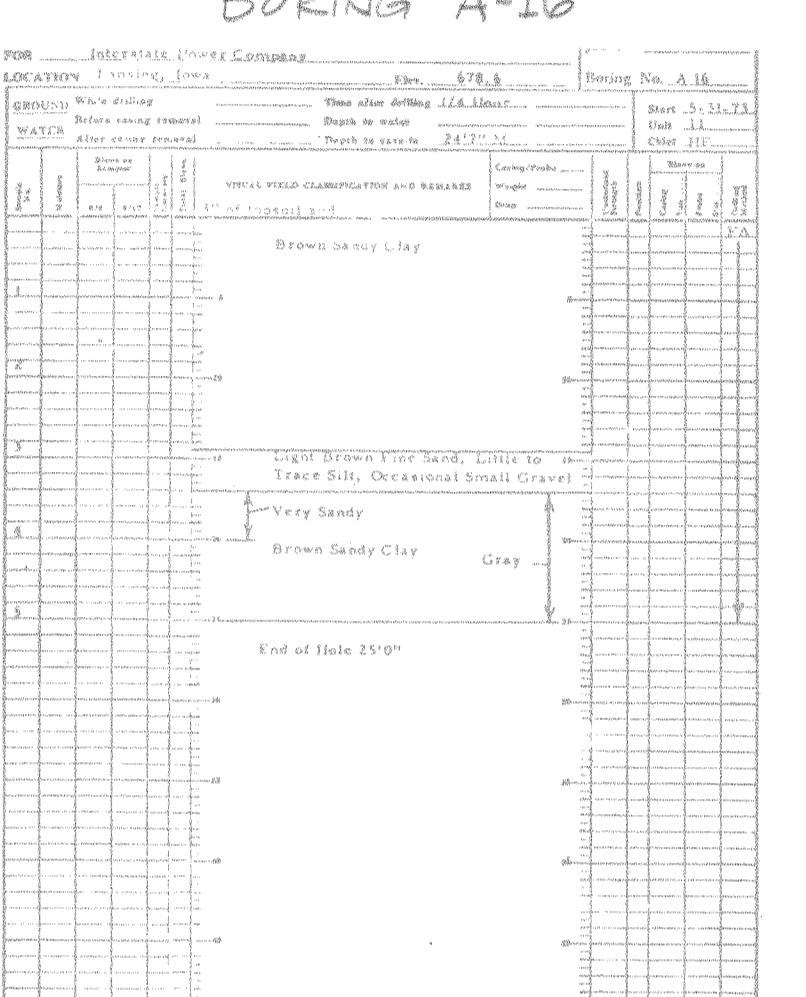
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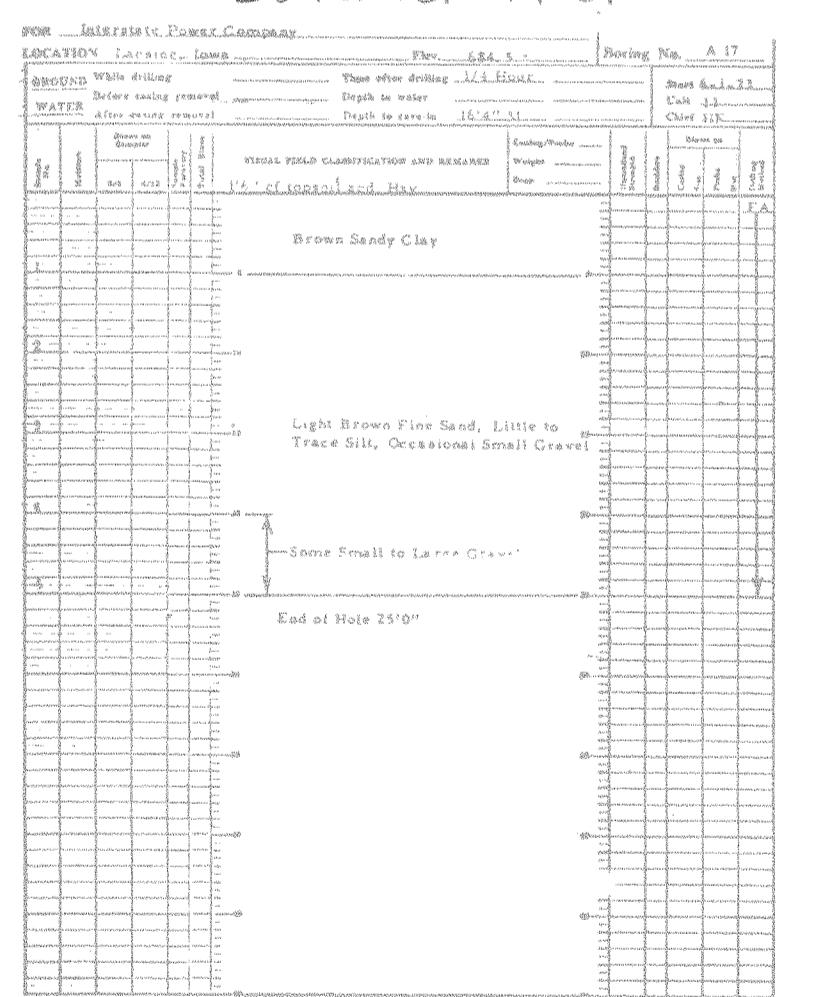
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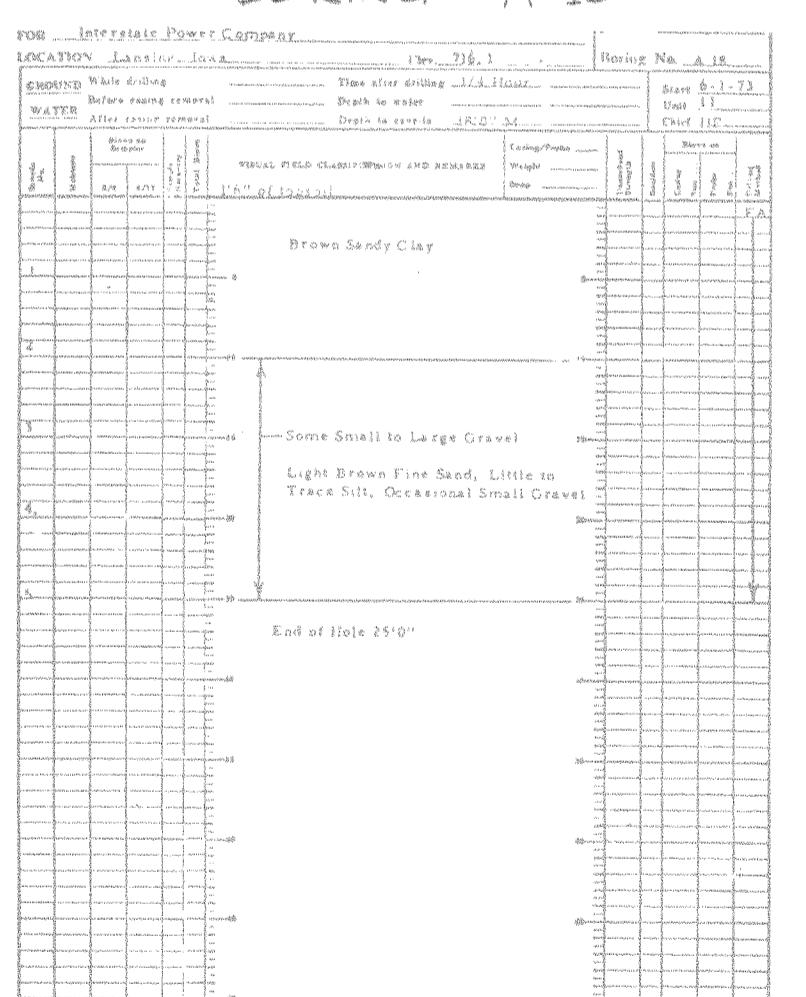
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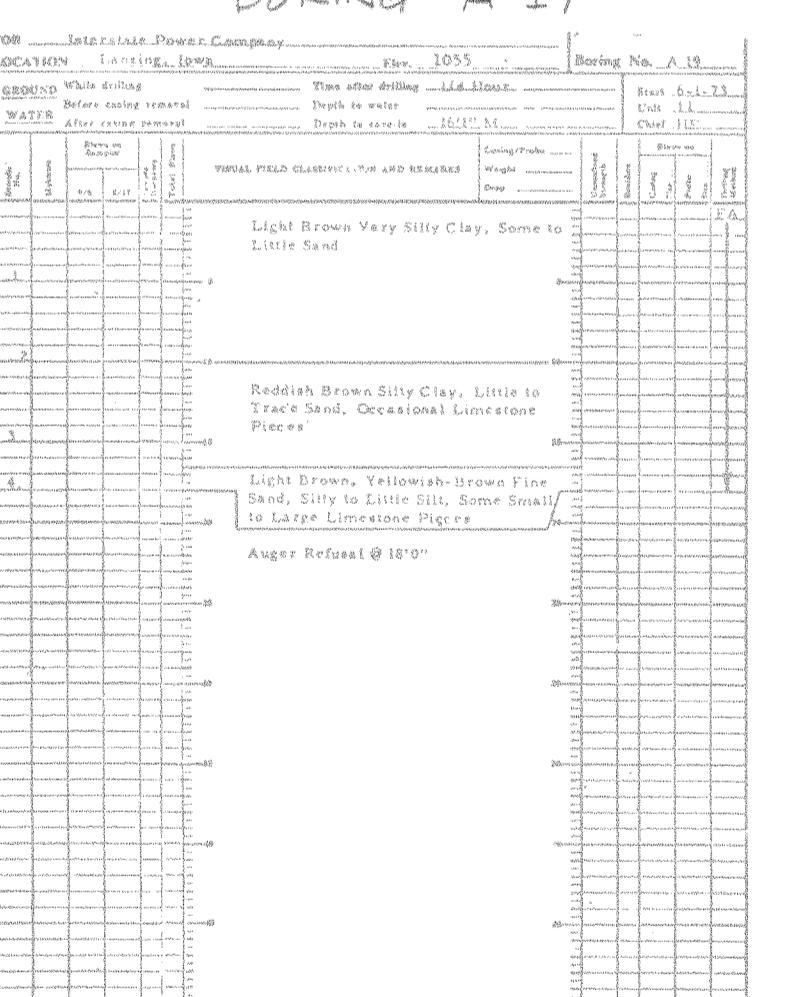
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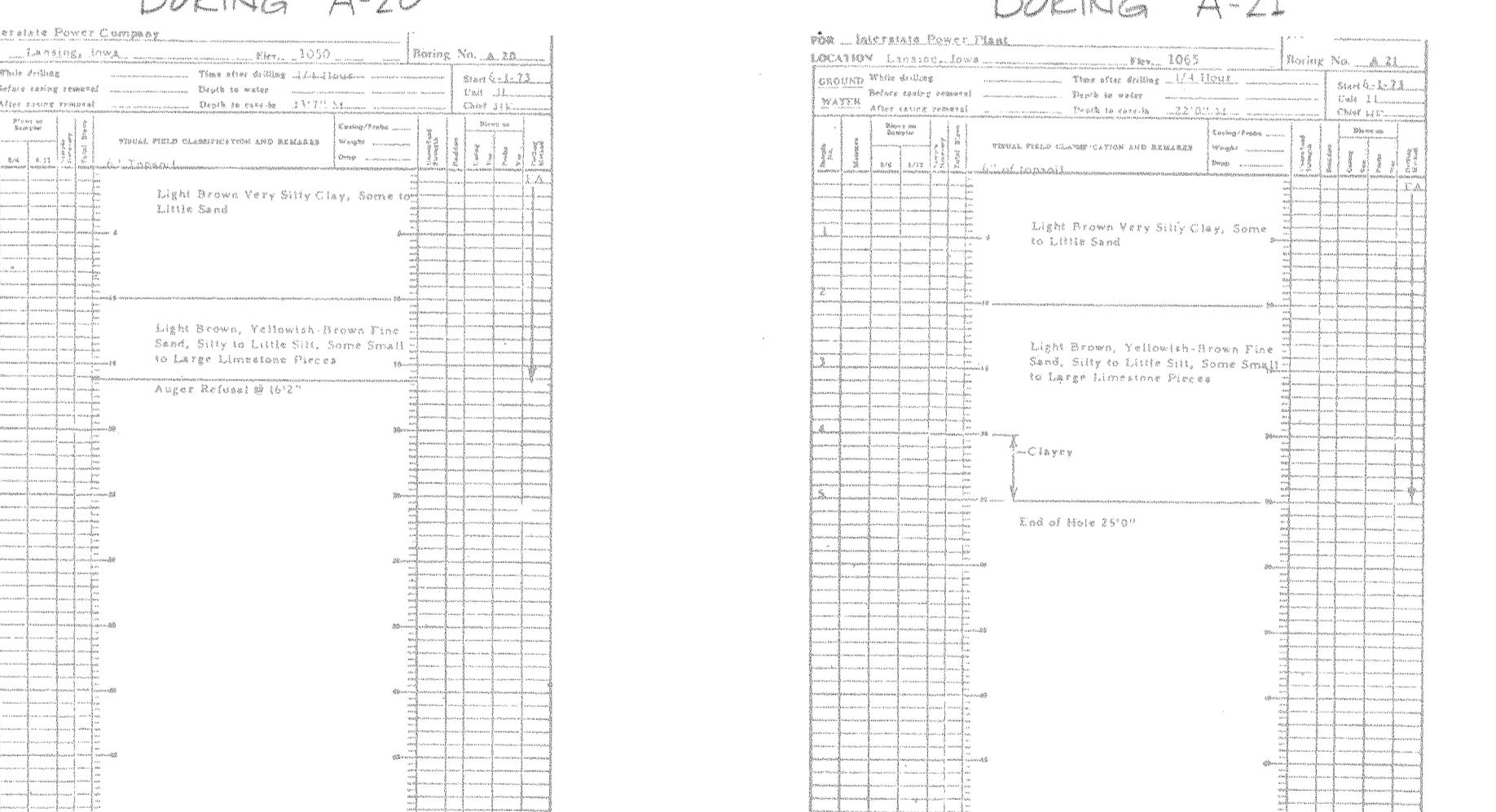
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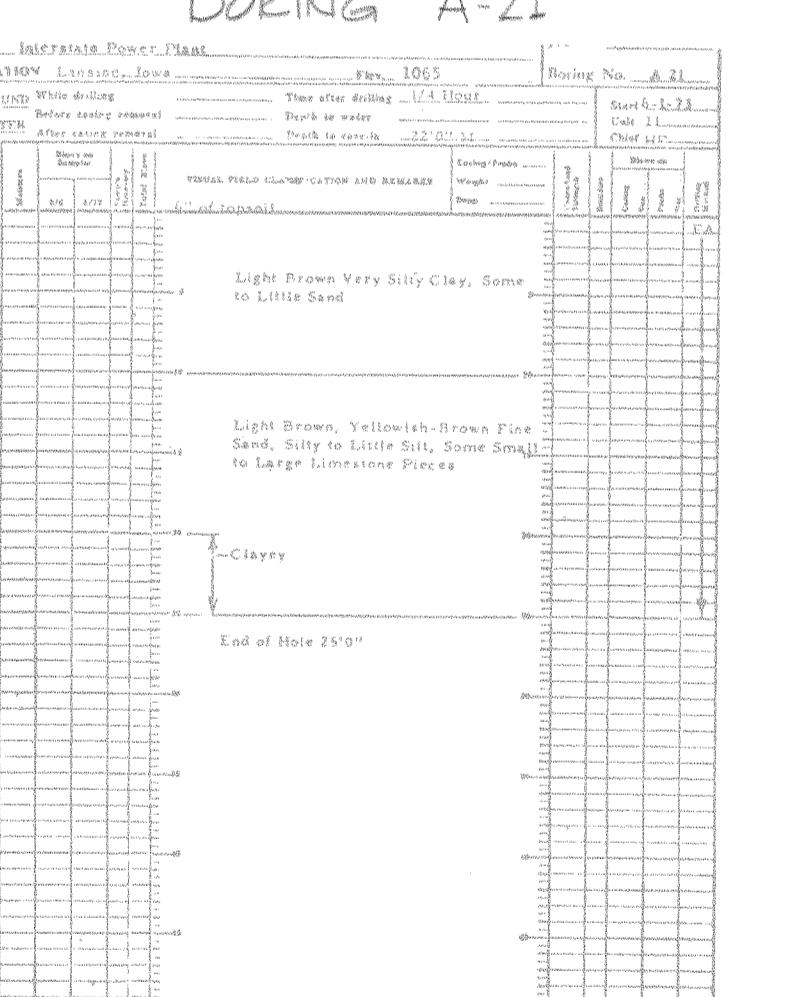
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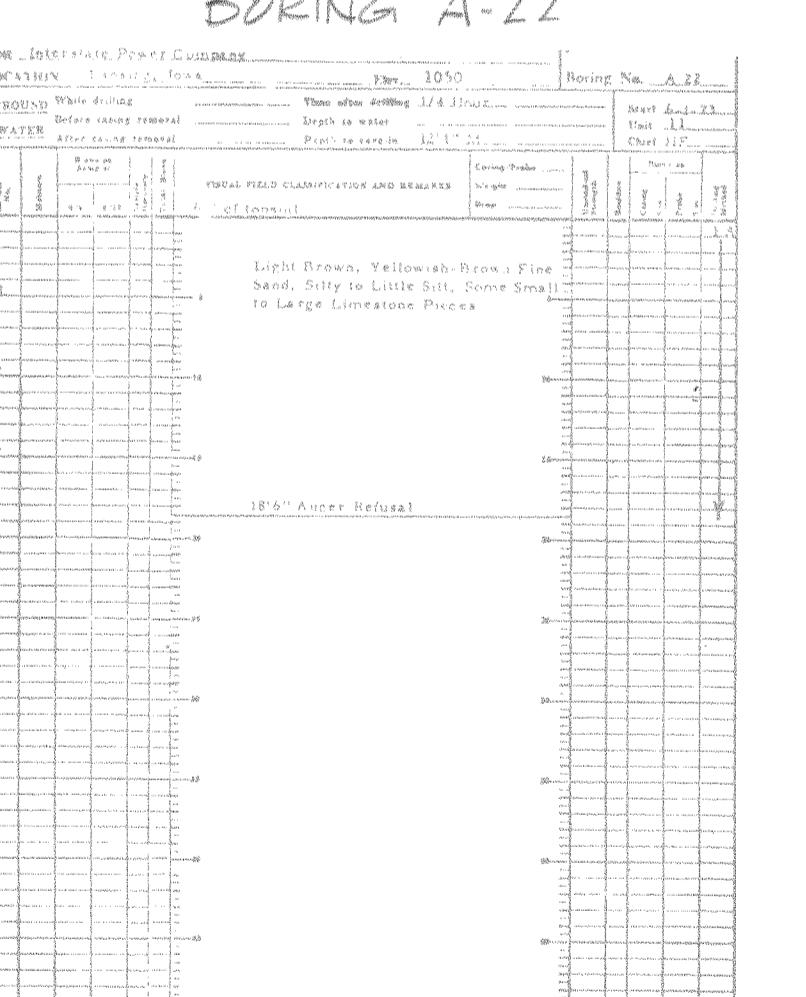
BORING A-20



BORING A-21



BORING A-22



REFERENCE DRAWINGS

NOTES

- LEGEND FOR DRILLING METHODS
- SS: Split-Spoon - 2^{1/2} O.D.
 - DC: Drove Gasing - 2^{1/2} I.D., except where noted
 - WO: Washed Out
 - RC: Rock Coring
 - RQD: Rock Quality Designator
 - FA: Flight Auger
 - HA: Hand Auger

I hereby certify that this plan, specification or report was prepared by me or under my direct personal supervision and control of a duly licensed Professional Engineer under the laws of the State of Iowa.

Signed _____ Date _____

H. Bergstrom, P.E. Reg. No. 4480

Date 9-10-73

By H. Bergstrom, P.E. Reg. No. 4480

Date 9-10-73

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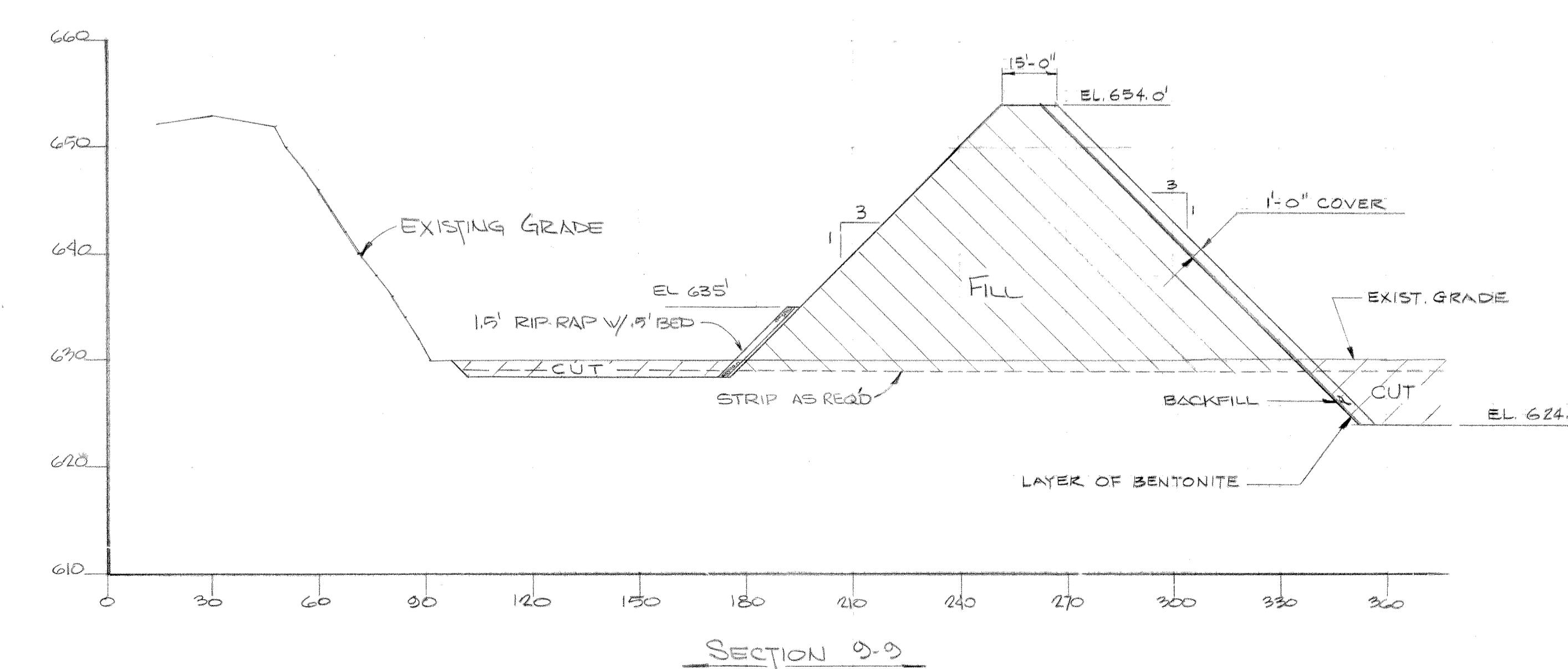
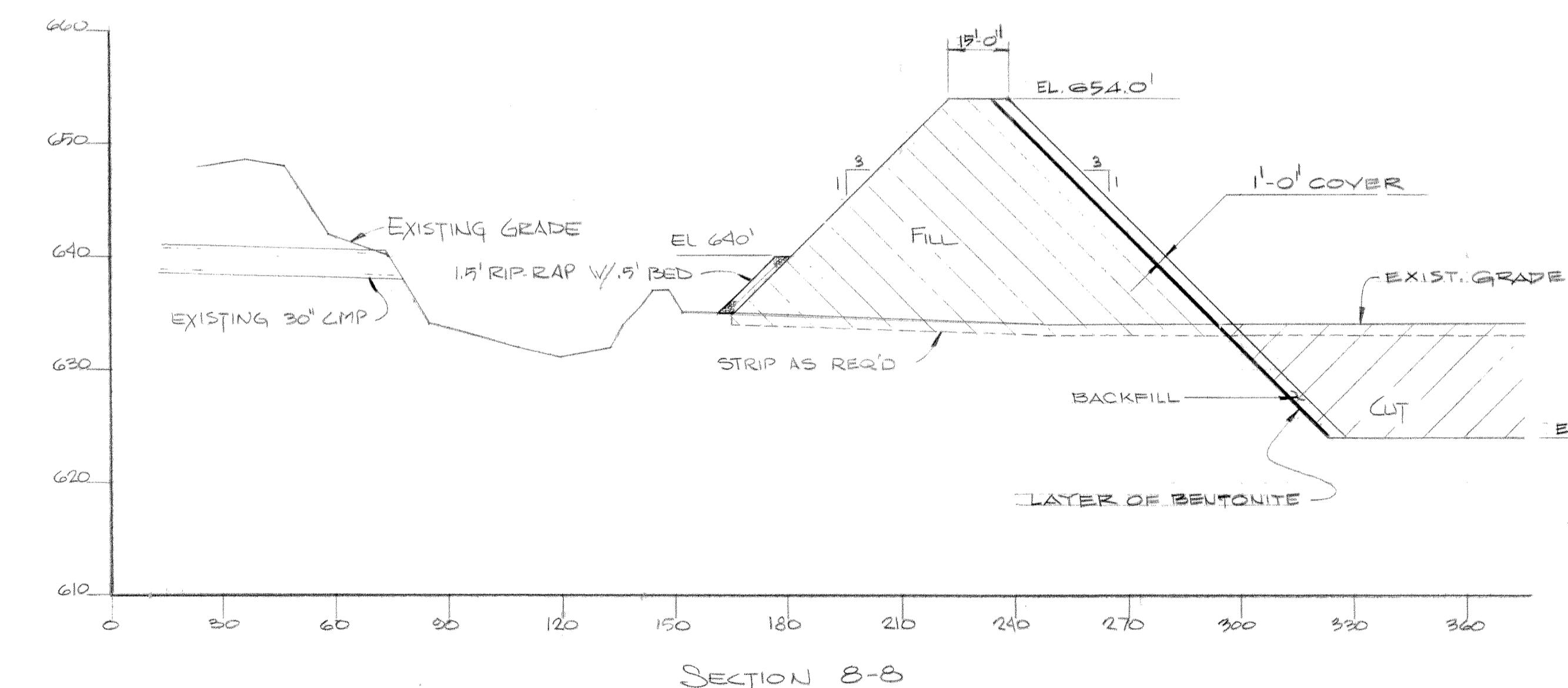
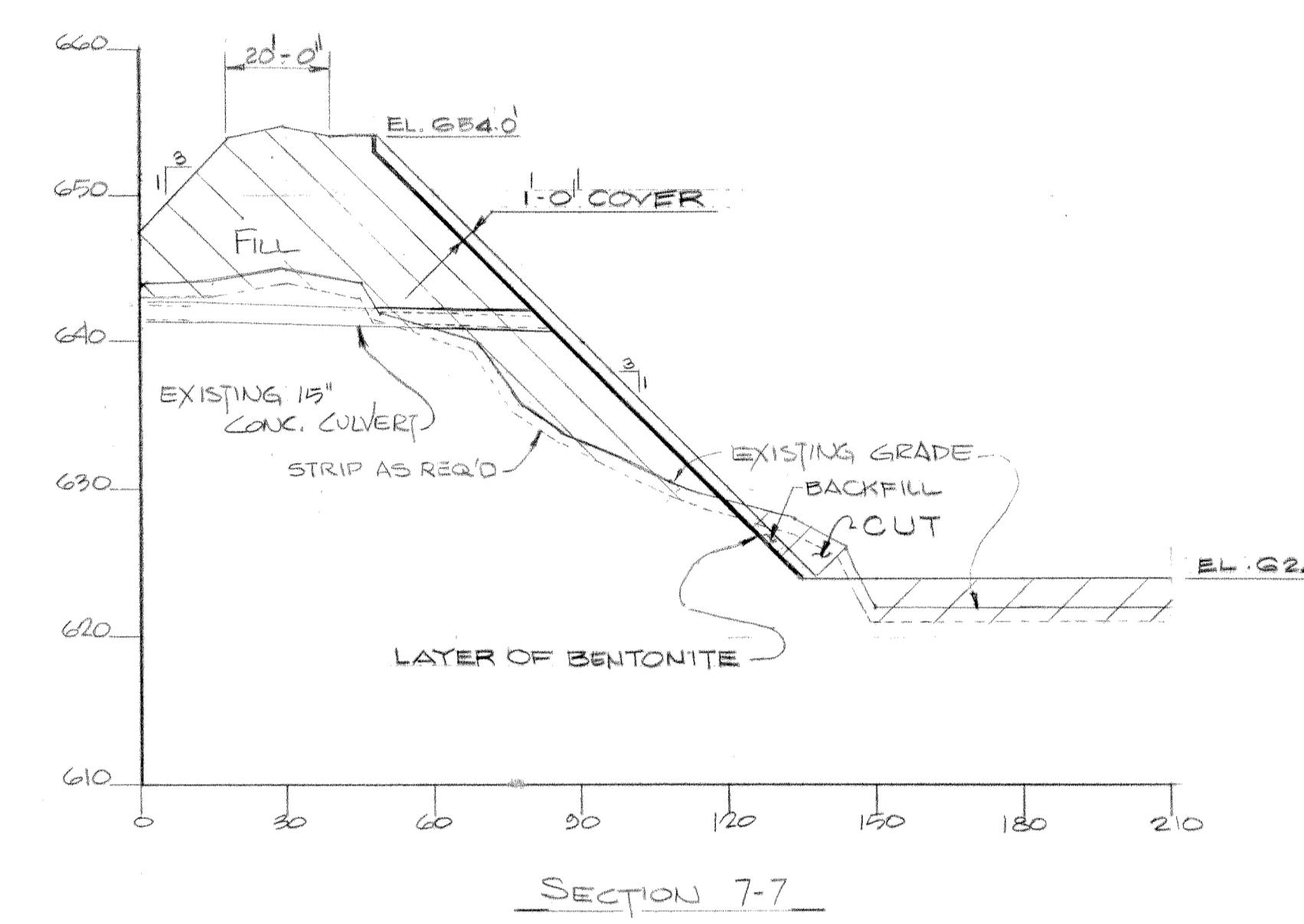
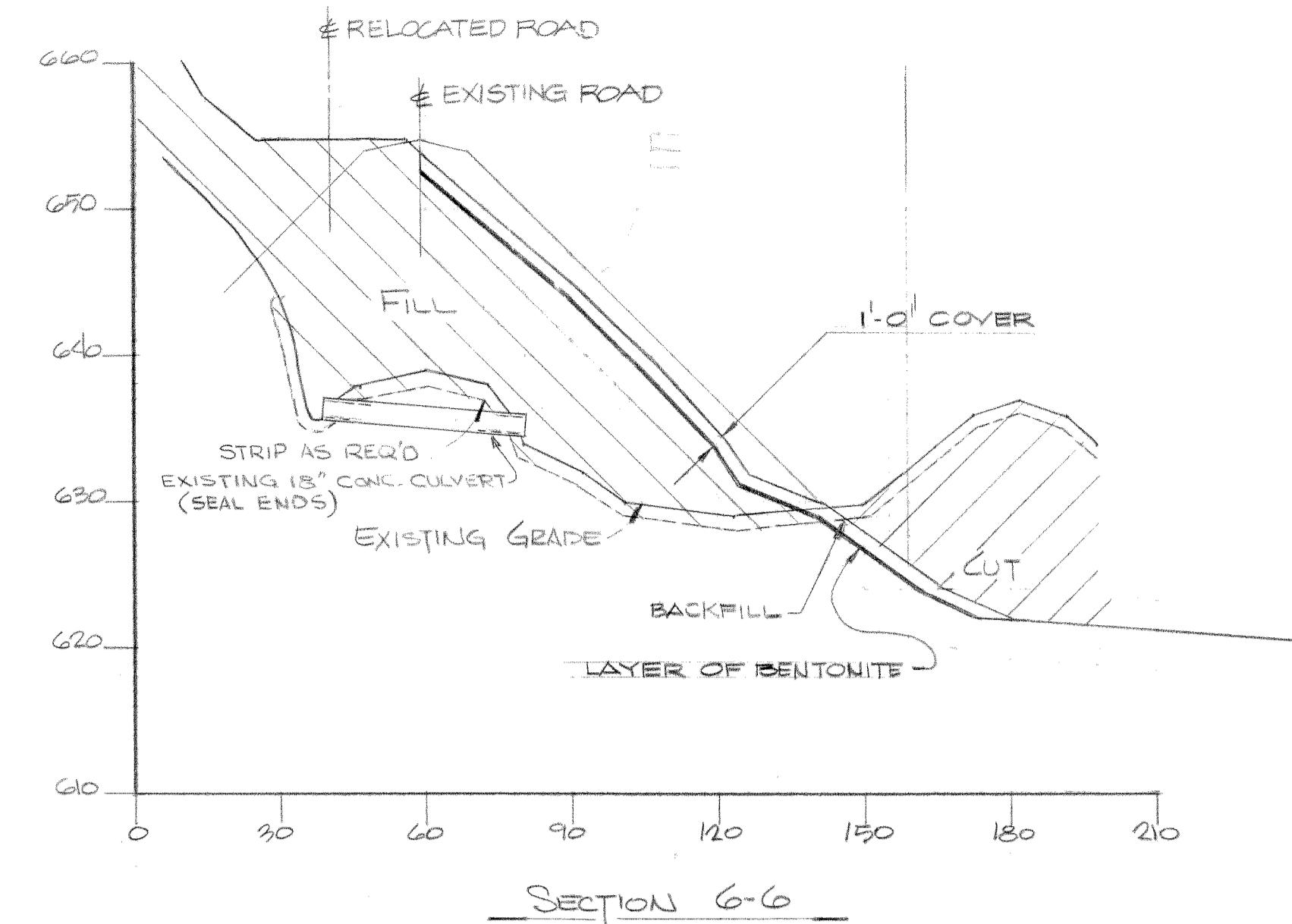
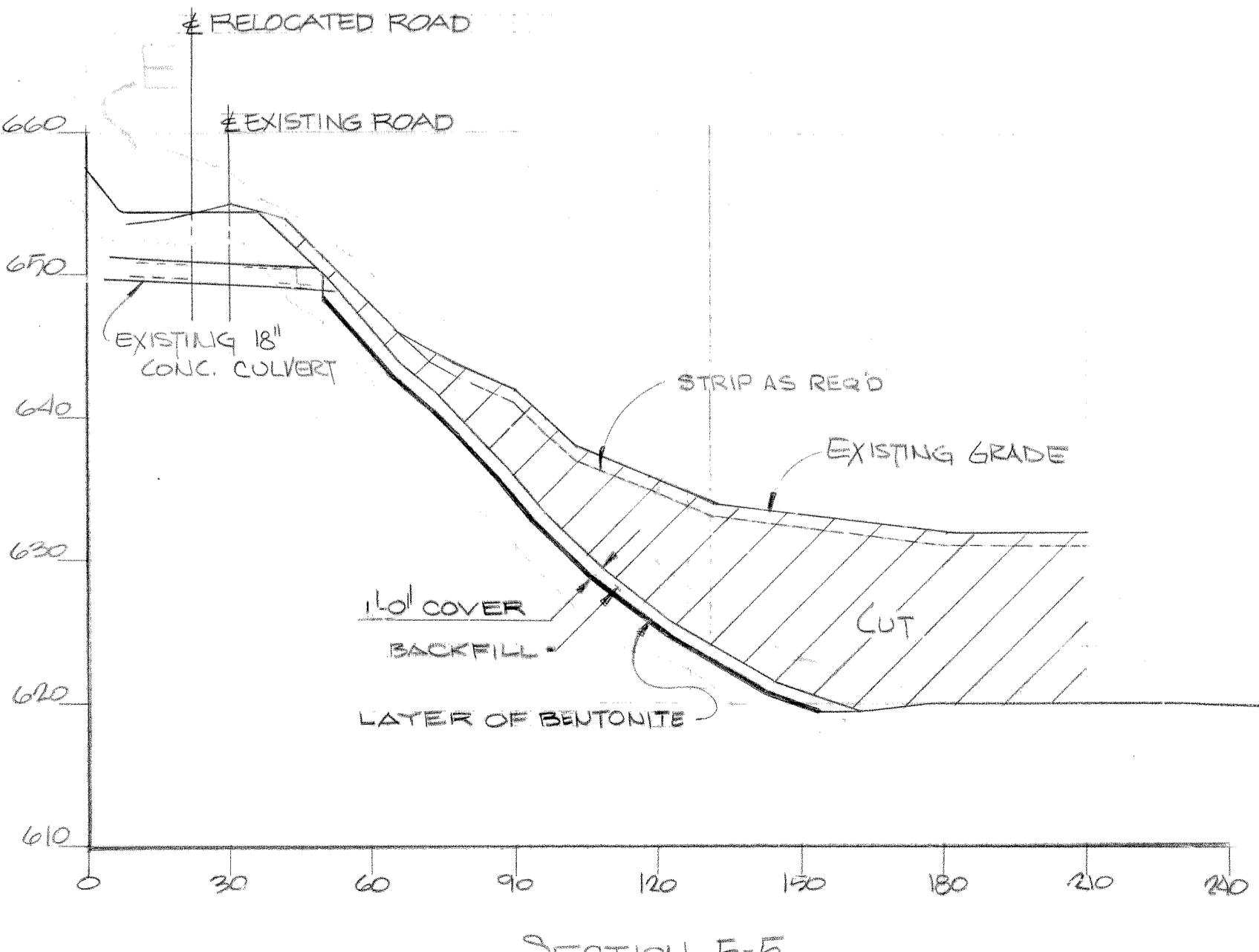
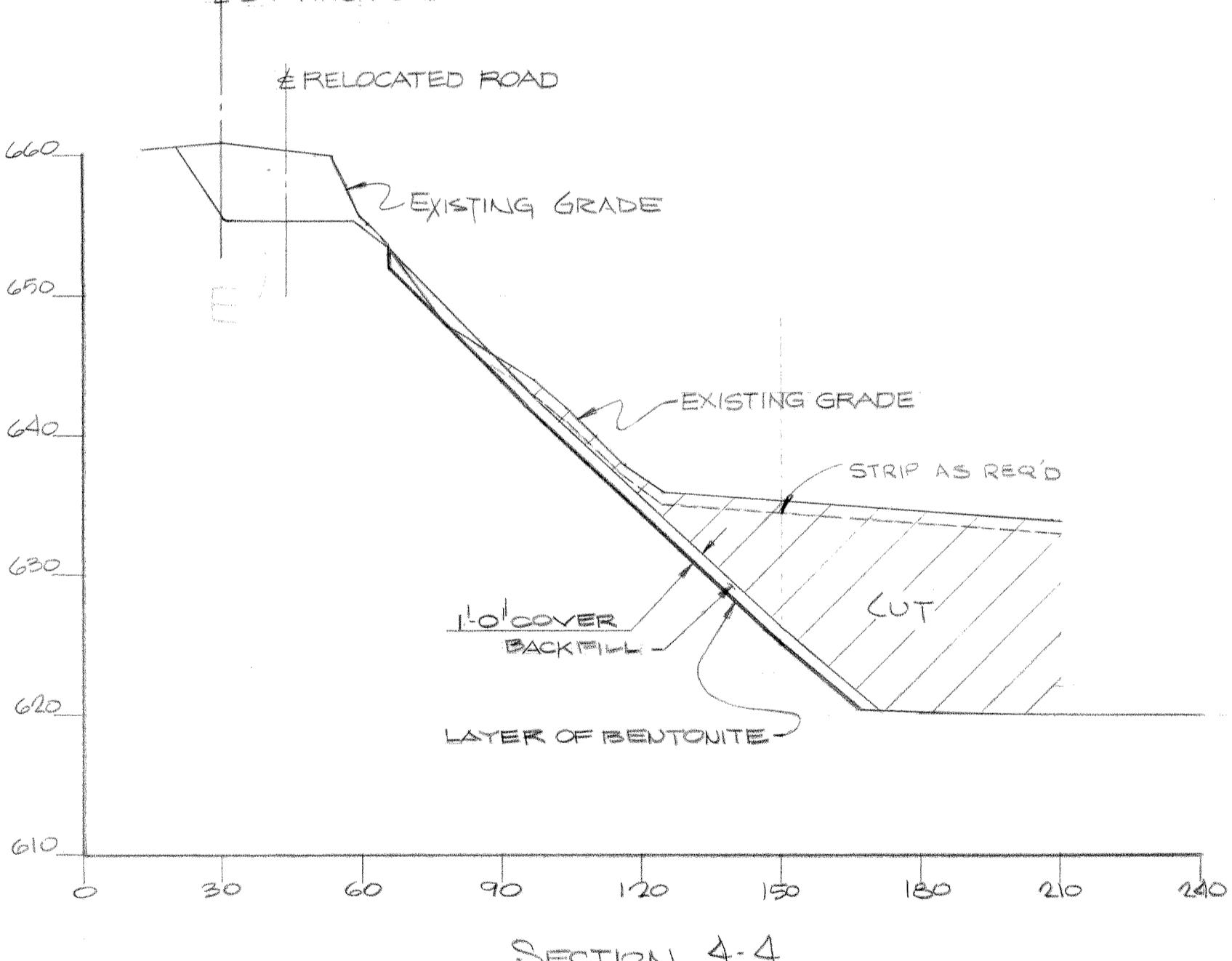
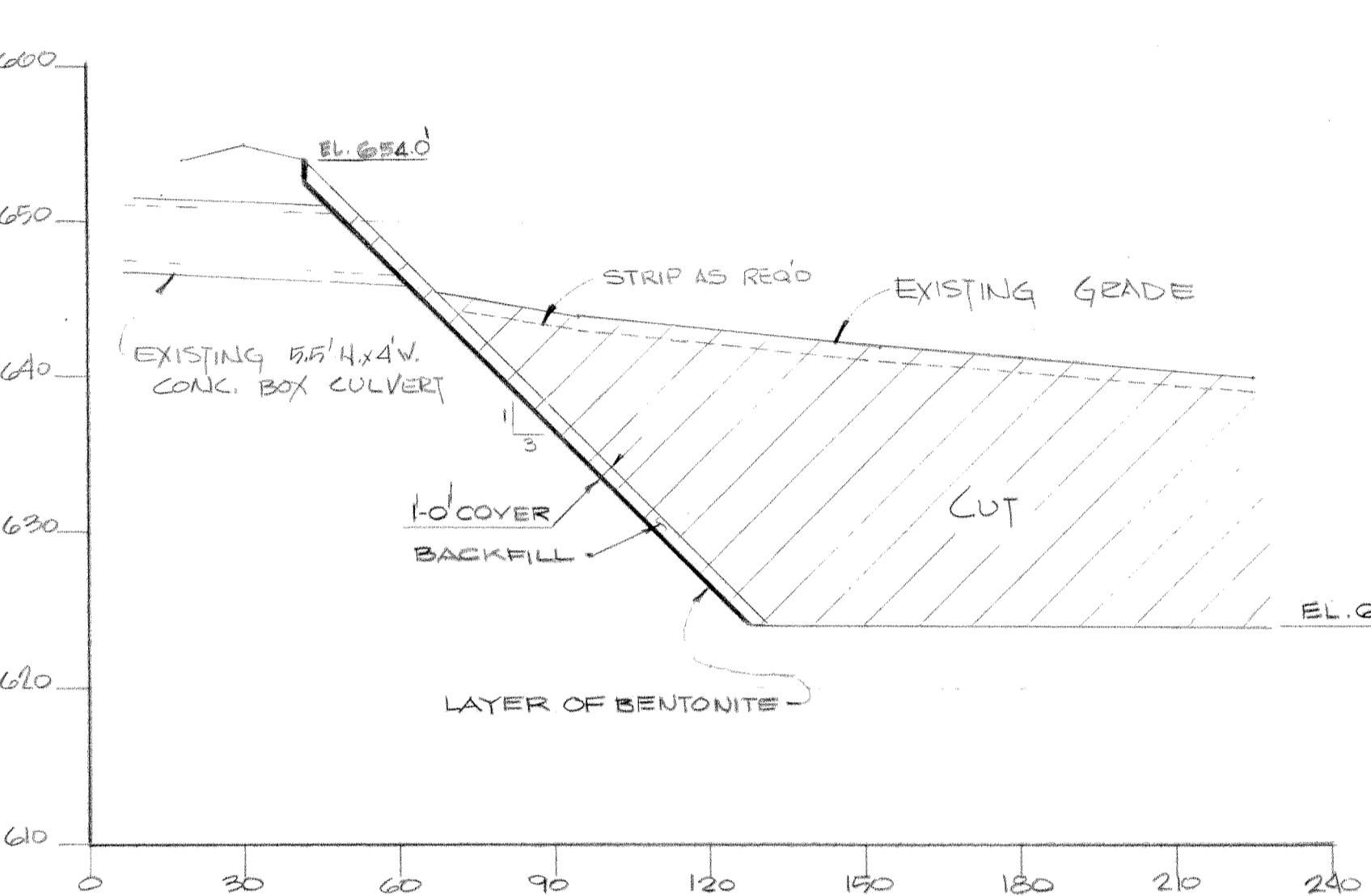
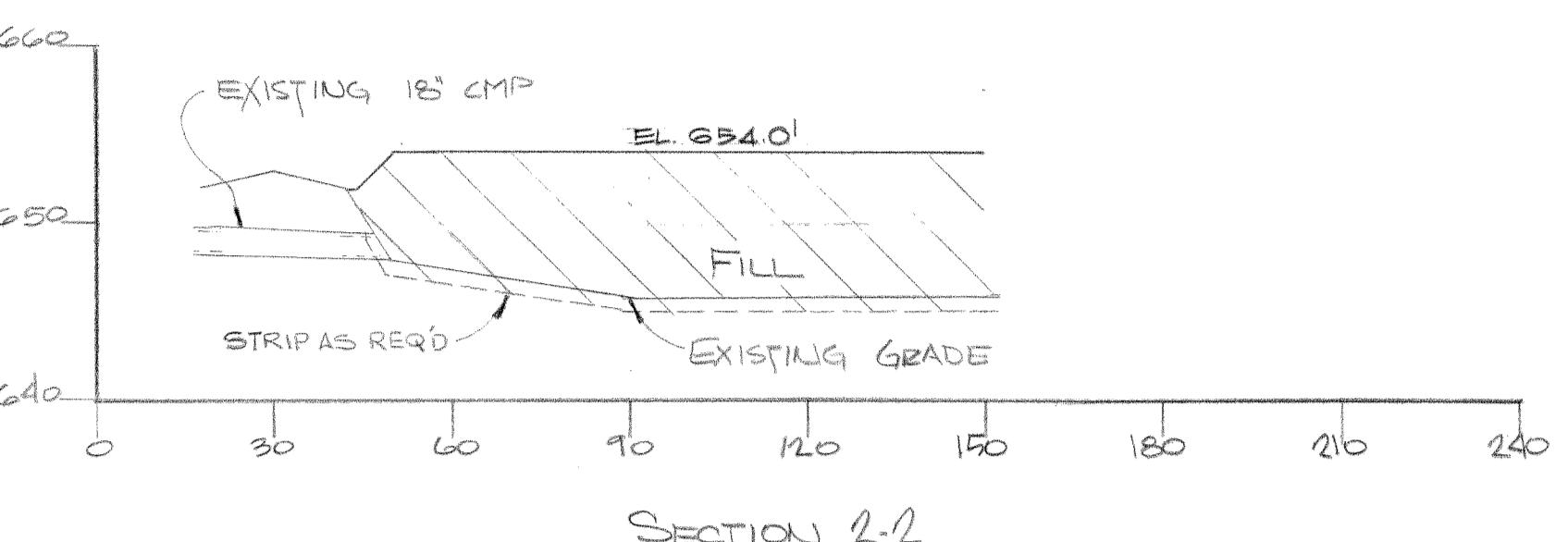
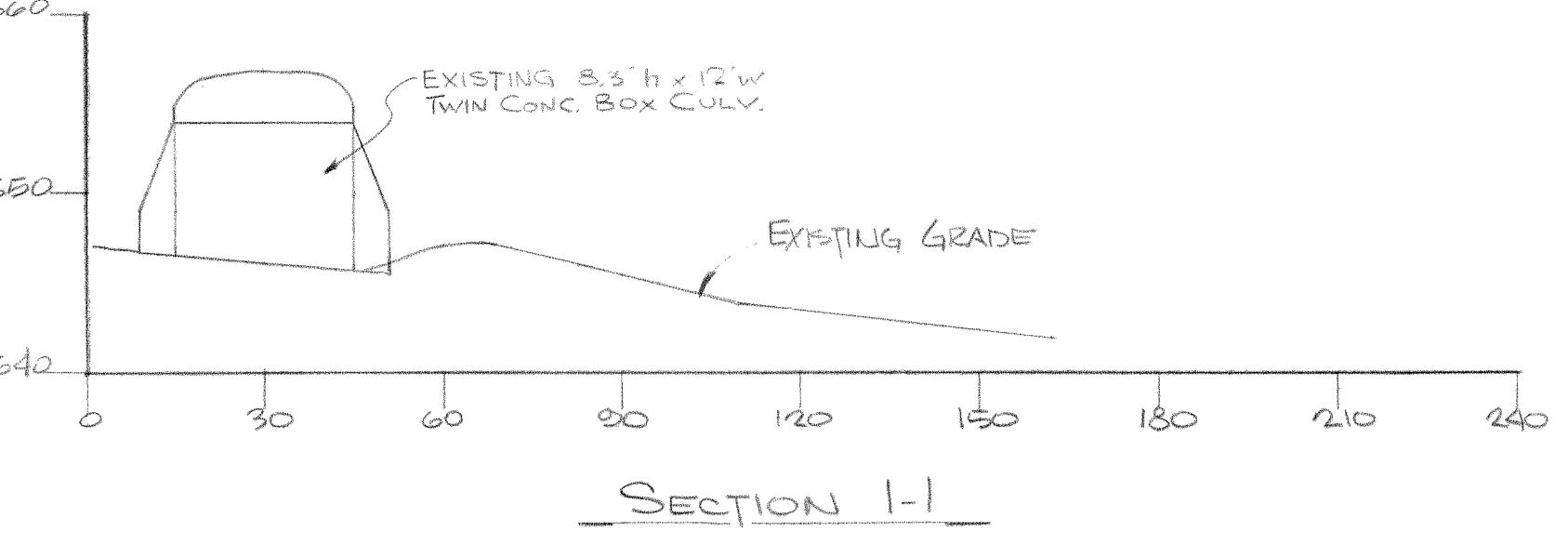
By H. Bergstrom, P.E. Reg. No. 4480

Date 9-10-73

By H. Bergstrom, P.E. Reg. No. 4480

Date 9-10-73

By H.



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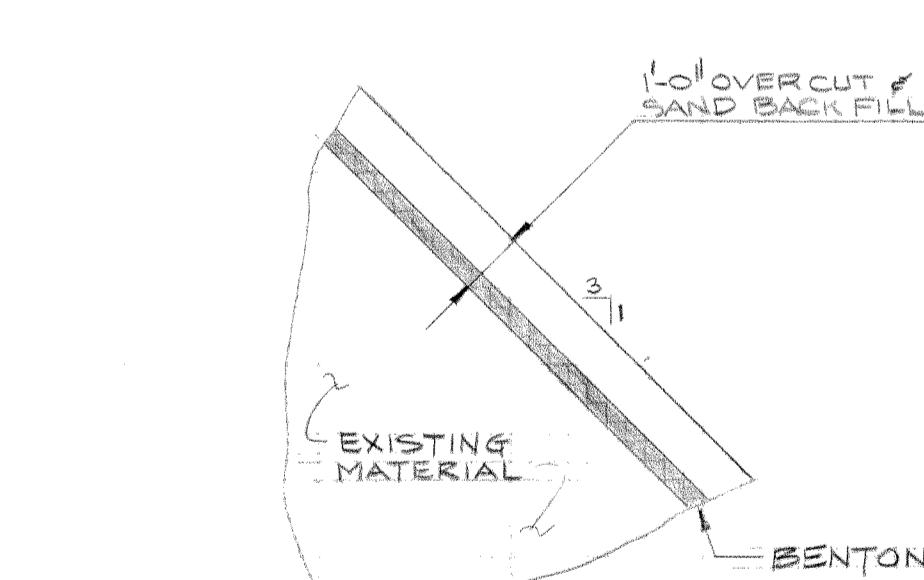
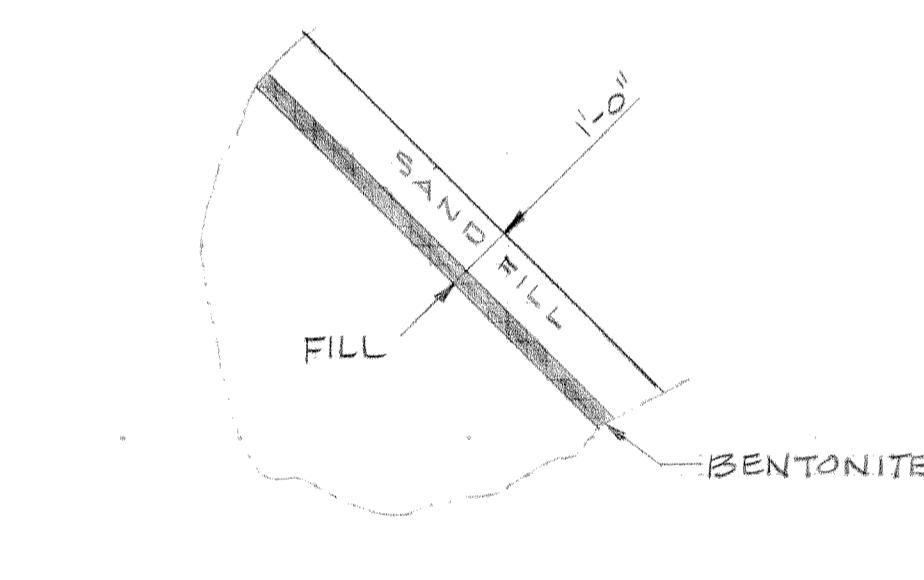
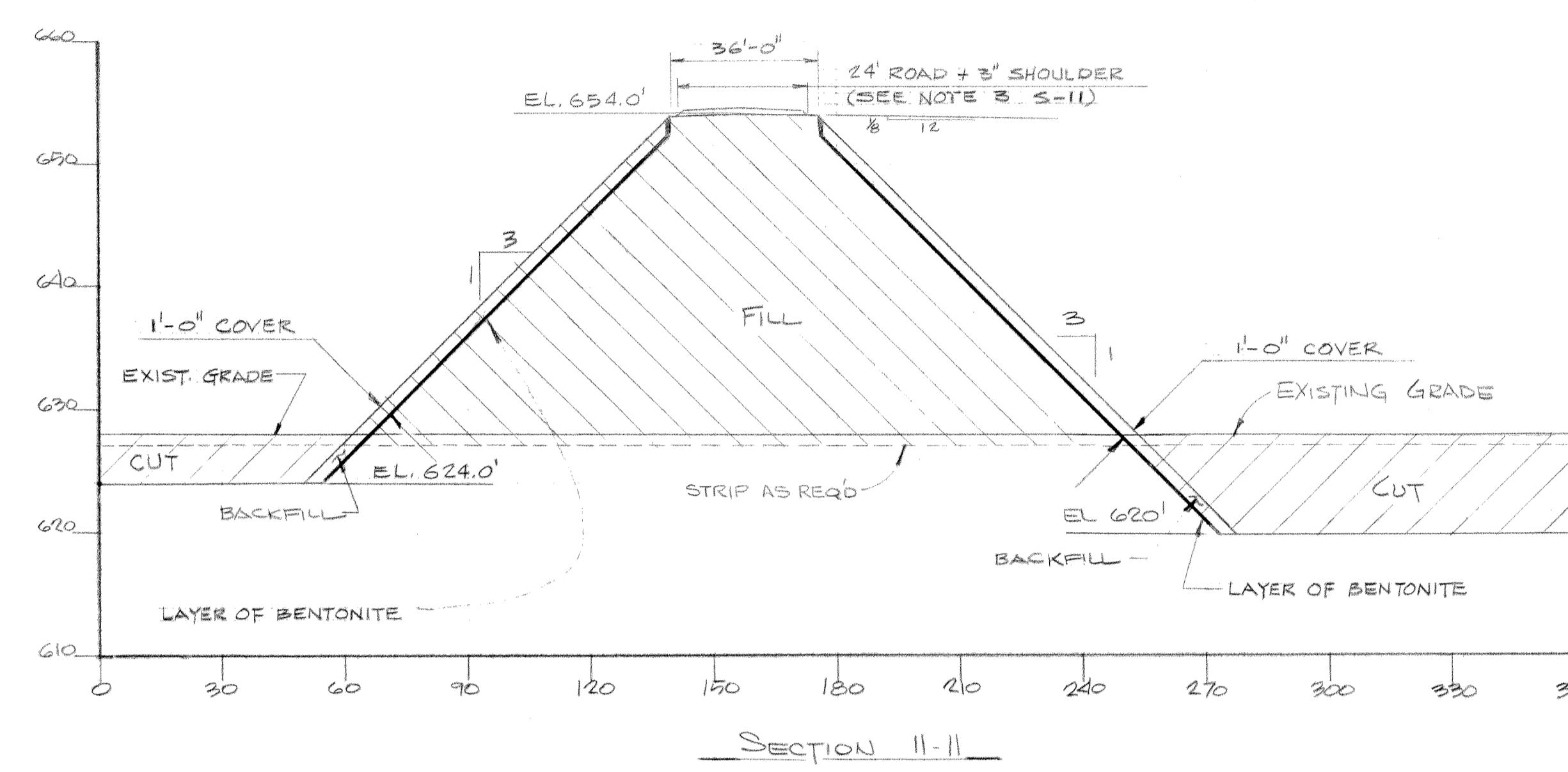
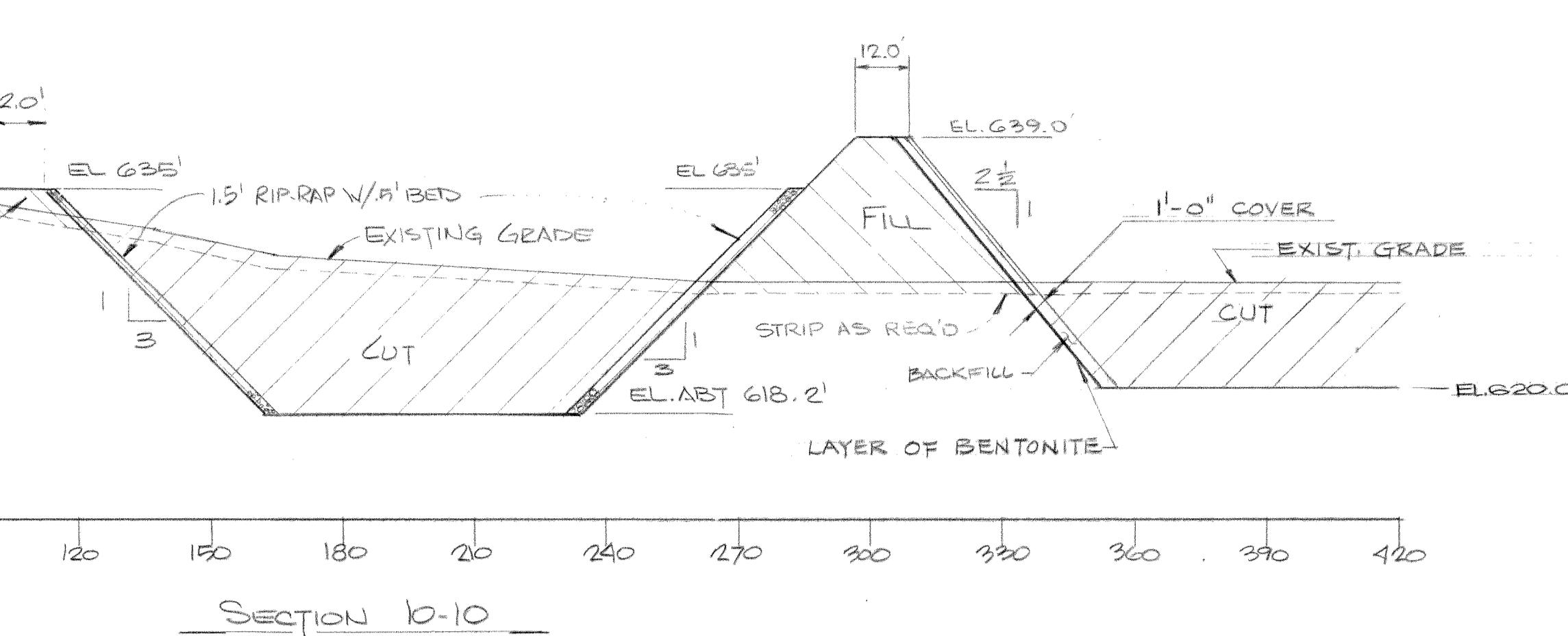
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NOTES

1. WORK THIS DVG. WITH DVG'S SHO'S 11
2. ALL FILL SHALL CONFORM TO SPEC G-3105.
3. ASH DIKE SECTIONS 4, 5 & 6 REVISED AS PER FIELD INFORMATION DATED 7/30/76.

REFERENCE DRAWINGS

- S-10 SITE DEVELOPMENT-COFFERDAM & DRESSING PLAN
S-11 SITE DEVELOPMENT-PLANT FILL - UNIT 4

I hereby certify that the plan, specification or report was prepared by me or under my direct personal supervision and that it has been duly rendered Professional Engineer under the laws of the State of Iowa.
Signed _____ Date _____
R. M. Boles 6-30-76

SITE DEVELOPMENT ASH DIKE SECTIONS - SHEET 1 LANSING POWER STATION INTERSTATE POWER COMPANY LANSING, IOWA

Drawing Release Record		
Rev.	Date	Init.
A	6-22-74	200
B	6-3-75	GIV Rev. B Cvr.
C	8-5-75	GIV Rev. B Cvr. 10-10
D	7-26-75	GIV Rev. B Cvr. 10-10
E	9-9-77	GIV Rev. B Cvr. 10-10

SCALE VERT 1'-0" HORIZ 1'-0"

DRAWN G.R. BOLE 5-20-74
CHECKED R.C. ODEGARD 5-28-74
ENGINEER J.H. GUTH 5-31-74
APPROVED R. M. BOLES 6-30-76
JOB NO. 4044-69
DRAWING NO. S-14

EXHIBIT B – 2015 Investigation

Alliant Energy
Interstate Power and Light Company
Lansing Generating Station
Lansing, Iowa

Unstable Area Determination



More Than Just A Probing Company

BORING LOG

CLIENT: Hard Hat

N NOT SURVEYED

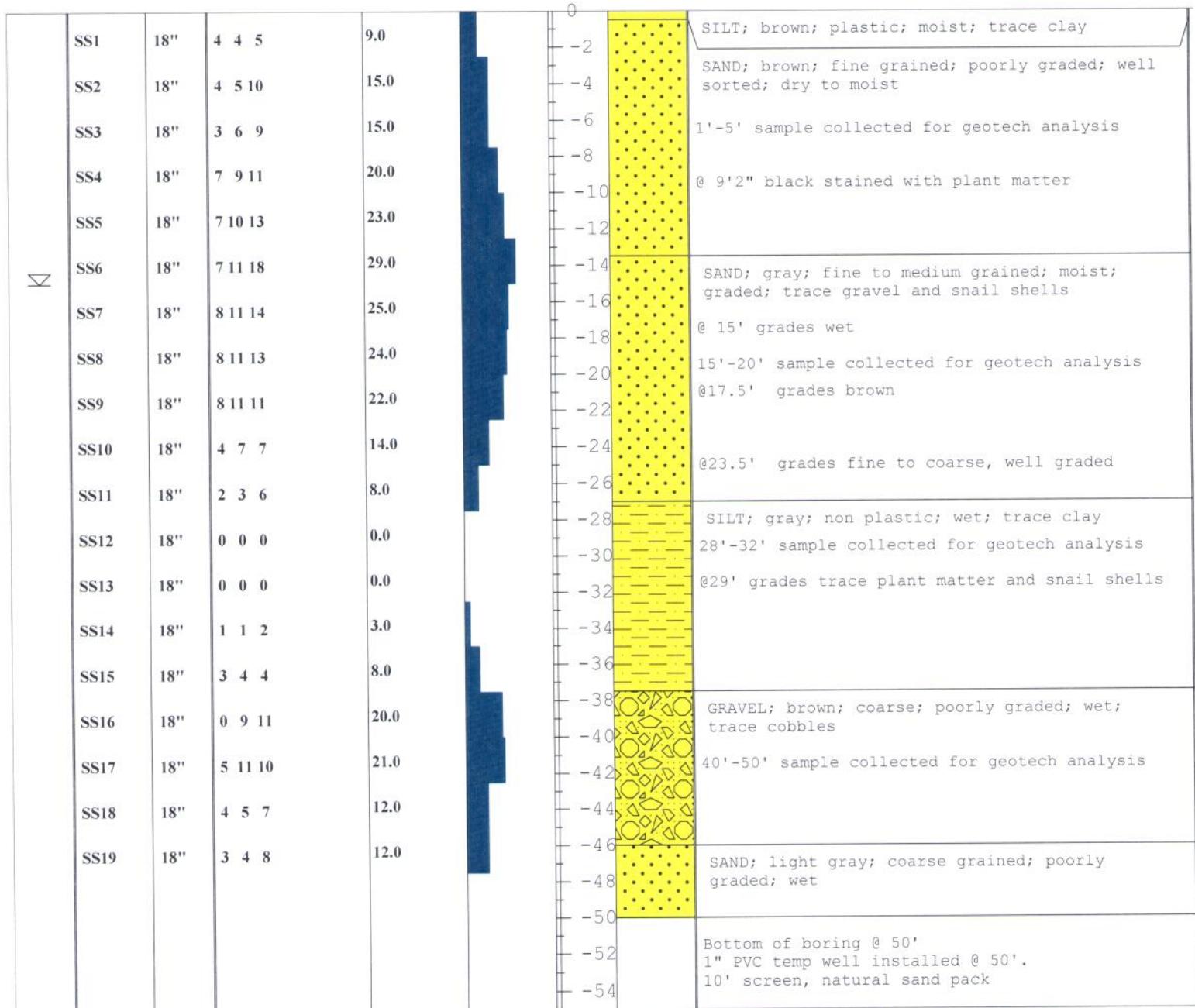
E NOT SURVEYED

PROJECT: Lansing, IA

BORING NO.: SBI

page 1 of 1

DEPTH TO WATER WHILE DRILLING	SAMPLE NO. AND TYPE	SAMPLE RECOVERY	SAMPLE INFORMATION BLOW COUNTS	N-VALUE	SOIL CONSISTENCY HISTOGRAM	DEPTH IN FEET	PROFILE	LOGGED BY: John Noyes
								EDITED BY: John Noyes CHECKED BY: Mark Loerop DATE BEGAN: 1/22/15 DATE FINISHED: 1/22/13/15 GROUND SURFACE ELEVATION: NOT MEASURED





BORING LOG

CLIENT: Hard Hat

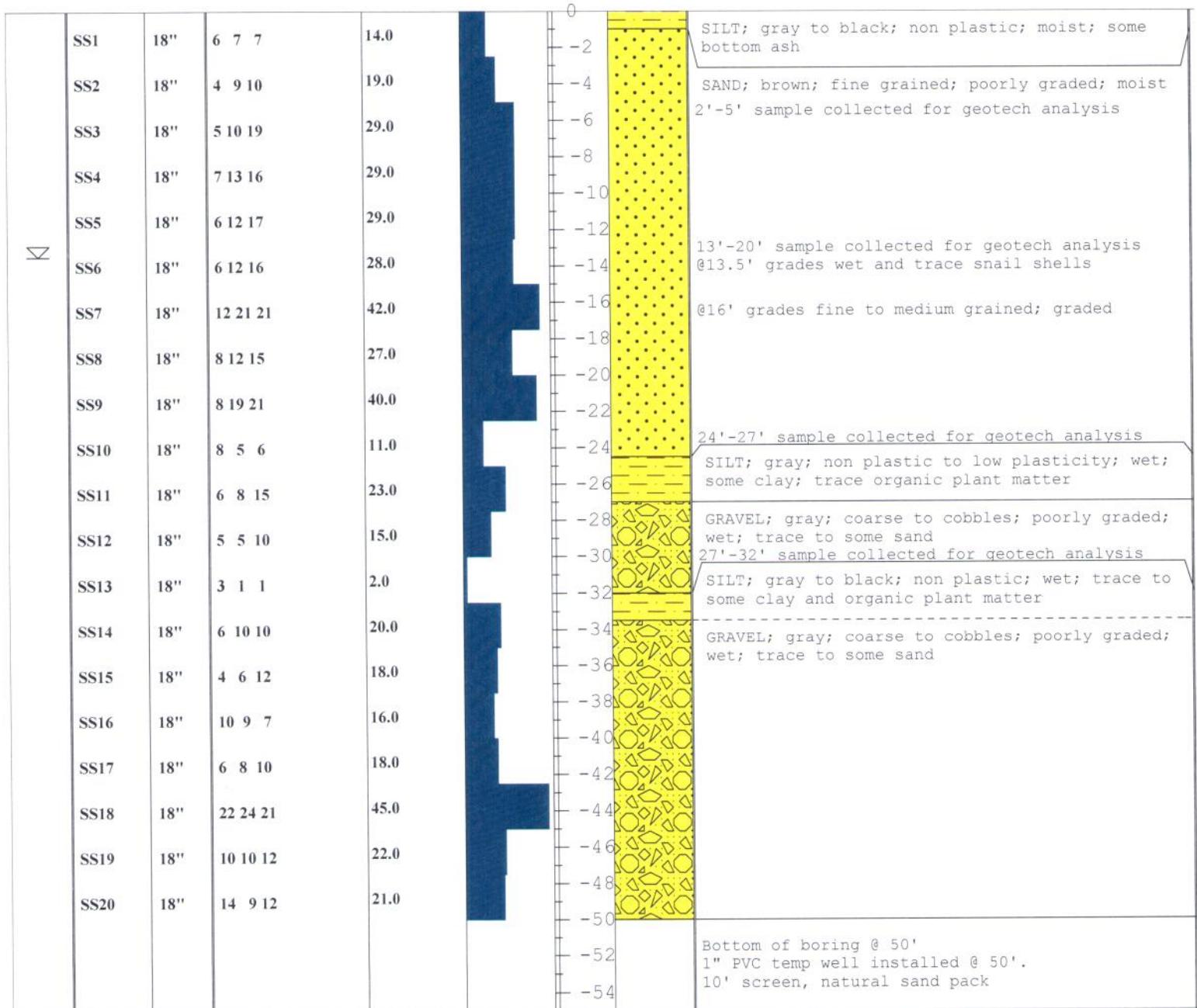
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E NOT SURVEYED

PROJECT:Lansing, IA

BORING NO.: SB3

page 1 of 1

DEPTH TO WATER WHILE DRILLING	SAMPLE NO. AND TYPE	SAMPLE RECOVERY	SAMPLE INFORMATION BLOW COUNTS	N-VALUE	SOIL CONSISTENCY HISTOGRAM	DEPTH IN FEET	PROFILE	LOGGED BY: John Noyes
								EDITED BY: John Noyes CHECKED BY: Mark Loerop DATE BEGAN: 1/22/15 DATE FINISHED: 1/22/15 GROUND SURFACE ELEVATION: NOT MEASURED





More Than Just A Probing Company

BORING LOG

CLIENT: Hard Hat

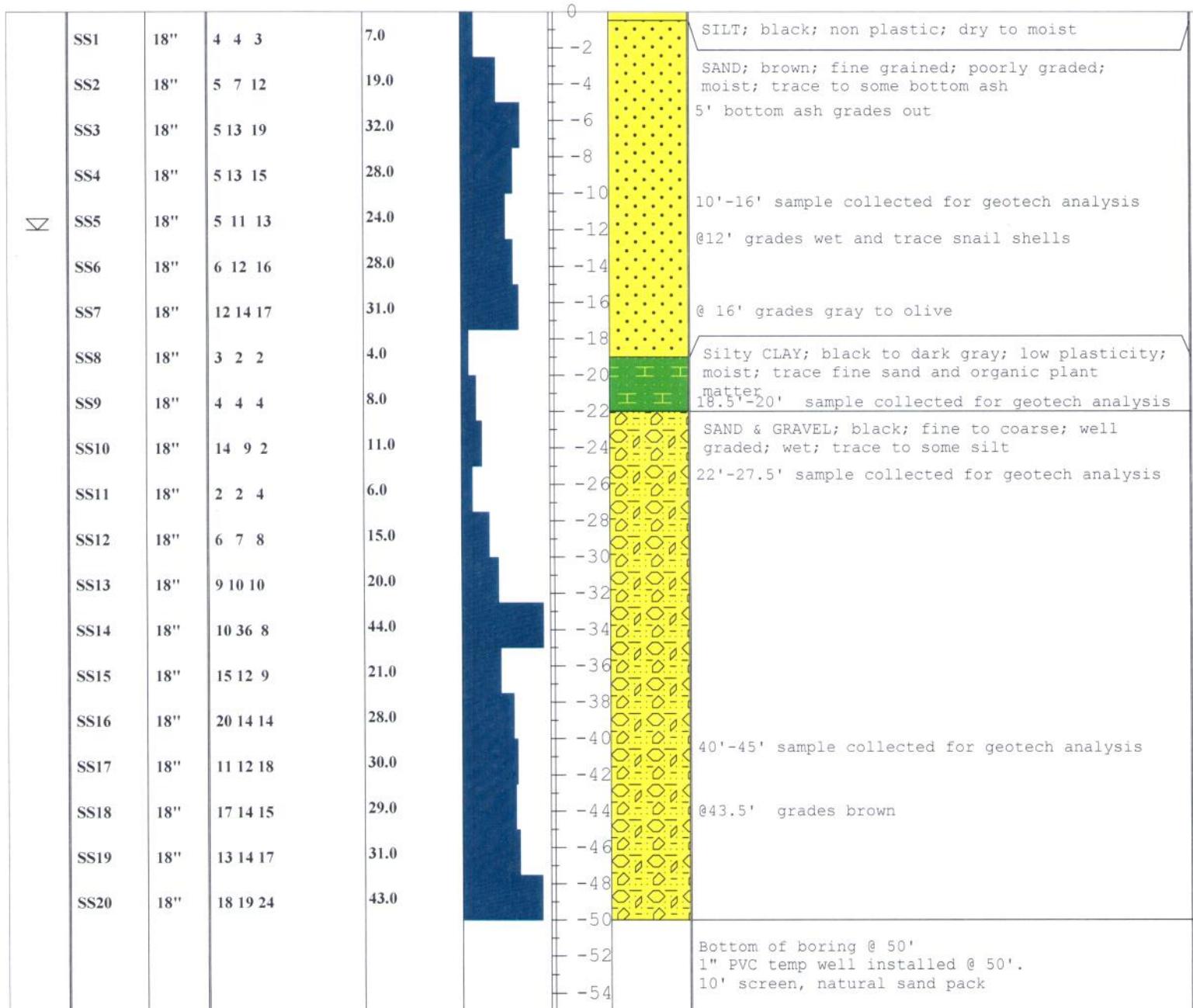
N NOT SURVEYED
E NOT SURVEYED

PROJECT:Lansing, IA

BORING NO.: SB5

page 1 of 1

DEPTH TO WATER WHILE DRILLING	SAMPLE NO. AND TYPE	SAMPLE RECOVERY	SAMPLE INFORMATION BLOW COUNTS	N-VALUE	SOIL CONSISTENCY HISTOGRAM	DEPTH IN FEET	PROFILE	LOGGED BY: John Noyes
								EDITED BY: John Noyes CHECKED BY: Mark Loerop DATE BEGAN: 1/23/15 DATE FINISHED: 1/23/15 GROUND SURFACE ELEVATION: NOT MEASURED





More Than Just A Probing Company

BORING LOG

CLIENT: Hard Hat

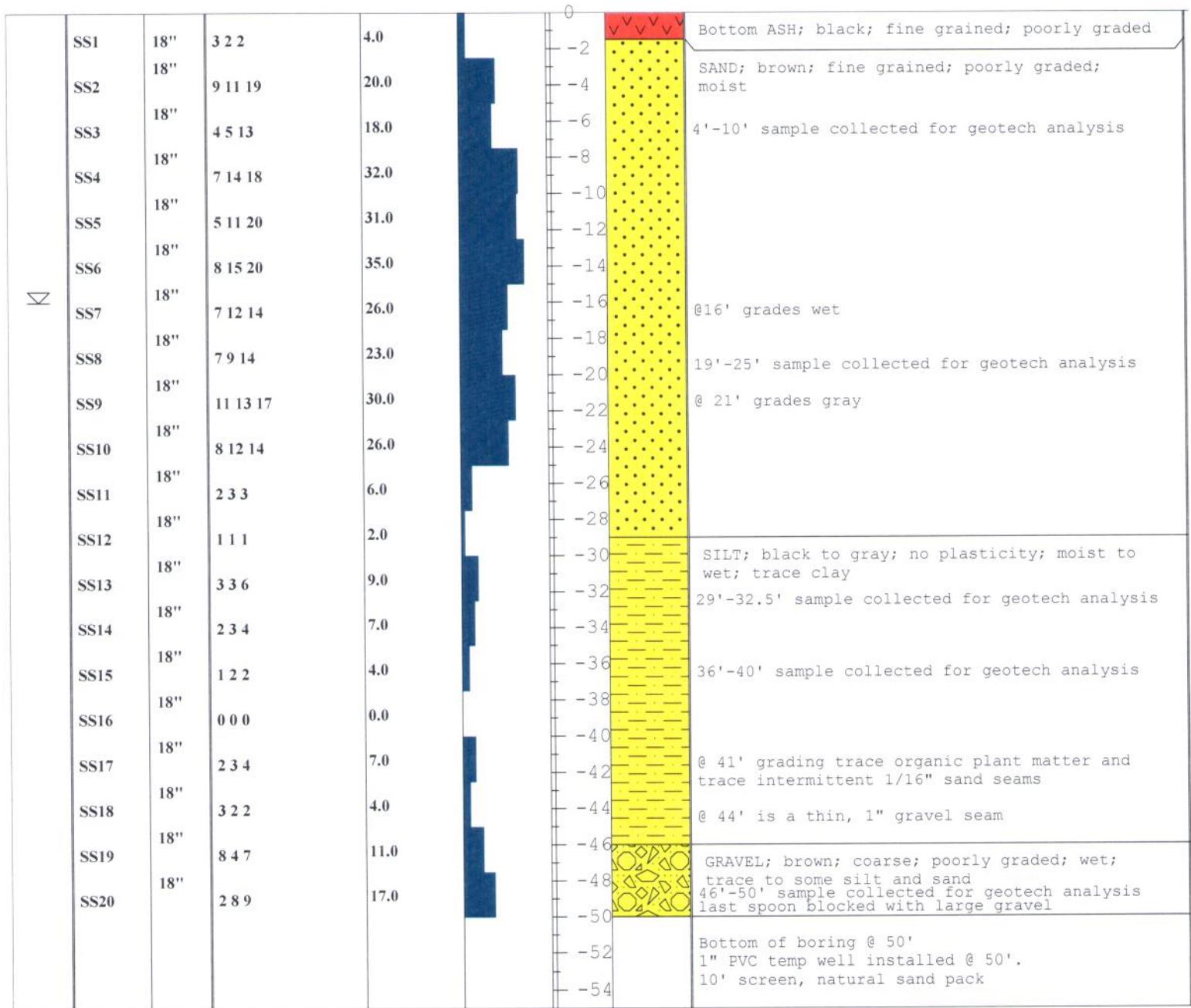
*N NOT SURVEYED
E NOT SURVEYED*

PROJECT: Lansing, IA

BORING NO.: SB7

page 1 of 1

DEPTH TO WATER WHILE DRILLING	SAMPLE NO. AND TYPE	SAMPLE RECOVERY	SAMPLE INFORMATION BLOW COUNTS	N VALUE	SOIL CONSISTENCY HISTOGRAM	DEPTH IN FEET	PROFILE	LOGGED BY: John Noyes
								EDITED BY: John Noyes CHECKED BY: Mark Loerop DATE BEGAN: 1/23/15 DATE FINISHED: 1/23/15 GROUND SURFACE ELEVATION: NOT MEASURED



APPENDIX B
UPDATE TO ADD SB-7
SEPARATE SIZING



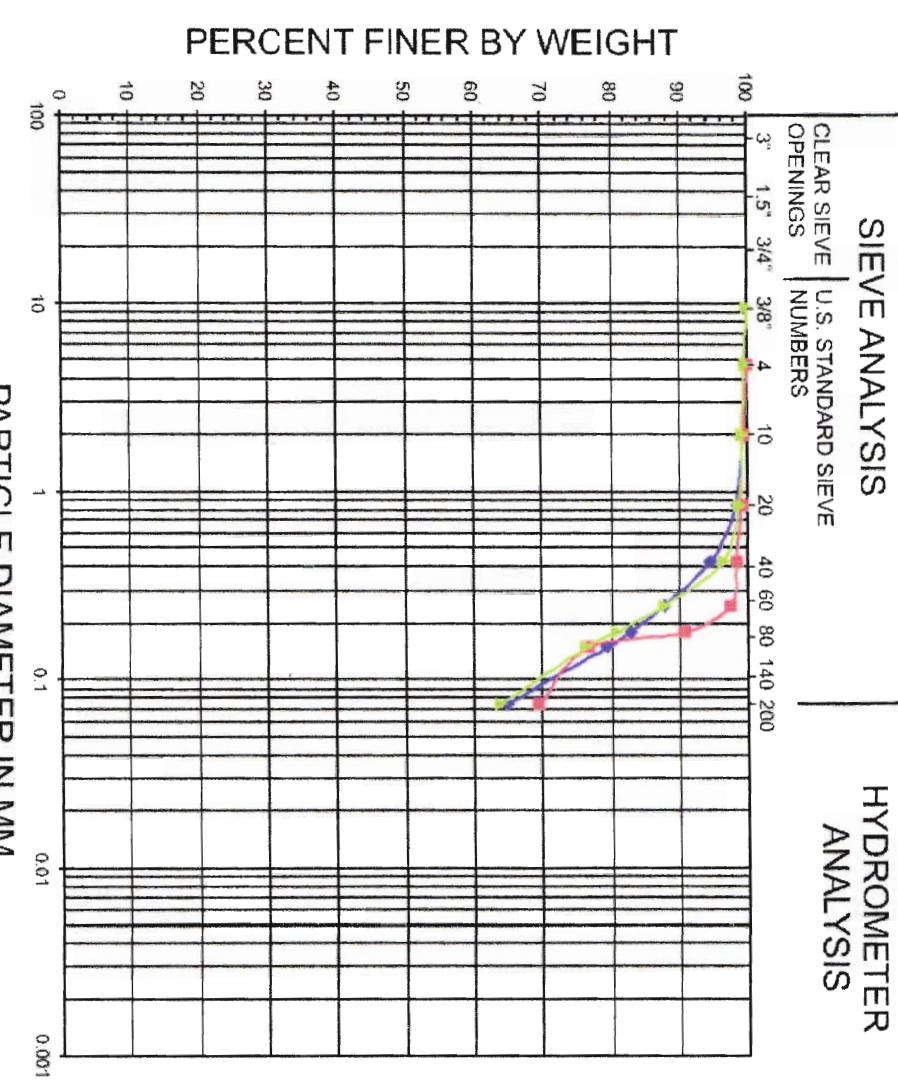
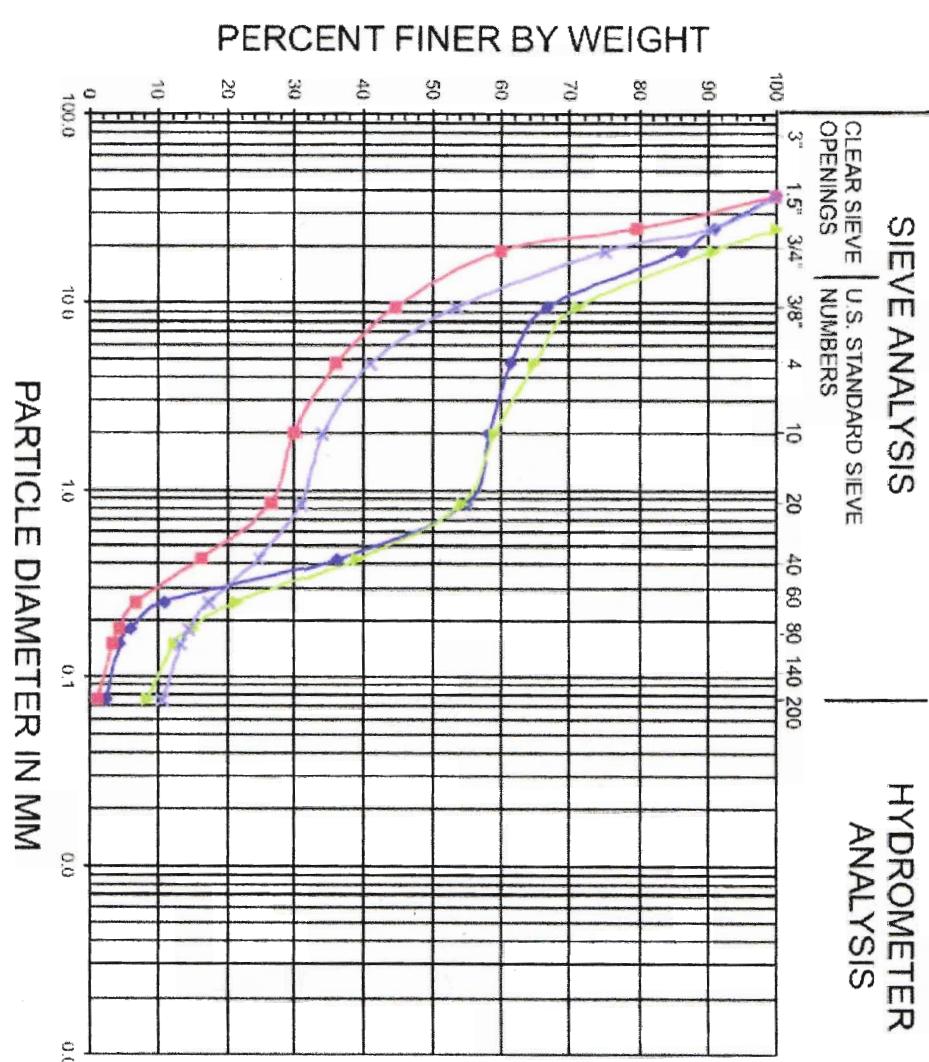
Particle Size Distribution



Particle Size Distribution



Particle Size Distribution



COBBLES	GRAVEL		SAND		SILT AND CLAY FRACTION
	coarse	fine	coarse	medium	
SB-1	40 - 50		SAND & GRAVEL		SW / GW
SB-3	27 - 32		SAND & GRAVEL		SW / GW
SB-5	22 - 27.5		SAND & GRAVEL		SW / GW
	SB-5	44 - 45	SAND & GRAVEL		SW / GW

COBBLES	GRAVEL		SAND		SILT AND CLAY FRACTION
	coarse	fine	coarse	medium	
SB-1	28 - 32		Sandy Silt		ML
SB-3	24.5 - 27		Sandy Silt		ML
SB-5	18.5 - 20		Sandy Silt		ML

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▲			SCALE: NONE	DATE: 5-14-15	
▲	DRAWN BY: JFD	CHECKED BY: TJH	APPROVED BY: MMW		
▲					
▲	SB-1	27 - 32	SAND & GRAVEL	SW / GW	16.5
▲	SB-3	24.5 - 27	SAND & GRAVEL	SW / GW	13.4
▲	SB-5	18.5 - 20	SAND & GRAVEL	SW / GW	32.1
▲	SB-5	44 - 45	SAND & GRAVEL	SW / GW	9.8
REV	DATE	BY	APP	DESCRIPTION	



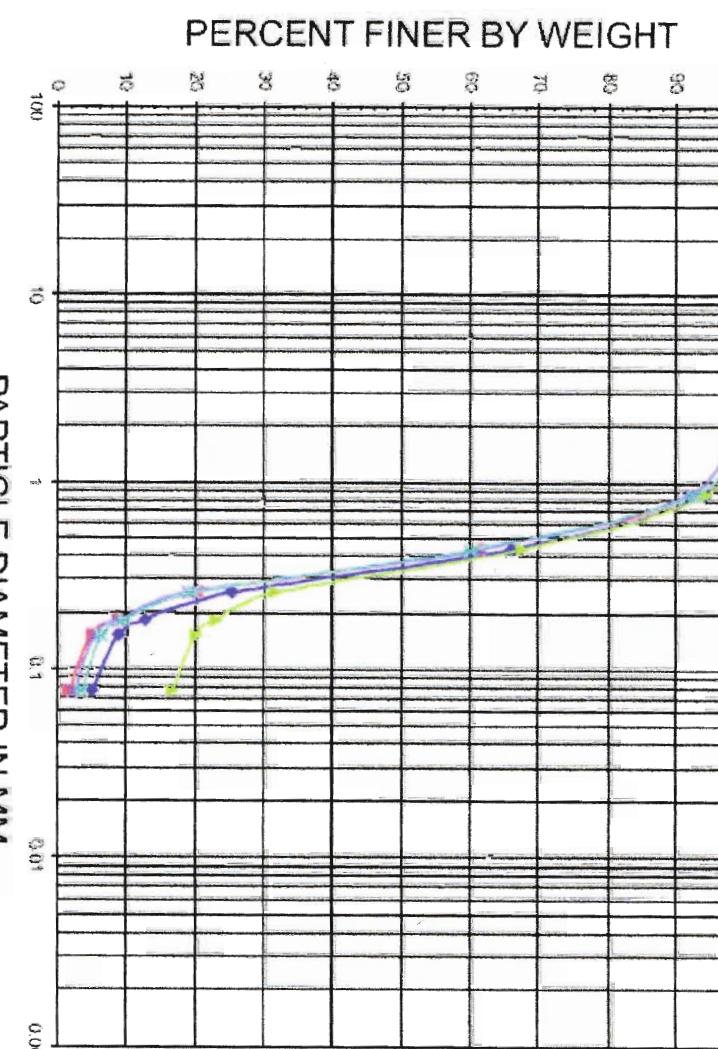
HARD HAT SERVICES
Engineering, Construction and Management Solutions

Particle Size Distribution

Project IPL - Lansing Generating Station Tested By Test America Date 2/3/2015
Boring No. SB-1, SB-3 & SB-5 "UPPER SAND"

SIEVE ANALYSIS

HYDROMETER ANALYSIS



COBBLES	GRAVEL			SAND			SILT AND CLAY FRACTION
	coarse	fine	coarse	medium	fine		
SB-1	1 - 5			Medium - Fine Sand		SP	4.1
SB-1	15 - 20			Medium - Fine Sand		SP	20.1
SB-3	2 - 5			Silt/Medium - Fine Sand		SM	3.1
SB-3	13 - 20			Medium - Fine Sand		SP	19.0
SB-5	10 - 16			Medium - Fine Sand		SP	13.3

SYMBOL	BORING	DEPTH (FT.)	SOIL DESCRIPTION			U.S.G.S.	W% %
▲	SB-1	1 - 5	Medium - Fine Sand		SP	4.1	
▲	SB-1	15 - 20	Medium - Fine Sand		SP	20.1	
▲	SB-3	2 - 5	Silt/Medium - Fine Sand		SM	3.1	
▲	SB-3	13 - 20	Medium - Fine Sand		SP	19.0	
▲	SB-5	10 - 16	Medium - Fine Sand		SP	13.3	

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RESERVED.

SCALE: NONE DATE: 5-14-15
DRAWN BY: JFD CHECKED BY: TUH APPROVED BY: MWL

CLIENT / LOCATION
INTERSTATE POWER AND LIGHT (IPL)
LANSING GENERATING STATION PROJECT
2320 POWER PLANT DR
LANSING, IA 52151

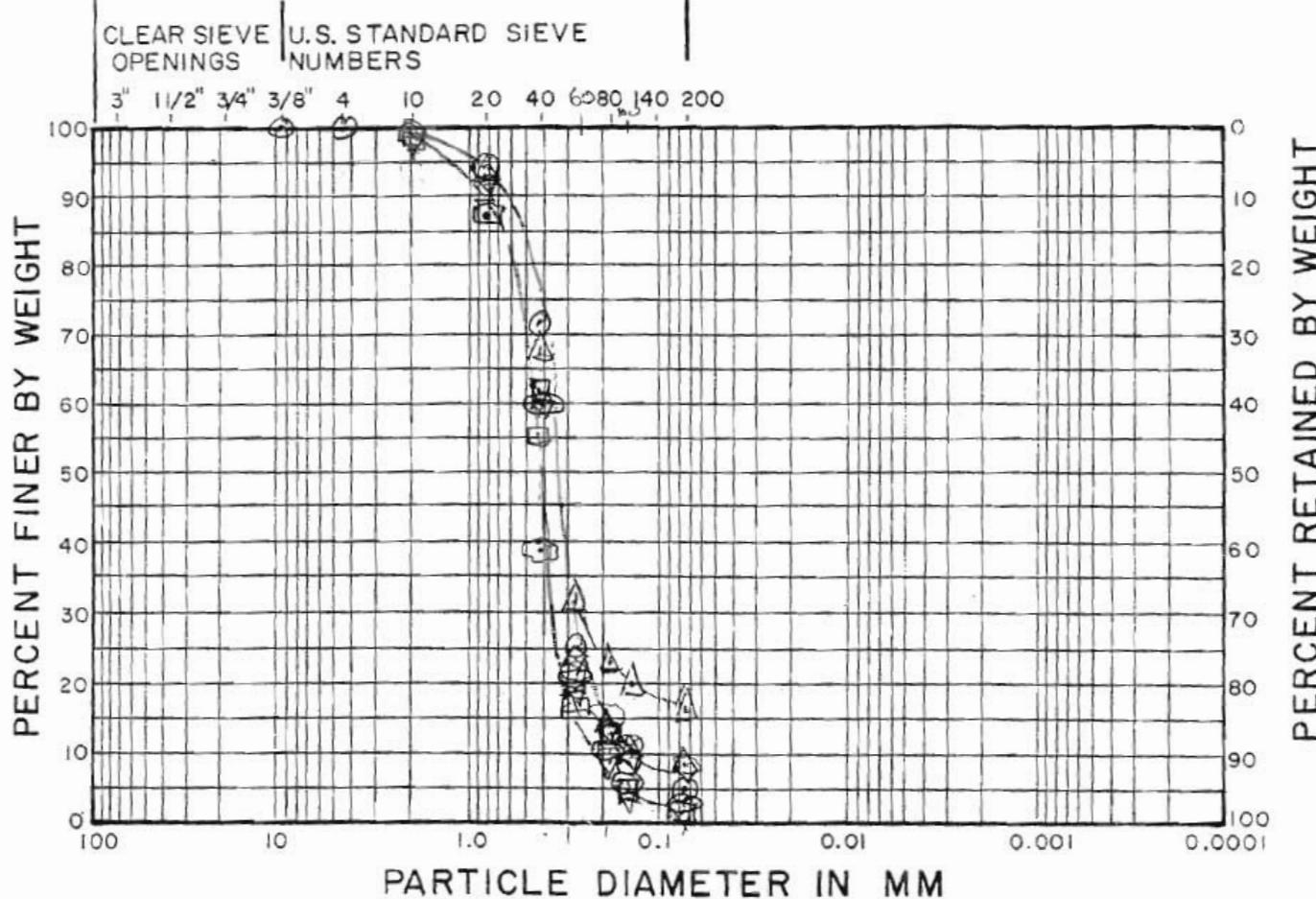
DRAWING DESCRIPTION
JOB 154.021.003
SHT. 9
DWG. 154021SW-08-12

HARD HAT SERVICES™
Engineering, Construction and Management Solutions

APPENDIX B
UPDATE TO ADD SB-T
SEPARATE SHEET

"UPPER SAND"

PROJECT _____ TESTED BY _____ DATE _____
 PROJECT NO. _____ CALC BY _____ DATE _____
 BORING NO. _____ CHKD BY _____ DATE _____

SIEVE ANALYSIS**HYDROMETER ANALYSIS**

COBBLES	GRAVEL		SAND			SILT AND CLAY FRACTION		
	coarse	fine	coarse	medium	fine			

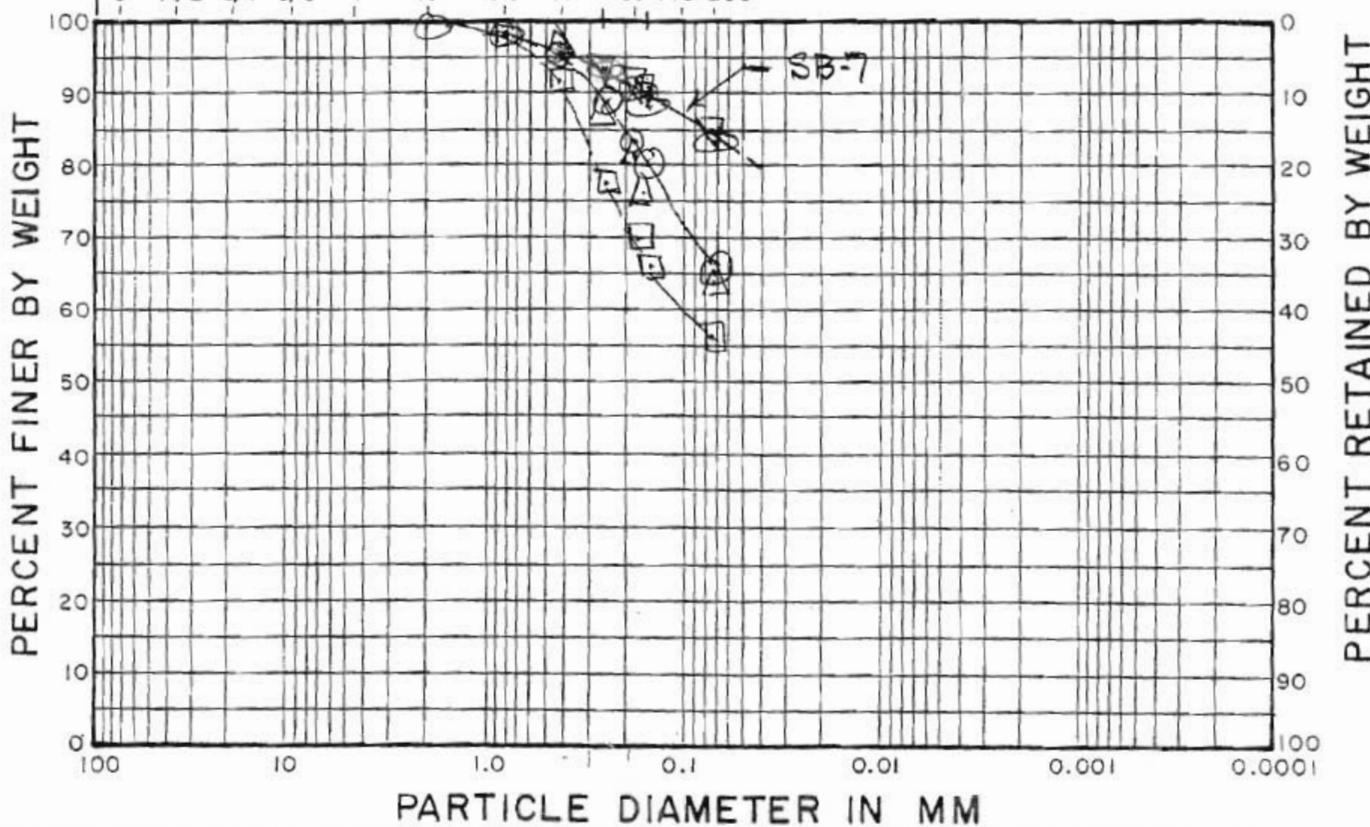
SYMBOL	BORING	SAMPLE	DEPTH	SOIL DESCRIPTION	U.S.G.S.	L.L.	R.L.	W%
●	SB-1		1-5	MED-FINE SAND	SP			4.1
□	SB-1		15-20	"	SP			20.1
△	SB-3		2-5	SILTY MED-FINE SAND	SM			3.1
▽	SB-3		13-20	MED-FINE SAND	SP			19.0
○	SB-5		10-16	"	SP			13.3
◇	SB-7		4-10	"	SP			3.1
■	SB-7		9-25	"	SP			17.1

"SANDY SILT"

PROJECT _____ TESTED BY _____ DATE _____
 PROJECT NO. _____ CALC BY _____ DATE _____
 BORING NO. _____ CHKD BY _____ DATE _____

SIEVE ANALYSIS**HYDROMETER ANALYSIS**CLEAR SIEVE | U.S. STANDARD SIEVE
OPENINGS | NUMBERS

3" 1 1/2" 3/4" 3/8" 4 10 20 40 80 140 200



COBBLES	GRAVEL		SAND			SILT AND CLAY FRACTION
	coarse	fine	coarse	medium	fine	

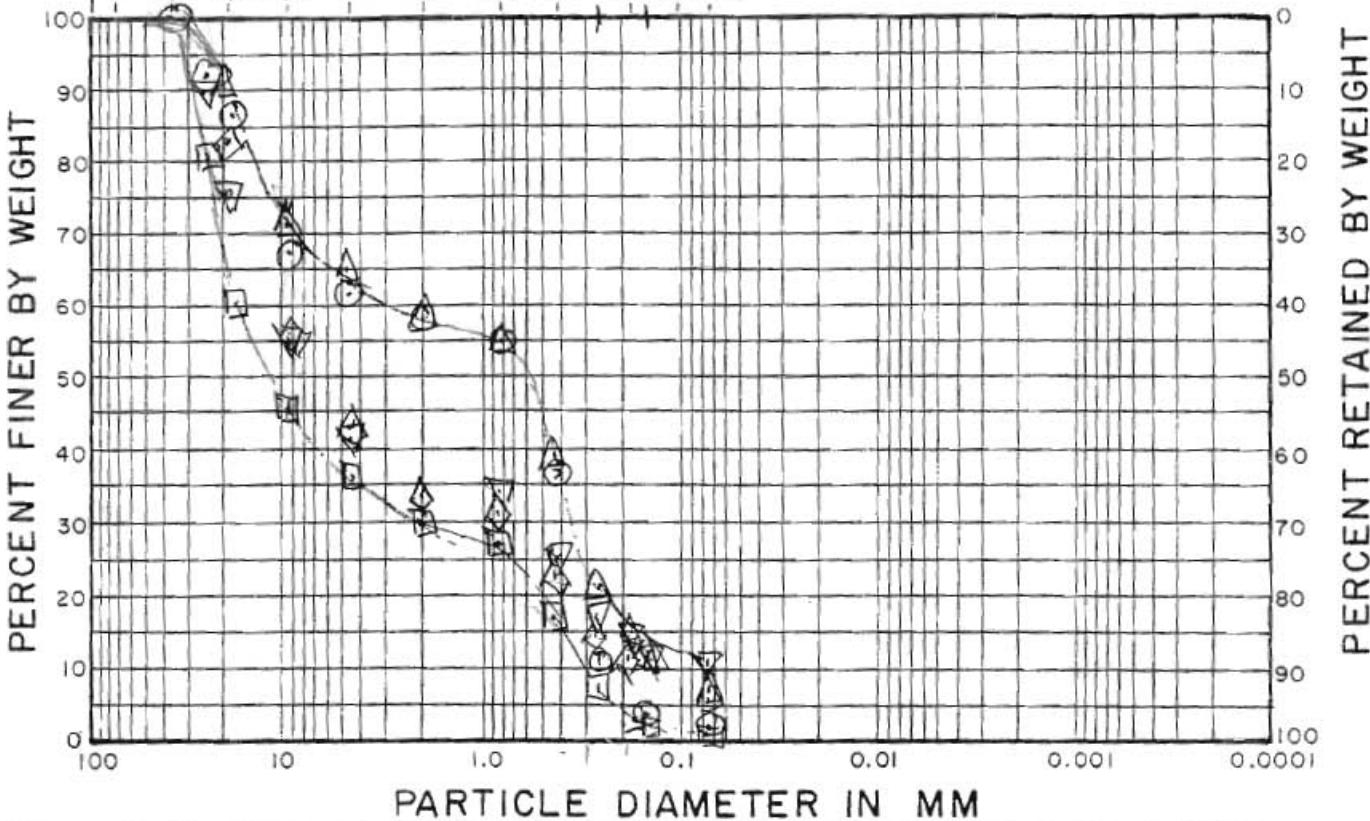
SYMBOL	BORING	SAMPLE	DEPTH	SOIL DESCRIPTION	U.S.C.S.	L.L.	R.L.	W%
(1)	SB-1		28-32	SANDY SILT	ML	28	26	36.1
(2)	SB-3		24.5-27	SANDY SILT	ML	27	23	25.4
(3)	SB-5		18.5-20	SANDY SILT	ML	24	20	21.8
(4)	SB-7		29-32.5	SANDY SILT	ML	29	25	27.0
(5)	SB-7		36-40	SANDY SILT	ML	31	26	35.7

"SANDY GRAVEL"

PROJECT _____ TESTED BY _____ DATE _____
 PROJECT NO. _____ CALC BY _____ DATE _____
 BORING NO. _____ CHKD BY _____ DATE _____

SIEVE ANALYSIS**HYDROMETER ANALYSIS**CLEAR SIEVE | U.S. STANDARD SIEVE
OPENINGS | NUMBERS

3" 1 1/2" 3/4" 3/8" 4 10 20 40 80 140 200



COBBLES	GRAVEL		SAND			SILT AND CLAY FRACTION
	coarse	fine	coarse	medium	fine	

SYMBOL	BORING	SAMPLE	DEPTH	SOIL DESCRIPTION	U.S.C.S.	L.L.	P.L.	W%
○	SB-1		40-50	SAND & GRAVEL	SW/GV			16.5
□	SB-3		27-32	"	"			13.4
△	SB-5		22-27.5	"	"			32.1
▽	SB-3		44-45	"	"			9.8
◇	SB-7		46-50	"	"			35.7

EXHIBIT C – Iowa Bedrock Map

Alliant Energy
Interstate Power and Light Company
Lansing Generating Station
Lansing, Iowa

Unstable Area Determination

BEDROCK GEOLOGIC MAP OF IOWA

1:500,000

Iowa Geological and Water Survey
Open File Map OFM-2010-01
March 2010

Primary Map Compilation By
Brian J. Witke, Raymond R. Anderson and John P. Pope
Iowa Geological and Water Survey, Iowa City, Iowa

Iowa Geological and Water Survey
Robert D. Libra, State Geologist
Iowa Department of Natural Resources
Richard Leopold, Director

ACKNOWLEDGEMENTS
Recognized for significant contributions to the map's production: Bill J. Bunker, James D. Gigheran, Greg A. Ludvigson, Robert M. McKay, Huaihai P. Liu, and Thomas R. Marshall.
Supported in part with funding from the U.S. Geological Survey - National Cooperative Geologic Mapping Program.


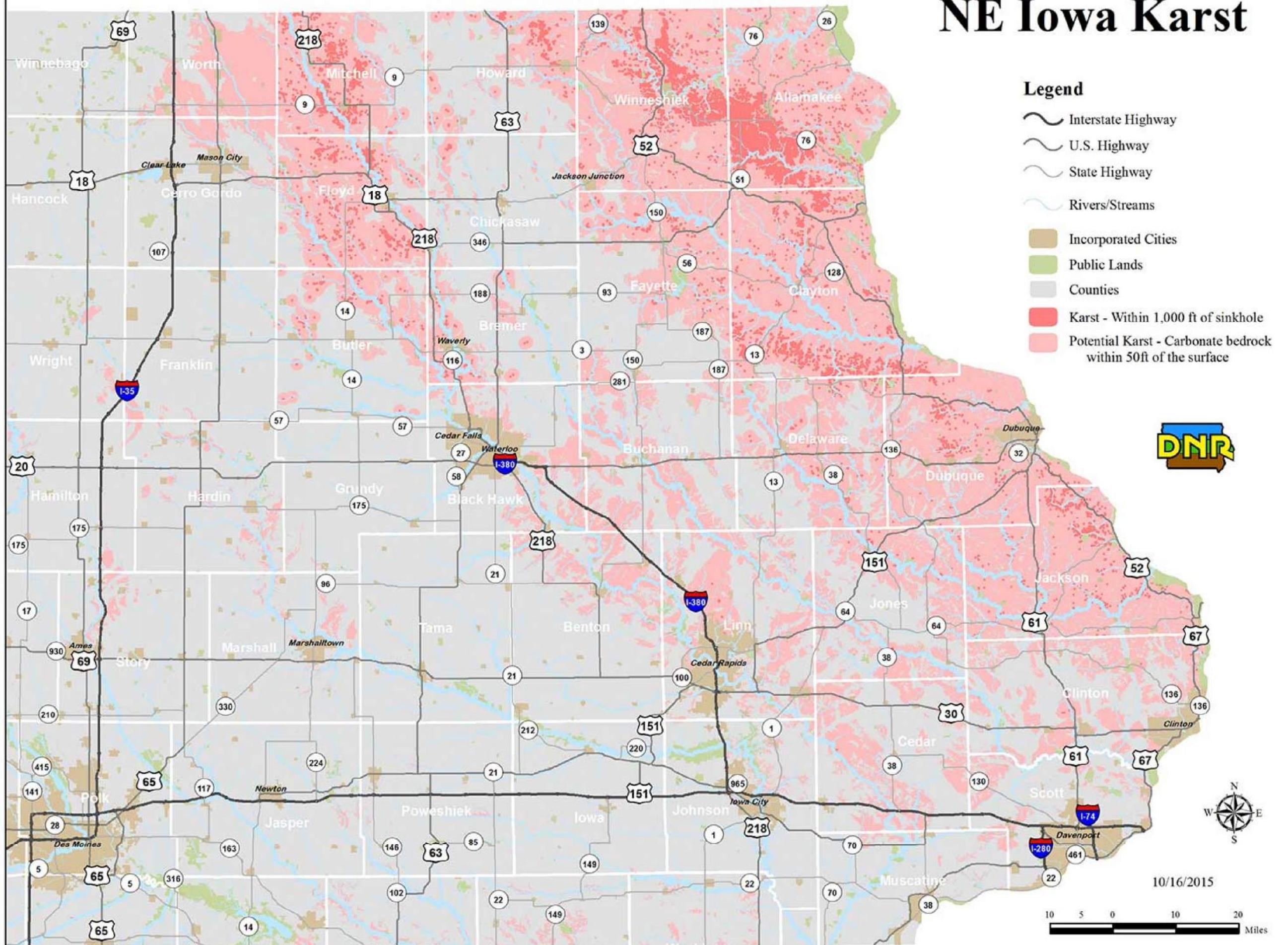


EXHIBIT D – Iowa Karst Maps

Alliant Energy
Interstate Power and Light Company
Lansing Generating Station
Lansing, Iowa

Unstable Area Determination

NE Iowa Karst



Map layers Legend

- AFO Siting Data
- Sinkholes
- Ag Drainage Well
- Wells
- Animal Feeding Operation
 - Active, Confined/Open
 - Active, Confinement
 - Active, Open Feedlot
 - Inactive
- Public Drainage Infrastructure
- Drainage Districts
- High Qty Wtr Resource (Rivers)
- High Qty Wtr Resource (Waterbody)
- Major Water Source (Rivers)
- Major Water Source (Lake)
- Surface Water
- Public Land
- Public Land Survey (PLSS)
- Designated Wetland
 - Designated Wetland
 - Wetland Buffer(2500ft)
- Sinkhole or Potential Karst
 - Sinkhole w/ 1000 ft radius
 - Karst and Potential Karst
- 100 Year Flood Plain
- Alluvial Soils

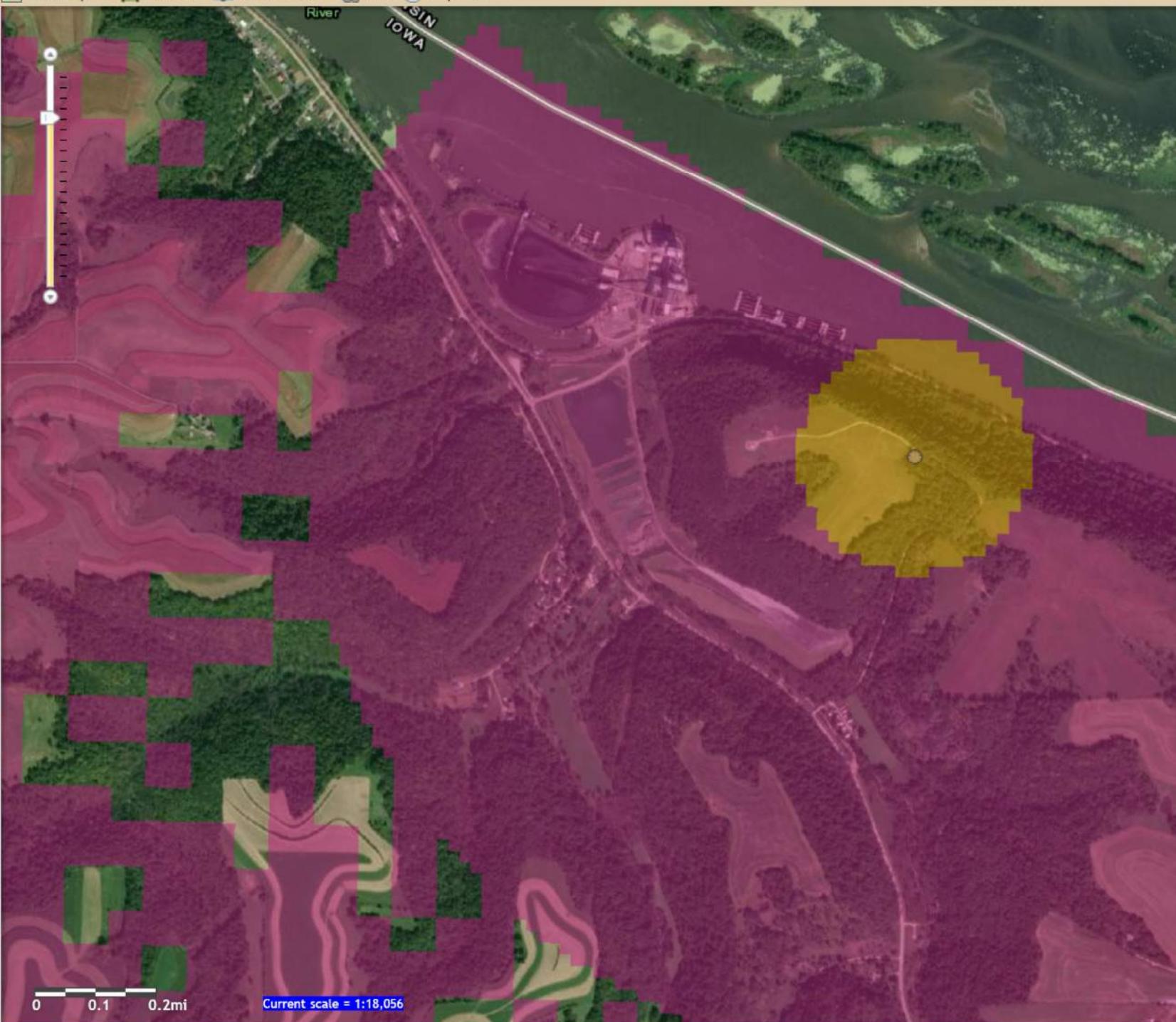
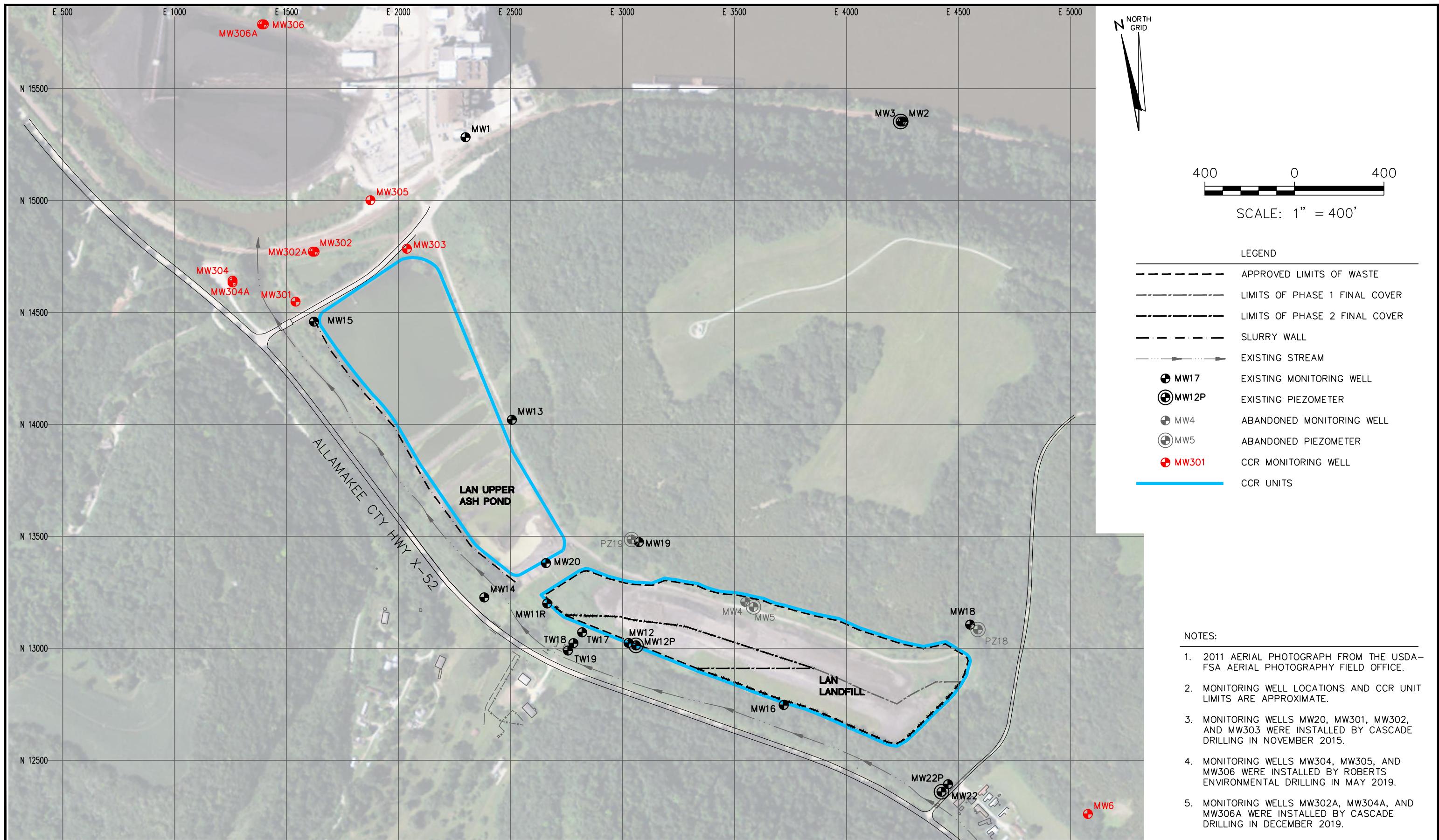


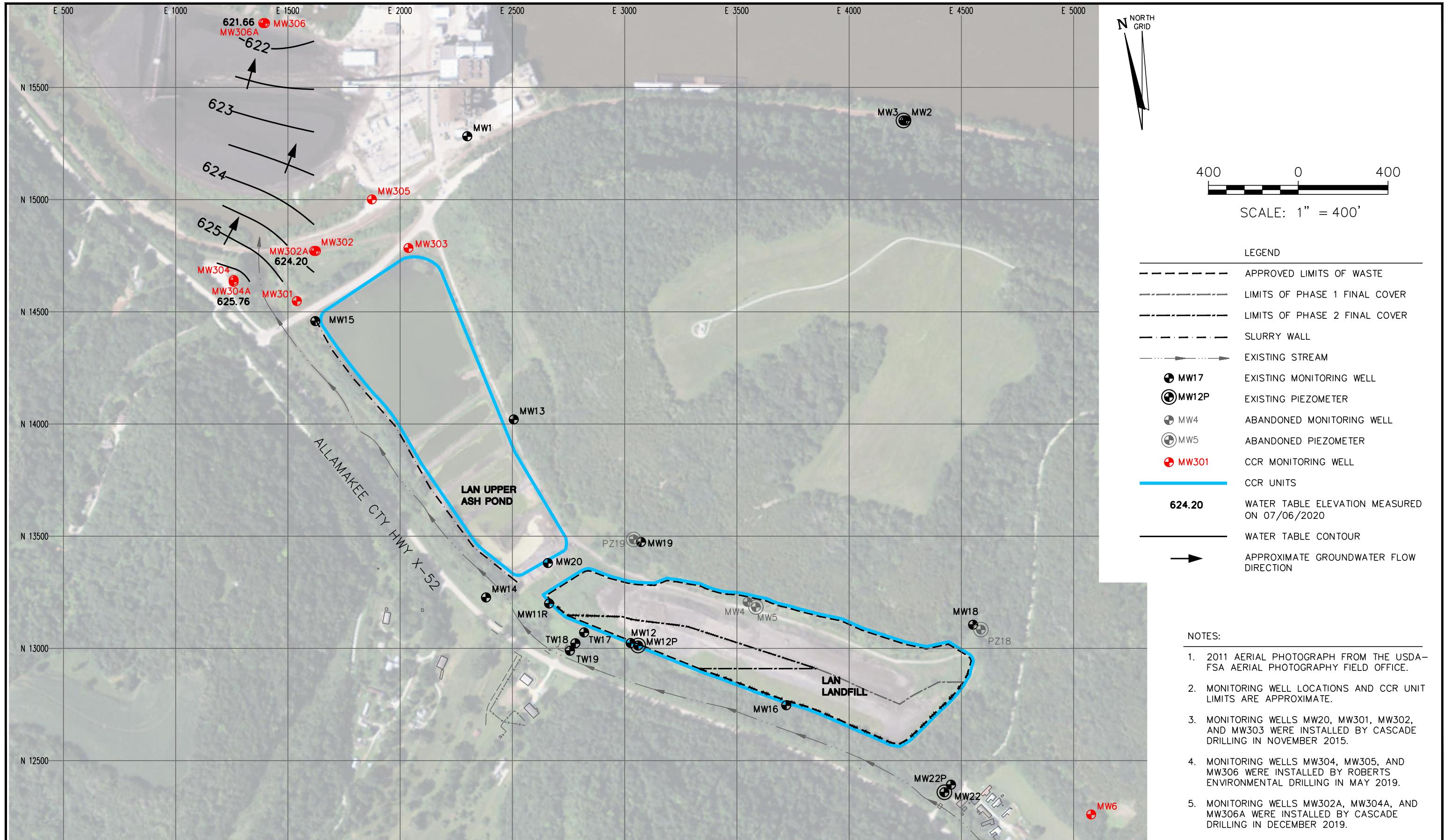
EXHIBIT E – Groundwater Info from SCS Engineers

Alliant Energy
Interstate Power and Light Company
Lansing Generating Station
Lansing, Iowa

Unstable Area Determination



PROJECT NO.	25220070.00	DRAWN BY:	BSS	FIGURE
DRAWN:	11/27/2019	CHECKED BY:	MDB	2
REVISED:	03/12/2020	APPROVED BY:	TK 03/12/2020	
ENGINEER	SCS ENGINEERS	CLIENT	ALLIANT ENERGY LANSING POWER STATION LANSING, IOWA	
	2830 DAIRY DRIVE MADISON, WI 53718-6751 PHONE: (608) 224-2830	INTERSTATE POWER AND LIGHT 2320 POWER PLANT DRIVE LANSING, IA 52151-9733		



PROJECT NO.	25220070.00	DRAWN BY:	BSS	DRAWN:	07/31/2020	CHECKED BY:	MDB	ENGINEER	SCS ENGINEERS	CLIENT	INTERSTATE POWER AND LIGHT 2320 POWER PLANT DRIVE LANSING, IA 52151-9733	SITE	ALLIANT ENERGY LANSING POWER STATION LANSING, IOWA	POTENSIOMETRIC SURFACE MAP JULY 6, 2020	FIGURE
REVISED:	07/31/2020	APPROVED BY:													
															2

Table 3. Vertical Hydraulic Gradient Summary
Interstate Power & Light - Lansing, Iowa / SCS Engineers Project #25220070.00

Vertical Hydraulic Gradients	MW4/MW5		MW2/MW3		MW12/MW12P		MW22/MW22P	
	MW4 screen bottom (feet amsl)	640.00	MW2 610.50		MW12 642.70		MW-22 650.27	
Piezometer effective screen midpoint (feet amsl)	MW5 625.00		MW3 595.00		MW12P 625.48		MW-22P 622.64	
Measurement Date	Distance between screen midpoints (feet)	Vertical Gradient (ft/ft) ⁽¹⁾	Distance between screen midpoints (feet)	Vertical Gradient (ft/ft) ⁽¹⁾	Distance between screen midpoints (feet)	Vertical Gradient (ft/ft) ⁽¹⁾	Distance between screen midpoints (feet)	Vertical Gradient (ft/ft) ⁽¹⁾
May 11, 2001	21.8	0.055	24.5	0.031	NI	NI	NI	NI
March 8, 2002	20.3	0.061	20.4	0.036	NI	NI	NI	NI
February 19, 2004	19.4	0.064	NM	NM	NI	NI	NI	NI
May 26, 2004	21.4	0.059	NM	NM	NI	NI	NI	NI
August 23, 2004	21.1	0.058	NM	NM	NI	NI	NI	NI
November 18, 2004	20.4	0.060	NM	NM	NI	NI	NI	NI
May 5, 2005	20.2	0.062	NM	NM	NI	NI	NI	NI
May 19, 2006	20.2	0.061	NM	NM	NI	NI	NI	NI
May 30, 2007	20.1	0.061	NM	NM	NI	NI	NI	NI
April 16, 2008	22.0	0.057	NM	NM	NI	NI	NI	NI
April 3, 2009	22.9	0.054	NM	NM	NI	NI	NI	NI
April 21, 2010	21.1	0.059	NM	NM	NI	NI	NI	NI
May 4, 2011	21.8	0.057	NM	NM	NI	NI	NI	NI
April 25, 2012	20.9	0.060	NM	NM	NI	NI	NI	NI
October 17, 2012	20.4	0.061	NM	NM	NI	NI	NI	NI
February 19-20, 2013	20.4	0.061	20.3	0.061	NI	NI	NI	NI
April 1, 2013	21.1	0.058	20.6	0.054	NI	NI	NI	NI
July 1, 2013	25.6	0.046	23.2	0.034	NI	NI	NI	NI
April 29, 2014	22.1	0.057	NM	NM	21.7	-0.013	NI	NI
May 29, 2014	21.8	0.013	22.4	0.006	21.4	-0.015	NI	NI
April 20, 2015	21.0	0.059	20.3	0.034	21.0	-0.013	NI	NI
April 28, 2016	20.8	0.060	20.4	0.028	20.9	-0.002	NI	NI
April 19-21, 2017	24.4	0.048	21.3	-0.001	22.7	-0.012	36.7	-0.025
April 16-17, 2018	ABANDONED		20.7	-0.161	22.0	-0.016	NM	NM
April 26, 2018	ABANDONED		20.7	-0.156	21.7	0.036	35.6	-0.031
April 15-16, 2019	ABANDONED		26.3	-0.143	23.0	-0.016	38.0	-0.048
June 20, 2019	ABANDONED		NM	NM	NM	NM	NM	NM
October 2, 2019	ABANDONED		NM	NM	NM	NM	NM	NM
December 5, 2019	ABANDONED		NM	NM	NM	NM	NM	NM
February 5, 2020	ABANDONED		NM	NM	NM	NM	NM	NM
May 20-21, 2020	ABANDONED		20.6	0.037	23.1	-0.018	38.6	-0.044
July 6, 2020	ABANDONED		NM	NM	NM	NM	NM	NM
August 19-21, 2020	ABANDONED		NM	NM	NM	NM	NM	NM
October 19-20, 2020	ABANDONED		20.4	0.041	22.8	-0.016	38.1	-0.044

Notes:

1: A positive vertical gradient indicates upward groundwater flow. A negative gradient indicates downward flow.

2: The screen midpoint for water table wells is calculated as the midpoint between the water table elevation and screen bottom elevation.

NM: Not Measured

NI: Not Installed

Created by:

Created by:
Last revision by:

Last revision by:

MDF

MDB
ACW

ACV
RM

Date: 8/9/2013

Date: 8/17/2015

Date: 10/22/2020

Table 2. Vertical Hydraulic Gradient Summary
Interstate Power & Light - Lansing, Iowa / SCS Engineers Project #25220070.00

Vertical Hydraulic Gradients	MW302/MW302A	MW304/MW304A	MW306/MW306A			
	MW302 screen bottom (feet amsl)	MW304 screen bottom (feet amsl)	MW306 screen bottom (feet amsl)			
Piezometer effective screen midpoint (feet amsl)	MW302A 592.43	MW304A 591.10	MW306A 587.06			
Measurement Date	Distance between screen midpoints (feet)	Vertical Gradient (ft/ft) ⁽¹⁾	Distance between screen midpoints (feet)			
May 20-21, 2020	29.9	-0.150	29.9	0.111	28.9	-0.001
July 6, 2020	NM	NM	NM	NM	NM	NM
August 19-21, 2020	29.8	-0.135	30.0	NM	28.9	0.009
October 19-20, 2020	29.6	-0.139	29.8	0.101	28.6	0.009

Notes:

1: A positive vertical gradient indicates upward groundwater flow. A negative gradient indicates downward flow.

2: The screen midpoint for water table wells is calculated as the midpoint between the water table elevation and screen bottom elevation.

NM: Not Measured

NI: Not Installed

Created by:

TK

Date: 10/23/2020

Last revision by:

TK

Date: 10/23/2020

Checked by:

NDK

Date: 10/23/2020

I:\25220070.00\Data and Calculations\Tables\[LAN_wlstat.xls]gradient (CCR Wells)