# Run-On and Run-Off Control Plan Update – Phase 1, Modules 1 through 6 and Phase 2, Modules 10 and 11

Columbia Dry Ash Disposal Facility Columbia Energy Center W8375 Murray Road Pardeeville, Wisconsin 53954

Prepared for:

Wisconsin Power and Light Company Columbia Energy Center W8375 Murray Road Pardeeville, Wisconsin 53954

#### SCS ENGINEERS

25222260.00 | February 1, 2023

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#### PE CERTIFICATION

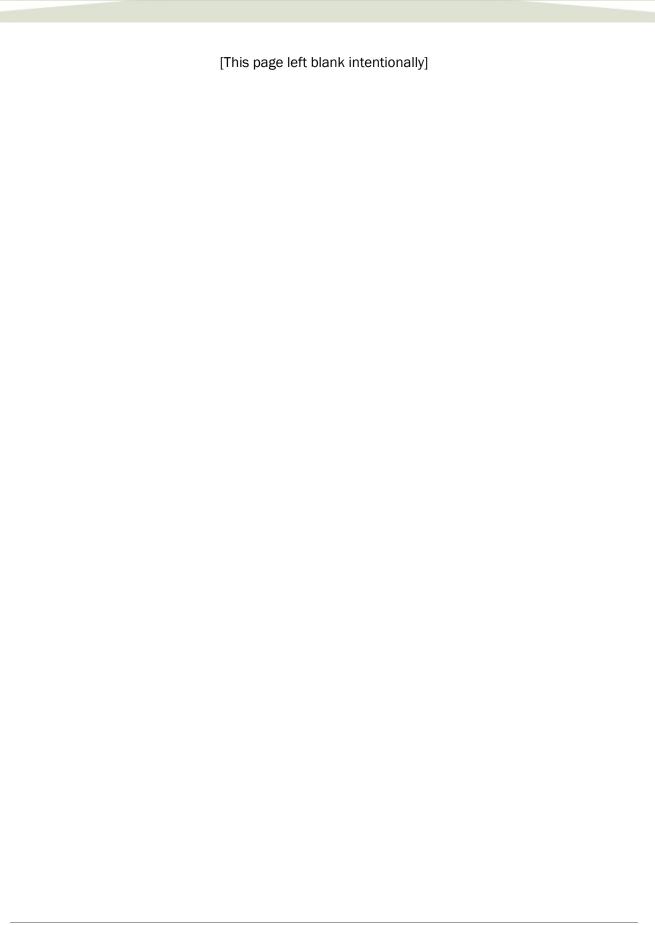


I, Phillip Gearing, hereby certify that I am a licensed professional engineer in the State of Wisconsin in accordance with the requirements of ch. A–E 4, Wis. Adm. Code; that this document has been prepared in accordance with the Rules of Professional Conduct in ch. A–E 8, Wis. Adm. Code; and that, to the best of my knowledge, all information contained in this document is correct and the document was prepared in compliance with all applicable requirements in chs. NR 500 to 538, Wis. Adm. Code.

#### Specifically,

 This Run-On and Run-Off Control Plan Update was prepared by me or under my direct supervision and meets the requirements of 40 CFR 257.81(c) and NR 514.07(10)(b)

11/1/4	/	
Mlfs Hear	an)	February 1, 2023
(signaturé)		(date)
Phillip E. Gearing		
(printed or typed name	<del>)</del>	
License number	<u>E-45115</u>	
My license renewal da	te isJuly 31, :	2024
Pages or sheets cover	ed by this seal:	
		ate - Phase 1, Modules 1 through 6
and Phase 2, Modules	3 10 and 11	
Columbia Dry Ash Disp	oosal Facility, Co	lumbia Energy Center
W8375 Murray Road	Pardeeville Wis	consin 5395/



#### 1.0 INTRODUCTION AND PROJECT SUMMARY

The Columbia Dry Ash Disposal Facility includes an active coal combustion residual (CCR) landfill, which currently consists of the following modules, located in Phase 1 and Phase 2 of the facility.

- Phase 1, Module 1 This module has received final cover over completed outer sideslope areas that will no longer receive additional CCR; intermediate cover has been placed over remaining areas.
- Phase 1, Module 2 This module has received intermediate cover over a majority of the in-place CCR.
- Phase 1, Module 3 This module has received intermediate cover over a majority of the in-place CCR.
- Phase 1, Module 4 This module is currently being filled.
- Phase 1, Module 5 This module was constructed in 2021 and is approved by Wisconsin Department of Natural Resources (WDNR) to receive CCR.
- Phase 1, Module 6 This module was constructed in 2021 and is approved by WDNR to receive CCR.
- Phase 2, Module 10 Module 10 liner construction began in 2022. The new module will be used for disposal following approval of the liner Construction Documentation Report, which will be submitted for WDNR review in 2023.
- Phase 2, Module 11 Module 11 liner construction began in 2022. The new module will be used for disposal following approval of the liner Construction Documentation Report, which will be submitted for WDNR review in 2023.

Phase 1, Modules 1-3 were previously described as separate existing CCR landfills although they are contiguous and are managed as a single landfill by the facility and by the WDNR. WPL clarified that Modules 1-3 are one existing CCR landfill under the federal CCR Rule. Phase 1, Modules 4-6 are considered a new CCR landfill that initiated construction after October 19, 2015, and are therefore managed as a separate CCR unit under the federal CCR Rule even though they are contiguous to Modules 1-3. In addition, the new CCR landfill will include Phase 2, Modules 10 and 11, which is near completion and will begin receiving CCR in 2023 after full WDNR approval.

Phase 2, Modules 7-9 and 12-13 are permitted with the WDNR, but have not been developed. If developed, the units will also be part of the new CCR landfill, as defined at 40 CFR 257.53 and NR 500.03. Construction of additional modules is not currently planned prior to retirement of the Columbia Energy Center, which is currently scheduled to occur no later than June 1, 2026.

Figure 1 shows the site location. Figure 2 shows the run-on and run-off drainage areas.

On behalf of Wisconsin Power and Light Company (WPL), SCS Engineers (SCS) has prepared this Run-On and Run-Off Control Plan Update for the Columbia (COL) Dry Ash Disposal Facility in accordance with 40 CFR 257.81(c)(1) and NR 514.07(10)(b) as follows.

**40 CFR 257.81(c)(4).** "The owner or operator of the CCR unit must prepare periodic run-on and run-off control system plans required by paragraph (c)(1) of this section every five years. The date of completing the initial plan is the basis for establishing the deadline to complete the first subsequent plan. The owner or operator may complete any required plan prior to the required deadline provided the owner or operator places the completed plan into the facility's operating record within a reasonable amount of time. In all cases, the deadline for completing a subsequent plan is based on

the date of completing the previous plan. For purposes of this paragraph (c)(4), the owner or operator has completed a periodic run-on and run-off control system plan when the plan has been placed in the facility's operating record as required by §257.105(g)(3)."

NR 514.07(10)(b)(4). "Modification every 5 years from the date of the most recent plan approval or whenever there is a change in conditions that may substantially affect the written plan in effect. The modification shall be requested by the owner or operator in accordance with s. NR 514.04 (6) prior to the 5-year deadline."

The initial Run-On and Run-Off Control Plan was completed in 2016, and updates were completed in 2018 prior to receipt of CCR in Phase 1, Module 4 and in 2021, prior to receipt of CCR in Phase 1, Modules 5 and 6.

#### 1.1 PERIODIC PLAN UPDATES

The following items have been updated in this plan prior to receipt of CCR in Phase 2, Modules 10 and 11:

- Run-On and Run-Off Drainage Areas Figure 2 has been updated to show topographic data for active landfill areas obtained during the most recent survey of the existing landfill in January 2023 and construction of Phase 2, Modules 10 and 11 in 2022. Additional intermediate cover has been placed in Modules 3, 4, 5, and 6 since the latest survey reducing the area contributing run-off as contact water. Modules 5 and 6 no longer have a temporary rain cover; however, rain cover may be used in the future to reduce the area contributing run-off as contact water (refer to Section 2.0). Additional intermediate cover will be added to active landfill areas as Modules 10 and 11 begin receiving CCR to maintain contributing run-off area.
- Storm Water Calculations Additional storm water calculations were completed for Modules 10 and 11 as described in Section 2.0.
- Primary Ash Pond The Primary Ash Pond will no longer accept contact water from the landfill. As needed, contact water will be transported to the plant for discharge through Outfall 003 rather than disposal at the Primary Ash Pond.
- No other changes impacting the run-on and run-off controls have been identified with this update.
- This update also incorporates the requirements of NR 514.07(10)(b), which became effective August 1, 2022.

#### 2.0 RUN-ON AND RUN-OFF CONTROL PLAN

**40 CFR 257.81(a).** "The owner or operator of an existing or new CCR landfill or any lateral expansion of a CCR landfill must design, construct, operate, and maintain:

(1) A run-on control system to prevent flow onto the active portion of the CCR unit during the peak discharge from a 24-hour, 25-year storm."

NR 514.07(10)(b). "A run-on and run-off control system plan that includes all of the following:

(1) A run-on and run-off control system designed in accordance with the requirements under s. NR 504.12 (2)."

NR 504.12 (2). "An existing or new CCR landfill or any lateral expansion of a CCR landfill shall be designed, constructed, operated, and maintained with a run-off and run-on control system in accordance with the requirements under s. NR 504.09 (1) (f) and (g) and all of the following:

(a) A run–on control system shall prevent flow onto the active portion of the CCR landfill during the peak discharge from a 24–hour, 25–year storm."

The entire facility has run-on and run-off control in place, as approved by the WDNR and further described below. Run-on is controlled by berms and swales around the perimeter of the landfill that divert storm water away from the landfill to a sedimentation basin.

**40 CFR 257.81(a)(2)** "A run-off control system from the active portion of the CCR unit to collect and control at least the water volume resulting from a 24-hour, 25-year storm."

NR 504.12 (2)(b) "A run-off control system from the active portion of the CCR landfill shall collect and control, at a minimum, the water volume resulting from a 24-hour, 25-year storm."

Run-off from the active portions of the facility is handled as leachate and is collected by a leachate collection system and internal swales, which route the contact water run-off to the Leachate/Surface Water Pond. Modules 4-6 and all module fills going forward will have intermediate cover added to reduce contact water that is directed to the pond. The contact water in the basin is used for dust control or other actions within the active landfill or, if needed, is transported with a water wagon to the generating station where it may be discharged through Outfall 003 inside the plant in accordance with a Wisconsin Pollutant Discharge Elimination System (WPDES) permit.

Run-off from areas outside existing CCR units and areas of the existing CCR units where final or intermediate cover is in place is diverted into the perimeter drainage swales, which drain to the South Sedimentation Basin and a lower are north of the landfill. Intermediate swales/berms and downslope channels on the final cover help minimize erosion of the final cover and divert water to the perimeter drainage system, and ultimately to the on-site detention/sedimentation basin. Per 40 CFR 257.81(b), this is consistent with the surface water requirements under 40 CFR 257.3-3.

In addition to these controls, a temporary rain cover may be installed to limit leachate and contact water production when needed. Storm water collected on the rain cover will be diverted to perimeter swales. The rain cover will be removed in sections to accommodate waste placement. As the rain cover is removed, new diversion berms will be constructed to form the perimeter of a storm water containment area. The berms will prevent contact water from running onto the rain cover and will anchor or ballast the rain cover at the new limits. When the rain cover has been fully removed, runoff will be controlled by the limits of the developed modules, and all water inside the lined waste limits will be managed as contact water.

#### 2.1 DESIGN CRITERIA

The storm water features described above are designed to handle run-on and run-off from a 25-year, 24-hour storm event, as required by 40 CFR 257.81(a)(1) and (2) and NR 504.12(2)(a) and (b). Storm water run-off calculations were updated in 2022. The calculations were performed assuming a 25-year, 24-hour precipitation depth of 4.91 inches, based on National Oceanic and Atmospheric Administration (NOAA) Atlas 14 precipitation data published in April 2013. The

detention/sedimentation basin and associated basin outlet structures are designed to safely pass run-off from a 100-year, 24-hour storm event.

Table 1. Storm Water Updates

Year Conducted	Description of Update	Included in Appendix A
Run-On and	Run-Off	
2000	Run-on calculations performed as part of the 2000 Plan of Operation Update; performed assuming 25-year, 24-hour precipitation depth of 4.7 inches, based on Technical Paper-40 (TP-40) precipitation data published in May 1961.	Yes, Included in Appendix A
2010	Run-off calculations performed as part of the 2010 Plan of Operation Update; performed assuming 25-year, 24-hour precipitation depth of 4.7 inches, based on TP-40 precipitation data published in May 1961.	Superseded by Phase 1, Modules 5 & 6
2015	Update to leachate/surface water pond calculations; performed assuming 25-year, 24-hour precipitation depth of 4.9 inches, based on NOAA Atlas 14 precipitation data published in April 2013.	Superseded by Phase 1, Module 4
2016	Update to run-on to a ditch along the north end of Module 3; performed assuming 25-year, 24-hour precipitation depth of 4.9 inches, based on NOAA Atlas 14 precipitation data published in April 2013.	Superseded by Phase 1, Module 4
2016	Calculations to evaluate installation of a rain cover in Module 3; performed assuming 25-year, 24-hour precipitation depth of 4.9 inches, based on NOAA Atlas 14 precipitation data published in April 2013.	Superseded by Phase 1, Module 4
2017	Update to leachate/surface water pond calculations with consideration of Phase 1, Module 4 construction; performed assuming 25-year, 24-hour precipitation depth of 4.9 inches, based on NOAA Atlas 14 precipitation data published in April 2013.	Superseded by Phase 1, Modules 5 & 6
2018	Calculations to evaluate installation of a rain cover in Module 4; performed assuming 25-year, 24-hour precipitation depth of 4.9 inches, based on NOAA Atlas 14 precipitation data published in April 2013.	Superseded by Phase 1, Modules 5 & 6
2018	Calculations to size swales and culverts to divert run-on as part of construction of Module 4, performed assuming 25-year, 24-hour precipitation depth of 4.9 inches, based on NOAA Atlas 14 precipitation data published in April 2013.	Superseded by Phase 1, Modules 5 & 6
2021	Update to leachate/surface water pond calculations with consideration of Phase 1, Modules 5 and 6 construction; performed assuming 25-year, 24-hour precipitation depth of 4.9 inches, based on NOAA Atlas 14 precipitation data published in April 2013.	Superseded by Phase 2, Modules 10 & 11
2021	Calculations to size swales and culverts to divert run-on as part of construction of Modules 5 and 6, performed assuming 25-year, 24-hour precipitation depth of 4.9 inches, based on NOAA Atlas 14 precipitation data published in April 2013.	Superseded by Phase 2, Modules 10 & 11

Year Conducted	Description of Update	Included in Appendix A			
Run-On and	Run-On and Run-Off				
2021	Calculations to confirm South Sedimentation Basin can handle storm water after construction of Modules 5 and 6, performed assuming 25-year, 24-hour precipitation depth of 4.9 inches, based on NOAA Atlas 14 precipitation data published in April 2013.	Superseded by Phase 2, Modules 10 & 11			
2022	Update to leachate/surface water pond calculations with consideration of Phase 2, Modules 10 and 11 construction; performed assuming 25-year, 24-hour precipitation depth of 4.9 inches, based on NOAA Atlas 14 precipitation data published in April 2013.	Yes, Included in Appendix A			
2022	Calculations to size swales and culverts to divert run-on as part of construction of Modules 10 and 11, performed assuming 25-year, 24-hour precipitation depth of 4.9 inches, based on NOAA Atlas 14 precipitation data published in April 2013.	Yes, Included in Appendix A			
2022	Calculations to confirm South Sedimentation Basin can handle storm water after construction of Modules 10 and 11, performed assuming 25-year, 24-hour precipitation depth of 4.9 inches, based on NOAA Atlas 14 precipitation data published in April 2013.	Yes, Included in Appendix A			

#### 2.2 DESIGN WITH CALCULATIONS

Storm water management design calculations are contained in **Appendix A**, as required by 40 CFR 257.81(c)(1) and NR 514.07(10)(b)(2). As described in **Section 2.1**, the calculations from the 2000 Plan of Operation Update and the 2022 calculations describe the storm water management design and provide calculations showing that the run-on control system will prevent flow onto the active portion of the CCR units during the peak discharge from a 25-year, 24-hour storm. The 2022 calculations also describe the storm water management design and provide calculations showing that the run-off control system for the active portions of the CCR units will collect and control the water volume resulting from a 25-year, 24-hour storm. The calculations were performed by or overseen by a professional engineer licensed in the State of Wisconsin.

#### 2.3 CONSTRUCTION

Existing storm water management features were constructed to site specifications with construction oversight directed by a professional engineer licensed in the State of Wisconsin. Construction documentation reports for the storm water management features were prepared, submitted to the WDNR, and approved by the WDNR. Any future construction features will have been previously approved.

#### 3.0 CERTIFICATIONS

**40 CFR 257.81(c)(5).** "The owner or operator must obtain a certification from a qualified professional engineer stating that the initial and periodic run-on and run-off control system plans meet the requirements of this section."

Phillip Gearing, PE, a licensed profession engineer in the State of Wisconsin, has overseen the preparation of this Run-On and Run-Off Control Plan. A certification statement is provided on **page iii** of this plan.

#### 4.0 RECORDKEEPING AND PERIODIC UPDATES

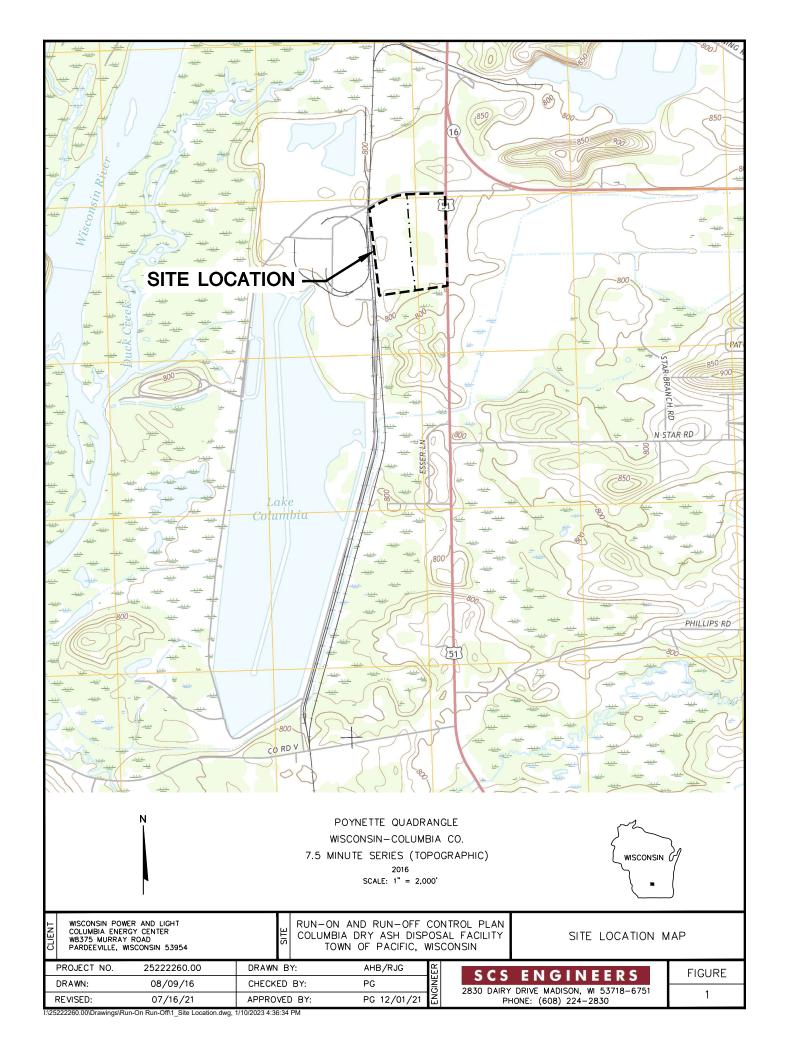
**40 CFR 257.81(d).** "The owner or operator of the CCR unit must comply with the recordkeeping requirements specified in section 257.105(g), the notification requirements specified in section 257.106(g), and the internet requirements specified in section 257.107(g)."

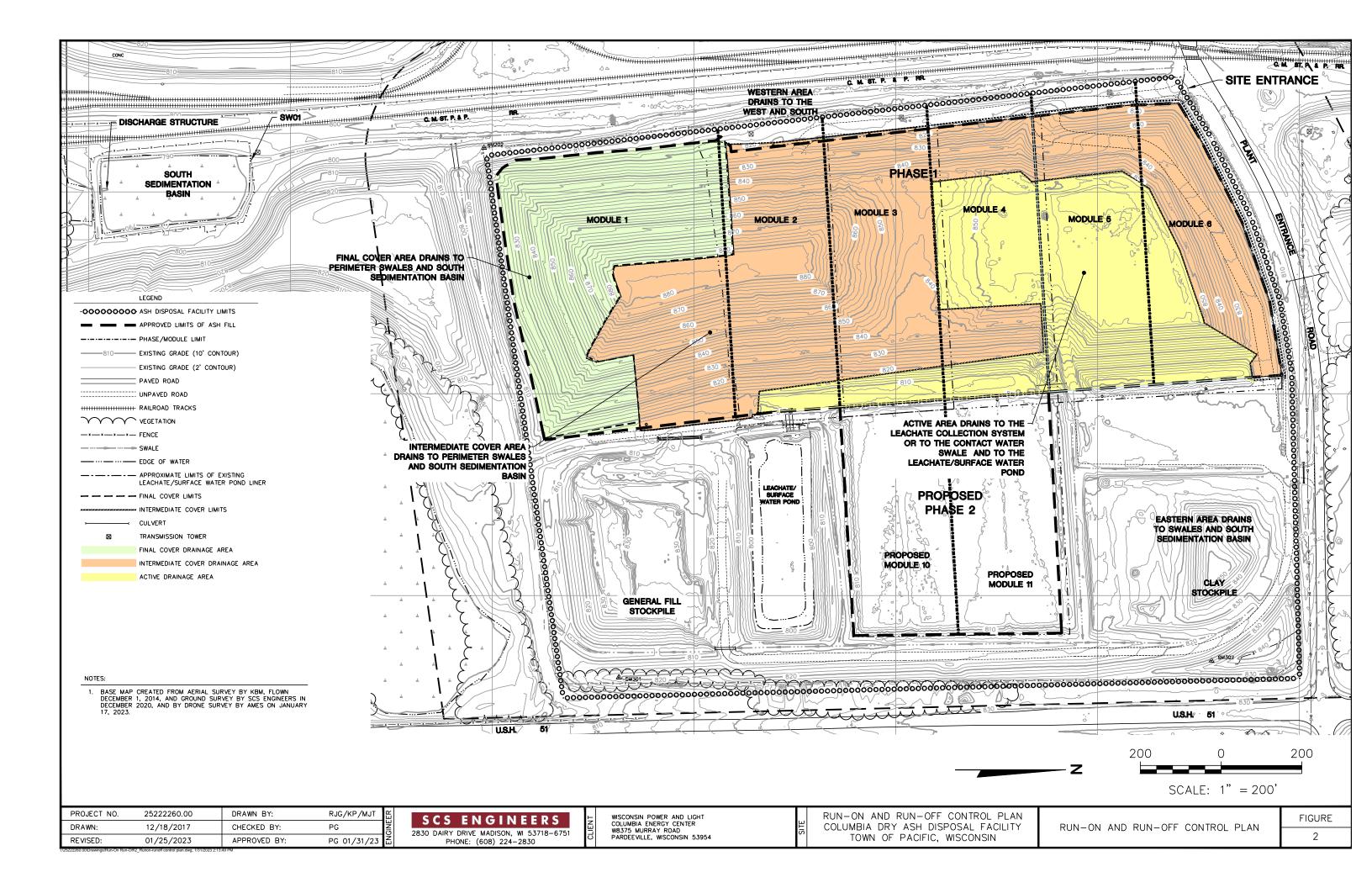
This Run-On and Run-Off Control Plan, and all periodic plans, will be placed in the facility's operating record and on Alliant Energy's CCR Rule Compliance Data and Information website, as will all amendments. Periodic plan updates will be completed at least every 5 years per 40 CFR 257.81(c)(4) and NR 514.07(10)(b)(4).

WPL will notify the State Director when this Run-On and Run-Off Control Plan, and all subsequent updates, are available in the facility's operating record and on the facility's website per 40 CFR 257.105(g), 257.106(g), and 257.107(g) and NR 506.17(2) and (3).

### Figures

- 1
- Site Location Map Run-On and Run-Off Control Plan 2





# Appendix A Storm Water Design Calculations

# Appendix A1 2000 Plan of Operations Update

#### **PURPOSE:**

The purpose of the surface water runoff calculations is to demonstrate that the surface water control features incorporated into the proposed design will collect and transfer surface water from the landfill in a controlled manner and will minimize erosion. The surface water runoff calculations were performed for the western half (Phase 1) of the landfill, which this 10-year Plan of Operation Update report addresses.

#### SITE GEOMETRY:

The surface water runoff from Phase 1 of the landfill will be routed to the existing South Sedimentation Basin. Diversion berms, downslope channels, and perimeter ditches are incorporated into the design to route the surface water to the southwestern corner of the landfill, where it is then routed to the South Sedimentation Basin. The South Sedimentation Basin was constructed during construction of Module 1 North. The south sedimentation pond discharges to a wetland area to the south of the pond.

#### **METHODOLOGIES:**

The following methods and procedures were used to demonstrate that the proposed surface water control features will collect and transfer surface water in controlled manner and minimize erosion potential:

#### Hydrograph Generation

Peak stormwater flows for the 25-year, 24-hour and 100-year, 24-hour storm events were calculated using the Quick TR-55 computer model developed by the National Resources Conservation Service (NRCS) (formerly known as the Soil Conservation Service (SCS)). The Quick TR-55 methods for computing hydrographs are based on the methodologies presented in the Urban Hydrology for Small Watersheds manual. The Quick TR-55 model is designed to simulate the surface runoff response of a watershed to a precipitation event. Input parameters for the model include precipitation depth for a particular storm event, contributing drainage areas, runoff curve numbers, and time of concentration.

The time of concentration calculations combine overland flow time (i.e., sheet flow), shallow concentrated flow time, and channel flow time. Curve numbers for a specified drainage area were also calculated using the methodologies and tables presented in TR-55 (see **Reference** section at the end of this appendix).

#### Diversion Berm, Downslope Channels, and Perimeter Ditch Sizing

These control structures are sized to channel the peak storm runoff to the sedimentation basin while maintaining low enough velocities to limit the erosion potential. The proposed design allows storm water which comes into contact with the final cover to be routed by diversion berms and downslope channels to the perimeter ditches, which will then transport the water to the south sedimentation basin.

Diversion berm, downslope channels, and perimeter ditch locations and details are shown on the Plan Sheets. A portion of the perimeter ditch along the western side of the landfill was constructed as part of the construction of Module 1 North.

In conjunction with the graphical peak discharge methods as presented in TR-55, the Flowmaster computer modeling program was used to assist in the design of these control structures. This program allows the user to input the channel geometry, the slope of the channel, an estimated Manning's "n" value for the channel, and the peak flow in the channel. The program then determines the peak flow depth and the peak velocity for the given geometry of the control feature.

The diversion berms, downslope channels, and perimeter ditches were sized by calculating the peak flow each structure would have to manage in a worst-case design scenario (i.e., surface water runoff from the largest area of landfill final cover during the 25-year, 24-hour storm event). The drainage structure was modeled using the Flowmaster computer model to verify channel depth and velocity in the structure.

#### Sedimentation Pond Sizing

The sedimentation pond sizing process involved determining the proper ratio of surface area to flowrate that would allow a 15 micron particle size to settle out during a design storm event.

A table presented in the <u>Erosion and Sediment Control Handbook</u> (Goldman et al., 1986) provides the surface area-to-discharge ratios required to achieve settlement of the desired particle sizes (see the **Reference** section of this appendix).

The Pond Pack 6.0 computer program was used in conjunction with accepted formulas and engineering calculations to size the sedimentation basins. Calculations were performed to determine the performance of the basins as follows:

- 1. The inflow hydrograph for the basin was calculated as part of the hydrograph computations. The regulations require that sediment basins be sized for a 25-year, 6-hour storm event. Sediment basin calculations for the Alliant Columbia Ash Disposal Facility were based on the basin's peak discharge during the 25-year, 24-hour storm which equals or exceeds the basin inflow for average rainfall intensity of the 25-year, 6-hour storm.
- 2. Outlet structures were designed to provide the necessary detention of peak stormwater runoff from the final cover for the 25-year, 24-hour storm event.
- 3. The inflow hydrograph was routed through the sedimentation pond using the Pond Pack 6.0 program to determine the basin's peak water elevation and discharge during the 25-year, 24-hour storm.
- 4. The emergency spillways for the sedimentation basins were sized for the 100-year, 24-hour storm event.

#### **ASSUMPTIONS:**

Summarized below are some of the major assumptions and data used in the computations:

1. Due to the presence of a drainage layer in the proposed landfill final cover, the soil for the landfill area was modeled between a Type B and C soil to account for greater water infiltration

through the cover. The final cover was modeled as a grassland in good condition, which resulted in a runoff curve number of 67.5.

- 2. SCS Type II storm was selected according to SCS storm distribution maps for the United States.
- 3. A 2-year, 24-hour storm event in the vicinity of the facility equates to 2.7 inches according to figures provided in TR-55.
- 4. A 25-year, 24-hour storm event in the vicinity of the facility equates to 4.7 inches according to precipitation data provided in TR-55.
- 5. A 100-year, 24-hour storm event in the vicinity of the facility equates to 5.9 inches according to precipitation data provided in TR-55.
- 6. Grass-lined berms and channels were designed for a maximum velocity of 4 feet per second (fps).
- 7. A Manning's "n" value of 0.045 was used to model a grass-lined berm or channel, as provided by the parameters set in the Flowmaster model.
- 8. Depths of channels were designed to be a minimum of 1 foot, with a minimum freeboard of 0.5 foot. Depths of diversion berms were designated to be a minimum of 2 feet, with a minimum of 0.5 foot of freeboard.
- 9. A 15-micron particle was targeted to be settled out of the water column. The 15-micron particle is classified as a medium-fine silt by the AASHTO Soil Classification System.

#### **RESULTS:**

Based on the results of the surface water runoff computations presented in this appendix, the proposed surface water control features will adequately handle the runoff from a 25-year, 24-hour storm event while minimizing erosion. The drainage features will be constructed as shown on the Plan Sheets.

All diversion berms and perimeter ditches will maintain greater than 0.5 foot of freeboard during the design storm event. The sedimentation basins will settle out particles 15 microns and larger in diameter and will dewater in no less than three days. The detailed calculations are included with this appendix.

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# Time of Concentration Calculations

Type.... Tc Calcs

Name.... LF TO S BASIN

Page 1.01

File.... I:\1370\Columbia.ppk

Title... Landfill runoff to south basin

Landfill Area (1/2)

TIME OF CONCENTRATION CALCULATOR

Landfill runoff to south basin

Segment #1: Tc: TR-55 Sheet Description: final cover slope

Mannings n .1900 Hydraulic Length 60.00 ft 2yr, 24hr P 2.7000 in Slope .050000 ft/ft

Avg. Velocity

.17 ft/sec

Segment #1 Time: .0989 hrs

Segment #2: Tc: TR-55 Sheet Description: final cover slope

Mannings n .1900 Hydraulic Length 60.00 ft 2yr, 24hr P 2.7000 in Slope .250000 ft/ft

Avg. Velocity .32 ft/sec

Segment #2 Time: .0520 hrs

Segment #3: Tc: TR-55 Shallow

Description: diversion berm

Hydraulic Length 1530.00 ft

Slope

.020000 ft/ft

Unpaved

Avg. Velocity 2.28 ft/sec

Segment #3 Time: .1863 hrs

S/N: H0M0L0862791 BT 2, Inc

Pond Pack Ver: 8-01-98 (61) Compute Time: 13:29:40 Date: 08-23-2000

Type.... Tc Calcs

Name.... LF TO S BASIN

Page 1.02

File.... I: $\1370\$ Columbia.ppk

Title... Landfill runoff to south basin

Landfill Area (2/2)

Segment #4: Tc: TR-55 Channel Description: perimeter ditch

Flow Area 32.0000 sq.ft

Wetted Perimeter 22.60 ft

Hydraulic Radius 1.42 ft

Slope .006000 ft/ft Slope Mannings n

.0300

Hydraulic Length 320.00 ft

Avg. Velocity 4.85 ft/sec

Segment #4 Time: .0183 hrs

\_\_\_\_\_\_\_

Total Tc: .3555 hrs

\_\_\_\_\_\_

West peripheral area leading Page 1.01 Type.... Tc Calcs Name.... PERIPH TO S BASI to west perimeter ditch (1/2) File.... I:\1370\COLUMBIA.PPK Title... Peripheral area to south basin (area outside of LF leading to basin) TIME OF CONCENTRATION CALCULATOR Peripheral area to south basin (area outside of LF leading to basin) Segment #1: Tc: TR-55 Sheet Description: flow into ditch Mannings n .1900 Hydraulic Length 10.00 ft 2yr, 24hr P 2.7000 in Slope .330000 ft/ft Avg. Velocity .25 ft/sec Segment #1 Time: .0111 hrs Segment #2: Tc: TR-55 Channel Description: flow along perimeter ditch Flow Area 22.0000 sq.ft Wetted Perimeter 17.60 ft
Hydraulic Radius 1.25 ft
Slope .006000 ft/ft
Mannings n .0300
Hydraulic Length 800.00 ft Avg. Velocity 4.46 ft/sec Segment #2 Time: .0498 hrs Segment #3: Tc: TR-55 Channel Description: flow along perimeter ditch 57.0000 sq.ft Flow Area Wetted Perimeter 29.00 ft
Hydraulic Radius 1.97 ft
Slope .006000 ft/ft
Mannings n .0300
Hydraulic Length 1010.00 ft Avg. Velocity 6.04 ft/sec Segment #3 Time: .0465 hrs

S/N: H0M0L0862791 BT 2, Inc

Type.... Tc Calcs Name.... PERIPH TO S BASI West peripheral area leading Page 1.02 to West perimeter ditch (z/z)

File.... I:\1370\COLUMBIA.PPK

Title... Peripheral area to south basin (area outside of LF

leading to basin)

Total Tc: .1073 hrs

S/N: H0M0L0862791 BT 2, Inc

Pond Pack Ver: 8-01-98 (61) Compute Time: 08:51:25 Date: 08-30-2000

Type.... Tc Calcs Northeast peripheral Page 1.01 area leading to east perimeter ditch Page 1.01 Name.... E PERIPHERAL File.... I:\1370\COLUMBIA.PPK (1/1) Title... Eastern peripheral area (north of leachate basin) leading to east ditch TIME OF CONCENTRATION CALCULATOR Eastern peripheral area (north of leachate basin) leading to east ditch Segment #1: Tc: TR-55 Sheet Mannings n .1900 Hydraulic Length 40.00 ft 2yr, 24hr P 2.7000 in Slope .425000 ft/ft Avg. Velocity .37 ft/sec Segment #1 Time: .0304 hrs Segment #2: Tc: TR-55 Sheet Mannings n .1900 Hydraulic Length 260.00 ft 2yr, 24hr P 2.7000 in Slope .023000 ft/ft .17 ft/sec Avg. Velocity Segment #2 Time: .4362 hrs Segment #3: Tc: TR-55 Shallow Hydraulic Length 520.00 ft .014000 ft/ft Slope Unpaved Avg. Velocity 1.91 ft/sec Segment #3 Time: .0757 hrs Total Tc: .5423 hrs \_\_\_\_\_\_

S/N: H0M0L0862791 BT 2, Inc

Pond Pack Ver: 8-01-98 (61) Compute Time: 14:58:36 Date: 08-29-2000

Type Tc Calcs Name BASIN PE File I:\1370\0 Title South pe	RIPHERAL COLUMBIA. ripheral	PPK area to	Southea area lea ditc south p	st/Sout ading to h (1/2) erimeter	h peri: South ) ditch	pheral perin	Page neter	1.01
TIME OF CONCENTRA				::::::::	:::::::	:::::::	:::::	:::::
South peripheral	area to	south p	erimeter	ditch	~	<b>-</b>		
Segment #1: Tc:	TR-55 Sh	eet						
Mannings n Hydraulic Length 2yr, 24hr P Slope	.1900 300.00 2.7000 .010000	ft in ft/ft						
Avg.Velocity	.12	ft/sec						
				Segment	#1 Time	e:	.6825	hrs
Segment #2: Tc:	TR-55 Sha	allow						
Hydraulic Length Slope Unpaved	110.00 .096000	ft ft/ft						
Avg.Velocity	5.00	ft/sec						
	. – – – – – – .			Segment	#2 Time	e: 	.0061	hrs
Segment #3: Tc:	TR-55 Sha	allow						
Hydraulic Length Slope Unpaved	550.00 .022000							
Avg.Velocity	2.39	ft/sec						
				Seament	#3 Time	٠.	0630	hra

S/N: H0M0L0862791 BT 2, Inc Pond Pack Ver: 8-01-98 (61) Compute Time: 15:25:03 Date: 08-29-2000

Type.... Tc Calcs

Name... BASIN PERIPHERAL

Southeast/south peripheral Page 1.02 area leading to south perimeter

ditch (2/2)

File.... I:\1370\COLUMBIA.PPK

Title... South peripheral area to south perimeter ditch

Segment #4: Tc: TR-55 Channel

Description: flow along south perimeter ditch

Flow Area 100.0000 sq.ft

Wetted Perimeter 32.40 ft

Hydraulic Radius 3.09 ft

Slope .012000 ft/ft

Slope Mannings n .0300

Hydraulic Length 1030.00 ft

Avg. Velocity 11.53 ft/sec

Segment #4 Time: .0248 hrs

Total Tc: .7773 hrs \_\_\_\_\_\_

Pond Pack Ver: 8-01-98 (61)

Compute Time: 15:25:03

Date: 08-29-2000

Type.... Tc Calcs Name.... LF TO S BASIN

Page 1.03 Equations used by PondPack to calculate Tc (1/2)

```
File.... I:\1370\Columbia.ppk
```

Title... Landfill runoff to south basin

Tc Equations used...

TC = (.007 \* ((n \* Lf)\*\*0.8)) / ((P\*\*.5) \* (Sf\*\*.4))

Where: Tc = Time of concentration, hrs

n = Mannings n

Lf = Flow length, ft

P = 2yr, 24hr Rain depth, inches

Sf = Slope, ft/ft

Unpaved surface:

V = 16.1345 \* (Sf\*\*0.5)

Paved surface:

V = 20.3282 \* (Sf\*\*0.5)

Tc = (Lf / V) / (3600sec/hr)

Where: V = Velocity, ft/sec

Sf = Slope, ft/ft

Tc = Time of concentration, hrs

Lf = Flow length, ft

Type.... Tc Calcs

Name.... LF TO S BASIN

Page 1.04 Equations used by Pond Pack to calculate To (2/2)

File... I:\1370\Columbia.ppk

Title... Landfill runoff to south basin

==== SCS Channel Flow ======

R = Aq / Wp

V = (1.49 \* (R\*\*(2/3)) \* (Sf\*\*-0.5)) / n

Tc = (Lf / V) / (3600sec/hr)

R = Hydraulic radius

Aq = Flow area, sq.ft.

Wp = Wetted perimeter, ft

V = Velocity, ft/sec

Sf = Slope, ft/ft

n = Mannings n

Tc = Time of concentration, hrs

Lf = Flow length, ft

S/N: H0M0L0862791 BT 2, Inc

Pond Pack Ver: 8-01-98 (61) Compute Time: 13:29:40 Date: 08-23-2000

# Hydrograph Generation

Type.... TR-55 Tabular Hyd.Input Data Name.... TO SOUTH BASIN

File.... I:\1370\COLUMBIA.PPK Title... Runoff to south basin

HYG Dir =  $I: \1370$ 

HYG file = S BASIN.HYG south basin 25

To South Basin 25-41, 24-hr Storm (1/z)

Page 2.01

TR-55 TABULAR HYDROGRAPH METHOD TYPE II Distribution 25yr, 24hr Rainfall Depth = 4.70 in

Total Area = 63.400 acres or .099063 sq.mi. Peak Discharge = 69 cfs WARNING: Drainage areas of two or more subareas differ by a factor of 5 or greater.

#### >>>> Input Parameters Used to Compute Hydrograph <<<<

Subarea Description	AREA (acres)	CN	Tc (hrs)	* Tt (hrs)	Precip. (in)	Runoff Ia/p (in) input/used
Landfill area W peripheral Basin area NE peripheral SE/5 periphera	29.600 4.600 1.800 13.700	67.5 67.5 98.0 67.5 67.5	.4000 .1000 .1000 .5000	.0000	4.70 4.70 4.70 4.70 4.70	1.63 I.20 .20 1.63 I.20 .20 4.46 I.01 .10 1.63 I.20 .20 1.63 I.20 .20

<sup>\*</sup> Travel time from subarea outfall to composite watershed outfall point.

#### >>>> Computer Modifications of Input Parameters <<<<<

Subarea Description	Input Tc (hrs)	Values * Tt (hrs)	Rounded Tc (hrs)		Ia/p Interpolate (Yes/No)	
andfill area peripheral	.3600	.0000	.40	.00	Yes Yes	
3asin area	.1000	.0000	* *	* *	No	Computed Ia/p < .1
E peripheral	.5400	.0000	.50	.00	Yes	
ES: periphera	.7800	.0000	.75	.00	Yes	

<sup>\*</sup> Travel time from subarea outfall to composite watershed outfall point.

S/N: H0M0L0862791 BT 2, Inc

Pond Pack Ver: 8-01-98 (61) Compute Time: 15:26:34 Date: 08-29-2000

I -- Subarea where user specified interpolation between Ia/p tables.

<sup>\*</sup> Tc & Tt are available in the hydrograph tables.

Type.... TR-55 Tabular Hyd.Peaks

Name.... TO SOUTH BASIN Tag: 25

Page 2.02

File... I:\1370\COLUMBIA.PPK
Title... Runoff to south basin

HYG Dir =  $I:\1370$ 

HYG file = S BASIN.HYG south basin 25

To South Basin 25-yr, 24-hr Storm (2/2)

TR-55 TABULAR HYDROGRAPH METHOD
TYPE II Distribution
25yr, 24hr Rainfall Depth = 4.70 in

#### >>>> Summary of Subarea Times to Peak <<<<

Peak Discharge at Composite Outfall (cfs)	Time to Peak at Composite Outfall (hrs)
<u>4</u> 0	12.3
. 11	12.1
13	12.1
17	12.4
13	12.6
69	12.4
	Composite Outfall (cfs)

S/N: H0M0L0862791 BT 2, Inc

Pond Pack Ver: 8-01-98 (61) Compute Time: 15:26:34 Date: 08-29-2000

Type.... TR-55 Tabular Hyd.Input Data Name.... TO SOUTH BASIN

Taq: 100

File.... I:\1370\COLUMBIA.PPK Title... Runoff to south basin

HYG Dir =  $I:\1370$ 

HYG file = S BASIN.HYG south basin 100

TR-55 TABULAR HYDROGRAPH METHOD TYPE II Distribution 100yr, 24hr Rainfall Depth = 5.90 in Page 2.07

To South Basin

100-yr, 24-hr

Total Area = 63.400 acres or .099063 sq.mi. Peak Discharge = 110 cfs WARNING: Drainage areas of two or more subareas differ by a factor of 5 or greater.

#### >>>> Input Parameters Used to Compute Hydrograph <<<<

Subarea Description	AREA (acres)	CN	Tc (hrs)	* Tt (hrs)	Precip.	Runoff Ia/p (in) input/used
Landfill area W peripheral Basin area E peripheral SE/S periphera	29.600 4.600 1.800 13.700	67.5 67.5 98.0 67.5	.4000 .1000 .1000 .5000	.0000	5.90 5.90 5.90 5.90 5.90	2.50 I.16 .16 2.50 I.16 .16 5.66 I.01 .10 2.50 I.16 .16 2.50 I.16 .16

<sup>\*</sup> Travel time from subarea outfall to composite watershed outfall point.

#### >>>> Computer Modifications of Input Parameters <<<<<

Subarea Description	Input Tc (hrs)	Values * Tt (hrs)	Rounded Tc (hrs)	Values * Tt (hrs)	Ia/p Interpolate (Yes/No)	
p				(111.0)	(165/NO)	messages
andfill area	.3600	.0000	.40	.00	Yes	
w peripheral	.1000	.0000	* *	* *	Yes	
Basin area	.1000	.0000	**	**	No	Computed Ia/p < .1
peripheral	.5400	.0000	.50	.00	Yes	
E/S periphera	.7800	.0000	.75	.00	Yes	

<sup>\*</sup> Travel time from subarea outfall to composite watershed outfall point.

\* Tc & Tt are available in the hydrograph tables.

S/N: H0M0L0862791 BT 2, Inc

Pond Pack Ver: 8-01-98 (61) Compute Time: 15:26:34 Date: 08-29-2000

I -- Subarea where user specified interpolation between Ia/p tables.

Type.... TR-55 Tabular Hyd.Peaks

Name.... TO SOUTH BASIN Tag: 100

Page 2.08

File.... I:\1370\COLUMBIA.PPK Title... Runoff to south basin

HYG Dir =  $I:\1370$ 

HYG file = S BASIN.HYG south basin 100

TR-55 TABULAR HYDROGRAPH METHOD TYPE II Distribution 100yr, 24hr Rainfall Depth = 5.90 in

>>>> Summary of Subarea Times to Peak <<<<

Subarea	Peak Discharge at Composite Outfall (cfs)	Time to Peak at Composite Outfall (hrs)
Landfill area	65	12.3
W peripheral	18	12.1
Basin area	16	12.1
<b>N</b> E peripheral .	27	12.4
SE/S periphera	21	12.6
Composite Watershed	110	12.4

S/N: H0M0L0862791 BT 2, Inc

Pond Pack Ver: 8-01-98 (61) Compute Time: 15:26:34 Date: 08-29-2000

## Diversion Berm, Downslope Swale, and Perimeter Ditch Sizzing Calculations

Worst- case diversion Berm ( Title... To for worst case diversion berm sizing calcs 

Segment #1: Tc: TR-55 Sheet

Type.... Tc Calcs

Name.... WORSTCASE DIV BE

File.... I:\1370\COLUMBIA.PPK

TIME OF CONCENTRATION CALCULATOR

Description: final cover slope - 25%

Tc for worst case diversion berm sizing calcs

Mannings n .1900 Hydraulic Length 95.00 ft 2yr, 24hr P 2.7000 in Slope .250000 ft/ft

Avg. Velocity .35 ft/sec

Segment #1 Time: . .0751 hrs

Segment #2: Tc: TR-55 Shallow Description: diversion berm

Hydraulic Length 2090.00 ft Slope .020000 ft/ft Unpaved

Avg. Velocity 2.28 ft/sec

Segment #2 Time: .2544 hrs

Total Tc: .3295 hrs \_\_\_\_\_\_

#### Worst-case diversion berm

Type.... TR-55 Tabular Hyd.Input Data Name.... WORSTCASE DIV BE Tag: 25

Page 1.01

File.... I:\1370\COLUMBIA.PPK

Title... Hydrograph for worst-case diversion berm sizing calcs

HYG Dir =  $I:\1370$ 

HYG file = NONE STORED WORSTCASE DIV BE 25

TR-55 TABULAR HYDROGRAPH METHOD
TYPE II Distribution
25yr, 24hr Rainfall Depth = 4.70 in

Total Area = 4.600 acres or .007187 sq.mi.

Peak Discharge = 7 cfs

>>>> Input Parameters Used to Compute Hydrograph <<<<

Subarea Description	AREA (acres)	CN		* Tt (hrs)			f Ia/p input/used
east side ph 1	4.600	67 <b>.</b> 5	.3000	.0000	4.70	1.63	I.20 .20

<sup>\*</sup> Travel time from subarea outfall to composite watershed outfall point. I -- Subarea where user specified interpolation between Ia/p tables.

#### >>>> Computer Modifications of Input Parameters <<<<<

Subarea Description	Input Tc (hrs)	Values * Tt (hrs)	Rounded Tc (hrs)		Ia/p Interpolated (Yes/No)	Ia/p Messages
east side ph 1	.3300	.0000	.30	.00	Yes	

<sup>\*</sup> Travel time from subarea outfall to composite watershed outfall point.

S/N: H0M0L0862791 BT 2, Inc

Worst-case diversion berm

Type.... TR-55 Tabular Hyd.Peaks

Name.... WORSTCASE DIV BE Tag:

Page 1.02

File.... I:\1370\COLUMBIA.PPK

Title... Hydrograph for worst-case diversion berm sizing calcs

HYG Dir = I:\1370\

HYG file = NONE STORED WORSTCASE DIV BE 25

TR-55 TABULAR HYDROGRAPH METHOD
TYPE II Distribution
25yr, 24hr Rainfall Depth = 4.70 in

25

>>>> Summary of Subarea Times to Peak <<<<

	Peak Discharge at	Time to Peak at
	Composite Outfall	Composite Outfall
Subarea	(cfs)	(hrs)
east side ph 1	7	12.2
Composite Watershed	7	12.2

S/N: H0M0L0862791 BT 2, Inc

## Worksheet Worksheet for Triangular Channel

Project Description	1
Worksheet	Triangular Channe
Flow Element	Triangular Channe
Method	Manning's Formula
Solve For	Channel Depth

Worst-case diversion berm

Input Data		
Mannings Coeffic	0.030	
Slope	020000	ft/ft
Left Side Slope	4.00	H:V
Right Side Slope	3.00	H:V
Discharge	7.00	cfs

Results		
Depth	0.75	ft
Flow Area	2.0	ft²
Wetted Perimi	5.47	ft
Top Width	5.25	ft
Critical Depth	0.76	ft
Critical Slope	0.019122	ft/ft
Velocity	3.55	ft/s
Velocity Head	0.20	ft
Specific Energ	0.95	ft
Froude Numb	1.02	
Flow Type	3upercritical	

Worst-case downslope channel Type.... Tc Calcs Page 1.01 Name.... WORST CASE FLUME File.... I:\1370\COLUMBIA.PPK Title... Tc for worst case downslope flume sizing calcs TIME OF CONCENTRATION CALCULATOR To for worst case downslope flume sizing calcs Segment #1: Tc: TR-55 Sheet Description: final cover slope - 5% Mannings n .1900 Hydraulic Length 60.00 ft 2yr, 24hr P 2.7000 in Slope .050000 ft/ft .17 ft/sec Avg. Velocity Segment #1 Time: .0989 hrs Segment #2: Tc: TR-55 Sheet Description: final cover slope - 25% Mannings n .1900 Hydraulic Length 60.00 ft 2yr, 24hr P 2.7000 in Slope .250000 ft/ft Avg. Velocity .32 ft/sec Segment #2 Time: .0520 hrs Segment #3: Tc: TR-55 Shallow Description: diversion berm Hydraulic Length 1790.00 ft Slope .020000 ft/ft Unpaved Avg. Velocity 2.28 ft/sec

Segment #3 Time: .2179 hrs

Total Tc: .3688 hrs

S/N: H0M0L0862791 BT 2, Inc

Worst-case downslope channel

Type.... TR-55 Tabular Hyd.Input Data Name.... WORST CASE FLUME Tag: 25

Page 1.01

File.... I:\1370\COLUMBIA.PPK

Title... Hydrograph for worst-case downslope flume sizing calcs

HYG Dir =  $I:\1370$ 

HYG file = NONE STORED WORST CASE FLUME 25

TR-55 TABULAR HYDROGRAPH METHOD
TYPE II Distribution
25yr, 24hr Rainfall Depth = 4.70 in

Total Area = 7.500 acres or .011719 sq.mi.

Peak Discharge = 10 cfs

>>>> Input Parameters Used to Compute Hydrograph <<<<

Subarea Description	AREA (acres)	CN	Tc (hrs)	* Tt (hrs)	Precip.		off n) in		
To SE flume	7.500	67.5	.4000	.0000	4.70	1.	63 I	.20	.20

<sup>\*</sup> Travel time from subarea outfall to composite watershed outfall point. I -- Subarea where user specified interpolation between Ia/p tables.

#### >>>> Computer Modifications of Input Parameters <<<<<

Subarea Description	Input Tc (hrs)	Values * Tt (hrs)	Rounded Tc (hrs)		<pre>Ia/p Interpolated   (Yes/No)</pre>	Ia/p Messages
To SE flume	.3700	.0000	.40	.00	Yes	

<sup>\*</sup> Travel time from subarea outfall to composite watershed outfall point.

S/N: H0M0L0862791 BT 2, Inc

Worst-case downslope channel

Type.... TR-55 Tabular Hyd.Peaks Name.... WORST CASE FLUME Tag: Page 1.02

25

File.... I:\1370\COLUMBIA.PPK

Title... Hydrograph for worst-case downslope flume sizing calcs

HYG Dir =  $I: \langle 1370 \rangle$ 

HYG file = NONE STORED WORST CASE FLUME 25

TR-55 TABULAR HYDROGRAPH METHOD TYPE II Distribution 25yr, 24hr Rainfall Depth = 4.70 in

>>>> Summary of Subarea Times to Peak <<<<

•	Peak Discharge at Composite Outfall	Time to Peak at Composite Outfall
Subarea	(cfs)	(hrs)
To SE flume	10	12.3
Composite Watershed	10	12.3

Project Description	
Worksheet	downslope flume
Flow Element	Trapezoidal Cha
Method	Manning's Form
Solve For	Channel Depth

Worst-case downslope channel (SW channel)

Input Data		
Mannings Coeffic	0.040	
Slope	200000	ft/ft
Left Side Slope	3.00	H : V
Right Side Slope	3.00	H : V
<b>Bottom Width</b>	10.00	ft
Discharge	10.00	cfs

Results		
Depth	0.18	ft
Flow Area	1.9	ft²
Wetted Perim	11.16	ft
Top Width	11.10	ft
Critical Depth	0.30	ft
Critical Slope	0.035988	ft/ft
Velocity	5.17	ft/s
Velocity Head	0.41	ft
Specific Enerç	0.60	ft
Froude Numb	2.18	
Flow Type 3	upercritical	

Project Description	
Worksheet	worst-case west perimeter
Flow Element	Trapezoidal Channel
Method	Manning's Formula
Solve For	Channel Depth

Worst-case west perimeter dutch

Input Data		
Mannings Coeffic	0.030	
Slope	006000	ft/ft
Left Side Slope	3.00	H : V
Right Side Slope	3.00	H : V
<b>Bottom Width</b>	5.00	ft
Discharge	31.00	cfs

Results		
Depth	1.13	ft
Flow Area	9.5	ft²
Wetted Perime	12.17	ft
Top Width	11.80	ft
Critical Depth	0.88	ft
Critical Slope	0.015659	ft/ft
Velocity	3.26	ft/s
Velocity Head	0.16	ft
Specific Enerç	1.30	ft
Froude Numb	0.64	
Flow Type	Subcritical	

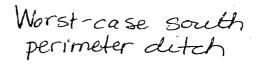
Project Description	··· ··· · · · · · · · · · · · · · ·
Worksheet	worst-case east perimeter
Flow Element	Trapezoidal Channel
Method	Manning's Formula
Solve For	Channel Depth

Worst-case east perimeter dutch

Input Data		
Mannings Coeffic	0.030	
Slope	005000	ft/ft
Left Side Slope	3.00	H:V
Right Side Slope	3.00	H:V
Bottom Width	10.00	ft
Discharge	57.00	cfs

Results		
Depth	1.23	ft
Flow Area	16.9	ft²
Wetted Perim	17.79	ft
Top Width	17.39	ft
Critical Depth	0.91	ft
Critical Slope	0.014803	ft/ft
Velocity	3.38	ft/s
Velocity Head	0.18	ft
Specific Enerç	1.41	ft
Froude Numb	0.61	
Flow Type	Subcritical	

Project Description	
Worksheet	worst case south perimeter
Flow Element	Trapezoidal Channel
Method	Manning's Formula
Solve For	Channel Depth



Input Data		
Mannings Coeffic	0.030	
Slope	012000	ft/ft
Left Side Slope	3.00	H:V
Right Side Slope	3.00	H : V
Bottom Width	10.00	ft
Discharge	70.00	cfs

Results		
Depth	1.08	ft
Flow Area	14.4	ft²
Wetted Perime	16.85	ft
Top Width	16.50	ft
Critical Depth	1.03	ft
Critical Slope	0.014316	ft/ft
Velocity	4.88	ft/s
Velocity Head	0.37	ft
Specific Energ	1.45	ft
Froude Numb	0.92	
Flow Type	Subcritical	

Project Description	1
Worksheet	ditch from SW corner of LF to \$
Flow Element	Trapezoidal Channel
Method	Manning's Formula
Solve For	Channel Depth

Ditch from SW corner of Landfill to South Basin

Input Data		
Mannings Coeffic	0.030	
Slope	006000	ft/ft
Left Side Slope	3.00	H:V
Right Side Slope	3.00	H:V
Bottom Width	15.00	ft
Discharge	69.00	cfs

Results		
Depth	1.07	ft
Flow Area	19.4	ft²
Wetted Perima	21.74	ft
Top Width	21.40	ft
Critical Depth	0.82	ft
Critical Slope	0.014896	ft/ft
Velocity	3.56	ft/s
Velocity Head	0.20	ft
Specific Епегç	1.26	ft
Froude Numb	0.66	
Flow Type	Subcritical	

# Basin Volume Computations

Type.... Vol: Planimeter

Name.... SOUTH BASIN

File.... I:\1370\COLUMBIA.PPK

Title... south basin volume

#### POND VOLUME CALCULATIONS

Page 1.01

Planimeter scale: 1.00 ft/in

Elevation (ft)	Planimeter (sq.in)	Area (acres)	A1+A2+sqr(A1*A2) (acres)	Volume (ac-ft)	Volume Sum (ac-ft)
789.00	62411.000	1.4328	.0000	.000	.000
790.00	68355.000	1.5692	4.5014	1.500	1.500
792.00	74865.000	1.7187	4.9301	3.287	4.787
794.00	82150.000	1.8859	5.4049	3.603	8.390

#### POND VOLUME EQUATIONS

\* Incremental volume computed by the Conic Method for Reservoir Volumes.

Volume = (1/3) \* (EL2-EL1) \* (Area1 + Area2 + sq.rt.(Area1\*Area2))

where: EL1, EL2 = Lower and upper elevations of the increment

Area1, Area2 = Areas computed for EL1, EL2, respectively

= Incremental volume between EL1 and EL2 Volume

# Outlet Structure Data

Type.... Outlet Input Data

Name.... SOUTH BASIN2

File.... I:\1370\COLUMBIA.PPK

Title... south basin outlet structure

#### REQUESTED POND WS ELEVATIONS:

Page 1.01

Min. Elev.= 789.50 ft Increment = 1.00 ft Max. Elev.= 794.00 ft

\*\*\*\*\*\*\*\*\*\*\*\*\*\*

---> Forward Flow Only (UpStream to DnStream) <--- Reverse Flow Only (DnStream to UpStream)

<---> Forward and Reverse Both Allowed

Structure	No.		Outfall	E1, ft	E2, ft
**					
Weir-Rectangular	e1	>	${\tt TW}$	793.000	794.000
Stand Pipe	s1	>	c1	791.000	794.000
Orifice-Circular	01	>	c1	789.500	794.000
Culvert-Circular	c1	>	$\mathtt{TW}$	789.000	794.000
TW SETUP, DS Channel			•	•	

S/N: H0M0L0862791 BT 2, Inc

Type.... Outlet Input Data Page 1.02

Name.... SOUTH BASIN2

File.... I:\1370\COLUMBIA.PPK

Title... south basin outlet structure

#### OUTLET STRUCTURE INPUT DATA

```
Structure ID = e1
Structure Type = Weir-Rectangular
-------
```

# of Openings = 1 Crest Elev. = 793.00 ft Weir Length = 10.00 ft Weir Coeff. = 3.300000

Weir TW effects (Use adjustment equation)

Structure ID = s1 Structure Type = Stand Pipe

# of Openings = 1
Invert Elev. = 791.00 ft
Diameter = 2.5000 ft
Orifice Area = 4.9087 sq.ft
Orifice Coeff. = .600
Weir Length = 7.85 ft
Weir Coeff. = 3.300
K, Submerged = .000
K, Reverse = 1.000
Kb, Barrel = .000000 (per ft of full flow)
Barrel Length = .0000

Structure ID = o1 Structure Type = Orifice-Circular \_\_\_\_\_\_\_

# of Openings = 72
Invert Elev. = 789.50 ft
Diameter = .0400 ft
Orifice Coeff. = .600

Type.... Outlet Input Data Page 1.03

Name.... SOUTH BASIN2

File.... I:\1370\COLUMBIA.PPK

Title... south basin outlet structure

#### OUTLET STRUCTURE INPUT DATA

```
Structure ID = c1
Structure Type = Culvert-Circular

No. Barrels = 1
Barrel Diameter = 1.2500 ft
Upstream Invert = 789.00 ft
Dnstream Invert = 788.50 ft
Horiz. Length = 50.00 ft
Barrel Length = 50.00 ft
Barrel Slope = .01000 ft/ft

OUTLET CONTROL DATA...
Mannings n = .0130
Ke = .9000 (forward entrance loss)
Kb = .023225 (per ft of full flow)
Kr = .9000 (reverse entrance loss)
HW Convergence = .001 +/- ft

INLET CONTROL DATA...
Equation form = 1
Inlet Control K = .0340
Inlet Control M = 1.5000
Inlet Control Y = .5400
T1 ratio (HW/D) = 1.258
T2 ratio (HW/D) = 1.420
Slope Factor = .500
```

Use unsubmerged inlet control Form 1 equ. below T1 elev. Use submerged inlet control Form 1 equ. above T2 elev.

In transition zone between unsubmerged and submerged inlet control, interpolate between flows at T1 & T2...

At T1 Elev = 790.57 ft ---> Flow = 4.80 cfs At T2 Elev = 790.77 ft ---> Flow = 5.49 cfs

> Structure ID = TW Structure Type = TW SETUP, DS Channel

#### FREE OUTFALL CONDITIONS SPECIFIED

```
CONVERGENCE TOLERANCES...

Maximum Iterations= 30

Min. TW tolerance = .01 ft

Max. TW tolerance = .01 ft

Min. HW tolerance = .01 ft

Max. HW tolerance = .01 ft
```

Name.... SOUTH BASIN2

File.... I:\1370\COLUMBIA.PPK

Title... south basin outlet structure

#### RATING TABLE FOR ONE OUTLET TYPE

Structure ID = e1 (Weir-Rectangular) Upstream ID = (Pond Water Surface) DNstream ID = TW (Pond Outfall)

Page 1.04

WS Elev, De	vice Q	Tail Water	Notes
WS Elev. ft	Q cfs	TW Elev Converg	computation Messages
789.50 790.50 791.00 791.50 792.50 793.00	.00	Free Outfall Free Outfall Free Outfall Free Outfall Free Outfall Free Outfall	WS below an invert; no flow.
793.50 794.00	11.67 33.00	Free Outfall Free Outfall	H=.50; Htw=.00; Qfree=11.67; H=1.00; Htw=.00; Qfree=33.00;

S/N: H0M0L0862791 BT 2, Inc

Name.... SOUTH BASIN2

File.... I:\1370\COLUMBIA.PPK

Title... south basin outlet structure

#### RATING TABLE FOR ONE OUTLET TYPE

Structure ID = s1 (Stand Pipe)

Upstream ID = (Pond Water Surface)

Page 1.05

DNstream ID = c1 (Culvert-Circular)

Pond WS. Elev. ft	Device Q cfs	HW HGL DS HGI	DS HGL	DS HGL Q SUM Error Error +/-ft +/-cfs	DS Chan. TW TW Error ft +/-ft
789.50	.00	WS below an inver	rt; no flow.	•••	Free Outfall
790.50	.00	WS below an inver			Free Outfall
791.00	.00	WS below an inver		`	Free Outfall
791.50	7.06	791.50 791.5 DS HGL+Loss > cre	0 791.50 est: Flow set	.000 .000 to Downstream	Free Outfall outlet
792.50	8.78	792.50 792.5 DS HGL+Loss > cre	792.50	.000 .000	Free Outfall
793.00	9.52	793.00 793.0 DS HGL+Loss > cre	0 793.00		Free Outfall
793.50	10.21	793.50 793.5 DS HGL+Loss > cre	0 793.50		Free Outfall
794.00	10.86	794.00 794.0 DS HGL+Loss > cre	0 794.00	.000 .000	Free Outfall

S/N: H0M0L0862791 BT 2, Inc

Name.... SOUTH BASIN2

File.... I:\1370\COLUMBIA.PPK

Title... south basin outlet structure

#### RATING TABLE FOR ONE OUTLET TYPE

Structure ID = o1 (Orifice-Circular)

Upstream ID = (Pond Water Surface)

DNstream ID = c1 (Culvert-Circular)

NUMBER OF OPENINGS = 72 EACH FLOW = SUM OF OPENINGS x FLOW FOR ONE OPENING

Page 1.06

Pond WS. Elev. ft	Device Q cfs		Converge DS HGL ft	DS HGL		Q SUM Error +/-cfs	DS Chan TW ft	Error +/-ft
789.50	.00	WS below a	n invert	; no flow.	•••		Free Ou	tfall
790.50	.43	790.50 H =.98	Free	789.42	.000	.000	Free Ou	tfall
791.00	.53	791.00 H =1.48	Free	789.47	.000	.000	Free Ou	tfall
791.50	.00	791.50	791.50	791.50 Full riser				
792.50	.00	792.50	792.50	792.50 Full riser		.000 Q=0 thi		
793.00	.00	793.00	793.00	793.00 Full riser		.000 Q=0 this		
793.50	.00	793.50	793.50		.000	.000	Free Ou	tfall
794.00	.00	794.00	794.00		.000	.000	Free Ou	tfall

S/N: H0M0L0862791 BT 2, Inc

Name.... SOUTH BASIN2

File.... I:\1370\COLUMBIA.PPK

Title... south basin outlet structure

#### RATING TABLE FOR ONE OUTLET TYPE

Structure ID = c1 (Culvert-Circular)

Mannings open channel maximum capacity: 6.95 cfs

Page 1.07

UPstream ID's= s1, o1

DNstream ID = TW (Pond Outfall)

Pond WS. Elev. ft	Device Q cfs	(into) Conver HW HGL DS HG ft ft	rge Next L DS HGL ft	DS HGL Q SUM Error Error +/-ft +/-cfs	DS Chan. TW TW Error ft +/-ft
789.50	.00	789.00 Free	e Free	.000 .000	Free Outfall
790.50	.43	789.42 Free CRIT.DEPTH CONTR		.000 .000 Et Dcr= .255ft	
791.00	.53	789.47 Free CRIT.DEPTH CONTR	Free	.000 .000	Free Outfall
791.50	7.06	791.50 Free INLET CONTROL	Free	.000 .000 HW =2.50	
792.50	8.78	792.50 Free INLET CONTROL	Free	.000 .000 HW =3.50	Free Outfall
793.00	9.52	793.00 Free INLET CONTROL	Free	.000 .000 HW =4.00	Free Outfall
793.50	10.21	793.50 Free INLET CONTROL	Free	.000 .000 HW =4.50	Free Outfall
794.00	10.86	794.00 Free INLET CONTROL	Free		Free Outfall

S/N: H0M0L0862791 BT 2, Inc

# Pond Routing Summary

Type.... Pond Routing Summary

Name.... SOUTH BASIN2

Tag: 25

Page 6.02

File.... I:\1370\COLUMBIA.PPK

Title... routing of hydrograph through south basin 25-4r, 24-hr Storm

South Basin

#### LEVEL POOL ROUTING SUMMARY

HYG Dir = I: 1370

Inflow HYG file = SBASIN.HYG - south basin Outflow HYG file = NONE STORED - SOUTH BASIN2 OUT 25

Pond Node Data = south basin Pond Volume Data = south basin Pond Outlet Data = south basin2

No Infiltration

#### INITIAL CONDITIONS

Starting WS Elev = 789.00 ft Starting Volume = .000 ac-ft Starting Outflow = .00 cfs
Starting Infiltr. = .00 cfs
Starting Total Qout= .00 cfs
Time Increment = .1000 hrs

#### INFLOW/OUTFLOW HYDROGRAPH SUMMARY

Peak Inflow = 69.00 cfs at 12.4000 hrs
Peak Outflow = 7.94 cfs at 14.1000 hrs — Peak discharge from basin

Peak Elevation = 792.01 ft - Peak water elevation

Peak Storage = 4.805 ac-ft

\_\_\_\_\_\_

#### MASS BALANCE (ac-ft)

+ Initial Vol = .000

+ HYG Vol IN = 8.872 .000 - Infiltration =

- HYG Vol OUT = 8.101

- Retained Vol = .769

Unrouted Vol = -.001 ac-ft (.016% of Inflow Volume)

WARNING: Inflow hydrograph truncated on left side. WARNING: Outflow hydrograph truncated on right side.

S/N: H0M0L0862791 BT 2, Inc



Job No. 1370 Client Alliant Job Columbia Plan of Op Update
Subject Basin Calcs

Calc. No.

Rev. No.

By BLP Date 8/23/00

Chk'd. MKH Date 8-31-00

Sheet No.

Basin Particle Size Settling Capability

Basin required to settle out ≥ 15 micron (0.015 mm) particle for a 25-yr, 24-hr Storm event.

From calculations, peak discharge from basin is 7.94 cfs and peak water elevation is 792:0 ft. The corresponding surface area of the basin at elevation 792.0 is 74,865 sf (see Basin Volume Computations Section The surface area to discharge ratio is therefore 74,865 sf = 19,429. sf/ofs

From the Erosion and Sediment Control Handbook, the required surface area to discharge ratio to settle out a 15 micron particle is 3,125 sp/cfs.

9,429 cfs/sf > 3,125 sp/cfs, therefore the basin is adequately sized to settle out a 15 micron particle

Name.... SOUTH BASIN2

File.... I:\1370\COLUMBIA.PPK

Title... routing of hydrograph through south basin

South Basin Outflow Hydrograph

Page 6.03

POND ROUTED TOTAL OUTFLOW HYG...

HYG file =

HYG ID = SOUTH BASIN2 OUT

HYG Tag

7.94 cfs Peak Discharge = 14.1000 hrs

Time to Peak =HYG Volume 8.101 ac-ft

Basin dewatering time-Begin discharge: 12.2

End discharge: 113.8 sa

Total discharge time: 101.6

or 4,2 days, while

is greater than the required minimum

of 3 days

WARNING: Hydrograph truncated on right side.

HYDROGRAPH ORDINATES (cfs) Time Output Time increment = .1000 hrs hrs Time on left represents time for first value in each row. 11.0000 .00 .00 .00 .00 Begin .24 3.82 discharge 6.00 .00 11.5000 .00 .00 .24 .00 12.0000 .00 .39 12.5000 .48 . 92 7.14 7.44 13.0000 7.31 7.55 7.64 7.72 7.83 7.87 13.5000 7.78 7.90 7.92 7.94 14.0000 7.93 7.94 7.94 7.93 14.5000 7.92 7.91 7.90 7.89 7.87 7.84 7.82 7.80 7.77 15.0000 7.75 7.73 7.71 7.68 15.5000 7.66 7.63 16.0000 7.60 7.57 7.54 7.51 7.48 16.5000 7.45 7.42 7.40 7.37 7.34 7.31 17.0000 7.28 7.26 7.23 7.20 17.5000 7.18 7.15 7.13 7.10 7.08 6.77 18.0000 6.96 6.60 6.44 6.28 18.5000 6.14 6.00 5.88 5.76 5.65 19.0000 5.55 5.45 5.36 5.27 5.19 19.5000 5.12 4.77 5.01 4.89 4.66 20.0000 4.55 4.46 4.36 4.28 4.20 20.5000 4.12 4.05 3.99 3.92 3.87 21.0000 3.81 3.76 3.71 3.67 3.63 3.55 21.5000 3.59 3.51 3.48 3.45 22.0000 3.42 3.40 3.37 3.35 3.33 22.5000 3.31 3.29 3.24 3.16 3.09 23.0000 3.02 2.95 2.89 2.84 2.78 23.5000 2.74 2.69 2.65 2.61 2.57 24.0000 2.53 2.47 2.37 2.29 2.21 24.5000 2.13 2.06 1.99 1.93 1.87 25.0000 1.82 1.77 1.72 1.67 1.60

S/N: H0M0L0862791 BT 2, Inc

Name.... SOUTH BASIN2

Tag:

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Page 6.04

South Basin

Outflow Hydrograph
(2/7)

File... I:\1370\COLUMBIA.PPK

Title... routing of hydrograph through south basin

WARNING: Hydrograph truncated on right side.

m i			RDINATES (cf		
Time hrs	Time on left		increment = time for fi		each row.
25.5000	1.50	1.40	1.32	1.23	1.15
26.0000	1.08	1.01	.95	.89	.83
26.5000	.78	.73	.69	.64	.60
27.0000	.56	.53	.53	.53	.53
27.5000	.53	.53	.53	.53	.53
28.0000 28.5000	.53	.52 .52	.52	.52	.52
29.0000	.52	.52	.52 .52	.52 .52	.52
29.5000	.52	.52	.52	.52	.52 .52
30.0000	.51	.51	.51	.51	.51
30.5000	.51	.51	.51	.51	.51
31.0000	.51	.51	.51	.51	.51
31.5000	.51	.51	.51	.51	.50
32.0000	.50	.50	.50	.50	.50
32.5000	.50	.50	.50	.50	.50
33.0000	.50	.50	.50	.50	.50
33.5000	.50	.50	.50	.50	.49
34.0000	.49	.49	.49	.49	.49
34.5000	.49	.49	.49	.49	.49
35.0000 35.5000	.49	.49	.49	.49	.49
36.0000	.49	.49 .48	.49 .48	.49	.48
36.5000	.48	.48	.48	.48 .48	.48 .48
37.0000	.10	.48	.48	.48	.48
37.5000	.48	.48	.48	.48	.48
38.0000	.47	.47	.47	.47	.47
38.5000	.47	.47	.47	.47	.47
39.0000	.47	.47	.47	.47	.47
39.5000	.47	.47	.47	.47	.47
40.0000	.47	.46	.46	.46	.46
40.5000	.46	.46	.46	.46	.46
41.0000	.46	.46	.46	.46	.46
41.5000	.46	.46	.46	.46	.46
42.0000 42.5000	.46 .45	.46 .45	.46	.45	.45
43.0000	.45	.45	.45 .45	.45 .45	.45
43.5000	.45	.45	.45	.45	.45
44.0000	.45	.45	.45	.45	.45
44.5000	.44	.44	.44	.44	.44
45.0000	.44	.44	.44	.44	.44
45.5000	.44	.44	.44	.44	.44
46.0000	. 44	.44	. 44	.44	.44
46.5000	.44	.44	.44	.43	.43

S/N: H0M0L0862791 BT 2, Inc

Name.... SOUTH BASIN2 Tag: 25

File.... I:\1370\COLUMBIA.PPK

Title... routing of hydrograph through south basin

South Basin Outflow Hydrograp (3/7)

Page 6.05

WARNING: Hydrograph truncated on right side:

Time hrs		YDROGRAPH ORI butput Time in represents t	ncrement = .	1000 hrs	each row.
47.0000	.43	.43	.43	.43	.43
47.5000	.43	.43	.43	.43	.43
48.0000 48.5000	.43	.43	.43	.42	.42
49.0000	.42	.42 .42	.42 .42	.42	.42
49.5000	.41	.41	.41	.41 .41	.41
50.0000	.41	.41	.41	.41	.41
50.5000	.40	.40	.40	.40	.40
51.0000	.40	.40	.40	.40	.40
51.5000	.39	.39	.39	.39	.39
52.0000	.39	.39	.39	.39	.39
52.5000	.39	.38	.38	.38	.38
53.0000	.38	.38	.38	.38	.38
53.5000	.38	.38	.38	.37	.37
54.0000	.37	.37	.37	.37	.37
54.5000	.37	.37	.37	.37	.37
55.0000 55.5000	.36	.36	.36	.36	.36
56.0000	.36	.36 .36	.36	.36	.36
56.5000	.35	.35	.35 .35	.35	.35
57.0000	.35	.35	.35	.35 .35	.35
57.5000	.34	.34	.34	.34	.34 .34
58.0000	.34	.34	.34	.34	.34
58.5000	.34	.34	.33	.33	.33
59.0000		.33	.33	.33	.33
59.5000	.33	.33	.33	.33	.33
60.0000	.33	.32	.32	.32	.32
60.5000	.32	.32	.32	.32	.32
61.0000	.32	.32	. 32	.32	.31
61.5000	.31	.31	.31	.31	.31
62.0000 62.5000	.31	.31	.31	.31	.31
63.0000	.31	.31 .30	.31	.30	.30
63.5000	.30	.30	.30 .30	.30 .30	.30
64.0000	.30	.30	.30	.29	.30 .29
64.5000	.29	.29	.29	.29	.29
65.0000	.29	.29	.29	.29	.29
65.5000	.29	.29	.29	.28	.28
66.0000	.28	.28	.28	.28	.28
66.5000	.28	.28	.28	.28	.28
67.0000	.28	.28	.28	.28	.27
67.5000	.27	.27	.27	.27	.27
68.0000	.27	.27	.27	.27	.27

S/N: H0M0L0862791 BT 2, Inc

Type.... Pond Routed HYG (total out) Name.... SOUTH BASIN2

Tag: 25 Page 6.06

File.... I:\1370\COLUMBIA.PPK

Title... routing of hydrograph through south basin

South Basin Outflow Hydrograp

WARNING: Hydrograph truncated on right side.

Time on left represents time for first value in each row.	Time			DINATES (cfs		
69,0000         .26		Time on left	represents	time for fir	st value in	each row.
69,5000         .26         .26         .26         .26         .26         .26         .26         .26         .26         .26         .26         .26         .26         .25         .24		I .				
70.0000         .26         .26         .26         .25         .25         .25           70.5000         .26         .26         .25         .25         .25         .25           71.0000         .25         .25         .25         .25         .25         .25           72.0000         .25         .25         .25         .25         .25         .25           72.5000         .24         .24         .24         .24         .24         .24           73.0000         .24         .24         .24         .24         .24         .24           73.5000         .24         .24         .24         .24         .24         .24           74.0000         .24         .24         .24         .24         .24         .24           74.5000         .23						
70.5000         .26         .26         .25         .25         .25           71.0000         .25         .25         .25         .25         .25         .25           71.5000         .25         .25         .25         .25         .25         .25           72.0000         .25         .25         .25         .25         .24         <						
71.0000         .25         .25         .25         .25         .25         .25         .25         .25         .25         .25         .25         .25         .25         .25         .25         .25         .25         .24						
71.5000         .25         .25         .25         .25         .25         .25         .25         .25         .25         .24		I .				
72.0000         .25         .25         .25         .24		I .				
72.5000         .24		1				
73.0000         .24         .24         .24         .24         .24         .24         .24         .24         .24         .24         .24         .24         .24         .24         .24         .24         .24         .24         .23         .22         .22         .22         .22						
73.5000         .24         .24         .24         .24         .24         .24         .24         .23         .22         .22         .22         .22         .22         .22         .22         .22         .22         .22         .22         .22         .22         .22         .22         .22						
74.0000         .24         .24         .24         .23         .23           74.5000         .23         .23         .23         .23         .23         .23           75.0000         .23         .23         .23         .23         .23         .23           75.5000         .23         .22         .22         .22         .22         .22         .22         .22         .22         .22         .22         .22         .22         .22         .22         .22         .22         <		1				
74.5000         .23         .22         .22         .22         .22         .22         .22         .22         .22         .22         .22         .22         .22         .22         .22         .22         .22         .22         .21	74.0000	.24				
75.0000         .23         .23         .23         .23         .23         .23         .23         .23         .23         .23         .23         .23         .23         .23         .23         .23         .23         .22         .21         .20         .20         .20         .20		.23	.23	.23		
76.0000         .23         .23         .22         .22         .22           76.5000         .22         .22         .22         .22         .22           77.0000         .22         .22         .22         .22         .22           77.5000         .22         .22         .22         .22         .22         .22           78.0000         .21         .20         .20         .20		.23	.23	.23	.23	
76.5000         .22         .21         .20         .20         .20         .20					.23	.23
77.0000         .22         .22         .22         .22         .22           77.5000         .22         .22         .22         .22         .22           78.0000         .22         .22         .21         .21         .21         .21           78.5000         .21         .20         .20         .20         .20         .20         .20         .20         .20         .20         <						
77.5000       .22       .22       .22       .22       .22       .22       .21       .20       .20       .20       .20       .20       .20       .20       .20       .20       <						
78.0000       .22       .22       .21       .21       .21         78.5000       .21       .21       .21       .21       .21       .21         79.0000       .21       .20		1				
78.5000       .21       .20       .20       .20       .20       .20       .20       .20       .20       .20       .20       .20       .20       .20       .20       .20       .20       .20       .20       .20       <						
79.0000         .21         .20						
79.5000         .21         .21         .21         .21         .21         .21         .21         .21         .21         .21         .20         .19						
80.0000       .21       .21       .20       .20       .20         80.5000       .20       .20       .20       .20       .20         81.0000       .20       .20       .20       .20       .20         81.5000       .20       .20       .20       .20       .20         82.0000       .20       .20       .20       .20       .19         82.5000       .19       .19       .19       .19       .19         83.0000       .19       .19       .19       .19       .19       .19         84.0000       .19       .19       .19       .19       .19       .19       .19         84.5000       .19		,				
80.5000       .20       .19       <						
81.0000       .20       .20       .20       .20       .20       .20       .20       .20       .20       .20       .20       .20       .20       .20       .20       .20       .19       <						
81.5000       .20       .20       .20       .20       .20       .20       .20       .20       .19       <						
82.0000       .20       .20       .20       .19         82.5000       .19       .19       .19       .19       .19         83.0000       .19       .19       .19       .19       .19       .19         84.0000       .19       .19       .19       .19       .19       .19       .19         84.5000       .19       .19       .19       .18       .18       .18       .18         85.0000       .18       .18       .18       .18       .18       .18       .18         86.0000       .18       .18       .18       .18       .18       .18       .18         87.0000       .18       .18       .18       .18       .18       .18       .18         87.5000       .17       .17       .17       .17       .17       .17       .17         88.5000       .17       .17       .17       .17       .17       .17       .17         89.0000       .17       .17       .17       .17       .17       .17       .17	81.5000	.20	.20			
82.5000       .19       .18       .18       .18       .18       .18       .18       .18       .18       .18       .18       .18       .18       <		.20	.20	.20		
83.5000       .19       .18       .18       .18       .18       .18       .18       .18       .18       .18       .18       .18       .18       .18       .18       .18       .18       .18       .19       .17       .17       .17       <			.19	.19	.19	
84.0000       .19       .18       .17       .17       .17       .17       .17       .17       .17       .17       .17       .17       .17       .17       .17       .17       .17       .17       .17       .17       <					.19	.19
84.5000       .19       .19       .18       .18       .18         85.0000       .18       .18       .18       .18       .18         85.5000       .18       .18       .18       .18       .18         86.0000       .18       .18       .18       .18       .18         87.0000       .18       .18       .17       .17       .17         87.5000       .17       .17       .17       .17       .17       .17         88.0000       .17       .17       .17       .17       .17       .17         89.0000       .17       .17       .17       .17       .17       .17						
85.0000       .18       .18       .18       .18       .18         85.5000       .18       .18       .18       .18       .18         86.0000       .18       .18       .18       .18       .18         86.5000       .18       .18       .18       .18       .18         87.0000       .18       .18       .17       .17       .17         87.5000       .17       .17       .17       .17       .17         88.0000       .17       .17       .17       .17       .17       .17         89.0000       .17       .17       .17       .17       .17       .17						
85.5000       .18       .18       .18       .18       .18         86.0000       .18       .18       .18       .18       .18         86.5000       .18       .18       .18       .18       .18         87.0000       .18       .18       .17       .17       .17         87.5000       .17       .17       .17       .17       .17         88.0000       .17       .17       .17       .17       .17         89.0000       .17       .17       .17       .17       .17         89.0000       .17       .17       .17       .17       .17						
86.0000       .18       .18       .18       .18       .18         86.5000       .18       .18       .18       .18       .18         87.0000       .18       .18       .17       .17       .17         87.5000       .17       .17       .17       .17       .17         88.0000       .17       .17       .17       .17       .17         88.5000       .17       .17       .17       .17       .17         89.0000       .17       .17       .17       .17       .17						
86.5000       .18       .18       .18       .18       .18         87.0000       .18       .18       .17       .17       .17         87.5000       .17       .17       .17       .17       .17       .17         88.0000       .17       .17       .17       .17       .17       .17         88.5000       .17       .17       .17       .17       .17       .17         89.0000       .17       .17       .17       .17       .17       .17						
87.0000       .18       .18       .17       .17       .17         87.5000       .17       .17       .17       .17       .17       .17         88.0000       .17       .17       .17       .17       .17       .17         88.5000       .17       .17       .17       .17       .17       .17         89.0000       .17       .17       .17       .17       .17       .17						
87.5000     .17     .17     .17     .17       88.0000     .17     .17     .17     .17       88.5000     .17     .17     .17     .17       89.0000     .17     .17     .17     .17	i					
88.0000     .17     .17     .17     .17     .17       88.5000     .17     .17     .17     .17     .17       89.0000     .17     .17     .17     .17     .17						
88.5000     .17     .17     .17     .17     .17       89.0000     .17     .17     .17     .17     .17						
89.0000 .17 .17 .17 .17 .17						
, — , — , — , — , — , — , — , — , — , —						

S/N: H0M0L0862791 BT 2, Inc

Name.... SOUTH BASIN2

File.... I:\1370\COLUMBIA.PPK

Tag:

Title... routing of hydrograph through south basin

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Page 6.07

South Basin

Outflow Hydrograpi (5/7)

WARNING: Hydrograph truncated on right side.

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90.5000	.16	.16	.16	.16	.16
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91.5000	.16	.16	.16	.16	.16
92.0000	.16	.16	.16	.16	.16
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93.0000	.15	.15	.15	.15	.15
93.5000	.15	.15	.15	.15	.15
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95.5000	14	.14	.14	.14	.14 .14
96.0000	.14	.14	.14	.14	.14
96.5000	.14	.14	.14	.14	.14
97.0000	.14	.14	.14	.14	.14
97.5000	.14	.14	.14	.14	.14
98.0000	.14	.14	.14	.14	.14
98.5000	.14	.13	.13	.13	.13
99.0000	.13	.13	.13	.13	.13
99.5000	.13	.13	.13	.13	.13
100.0000	.13	.13	.13	.13	.13
100.5000	.13	.13	.13	.13	.13
101.0000	.13	.13	.13	.13	.13
101.5000	.13	.13	.13	.13	.12
102.0000	.12	.12	.12	.12	.12
102.5000	.12	.12	.12	.12	.12
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104.0000	.12	.12	.12	.12 .12	.12 .12
104.5000	.12	.12	.12	.12	.12
105.0000	.12	.12	.12	.12	.12
105.5000	.12	.11	.11	.11	.11
106.0000	.11	.11	.11	.11	.11
106.5000	.11	.11	.11	.11	.11
107.0000	.11	.11	.11	.11	.11
107.5000	.11	.11	.11	.11	.11
108.0000	.11	.11	.11	.11	.11
108.5000	.11	.11	.11	.11	.11
109.0000	.11	.11	.11	.11	.11
109.5000	.11	.10	.10	.10	.10
110.0000	.10	.10	.10	.10	.10
110.5000	.10	.10	.10	.10	.10
111.0000	.10	.10	.10	.10	.10

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Page 6.08

South Basin Outflow Hydrograph

(6/7)

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Title... routing of hydrograph through south basin

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hrs	Time on left	represents t	ime for fir	st value in	each row.
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112.0000	.10	.10	.10	.10	.10
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116.5000	.09	.09	.09	.09	.09
117.0000	.09	.09	.09	.09	.09
117.5000	.09	.09	.09	.09	.09
118.0000	.09	.09	.09	.09	.09
118.5000	.09	.09	.09	.08	.08
119.0000	.08	.08	.08	.08	.08
119.5000	.08	.08	.08	.08	.08
120.0000	.08	.08	.08	.08	.08
120.5000	.08	.08	.08	.08	.08
121.0000	.08	.08	.08	.08	.08
121.5000 122.0000	.08	.08	.08	.08	.08
122.5000	.08	.08 .08	.08 .08	.08	.08
123.0000	.08	.08	.08	.08 .08	.08 .08
123.5000	.08	.08	.08	.08	.08
124.0000	.08	.08	.08	.07	.07
124.5000	.07	.07	.07	.07	.07
125.0000	.07	.07	.07	.07	.07
125.5000	.07	.07	.07	.07	.07
126.0000	.07	.07	.07	.07	.07
126.5000	.07	.07	.07	.07	.07
127.0000	.07	.07	.07	.07	.07
127.5000	.07	.07	.07	.07	.07
128.0000	.07	.07	.07	.07	.07
128.5000	.07	.07	.07	.07	.07
129.0000 129.5000	.07 .07	.07 .07	.07 .07	.07	.07
130.0000	.07	.07	.07	.07 .07	.07 .07
130.5000	.07	.06	.06	.06	.07
131.0000	.06	.06	.06	.06	.06
131.5000	.06	.06	.06	.06	.06
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Title... routing of hydrograph through south basin

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Page 6.09

South Basin Outflow Hydrograf (7/7)

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134.0000	.06	.06	.06	.06	.06
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135.0000	.06	.06	.06	.06	.06
135.5000	.06	.06	.06	.06	.06
136.0000	.06	.06	.06	.06	.06
136.5000	.06	.06	.06	.06	.06
137.0000	.06	.06	.06	.06	.06
137.5000	.06	.06	.06	.06	.05
138.0000	.05	.05	.05	.05	.05
138.5000 139.0000	.05	.05	.05	.05	.05
139.5000	.05	.05 .05	.05	.05	.05
140.0000	.05	.05	.05	.05	.05
140.5000	.05	.05	.05 .05	.05	.05
141.0000	.05	.05	.05	.05	.05
141.5000	.05	.05	.05	.05 .05	.05
142.0000	.05	.05	.05	.05	.05 .05
142.5000	.05	.05	.05	.05	.05
143.0000	.05	.05	.05	.05	.05
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149.0000	.04	.04	.04	.04	.04
149.5000	.04	.04	.04	.04	.04
150.0000	.04	.04	.04	.04	.04
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151.0000	.04	.04	.04	.04	.04
151.5000	.04	.04	.04	.04	.04
152.0000	.04	.04	.04	.04	.04
152.5000	.04	.04	.04	.04	.04
153.0000	.04	.04	.04	.04	.04
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S/N: H0M0L0862791 BT 2, Inc

Type.... Pond Routing Summary

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Page 6.02

File.... I:\1370\COLUMBIA.PPK

Title... routing of hydrograph through south basin

South Basin 100-yr, 24-hr Storm

#### LEVEL POOL ROUTING SUMMARY

HYG Dir =  $I: \langle 1370 \rangle$ 

Inflow HYG file = SBASIN.HYG - south basin Outflow HYG file = NONE STORED - SOUTH BASIN2 OUT 100

Pond Node Data = south basin Pond Volume Data = south basin Pond Outlet Data = south basin2

No Infiltration

#### INITIAL CONDITIONS

\_\_\_\_\_ Starting WS Elev = 789.00 ft Starting Volume = .000 ac-ft
Starting Outflow = .00 cfs
Starting Infiltr. = .00 cfs
Starting Total Qout= .00 cfs
Time Increment = .1000 hrs

#### INFLOW/OUTFLOW HYDROGRAPH SUMMARY

Peak Inflow = 110.00 cfs at 12.4000 hrs

Peak Outflow = 16.79 cfs at 13.7000 hrs — Peak discharge

from basin

Peak Elevation = 793.29 ft - Peak water elevation Peak Storage = 7.080 ac-ft

#### MASS BALANCE (ac-ft)

\_\_\_\_\_\_ + Initial Vol = .000

+ HYG Vol IN =

13.207

- Infiltration = .000 - HYG Vol OUT = 12.435

- Retained Vol =

Unrouted Vol = -.001 ac-ft (.011% of Inflow Volume)

WARNING: Inflow hydrograph truncated on left side. WARNING: Outflow hydrograph truncated on right side.

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## References

#### Sheet flow

Sheet flow is flow over plane surfaces. It usually occurs in the headwater of streams. With sheet flow, the friction value (Manning's n) is an effective roughness coefficient that includes the effect of raindrop impact; drag over the plane surface; obstacles such as litter, crop ridges, and rocks; and erosion and transportation of sediment. These n values are for very shallow flow depths of about 0.1 foot or so. Table 3-1 gives Manning's n values for sheet flow for various surface conditions.

For sheet flow of less than 300 feet, use Manning's kinematic solution (Overton and Meadows 1976) to compute  $T_t$ :

$$T_t = \frac{0.007 \text{ (nL)0.8}}{\text{(P_2)0.5 s0.4}}$$
 [Eq. 3-3]

Table 3-1.—Roughness coefficients (Manning's π) for sheet flow

Surface description	n¹
Smooth surfaces (concrete, asphalt, gravel, or bare soil)	0.011
Fallow (no residue)	0.05
Cultivated soils:  Residue cover ≤20%	0.06 0.17
Grass: Short grass prairie Dense grasses² Bermudagrass	0.15 7 Ave = 0.24 5 0.19 0.41
Range (natural)	0.13
Woods: <sup>3</sup> Light underbrush Dense underbrush	0.40 0.80

<sup>&</sup>lt;sup>1</sup>The n values are a composite of information compiled by Engman (1986).

#### where

 $T_t = \text{travel time (hr)},$ 

n = Manning's roughness coefficient (table 3-1),

L = flow length (ft),

 $P_2 = 2$ -year, 24-hour rainfall (in), and

s = slope of hydraulic grade line (land slope, ft/ft).

This simplified form of the Manning's kinematic solution is based on the following: (I) shallow steady uniform flow, (2) constant intensity of rainfall excess (that part of a rain available for runoff), (3) rainfall duration of 24 hours, and (4) minor effect of infiltration on travel time. Rainfall depth can be obtained from appendix B.

#### Shallow concentrated flow

After a maximum of 300 feet, sheet flow usually becomes shallow concentrated flow. The average velocity for this flow can be determined from figure 3-1, in which average velocity is a function of watercourse slope and type of channel. For slopes less than 0.005 ft/ft, use equations given in appendix F for figure 3-1. Tillage can affect the direction of shallow concentrated flow. Flow may not always be directly down the watershed slope if tillage runs across the slope.

After determining average velocity in figure 3-1, use equation 3-1 to estimate travel time for the shallow concentrated flow segment.

#### Open channels

Open channels are assumed to begin where surveyed cross section information has been obtained, where channels are visible on aerial photographs, or where blue lines (indicating streams) appear on United States Geological Survey (USGS) quadrangle sheets. Manning's equation or water surface profile information can be used to estimate average flow velocity. Average flow velocity is usually determined for bank-full elevation.

alliculdes species such as weeping lovegrass, bluegrass, buffalo grass, blue grama grass, and native grass mixtures.

When selecting n, consider cover to a height of about 0.1 ft. This is the only part of the plant cover that will obstruct sheet flow.

Table 2-2c.-Runoff curve numbers for other agricultural lands1

Cover description	Curve numbers for hydrologic soil group—				
Cover type	Hydrologic condition	A	В	С	D
Pasture, grassland, or range—continuous	Poor	68	79	86	89
forage for grazing. <sup>2</sup>	Fair	49	69	79	84
torage to grazing.	Good	39	61 Ave	74) =67.5	80
Meadow—continuous grass, protected from grazing and generally mowed for hay.		30	58	71	78
Burk hand mad mixture with house	Poor	48	67	77	83
Brush—brush-weed-grass mixture with brush	Fair	35	56,	70	. 77
the major element. <sup>3</sup>	Good	430	48	65	73
Voods—grass combination (orchard	Poor	57	73	82	86
or tree farm).5	Fair	43	65	76	82
of thee faith.	Good	32	58	72	79
Voods. <sup>6</sup>	Poor	45	66	77	83
ii vousi	Fair	36	60	73	79
	Good	430	55	70	77
Farmsteads—buildings, lanes, driveways, and surrounding lots.		59	74	82	86

 $<sup>^{1}</sup>$ Average runoff condition, and  $I_{\rm n}=0.2$ S.

a.6

<sup>&</sup>lt;sup>2</sup>Poor: <50% ground cover or heavily grazed with no mulch.

Fair: 50 to 75% ground cover and not heavily grazed.

Good: >75% ground cover and lightly or only occasionally grazed.

<sup>&</sup>lt;sup>3</sup>Poor: <50% ground cover.

Fair: 50 to 75% ground cover.

Good: >75% ground cover.

<sup>4</sup>Actual curve number is less than 30; use CN = 30 for runoff computations.

<sup>&</sup>lt;sup>5</sup>CN's shown were computed for areas with 50% woods and 50% grass (pasture) cover. Other combinations of conditions may be computed from the CN's for woods and pasture.

<sup>\*</sup>Poor: Forest litter, small trees, and brush are destroyed by heavy grazing or regular burning.

Fair: Woods are grazed but not burned, and some forest litter covers the soil.

Good: Woods are protected from grazing, and litter and brush adequately cover the soil.

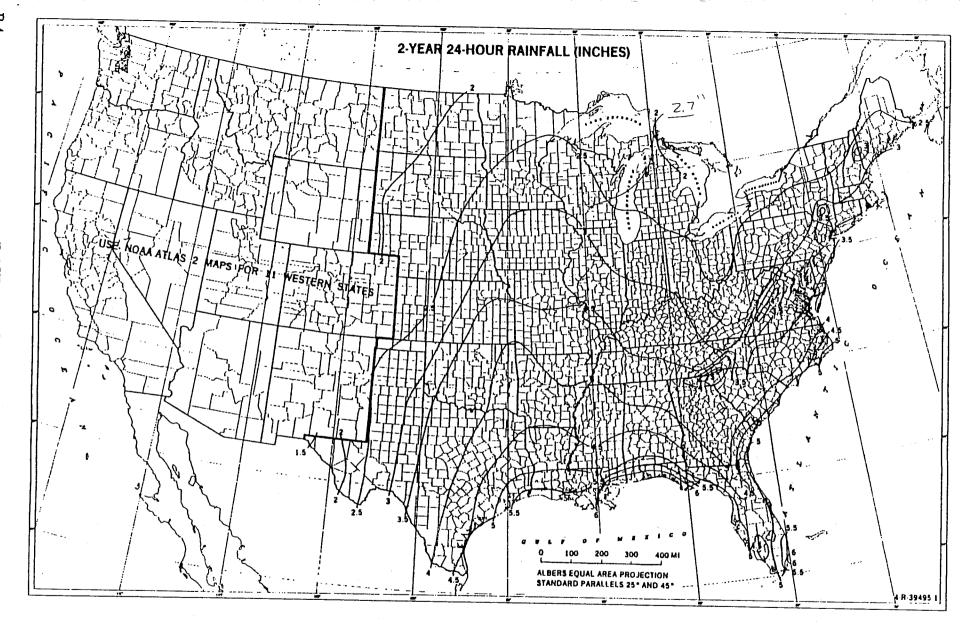


Figure Il-3.—Two-year, 24-hour rainfall.

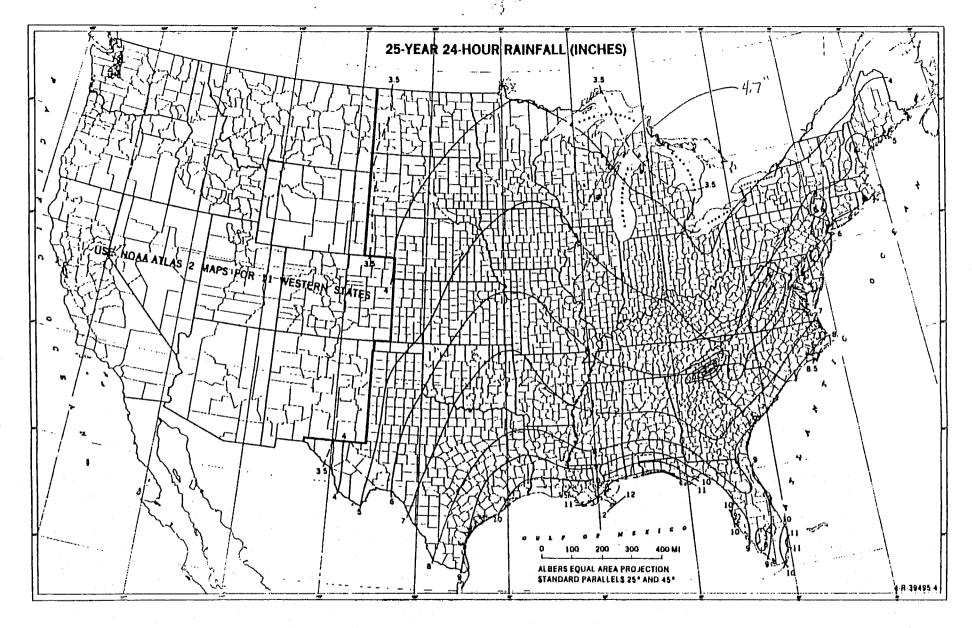


Figure B-6.-Twenty-five-year, 24-hour rainfall.

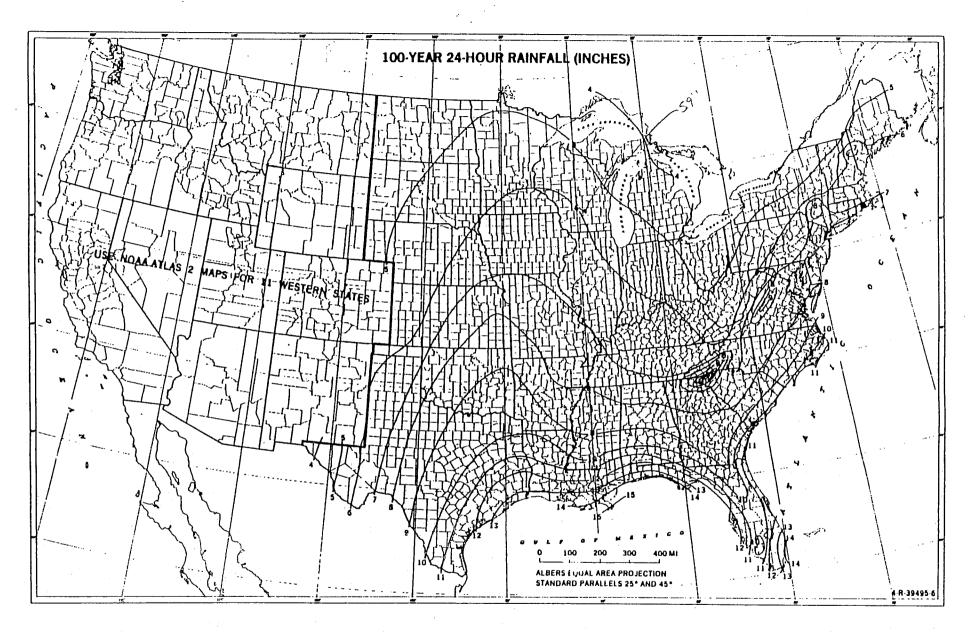


TABLE 8.1 Surface Area Requirements of Sediment Traps and Basins

	Pa	irticle size, mm		g velocity, c (m/sec)	Surface area ft <sup>1</sup> per ft <sup>3</sup> /sec discharge	requirements, (m² per m³/sec discharge)
	0.5	(coarse sand)	0.19	(0.058)	6.3	(20.7)
	0.2	(inedium sand)	0.067	(0.020)	17.9	(58.7)
	0.1	(fine sand)	0.023	(0.0070)	52.2	(171.0)
	0.05	(conrae ailt)	0.0062	(0.0019)	193.6	(635.0)
ء 15ء	<b>0.02</b>	(medium silt)	0.00096	(0.00029)	(1,250.0)	(4,101.0)
> ران.	0.01	(fine silt)	0.00024	(0.000073)	(5,000.0)	(16,404.0)
	0.005	i (clay)	0.0000	(810000.0)	20,000.0	(65,617.0)

weight composed of particles in the 0.01- to 0.02-mm range. A surface area 4 times larger would be needed to capture 5 percent more of this soil.

A balance between the cost-effectiveness of a certain basin size and the desire to capture fine particles must be achieved. It is desirable to capture the very small soil particles (clays and fine silts) because they cause turbidity and other water quality problems. However, Table 8.1 shows that a basin would have to be very large to capture particles smaller than 0.02 mm, particularly clay particles 0.005 mm and smaller. Because of the high cost of trapping very small particles, the authors recommend 0.02 as the design particle size for sediment basins except in areas with coarse soils, where a larger design particle may be used. The 0.02-mm particle is classified as a medium silt by the AASHTO soil classification system.

#### 8.2d Basin Discharge Rate

The peak discharge, calculated by the rational or another approved method, is used to size the basin riser. During any major storm, a sediment basin should fill with water to the top of its riser and then discharge at the rate of inflow to the basin. A sediment basin is not designed with a large water storage volume as is a reservoir. If the Inflow exceeds the design peak flow used to size the riser, the overflow should discharge down an emergency spillway.

#### 8.2e Design Runoff Rate

In the equation for surface area of a sediment basin, the discharge rate Q is a variable to be chosen by the designer. The above discussion of basin discharge rate shows that the discharge rate is, to a large extent, equal to the inflow. The riser is sized to handle the peak inflow to the basin. The authors suggest determining the surface area by the average runoff of a 10-year, 6-hr storm instead

of the peak flow. A substantial savings in size, and therefore cost, is obtained, and basin efficiency is not significantly decreased.

Consider a basin designed to capture the 0.02-mm particle at the average runoff rate. The average rainfall per hour is 17 percent of the total rainfall in a 6-hr storm (Sec. 4.1f). On a site with soils with a moderately high clay content, under ideal settling conditions this basin would retain about 62 percent of the eroded soil (i.e., 62 percent of the soil, by weight, is composed of 0.02-mm or larger particles).

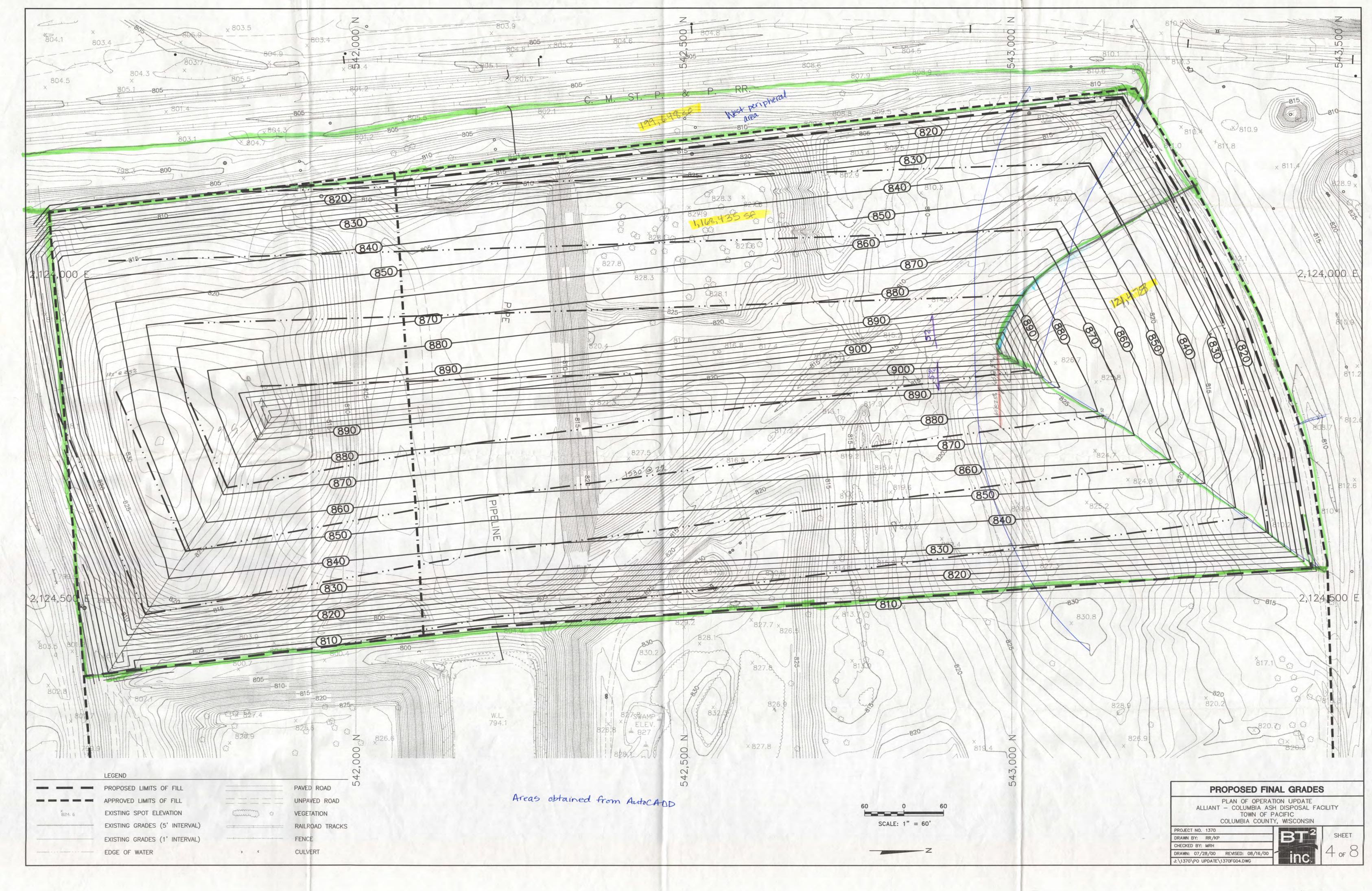
If the surface area of this basin were instead designed for the peak flow, it would be roughly 3 times larger. According to data from the U.S. Bureau of Reclamation (10), 25 percent of the total rainfall in a 6-hr storm falls in a 3-hr period (Fig. 4.2). Since the rainfall intensity i value is in units of inches (or millimeters) per hour, the peak flow can be calculated by using an i value of 50 percent of the 6-hr total. Since basin surface area is directly proportional to the discharge rate ( $A = 1.2Q/V_*$ ) and the peak discharge rate in a 6-hr storm is 2.9 times the average rate ( $50\% = 2.9 \times 17\%$ ), the surface area sized for the peak flow would be about 3 times the surface area sized for the average flow. The basin sized for the peak flow would capture, during most of the storm except the peak, particles with approximately one-third the settling velocity of the design particle. Since the 0.02-mm particle settles at 0.00096 ft/sec (0.00029 m/sec), particles with a settling velocity of 0.00032 ft/sec (0.000098 m/sec) would then be captured. These are approximately 0.01-mm particles.

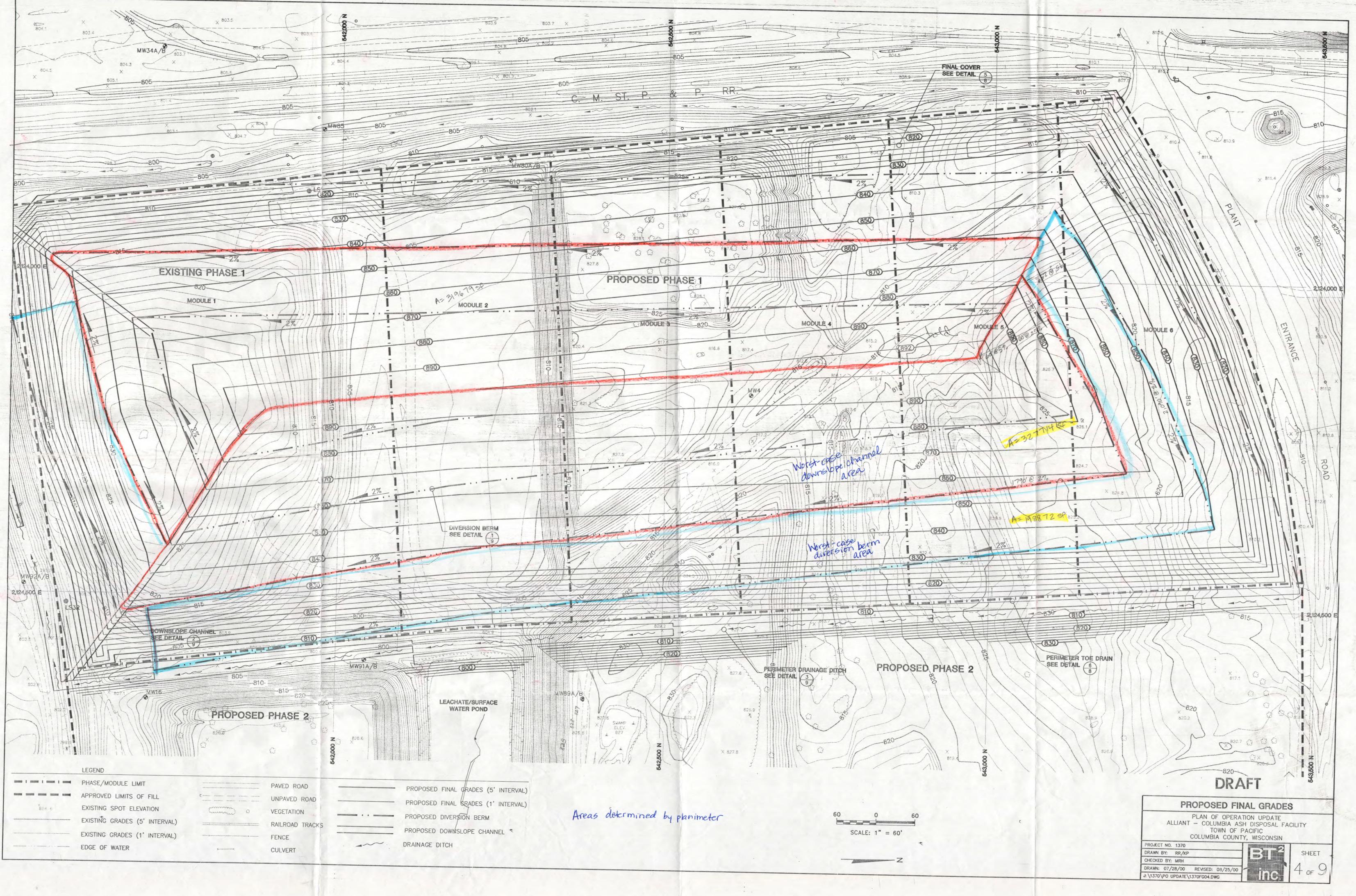
Suppose a basin on a site with clayey soils were sized by using the peak runoff rate. For the purpose of illustration, suppose the soil composition were typical of the San Francisco Bay Area as in the preceding example (62 percent of particles, by weight, greater than 0.02 mm and 5 percent, by weight, from 0.01 to 0.02 mm). A basin with a large surface area based on the peak runoff would capture the 0.01- to 0.02-mm particles as well as particles greater than 0.02 mm, or 67 percent of the eroded material. The basin efficiency would be increased 8 percent (5/62) by tripling the surface area. Thus it is generally much more cost-effective to size a basin by using the average runoff rather than the peak, and basin efficiency will not be significantly lower.

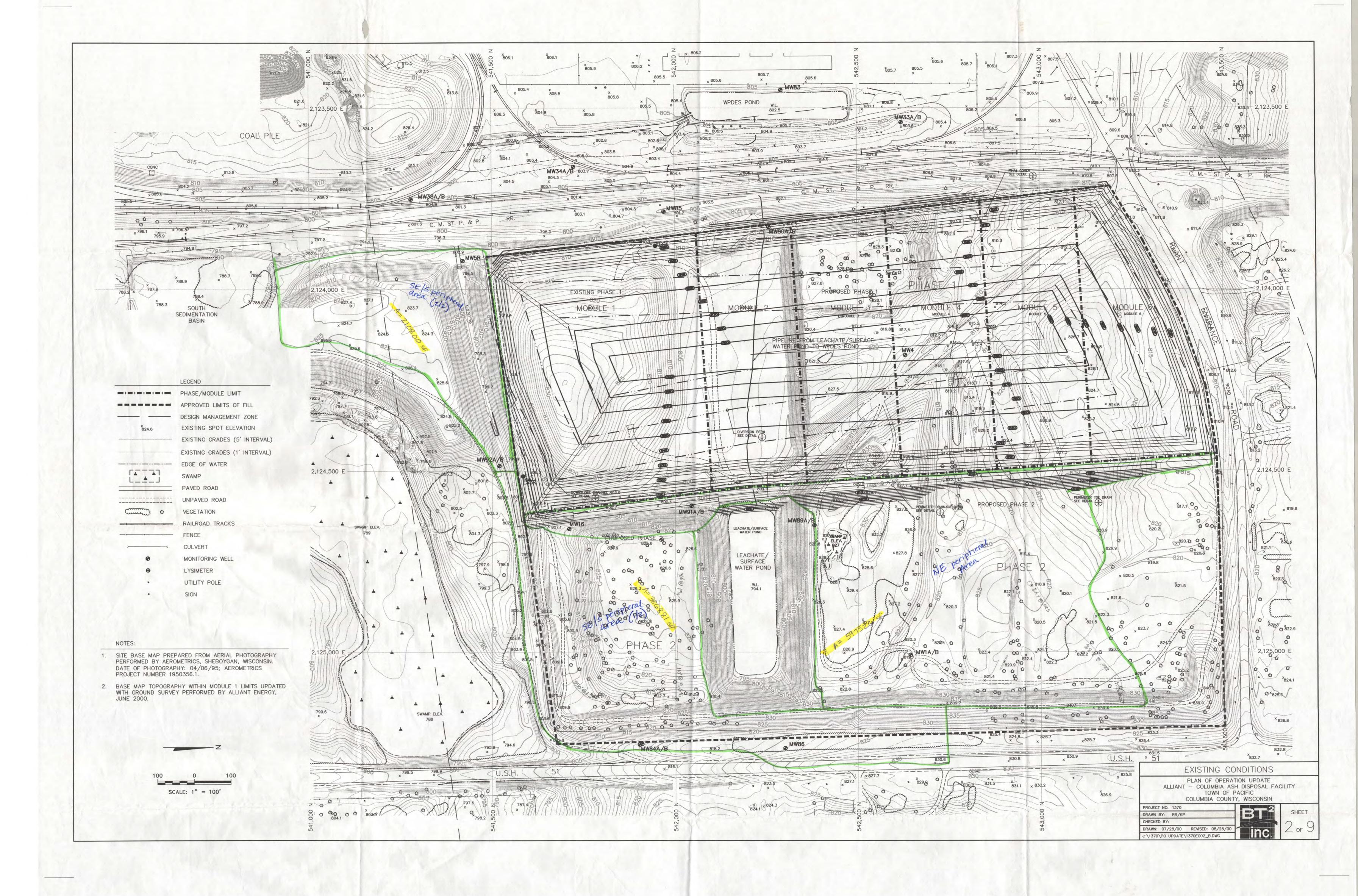
# 8.2f Settling Depth

If a basin is too shallow, water flowing rapidly through the basin may resuspend settled particles and decrease efficiency of capture. A similar problem occurs in grit-settling chambers at sewage treatment plants, where velocity must be controlled to prevent particle resuspension. An equation that describes scour in a grit chamber (2) is:

$$V_{\text{scour}} = \frac{1.486}{n} \times \left[ r^{1/6} \times h(S_s - 1) \times \frac{d}{304.8} \right]^{1/2}$$







# Appendix A2

Leachate/Surface Water Pond Capacity Evaluation

SCS	ENGINEERS	SHEET NO.		1
Job No.	25220183.00	CALC. NO.		
Job:	Columbia Energy Center	REV. NO.		
Client	WPL	BY	RJG	DATE 05/25/22
Subject	Module 10/11 - Leachate/Surface Water Pond Evalu	ation CHK'D.	MT	DATE 05/25/22

#### **Purpose:**

The purpose of the leachate/surface water pond evaluation is to determine the following based on the as-built leachate/surface water pond top of liner elevation of 796.97 (see Background section below):

- The maximum amount of open area during each filling phase in order to maintain the peak water elevation resulting from the 25-year, 24-hour storm event at the maximum allowable 796.97.
- The amount of open area allowable with pond closure filling in order to maintain the peak water elevation resulting from the 25-year, 24-hour storm event at the maximum allowable 796.97.
- Based on the amount of allowable open area determined from the above, determine the maximum starting water elevations in the leachate/surface water pond to accommodate 1, 2, 5, and 10-year, 24-hour storm events without overtopping.

#### **Background:**

- During construction of Module 2, the top of the leachate/surface water pond liner was determined to be at elevation 796.97.
- Previous calculations submitted to the WDNR on January 30, 2018, evaluated the leachate/surface water pond capacity based on the as-built pond liner elevation.
- A similar evaluation was performed for Module 3 and 4 construction and then Module 5 and 6 construction that produced a chart of maximum leachate/surface water pond starting elevations vs. rainfall storage capacity.
- Portions of Modules 1, 2, 3, and 4 currently have final or intermediate cover in place and Module 5 and 6 currently have rain cover (see **Figure 1 through 4**).
- Module 10 and 11 will be constructed in 2022.

#### Approach:

- Use the previously developed HydroCAD storm water model to model the below four filling scenarios.
  - 1. Filling Phase 0 Assumes portions of Module 2, 3, 4, 5, and 6 contributing to the leachate/surface water pond while material is placed from the pond closure and the plant. See **Figure 1** for filling grades and contributing area
  - 2. Filling Phase 1 Assumes portions of Module 2, 3, 4, 5, and 6 contributing to the leachate/surface water pond while material is placed from the pond closure and the plant. See **Figure 2** for filling grades and contributing area
  - 3. Filling Phase 2 Assumes portions of Module 2, 3, 4, 5, and 6 contributing to the leachate/surface water pond while material is placed from the pond closure and the plant. See **Figure 3** for filling grades and contributing area.

SCS	ENGINEERS	SHEET NO.		2
Job No.	25220183.00	CALC. NO.		
Job:	Columbia Energy Center	REV. NO.		
Client	WPL	BY	RJG	DATE 05/25/22
Subject	Module 10/11 - Leachate/Surface Water Pond Evaluation	CHK'D.	MT	DATE 05/25/22

- 4. Filling Phase 3 Assumes portions of Module 2, 3, 4, 5, and 6 contributing to the leachate/surface water pond while material is placed from the pond closure and the plant. See **Figure 4** for filling grades and contributing area.
- 5. Filling Phase 4 Assumes portions of Module 2, 3, 4, 5, 6, 10, and 11 contributing to the leachate/surface water pond while material is placed from the pond closure and the plant. See **Figure 5** for filling grades and contributing area.

#### **Assumptions:**

- Ash surfaces and intermediate cover areas were assumed to be impermeable (CN=98).
- The top of pond liner elevation is 796.97 (see Background section).
- Time of Concentration is 20 minutes for open areas.

#### **Results:**

- 1. Maximum allowable open area during filling and prior to permeter grade/Module 10 and 11 construction is 7.78 acres.
- 2. Maximum allowable open area during filling and after perimeter grades/Module 10 and 11 base grades are completed is 8.51 acres.

#### 3. <u>Filling Phase 0:</u>

- The contributing area of landfill to the leachate/surface water pond is 7.45 acres for the leachate/surface water pond to accommodate the runoff from a 25-year, 24-hour storm without overtopping.
- The remainder of landfill would need to be closed/covered with final or intermediate cover and routed away from the pond.
- **Figure 1** shows a proposed filling sequence, and **Figure 1a** shows the various operating levels of the leachate/surface water pond to accommodate the various storm events with the additional cover in place.

#### 4. Filling Phase 1:

- The contributing area of landfill to the leachate/surface water pond is 7.78 acres for the leachate/surface water pond to accommodate the runoff from a 25-year, 24-hour storm without overtopping.
- The remainder of landfill would need to be closed/covered with final or intermediate cover and routed away from the pond.
- **Figure 2** shows a proposed filling sequence, and **Figure 2a** shows the various operating levels of the leachate/surface water pond to accommodate the various storm events with the additional cover in place.

#### 5. Filling Phase 2:

• The contributing area of landfill to the leachate/surface water pond is 7.69 acres for the leachate/surface water pond to accommodate the runoff from a 25-year, 24-hour storm without overtopping.

SCS	ENGINEERS	SHEET NO.		3
Job No.	25220183.00	CALC. NO.		
Job:	Columbia Energy Center	REV. NO.		
Client	WPL	BY	RJG	DATE 05/25/22
Subject	Module 10/11 - Leachate/Surface Water Pond Evaluati	on CHK'D.	MT	DATE 05/25/22

- The remainder of landfill would need to be closed/covered with final or intermediate cover and routed away from the pond.
- **Figure 3** shows a proposed filling sequence, and **Figure 3a** shows the various operating levels of the leachate/surface water pond to accommodate the various storm events with the additional cover in place.

#### 6. Filling Phase 3:

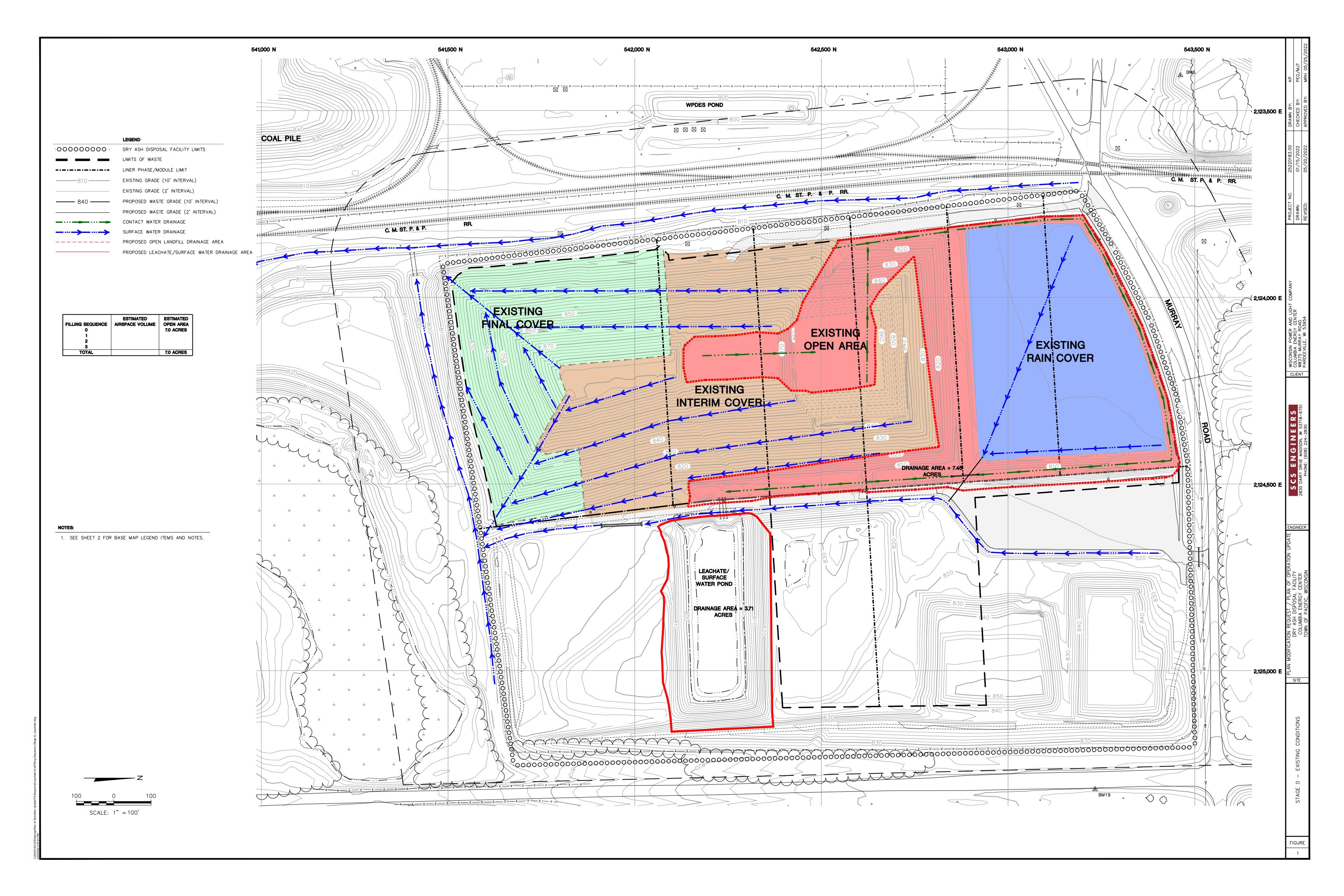
- The contributing area of landfill to the leachate/surface water pond is 7.64 acres for the leachate/surface water pond to accommodate the runoff from a 25-year, 24-hour storm without overtopping.
- The remainder of landfill would need to be closed/covered with final or intermediate cover and routed away from the pond.
- **Figure 4** shows a proposed filling sequence, and **Figure 4a** shows the various operating levels of the leachate/surface water pond to accommodate the various storm events with the additional cover in place.

#### 7. Filling Phase 4:

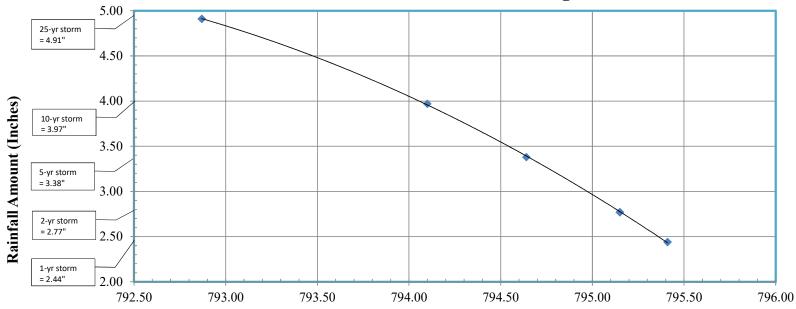
- The contributing area of landfill to the leachate/surface water pond is 8.44 acres for the leachate/surface water pond to accommodate the runoff from a 25-year, 24-hour storm without overtopping.
- The remainder of landfill would need to be closed/covered with final or intermediate cover and routed away from the pond.
- **Figure 5** shows a proposed filling sequence, and **Figure 5a** shows the various operating levels of the leachate/surface water pond to accommodate the various storm events with the additional cover in place.

The HydroCAD reports for the maximum open contributing area, each scenario modeled are attached.

I:\25220183.00\Data and Calculations\Leachate\_Surface Water Pond Evaluation\Leachate\_Surface Water Pond Evaluation\_Mod 5\_6 calc writeup.docx



# Figure 1A Columbia Energy Center Phase 0 Filling- Open Landfill Area Leachate/Surface Water Pond Maximum Starting Water Elevation



#### Leachate/Surface Water Pond Maximum Starting Water Elevation (ft)

#### Notes/Assumptions:

- 1. Maximum starting water elevations based on 2011 Mod 2 as-built survey which determined the top of pond liner elevation = 796.97.
- 2. Maximum starting water elevation assumes no freeboard.
- 3. Previously developed HydroCAD model utilized with curve number for intermediate cover areas and ash surfaces assumed at CN = 98.
- 4. HydroCAD model assumes drainage areas contributing to pond include (Figure 1):
  - Landfill open area = 7.46 acres.
  - Leachate/Surface Water Pond Area, 3.71 acres.
- 5. Maximum open area per HydroCAD model during filling is 7.78 acres.

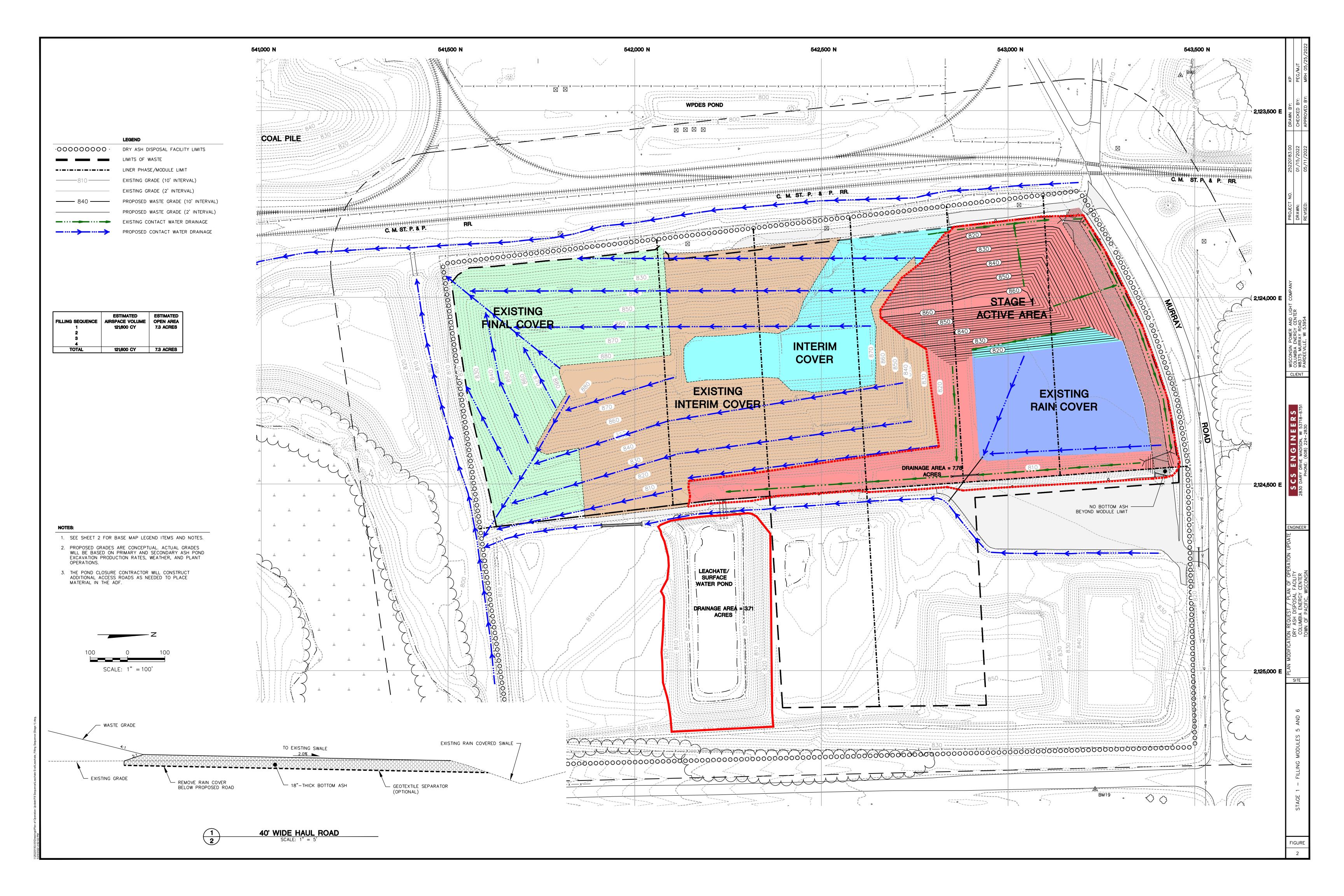
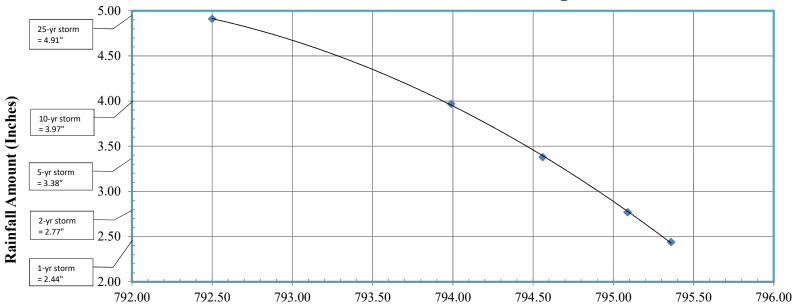


Figure 2A
Columbia Energy Center
Phase 1 Filling- Open Landfill Area
Leachate/Surface Water Pond Maximum Starting Water Elevation



#### Notes/Assumptions:

- 1. Maximum starting water elevations based on 2011 Mod 2 as-built survey which determined the top of pond liner elevation = 796.97.
- 2. Maximum starting water elevation assumes no freeboard.
- 3. Previously developed HydroCAD model utilized with curve number for intermediate cover areas and ash surfaces assumed at CN = 98.
- 4. HydroCAD model assumes drainage areas contributing to pond include (Figure 1):
  - Landfill open area = 7.78 acres.
  - Leachate/Surface Water Pond Area, 3.71 acres.
- 5. Maximum open area per HydroCAD model during filling is 7.78 acres.

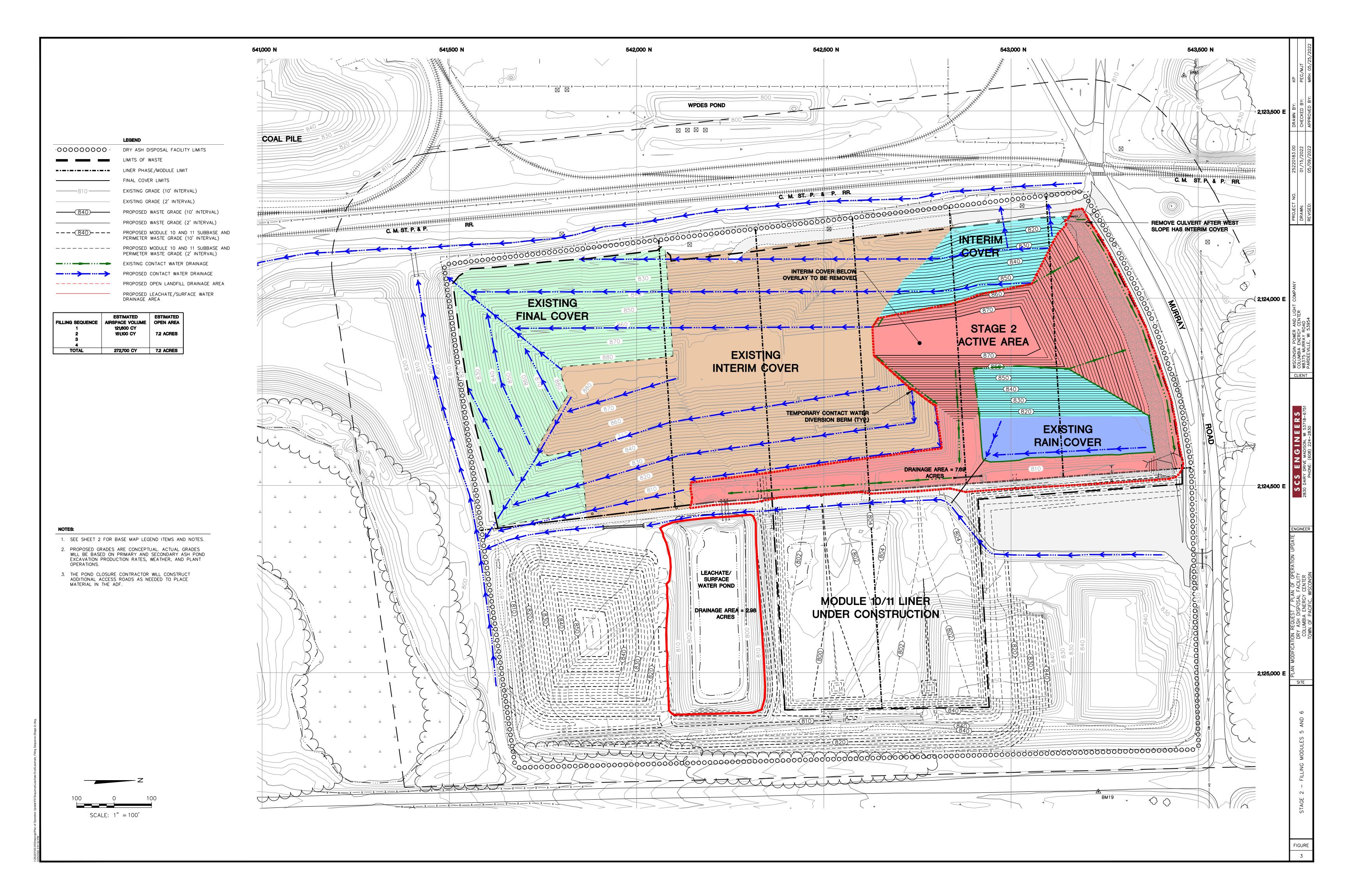
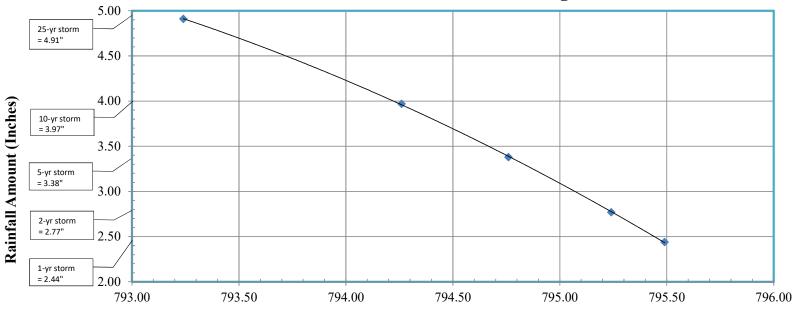


Figure 3A
Columbia Energy Center
Phase 2 Filling- Open Landfill Area
Leachate/Surface Water Pond Maximum Starting Water Elevation



#### Notes/Assumptions:

- 1. Maximum starting water elevations based on 2011 Mod 2 as-built survey which determined the top of pond liner elevation = 796.97.
- 2. Maximum starting water elevation assumes no freeboard.
- 3. Previously developed HydroCAD model utilized with curve number for intermediate cover areas and ash surfaces assumed at CN = 98.
- 4. HydroCAD model assumes drainage areas contributing to pond include (Figure 1):
  - Landfill open area = 7.69 acres.
  - Leachate/Surface Water Pond Area, 2.98 acres.
- 5. Maximum open area per HydroCAD model during filling is 8.51 acres.

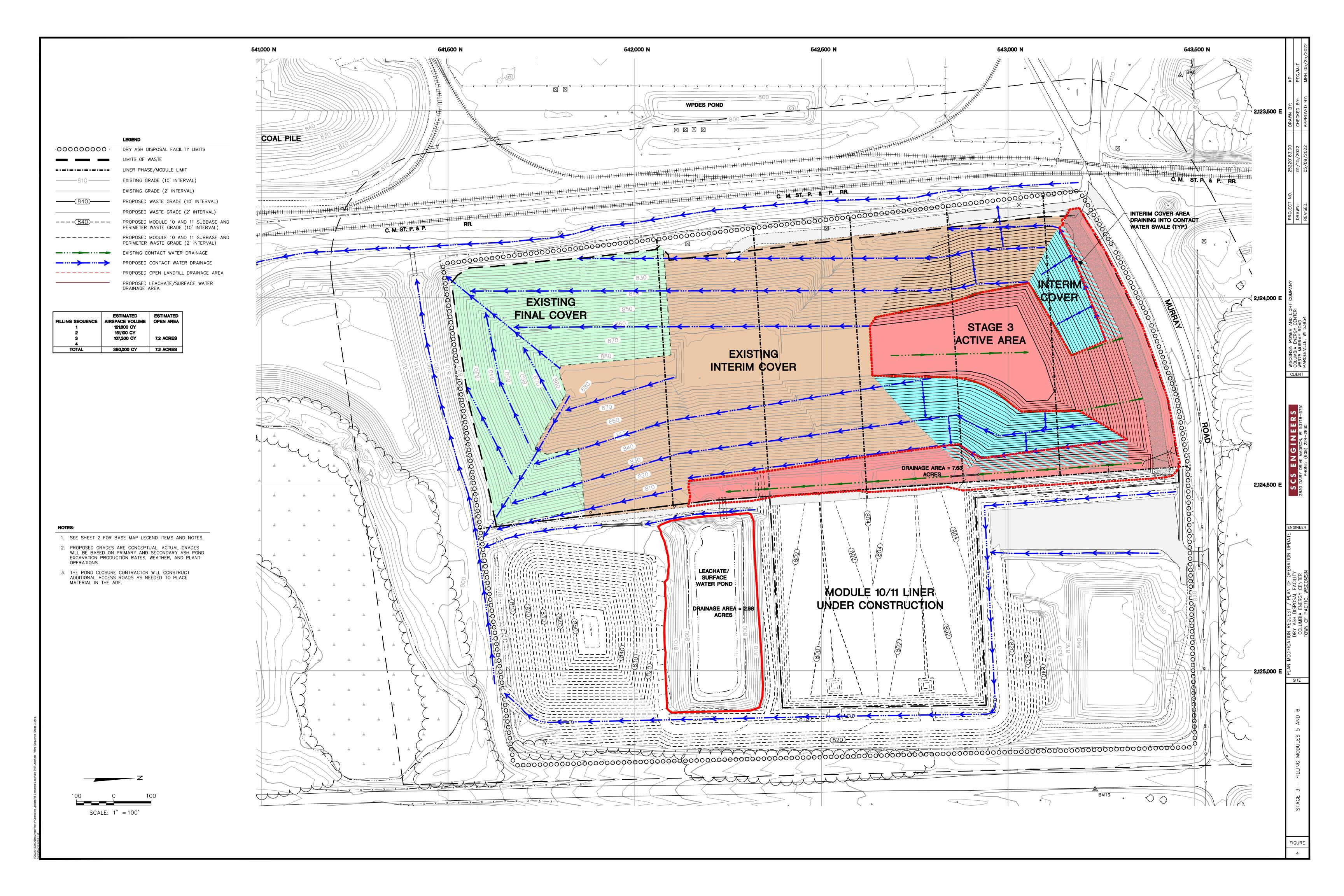
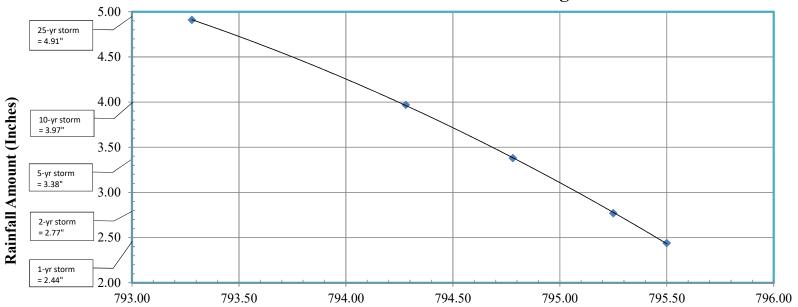


Figure 4A
Columbia Energy Center
Phase 3 Filling- Open Landfill Area
Leachate/Surface Water Pond Maximum Starting Water Elevation



#### Notes/Assumptions:

- 1. Maximum starting water elevations based on 2011 Mod 2 as-built survey which determined the top of pond liner elevation = 796.97.
- 2. Maximum starting water elevation assumes no freeboard.
- 3. Previously developed HydroCAD model utilized with curve number for intermediate cover areas and ash surfaces assumed at CN = 98.
- 4. HydroCAD model assumes drainage areas contributing to pond include (Figure 1):
  - Landfill open area = 7.64 acres.
  - Leachate/Surface Water Pond Area, 2.98 acres.
- 5. Maximum open area per HydroCAD model during filling is 8.51 acres.

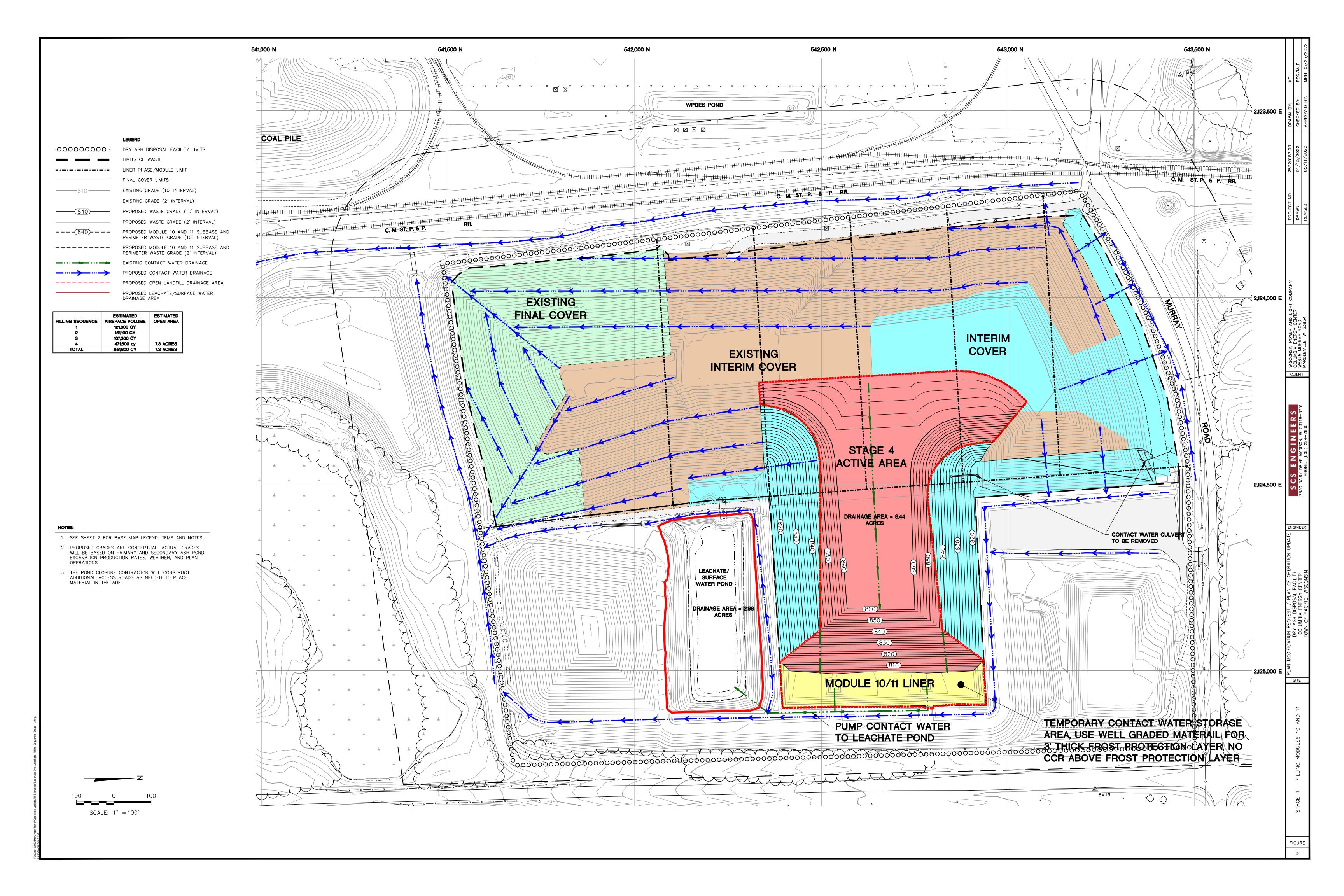
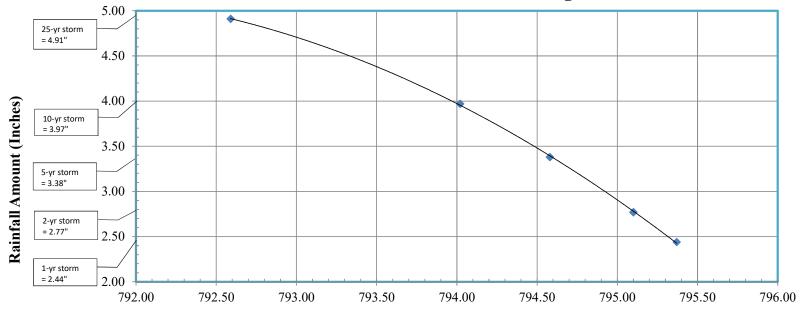
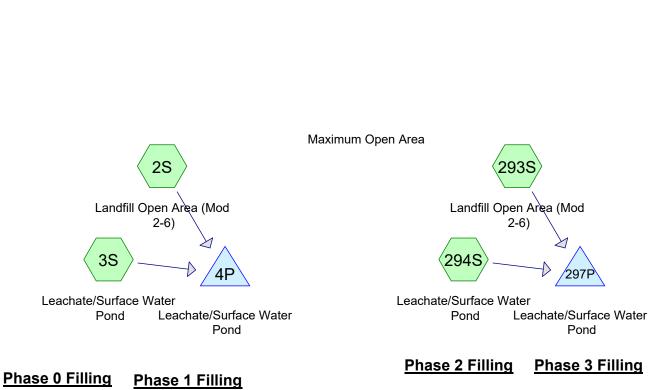


Figure 5A
Columbia Energy Center
Phase 4 Filling- Open Landfill Area
Leachate/Surface Water Pond Maximum Starting Water Elevation

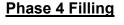


#### Notes/Assumptions:

- 1. Maximum starting water elevations based on 2011 Mod 2 as-built survey which determined the top of pond liner elevation = 796.97.
- 2. Maximum starting water elevation assumes no freeboard.
- 3. Previously developed HydroCAD model utilized with curve number for intermediate cover areas and ash surfaces assumed at CN = 98.
- 4. HydroCAD model assumes drainage areas contributing to pond include (Figure 1):
  - Landfill open area = 8.44 acres.
  - Leachate/Surface Water Pond Area, 2.98 acres.
- 5. Maximum open area per HydroCAD model during filling is 8.51 acres.















Outflow=0.00 cfs 0.000 af

Time span=0.00-33.00 hrs, dt=0.05 hrs, 661 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 2S: Landfill Open Area	Runoff Area=7.780 ac 100.00% Impervious Runoff Depth=4.67" Tc=20.0 min CN=98 Runoff=31.75 cfs 3.030 af
Subcatchment3S: Leachate/Surface	Runoff Area=3.710 ac 100.00% Impervious Runoff Depth=4.67" Tc=0.0 min CN=98 Runoff=26.38 cfs 1.445 af
Subcatchment 293S: Landfill Open Area	Runoff Area=8.510 ac 100.00% Impervious Runoff Depth=4.67" Tc=20.0 min CN=98 Runoff=34.73 cfs 3.314 af
Subcatchment 294S: Leachate/Surface	Runoff Area=2.980 ac 100.00% Impervious Runoff Depth=4.67" Tc=0.0 min CN=98 Runoff=21.19 cfs 1.161 af
Pond 4P: Leachate/SurfaceWater Pond	Peak Elev=796.97' Storage=197,946 cf Inflow=40.23 cfs 4.475 af Outflow=0.00 cfs 0.000 af
Pond 297P: Leachate/SurfaceWater Pond	dPeak Elev=796.97' Storage=197,946 cf Inflow=39.03 cfs 4.475 af

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# **Summary for Subcatchment 2S: Landfill Open Area (Mod 2-6)**

3.030 af. Depth= 4.67" Runoff 31.75 cfs @ 12.28 hrs, Volume= Routed to Pond 4P: Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 25-yr, 24-hr storm Rainfall=4.91"

	Area	(ac)	CN	Desc	cription					
*	7.	075	98	Mod	Mod 2 - 6 Open Area					
*	0.	705	98	Acce	ess Road					
	7.	780	98	Weig	ghted Aver	age				
	7.	7.780 100.00% Impervious Area								
	Тс	Leng	th	Slope	Velocity	Capacity	Description			
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)				
-	20.0			•			Direct Entry, Estimated			

# Summary for Subcatchment 3S: Leachate/Surface Water Pond

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

26.38 cfs @ 12.04 hrs, Volume= 1.445 af, Depth= 4.67"

Routed to Pond 4P: Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 25-yr, 24-hr storm Rainfall=4.91"

_	Area	(ac)	CN	Desc	cription					
*	3.	710	98	Lead	_eachate Surface Water Pond					
	3.710 100.00% Impervious Area									
	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
	0.0						Direct Entry,			

# Summary for Subcatchment 293S: Landfill Open Area (Mod 2-6)

Runoff 34.73 cfs @ 12.28 hrs, Volume= 3.314 af, Depth= 4.67" Routed to Pond 297P: Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 25-yr, 24-hr storm Rainfall=4.91"

	Area (ac)	CN	Description
*	8.510	98	Mod 2 - 11 Open Area
	8.510		100.00% Impervious Area

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Tc	Length	Slope	Velocity	Capacity	Description	
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
20.0					Direct Entry, E	stimated

# Summary for Subcatchment 294S: Leachate/Surface Water Pond

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff 21.19 cfs @ 12.04 hrs, Volume= 1.161 af, Depth= 4.67" Routed to Pond 297P: Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 25-yr, 24-hr storm Rainfall=4.91"

	Area	(ac)	CN	Desc	cription						
*	2.	980	98	Lead	eachate Surface Water Pond						
	2.	980 100.00% Impervious Area									
	Тс	Lengt	th	Slope	Velocity	Capacity	Description				
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)					
	0.0						Direct Entry,				

# Summary for Pond 4P: Leachate/Surface Water Pond

11.490 ac,100.00% Impervious, Inflow Depth = 4.67" for 25-yr, 24-hr storm event Inflow Area =

Inflow 40.23 cfs @ 12.06 hrs, Volume= 4.475 af

Outflow 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs

Starting Elev= 792.50' Surf.Area= 11,070 sf Storage= 3,030 cf

Peak Elev= 796.97' @ 25.15 hrs Surf.Area= 61,611 sf Storage= 197,946 cf (194,915 cf above start)

Flood Elev= 796.97' Surf.Area= 61,588 sf Storage= 197,647 cf (194,617 cf above start)

123.466

141.736

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no outflow)

66.581

75,155

798.00

00.008

Volume	Invert	Avail.S	torage	Storage	e Description	
#1	792.00'	405	,390 cf	Custon	n Stage Data (Pr	rismatic)Listed below (Recalc)
Elevation (feet)		Area sq-ft)		.Store c-feet)	Cum.Store (cubic-feet)	
792.00		1,051		0	0	
794.00 796.00		1,126 5,885		12,177 98,011	42,177 140,188	

263.654

405,390

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# Summary for Pond 297P: Leachate/Surface Water Pond

Inflow Area = 11.490 ac,100.00% Impervious, Inflow Depth = 4.67" for 25-yr, 24-hr storm event

Inflow = 39.03 cfs @ 12.27 hrs, Volume= 4.475 af

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs

Starting Elev= 792.50' Surf.Area= 11,070 sf Storage= 3,030 cf

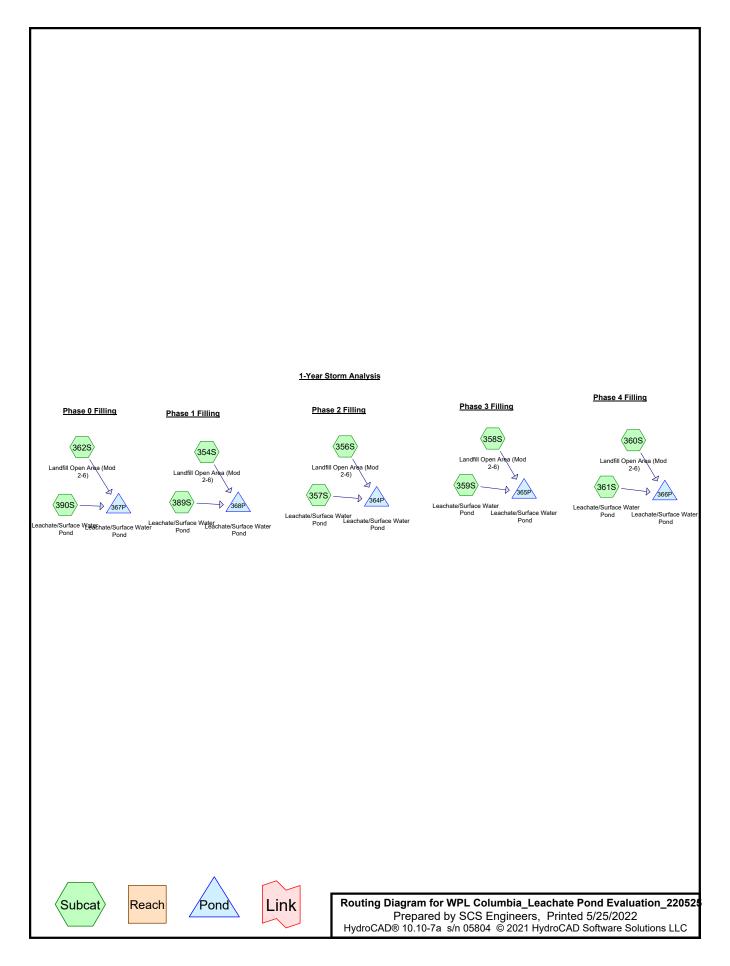
Peak Elev= 796.97' @ 25.15 hrs Surf.Area= 61,611 sf Storage= 197,946 cf (194,915 cf above start)

Flood Elev= 796.97' Surf.Area= 61,588 sf Storage= 197,647 cf (194,617 cf above start)

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Volume	Invert	Avail.Storage	Storage Description
#1	792.00'	405,390 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
792.00	1,051	0	0
794.00	41,126	42,177	42,177
796.00	56,885	98,011	140,188
798.00	66,581	123,466	263,654
800.00	75,155	141,736	405,390



Time span=0.00-33.00 hrs, dt=0.05 hrs, 661 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 354S: Landfill Open Area Runoff Area=339,047 sf 100.00% Impervious Runoff Depth=2.21" Tc=20.0 min CN=98 Runoff=15.52 cfs 1.434 af

Subcatchment 356S: Landfill Open Area Runoff Area=335,031 sf 100.00% Impervious Runoff Depth=2.21"

Tc=20.0 min CN=98 Runoff=15.34 cfs 1.417 af

Subcatchment 357S: Leachate/Surface Runoff Area=2.980 ac 100.00% Impervious Runoff Depth=2.21" Tc=0.0 min CN=98 Runoff=10.38 cfs 0.549 af

Subcatchment 358S: Landfill Open Area Runoff Area=332,594 sf 100.00% Impervious Runoff Depth=2.21"

Tc=20.0 min CN=98 Runoff=15.23 cfs 1.407 af

Subcatchment 359S: Leachate/Surface Runoff Area=2.980 ac 100.00% Impervious Runoff Depth=2.21"

Tc=0.0 min CN=98 Runoff=10.38 cfs 0.549 af

Subcatchment 360S: Landfill Open Area Runoff Area=367,758 sf 100.00% Impervious Runoff Depth=2.21"

Tc=20.0 min CN=98 Runoff=16.84 cfs 1.556 af

Subcatchment 361S: Leachate/Surface Runoff Area=2.980 ac 100.00% Impervious Runoff Depth=2.21"
Tc=0.0 min CN=98 Runoff=10.38 cfs 0.549 af

Subcatchment 362S: Landfill Open Area Runoff Area=324,737 sf 100.00% Impervious Runoff Depth=2.21"

Tc=20.0 min CN=98 Runoff=14.87 cfs 1.374 af

Subcatchment 389S: Leachate/Surface Runoff Area=3.706 ac 100.00% Impervious Runoff Depth=2.21" Tc=0.0 min CN=98 Runoff=12.91 cfs 0.683 af

Subcatchment 390S: Leachate/Surface Runoff Area=3.706 ac 100.00% Impervious Runoff Depth=2.21"
Tc=0.0 min CN=98 Runoff=12.91 cfs 0.683 af

Pond 364P: Leachate/SurfaceWater Pond Peak Elev=796.97' Storage=197,850 cf Inflow=17.45 cfs 1.966 af Outflow=0.00 cfs 0.000 af

Pond 365P: Leachate/Surface Water Pond Peak Elev=796.97' Storage=197,930 cf Inflow=17.34 cfs 1.956 af Outflow=0.00 cfs 0.000 af

Pond 366P: Leachate/Surface Water Pond Peak Elev=796.97' Storage=197,593 cf Inflow=18.94 cfs 2.105 af Outflow=0.00 cfs 0.000 af

Pond 367P: Leachate/Surface Water Pond Peak Elev=796.97' Storage=197,577 cf Inflow=19.31 cfs 2.056 af Outflow=0.00 cfs 0.000 af

Pond 368P: Leachate/Surface Water Pond Peak Elev=796.97' Storage=197,611 cf Inflow=19.60 cfs 2.117 af Outflow=0.00 cfs 0.000 af

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# **Summary for Subcatchment 354S: Landfill Open Area (Mod 2-6)**

Runoff = 15.52 cfs @ 12.29 hrs, Volume= 1.434 af, Depth= 2.21"

Routed to Pond 368P : Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 1-yr, 24-hr storm Rainfall=2.44"

	Α	rea (sf)	CN [	Description					
*	3	39,047	98 N	Mod 2 - 6 Open Area					
	339,047 100.00% Impervious Are				pervious A	rea			
	Тс	3	Slope	,	Capacity	Description			
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	20.0					Direct Entry, Estimated			

# **Summary for Subcatchment 356S: Landfill Open Area (Mod 2-6)**

Runoff = 15.34 cfs @ 12.29 hrs, Volume= 1.417 af, Depth= 2.21"

Routed to Pond 364P: Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 1-yr, 24-hr storm Rainfall=2.44"

_	Α	rea (sf)	CN [	Description					
*	3	35,031	98 <b>N</b>	Mod 2 - 6 Open Area					
	335,031 100.00% Impervious Are					rea			
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
-	20.0	(ieet)	(11/11)	(II/Sec)	(CIS)	Direct Entry, Estimated			

# Summary for Subcatchment 357S: Leachate/Surface Water Pond

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff = 10.38 cfs @ 12.04 hrs, Volume= 0.549 af, Depth= 2.21"

Routed to Pond 364P : Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 1-yr, 24-hr storm Rainfall=2.44"

	Area (ac)	CN	Description
*	2.980	98	Leachate Surface Water Pond
	2.980		100.00% Impervious Area

WPL Columbia\_Leachate Pond Evaluation\_22MSE 24-hr 4 1-yr, 24-hr storm Rainfall=2.44"
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	_	•			Description		
 (min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
0.0		Direct Entry,					

# **Summary for Subcatchment 358S: Landfill Open Area (Mod 2-6)**

Runoff = 15.23 cfs @ 12.29 hrs, Volume= 1.407 af, Depth= 2.21"

Routed to Pond 365P: Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 1-yr, 24-hr storm Rainfall=2.44"

_	Α	rea (sf)	CN [	Description					
*	3	32,594	98 N	Mod 2 - 6 Open Area					
	332,594 100.00% Impervious Are					rea			
	Тс	3	Slope	,	Capacity	Description			
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	20.0					Direct Entry, Estimated			

# Summary for Subcatchment 359S: Leachate/Surface Water Pond

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff = 10.38 cfs @ 12.04 hrs, Volume= 0.549 af, Depth= 2.21"

Routed to Pond 365P: Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 1-yr, 24-hr storm Rainfall=2.44"

_	Area	(ac)	CN	Desc	cription		
*	* 2.980 98 Leachate Surface Water Pond						
	2.980 100.00% Impervious Area						
	Тс	Lengt	h S	Slope	Velocity	Capacity	Description
_	(min)	(fee	t)	(ft/ft)	(ft/sec)	(cfs)	
_	0.0						Direct Entry,

#### **Summary for Subcatchment 360S: Landfill Open Area (Mod 2-6)**

Runoff = 16.84 cfs @ 12.29 hrs, Volume= 1.556 af, Depth= 2.21" Routed to Pond 366P : Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 1-yr, 24-hr storm Rainfall=2.44"

WPL Columbia\_Leachate Pond Evaluation\_22MSE 24-hr 4 1-yr, 24-hr storm Rainfall=2.44"
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	Α	rea (sf)	CN I	Description					
*	3	67,758	98 I	Mod 2 - 11 Open Area					
	3	67,758		100.00% Im	pervious A	rea			
	Тс	Length	Slope	Velocity	Capacity	Description			
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	20.0					Direct Entry, Estimated			

# Summary for Subcatchment 361S: Leachate/Surface Water Pond

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff = 10.38 cfs @ 12.04 hrs, Volume= 0.549 af, Depth= 2.21" Routed to Pond 366P : Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 1-yr, 24-hr storm Rainfall=2.44"

	Area	(ac)	CN	Desc	cription					
*	2.	980	98	Lead	eachate Surface Water Pond					
	2.980 100.00% Impervious Area									
	Тс	Leng	th	Slope	Velocity	Capacity	Description			
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	·			
	0.0						Direct Entry.			

# Summary for Subcatchment 362S: Landfill Open Area (Mod 2-6)

Runoff = 14.87 cfs @ 12.29 hrs, Volume= 1.374 af, Depth= 2.21" Routed to Pond 367P : Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 1-yr, 24-hr storm Rainfall=2.44"

_	Α	rea (sf)	CN E	Description					
*	3	24,737	98 N	Mod 2 - 6 Open Area					
	324,737 100.00% Impervious Are				npervious A	ırea			
	Тс	Length	Slope	Velocity	Capacity	Description			
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	20.0					Direct Entry, Estimated			

# Summary for Subcatchment 389S: Leachate/Surface Water Pond

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff = 12.91 cfs @ 12.04 hrs, Volume= 0.683 af, Depth= 2.21" Routed to Pond 368P : Leachate/Surface Water Pond

# WPL Columbia\_Leachate Pond Evaluation\_22MSE 24-hr 4 1-yr, 24-hr storm Rainfall=2.44"

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Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 1-yr, 24-hr storm Rainfall=2.44"

_	Area	(ac)	CN	Desc	cription				
*	3.	706	98	B Leachate Surface Water Pond					
	3.706 100.00% Impervious Area								
	Tc	Lengt	h S	Slope	Velocity	Capacity	Description		
_	(min)	(fee	t)	(ft/ft)	(ft/sec)	(cfs)			
	0.0						Direct Entry,		

# Summary for Subcatchment 390S: Leachate/Surface Water Pond

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff = 12.91 cfs @ 12.04 hrs, Volume= 0.683 af,

0.683 af, Depth= 2.21"

Routed to Pond 367P: Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 1-yr, 24-hr storm Rainfall=2.44"

_	Area	(ac)	CN	Desc	cription					
4	3.	706	98	Leac	Leachate Surface Water Pond					
_	3.706 100.00% Impervious Area									
	Тс			•	,	- 1 /	Description			
_	(min)	(fee	t)	(ft/ft)	(ft/sec)	(cfs)				
	0.0						Direct Entry,			

# Summary for Pond 364P: Leachate/Surface Water Pond

Inflow Area = 10.671 ac,100.00% Impervious, Inflow Depth = 2.21" for 1-yr, 24-hr storm event

Inflow = 17.45 cfs @ 12.27 hrs, Volume= 1.966 af

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs Starting Elev= 795.49' Surf.Area= 52,866 sf Storage= 112,201 cf

Peak Elev= 796.97' @ 25.15 hrs Surf.Area= 61,604 sf Storage= 197,850 cf (85,648 cf above start)

Flood Elev= 796.97' Surf.Area= 61,588 sf Storage= 197,647 cf (85,446 cf above start)

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Volume	Invert	Avail.Storage	Storage Description
#1	792.00'	405,390 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

# WPL Columbia\_Leachate Pond Evaluation\_22MSE 24-hr 4 1-yr, 24-hr storm Rainfall=2.44" Prepared by SCS Engineers Printed 5/25/2022

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Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
792.00	1,051	0	0
794.00	41,126	42,177	42,177
796.00	56,885	98,011	140,188
798.00	66,581	123,466	263,654
800.00	75,155	141,736	405,390

# Summary for Pond 365P: Leachate/Surface Water Pond

Inflow Area = 10.615 ac,100.00% Impervious, Inflow Depth = 2.21" for 1-yr, 24-hr storm event

Inflow = 17.34 cfs @ 12.27 hrs, Volume= 1.956 af

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs

Starting Elev= 795.50' Surf.Area= 52,945 sf Storage= 112,730 cf

Peak Elev= 796.97' @ 25.15 hrs Surf.Area= 61,610 sf Storage= 197,930 cf (85,199 cf above start)

Flood Elev= 796.97' Surf.Area= 61,588 sf Storage= 197,647 cf (84,917 cf above start)

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no outflow)

75,155

800.00

Volume	Invert	Avail.Storage	Storage	Description			
#1	792.00'	405,390 cf	Custom	Custom Stage Data (Prismatic)Listed below (Recalc)			
Elevation (feet)			ic.Store pic-feet)	Cum.Store (cubic-feet)			
792.00	1	1,051	0	0			
794.00	41	1,126	42,177	42,177			
796.00	56	5,885	98,011	140,188			
798.00	66	S,581 ´	123,466	263,654			

# Summary for Pond 366P: Leachate/Surface Water Pond

405.390

Inflow Area = 11.423 ac,100.00% Impervious, Inflow Depth = 2.21" for 1-yr, 24-hr storm event

Inflow = 18.94 cfs @ 12.27 hrs, Volume= 2.105 af

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs

Starting Elev= 795.37' Surf.Area= 51,921 sf Storage= 105,914 cf

Peak Elev= 796.97' @ 25.15 hrs Surf.Area= 61,583 sf Storage= 197,593 cf (91,679 cf above start)

Flood Elev= 796.97' Surf.Area= 61,588 sf Storage= 197,647 cf (91,733 cf above start)

141,736

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

# WPL Columbia\_Leachate Pond Evaluation 22MSE 24-hr 4 1-yr, 24-hr storm Rainfall=2.44"

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Volume	Invert	Avail.S	torage	Storage	Description		
#1	792.00'	405	,390 cf	Custon	n Stage Data (Pri	smatic)Listed belo	ow (Recalc)
Elevation (feet)		.Area (sq-ft)		:.Store c-feet)	Cum.Store (cubic-feet)		
792.00		1,051	•	0	0		
794.00	4	1,126	4	12,177	42,177		
796.00	5	6,885	(	98,011	140,188		
798.00	6	6,581	12	23,466	263,654		
800.00	7	5,155	14	11,736	405,390		

# Summary for Pond 367P: Leachate/Surface Water Pond

11.161 ac,100.00% Impervious, Inflow Depth = 2.21" for 1-yr, 24-hr storm event Inflow Area =

Inflow 19.31 cfs @ 12.05 hrs, Volume= 2.056 af

0.00 cfs @ 0.00 hrs, Volume= Outflow 0.000 af, Atten= 100%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs

Starting Elev= 795.41' Surf.Area= 52,236 sf Storage= 107,997 cf

Peak Elev= 796.97' @ 25.15 hrs Surf.Area= 61,582 sf Storage= 197,577 cf (89,579 cf above start)

Flood Elev= 796.97' Surf.Area= 61,588 sf Storage= 197,647 cf (89,650 cf above start)

Avail Storage Storage Description

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no outflow)

Invert

Volume

VOIGITIC	IIIVCIL	Avaii.Otorage		Otorage		
#1	792.00'	405	,390 cf	Custon	n Stage Data (P	rismatic)Listed below (Recalc)
Elevation (feet)		.Area sq-ft)	Inc. (cubic	Store -feet)	Cum.Store (cubic-feet)	
792.00		1,051		0	0	
794.00	4	1,126	4:	2,177	42,177	
796.00	50	6,885	98	3,011	140,188	
798.00	66	6,581		3,466	263,654	
800.00	7	5,155	14	1,736	405,390	

# Summary for Pond 368P: Leachate/Surface Water Pond

11.489 ac,100.00% Impervious, Inflow Depth = 2.21" for 1-yr, 24-hr storm event Inflow Area =

Inflow 19.60 cfs @ 12.06 hrs, Volume= 2.117 af

0.00 cfs @ 0.00 hrs, Volume= Outflow 0.000 af, Atten= 100%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs Starting Elev= 795.36' Surf.Area= 51,842 sf Storage= 105.395 cf

Peak Elev= 796.97' @ 25.15 hrs Surf.Area= 61,585 sf Storage= 197,611 cf (92,216 cf above start)

Flood Elev= 796.97' Surf.Area= 61,588 sf Storage= 197,647 cf (92,252 cf above start)

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

**COL POO Filling** 

# WPL Columbia\_Leachate Pond Evaluation\_22MSE 24-hr 4 1-yr, 24-hr storm Rainfall=2.44"

Invert

Volume

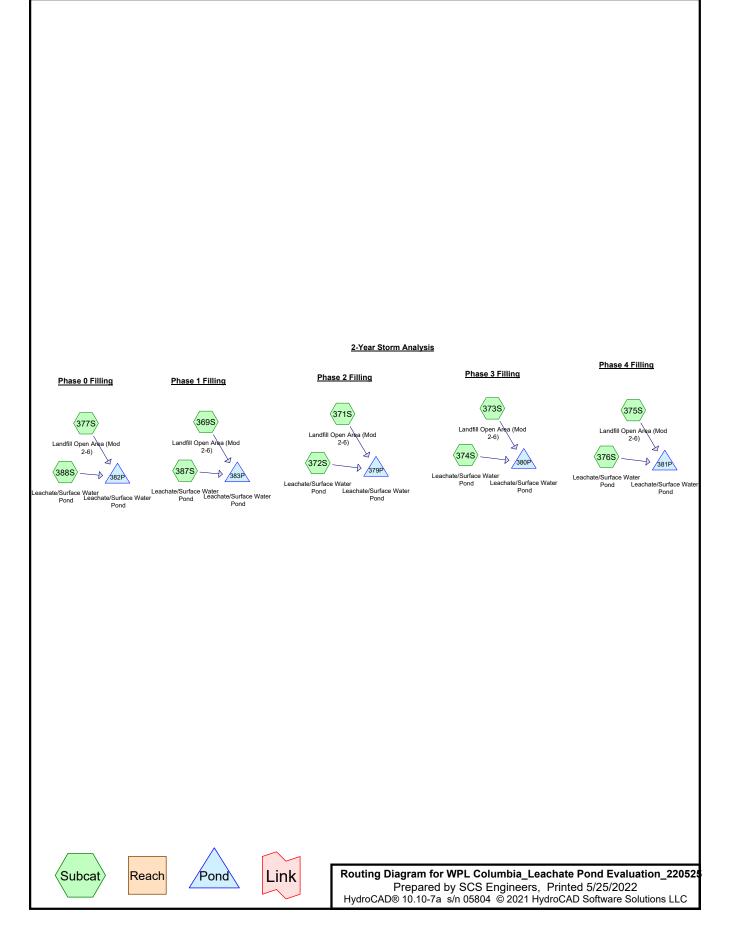
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Avail.Storage Storage Description

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#1	792.00'	405,390 cf	Custon	n Stage Data (P	rismatic)Listed below (Recalc)
Elevation (feet)	Surf.Area (sg-ft		.Store c-feet)	Cum.Store (cubic-feet)	
792.00	1,05		0	0	
794.00	41,126	6 4	2,177	42,177	
796.00	56,885	5 9	8,011	140,188	
798.00	66,58	1 12	3,466	263,654	
800.00	75,155	5 14	1,736	405,390	



Outflow=0.00 cfs 0.000 af

Time span=0.00-33.00 hrs, dt=0.05 hrs, 661 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 369S: Landfill Open Area Runoff Area=339,047 sf 100.00% Impervious Runoff Depth=2.54" Tc=20.0 min CN=98 Runoff=17.70 cfs 1.647 af Subcatchment 371S: Landfill Open Area Runoff Area = 335,031 sf 100.00% Impervious Runoff Depth = 2.54" Tc=20.0 min CN=98 Runoff=17.49 cfs 1.628 af Subcatchment 372S: Leachate/Surface Runoff Area=2.980 ac 100.00% Impervious Runoff Depth=2.54" Tc=0.0 min CN=98 Runoff=11.83 cfs 0.631 af Subcatchment 373S: Landfill Open Area Runoff Area=332,594 sf 100.00% Impervious Runoff Depth=2.54" Tc=20.0 min CN=98 Runoff=17.37 cfs 1.616 af Subcatchment 374S: Leachate/Surface Runoff Area=2.980 ac 100.00% Impervious Runoff Depth=2.54" Tc=0.0 min CN=98 Runoff=11.83 cfs 0.631 af Subcatchment 375S: Landfill Open Area Runoff Area = 367,758 sf 100.00% Impervious Runoff Depth = 2.54 Tc=20.0 min CN=98 Runoff=19.20 cfs 1.787 af Runoff Area=2.980 ac 100.00% Impervious Runoff Depth=2.54" Subcatchment 376S: Leachate/Surface Tc=0.0 min CN=98 Runoff=11.83 cfs 0.631 af Subcatchment 377S: Landfill Open Area Runoff Area=324,737 sf 100.00% Impervious Runoff Depth=2.54" Tc=20.0 min CN=98 Runoff=16.96 cfs 1.578 af Runoff Area=3.706 ac 100.00% Impervious Runoff Depth=2.54" Subcatchment 387S: Leachate/Surface Tc=0.0 min CN=98 Runoff=14.72 cfs 0.784 af Runoff Area=3.706 ac 100.00% Impervious Runoff Depth=2.54" Subcatchment 388S: Leachate/Surface Tc=0.0 min CN=98 Runoff=14.72 cfs 0.784 af Pond 379P: Leachate/SurfaceWater Pond Peak Elev=796.97' Storage=197,593 cf Inflow=19.90 cfs 2.258 af Outflow=0.00 cfs 0.000 af Pond 380P: Leachate/Surface Water Pond Peak Elev=796.97' Storage=197,587 cf Inflow=19.77 cfs 2.246 af Outflow=0.00 cfs 0.000 af Pond 381P: Leachate/Surface Water Pond Peak Elev=796.97' Storage=197,471 cf Inflow=21.61 cfs 2.417 af Outflow=0.00 cfs 0.000 af Pond 382P: Leachate/SurfaceWater Pond Peak Elev=796.97' Storage=197,558 cf Inflow=22.04 cfs 2.362 af Outflow=0.00 cfs 0.000 af

Pond 383P: Leachate/Surface Water Pond Peak Elev=796.97' Storage=197,589 cf Inflow=22.37 cfs 2.431 af

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#### Summary for Subcatchment 369S: Landfill Open Area (Mod 2-6)

1.647 af. Depth= 2.54" Runoff 17.70 cfs @ 12.29 hrs, Volume= Routed to Pond 383P: Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 2-yr, 24-hr storm Rainfall=2.77"

	Α	rea (sf)	CN [	Description					
*	3	39,047	98 N	Mod 2 - 6 Open Area					
	339,047 100.00% Imperv				npervious A	rea			
	Тс	Length	Slope	Velocity	Capacity	Description			
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	20.0					Direct Entry, Estimated			

#### **Summary for Subcatchment 371S: Landfill Open Area (Mod 2-6)**

17.49 cfs @ 12.29 hrs, Volume= 1.628 af, Depth= 2.54" Runoff Routed to Pond 379P: Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 2-yr, 24-hr storm Rainfall=2.77"

	А	rea (sf)	CN E	Description					
*	3	35,031	98 N	Mod 2 - 6 Open Area					
	335,031 100.00% Impervious Ar				npervious A	rea			
	Tc	Length	Slope	Velocity	Capacity	Description			
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	20.0					Direct Entry, Estimated			

### Summary for Subcatchment 372S: Leachate/Surface Water Pond

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

11.83 cfs @ 12.04 hrs, Volume= 0.631 af, Depth= 2.54" Runoff Routed to Pond 379P: Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 2-yr, 24-hr storm Rainfall=2.77"

	Area (ac)	CN	Description
*	2.980	98	Leachate Surface Water Pond
	2.980		100.00% Impervious Area

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	_	•			Description
 (min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
0.0					Direct Entry,

#### **Summary for Subcatchment 373S: Landfill Open Area (Mod 2-6)**

Runoff = 17.37 cfs @ 12.29 hrs, Volume= 1.616 af, Depth= 2.54"

Routed to Pond 380P: Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 2-yr, 24-hr storm Rainfall=2.77"

	Α	rea (sf)	CN [	Description					
*	3	32,594	98 <b>N</b>	Mod 2 - 6 Open Area					
	332,594 100.00% Impervious A			00.00% Im	pervious A	rea			
	Tc	9	Slope	Velocity	Capacity	Description			
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	20.0					Direct Entry, Estimated			

#### Summary for Subcatchment 374S: Leachate/Surface Water Pond

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff = 11.83 cfs @ 12.04 hrs, Volume= 0.631 af, Depth= 2.54"

Routed to Pond 380P: Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 2-yr, 24-hr storm Rainfall=2.77"

_	Area	(ac)	CN	Desc	cription			
*	2.	2.980 98 Leachate Surface Water Pond						
2.980 100.00% Imperviou					00% Impe	rvious Area	1	
	Тс	Lengt	h S	Slope	Velocity	Capacity	Description	
_	(min)	(fee	t)	(ft/ft)	(ft/sec)	(cfs)		
_	0.0						Direct Entry,	

#### **Summary for Subcatchment 375S: Landfill Open Area (Mod 2-6)**

Runoff = 19.20 cfs @ 12.29 hrs, Volume= 1.787 af, Depth= 2.54" Routed to Pond 381P : Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 2-yr, 24-hr storm Rainfall=2.77"

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	Α	rea (sf)	CN I	Description					
*	3	67,758	98 1	Mod 2 - 11 Open Area					
	367,758 100.00% Impervious Ar				pervious A	rea			
	Тс	Length	Slope	Velocity	Capacity	Description			
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	·			
	20.0					Direct Entry, Estimated			

#### Summary for Subcatchment 376S: Leachate/Surface Water Pond

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff = 11.83 cfs @ 12.04 hrs, Volume= 0.631 af, Depth= 2.54" Routed to Pond 381P : Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 2-yr, 24-hr storm Rainfall=2.77"

	Area	(ac)	CN	Desc	cription					
*	2.	.980	98	Lead	eachate Surface Water Pond					
2.980 100.00% Impervious Area						1				
	Тс	Leng		Slope	,	- 1 /	Description			
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)				
	0.0						Direct Entry,			

#### **Summary for Subcatchment 377S: Landfill Open Area (Mod 2-6)**

Runoff = 16.96 cfs @ 12.29 hrs, Volume= 1.578 af, Depth= 2.54" Routed to Pond 382P : Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 2-yr, 24-hr storm Rainfall=2.77"

_	Α	rea (sf)	CN E	N Description					
*	3	24,737	98 N	Mod 2 - 6 Open Area					
	324,737 100.00% Impervio			00.00% Im	npervious A	ırea			
	Тс	Length	Slope	Velocity	Capacity	Description			
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	20.0					Direct Entry, Estimated			

#### Summary for Subcatchment 387S: Leachate/Surface Water Pond

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff = 14.72 cfs @ 12.04 hrs, Volume= 0.784 af, Depth= 2.54" Routed to Pond 383P : Leachate/Surface Water Pond

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Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 2-yr, 24-hr storm Rainfall=2.77"

_	Area	(ac)	CN	Desc	Description					
*	3.	706	6 98 Leachate Surface Water Pond							
3.706 100.00% Impervious Area						a				
	Tc	Lengt	h S	Slope	Velocity	Capacity	Description			
_	(min)	(fee	t)	(ft/ft)	(ft/sec)	(cfs)				
	0.0						Direct Entry,			

#### Summary for Subcatchment 388S: Leachate/Surface Water Pond

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff = 14.72 cfs @ 12.04 hrs, Volume= 0.784 af, Depth= 2.54"

Routed to Pond 382P: Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 2-yr, 24-hr storm Rainfall=2.77"

_	Area (ac) CN Description						
4	3.	3.706 98 Leachate Surface Water Pond					
_	3.706 100.00% Impervious Area						
	Тс			•	,	- 1 /	Description
_	(min)	(fee	t)	(ft/ft)	(ft/sec)	(cfs)	
	0.0						Direct Entry,

#### Summary for Pond 379P: Leachate/Surface Water Pond

Inflow Area = 10.671 ac,100.00% Impervious, Inflow Depth = 2.54" for 2-yr, 24-hr storm event

Inflow = 19.90 cfs @ 12.27 hrs, Volume= 2.258 af

Outflow =  $0.00 \text{ cfs } \bar{\text{@}}$  0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs Starting Elev= 795.24' Surf.Area= 50,897 sf Storage= 99,231 cf

Peak Elev= 796.97' @ 25.15 hrs Surf.Area= 61,583 sf Storage= 197,593 cf (98,362 cf above start)

Flood Elev= 796.97' Surf.Area= 61,588 sf Storage= 197,647 cf (98,416 cf above start)

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Volume	Invert	Avail.Storage	Storage Description
#1	792.00'	405,390 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

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Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
792.00	1,051	0	0
794.00	41,126	42,177	42,177
796.00	56,885	98,011	140,188
798.00	66,581	123,466	263,654
800.00	75,155	141,736	405,390

#### Summary for Pond 380P: Leachate/Surface Water Pond

Inflow Area = 10.615 ac,100.00% Impervious, Inflow Depth = 2.54" for 2-yr, 24-hr storm event

19.77 cfs @ 12.27 hrs, Volume= 2.246 af Inflow =

0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min Outflow

Routing by Stor-Ind method, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs

Starting Elev= 795.25' Surf.Area= 50,975 sf Storage= 99,740 cf

Peak Elev= 796.97' @ 25.15 hrs Surf.Area= 61,583 sf Storage= 197,587 cf (97,847 cf above start)

Flood Elev= 796.97' Surf.Area= 61,588 sf Storage= 197,647 cf (97,907 cf above start)

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert	Avail.Sto	orage	Storage	Description			
#1	792.00'	405,390 cf		Custom Stage Data (Prismatic)Listed below (Recalc)				
Elevation (feet)	Surf.Area (sq-ft)		Inc.Store (cubic-feet)		Cum.Store (cubic-feet)			
792.00		1,051		0	0			
794.00	4	1,126	4	2,177	42,177			
796.00	50	6,885	9	8,011	140,188			
798.00	60	6,581	12	3,466	263,654			
800.00	7:	5,155	14	1,736	405,390			

#### Summary for Pond 381P: Leachate/Surface Water Pond

Inflow Area = 11.423 ac,100.00% Impervious, Inflow Depth = 2.54" for 2-yr, 24-hr storm event

Inflow 21.61 cfs @ 12.27 hrs, Volume= 2.417 af

Outflow 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs

Starting Elev= 795.10' Surf.Area= 49,793 sf Storage= 92,183 cf

Peak Elev= 796.97' @ 25.15 hrs Surf.Area= 61,574 sf Storage= 197,471 cf (105,288 cf above start)

Flood Elev= 796.97' Surf.Area= 61,588 sf Storage= 197,647 cf (105,464 cf above start)

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

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Volume	Invert	Avail.S	torage	Storage	e Description				
#1	792.00'	405	405,390 cf <b>C</b>		Custom Stage Data (Prismatic)Listed below (Recalc)				
Elevation (feet)			Inc.Store (cubic-feet)		Cum.Store (cubic-feet)				
792.00		1,051	0		0				
794.00		1,126	4	12,177	42,177				
796.00	5	6,885		98,011	140,188				
798.00	6	6,581	12	23,466	263,654				
800.00	7	5,155	14	11,736	405,390				

#### Summary for Pond 382P: Leachate/Surface Water Pond

Inflow Area = 11.161 ac,100.00% Impervious, Inflow Depth = 2.54" for 2-yr, 24-hr storm event

Inflow = 22.04 cfs @ 12.05 hrs, Volume= 2.362 af

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs

Starting Elev= 795.15' Surf.Area= 50,187 sf Storage= 94,682 cf

Peak Elev= 796.97' @ 25.15 hrs Surf.Area= 61,581 sf Storage= 197,558 cf (102,876 cf above start)

Flood Elev= 796.97' Surf.Area= 61,588 sf Storage= 197,647 cf (102,965 cf above start)

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Invert Avail Storage Storage Description

Center-of-Mass det. time= (not calculated: no outflow)

\/al.....

volume	olume invert Avail.Sid		otorage	Storage	Description						
#1	792.00'	405	,390 cf	Custon	n Stage Data	(Prism	<b>atic)</b> Liste	ed below	(Recalc	)	
Elevation (feet)		.Area sq-ft)		.Store c-feet)	Cum.Stor (cubic-fee						
792.00	•	1,051		0		0					
794.00	4	1,126	4	2,177	42,17	<b>'</b> 7					
796.00	56	5,885	9	8,011	140,18	38					
798.00	66	3,581	12	3,466	263,65	54					
800.00	75	5,155	14	1,736	405,39	<del>)</del> 0					

#### Summary for Pond 383P: Leachate/Surface Water Pond

Inflow Area = 11.489 ac,100.00% Impervious, Inflow Depth = 2.54" for 2-yr, 24-hr storm event

Inflow = 22.37 cfs @ 12.06 hrs, Volume= 2.431 af

Outflow =  $0.00 \text{ cfs } \bar{\textcircled{0}}$  0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs

Starting Elev= 795.09' Surf.Area= 49,715 sf Storage= 91,685 cf

Peak Elev= 796.97' @ 25.15 hrs Surf.Area= 61,583 sf Storage= 197,589 cf (105,904 cf above start)

Flood Elev= 796.97' Surf.Area= 61,588 sf Storage= 197,647 cf (105,962 cf above start)

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

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## WPL Columbia\_Leachate Pond Evaluation\_22MSE 24-hr 4 2-yr, 24-hr storm Rainfall=2.77"

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Invert

Volume

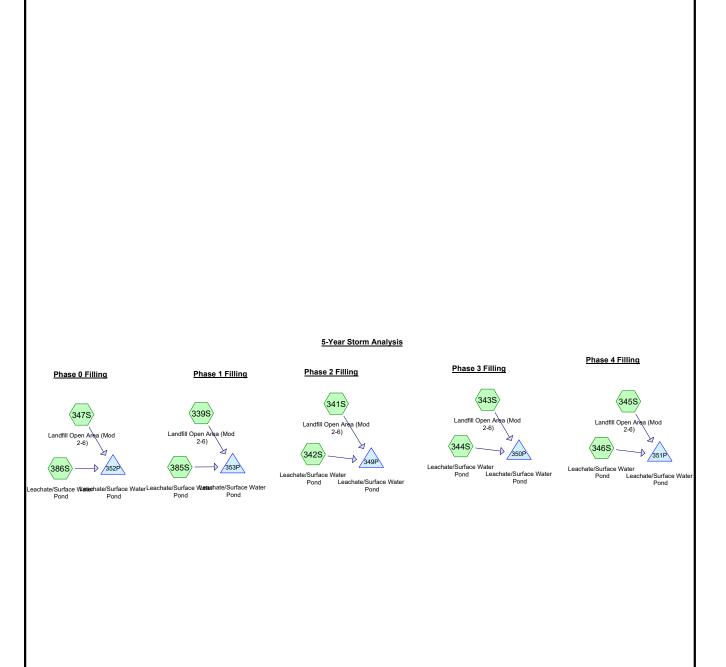
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<u>Ра</u>	g	е	9

#1	792.00' 4	05,390 cf <b>Custo</b>	m Stage Data (P	rismatic)Listed below (Recalc)
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
792.00	1,051	0	0	
794.00	41,126	42,177	42,177	
796.00	56,885	98,011	140,188	
798.00	66,581	123,466	263,654	
800.00	75,155	141,736	405,390	

Avail.Storage Storage Description











Time span=0.00-33.00 hrs, dt=0.05 hrs, 661 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

 Subcatchment 339S: Landfill Open Area
 Runoff Area=339,047 sf
 100.00% Impervious
 Runoff Depth=3.15"

 Tc=20.0 min
 CN=98
 Runoff=21.73 cfs
 2.041 af

 Subcatchment 341S: Landfill Open Area
 Runoff Area=335,031 sf
 100.00% Impervious
 Runoff Depth=3.15"

 Tc=20.0 min
 CN=98
 Runoff Depth=3.15"

 Tc=0.0 min
 CN=98
 Runoff Depth=3.15"

 Tc=20.0 min
 CN=98
 Runoff Depth=3.15"

 Tc=0.0 min
 CN=98
 Runoff Depth=3.15"

 Tc=0.0 min
 CN=98
 Runoff Depth=3.15"

 Tc=0.0 min
 CN=98
 Runoff Depth=3.15"

 Runoff Depth=3.15"
 Runoff Depth=3.15"

Subcatchment 345S: Landfill Open Area Runoff Area=367,758 sf 100.00% Impervious Runoff Depth=3.15" Tc=20.0 min CN=98 Runoff=23.57 cfs 2.214 af

Subcatchment 346S: Leachate/Surface Runoff Area=2.980 ac 100.00% Impervious Runoff Depth=3.15" Tc=0.0 min CN=98 Runoff=14.51 cfs 0.781 af

Subcatchment 347S: Landfill Open Area Runoff Area=324,737 sf 100.00% Impervious Runoff Depth=3.15"
Tc=20.0 min CN=98 Runoff=20.81 cfs 1.955 af

Subcatchment 385S: Leachate/Surface Runoff Area=3.706 ac 100.00% Impervious Runoff Depth=3.15" Tc=0.0 min CN=98 Runoff=18.04 cfs 0.972 af

Subcatchment 386S: Leachate/Surface Runoff Area=3.706 ac 100.00% Impervious Runoff Depth=3.15" Tc=0.0 min CN=98 Runoff=18.04 cfs 0.972 af

Pond 349P: Leachate/SurfaceWater Pond Peak Elev=796.97' Storage=197,605 cf Inflow=24.41 cfs 2.798 af Outflow=0.00 cfs 0.000 af

Pond 350P: Leachate/Surface Water Pond Peak Elev=796.97' Storage=197,910 cf Inflow=24.26 cfs 2.784 af Outflow=0.00 cfs 0.000 af

Pond 351P: Leachate/Surface Water Pond Peak Elev=796.97' Storage=197,834 cf Inflow=26.51 cfs 2.995 af Outflow=0.00 cfs 0.000 af

Pond 352P: Leachate/Surface Water Pond Peak Elev=796.97' Storage=197,602 cf Inflow=27.07 cfs 2.927 af Outflow=0.00 cfs 0.000 af

Pond 353P: Leachate/SurfaceWater Pond Peak Elev=796.97' Storage=197,686 cf Inflow=27.48 cfs 3.013 af Outflow=0.00 cfs 0.000 af

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#### **Summary for Subcatchment 339S: Landfill Open Area (Mod 2-6)**

Runoff = 21.73 cfs @ 12.29 hrs, Volume= 2.041 af, Depth= 3.15"

Routed to Pond 353P: Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 5-yr, 24-hr storm Rainfall=3.38"

_	Α	rea (sf)	CN D	escription)		
*	3	39,047	98 N	1od 2 - 6 C	pen Area	
	339,047 100.00% Impervious Are				pervious A	rea
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	20.0	(1001)	(1010)	(10/300)	(013)	Direct Entry, Estimated

#### **Summary for Subcatchment 341S: Landfill Open Area (Mod 2-6)**

Runoff = 21.47 cfs @ 12.29 hrs, Volume= 2.017 af, Depth= 3.15" Routed to Pond 349P : Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 5-yr, 24-hr storm Rainfall=3.38"

_	A	rea (sf)	CN D	<u>escription</u>		
*	3	35,031	98 N	/lod 2 - 6 C	pen Area	
	3	35,031	100.00% Impervious Ar			rea
	Tc	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	20.0					Direct Entry, Estimated

### Summary for Subcatchment 342S: Leachate/Surface Water Pond

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff = 14.51 cfs @ 12.04 hrs, Volume= 0.781 af, Depth= 3.15" Routed to Pond 349P : Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 5-yr, 24-hr storm Rainfall=3.38"

	Area (ac)	CN	Description
*	2.980	98	Leachate Surface Water Pond
2.980			100.00% Impervious Area

WPL Columbia\_Leachate Pond Evaluation\_22MSE 24-hr 4 5-yr, 24-hr storm Rainfall=3.38"
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		_		•		Description
(m	in)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
0.0 Direct Entry,				Direct Entry,		

#### **Summary for Subcatchment 343S: Landfill Open Area (Mod 2-6)**

Runoff = 21.31 cfs @ 12.29 hrs, Volume= 2.002 af, Depth= 3.15"

Routed to Pond 350P: Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 5-yr, 24-hr storm Rainfall=3.38"

	Α	rea (sf)	CN [	Description					
*	3	32,594	98 <b>N</b>	Mod 2 - 6 Open Area					
	332,594 100.00% Impervious A			00.00% Im	pervious A	rea			
	Tc	9	Slope	Velocity	Capacity	Description			
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	20.0					Direct Entry, Estimated			

#### Summary for Subcatchment 344S: Leachate/Surface Water Pond

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff = 14.51 cfs @ 12.04 hrs, Volume= 0.781 af, Depth= 3.15"

Routed to Pond 350P: Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 5-yr, 24-hr storm Rainfall=3.38"

_	Area	(ac)	CN	Desc	cription			
*	2.	2.980 98 Leachate Surface Water Pond						
	2.980 100.00% Impervious Area							
	Тс	Leng	th :	Slope	Velocity	Capacity	Description	
(min) (feet) (ft/ft) (ft/sec) (cfs)								
	0.0						Direct Entry,	

#### **Summary for Subcatchment 345S: Landfill Open Area (Mod 2-6)**

Runoff = 23.57 cfs @ 12.29 hrs, Volume= 2.214 af, Depth= 3.15" Routed to Pond 351P : Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 5-yr, 24-hr storm Rainfall=3.38"

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	Α	rea (sf)	CN I	Description						
*	3	67,758	98 I	Mod 2 - 11 Open Area						
	3	67,758		100.00% Im	rea					
	Тс	Length	Slope	Velocity	Capacity	Description				
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	20.0					Direct Entry, Estimated				

#### Summary for Subcatchment 346S: Leachate/Surface Water Pond

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff = 14.51 cfs @ 12.04 hrs, Volume=

0.781 af, Depth= 3.15"

Routed to Pond 351P: Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 5-yr, 24-hr storm Rainfall=3.38"

	Area	(ac)	CN	Desc	cription		
*	2.	.980	98	Lead	hate Surfa	ace Water F	Pond
	2.	.980		100.	00% Impe	rvious Area	1
	Тс	Leng		Slope	,	- 1 /	Description
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
	0.0						Direct Entry,

#### **Summary for Subcatchment 347S: Landfill Open Area (Mod 2-6)**

Runoff = 20.81 cfs @ 12.29 hrs, Volume= 1.955 af, Depth= 3.15" Routed to Pond 352P : Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 5-yr, 24-hr storm Rainfall=3.38"

_	Α	rea (sf)	CN E	N Description					
*	3	24,737	98 N	Mod 2 - 6 Open Area					
	324,737 100.00% Impervious Area								
	Тс	Length	Slope	Velocity	Capacity	Description			
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	20.0					Direct Entry, Estimated			

#### Summary for Subcatchment 385S: Leachate/Surface Water Pond

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff = 18.04 cfs @ 12.04 hrs, Volume= 0.972 af, Depth= 3.15"

Routed to Pond 353P: Leachate/Surface Water Pond

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Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 5-yr, 24-hr storm Rainfall=3.38"

_	Area	(ac)	CN	Desc	cription					
*	3.	706	98	Lead	Leachate Surface Water Pond					
	3.706 100.00% Impervious Area									
Tc Length Slope Velocity Capacity Description						Description				
_	(min)	(fee	t)	(ft/ft)	(ft/sec)	(cfs)				
	0.0						Direct Entry,			

#### Summary for Subcatchment 386S: Leachate/Surface Water Pond

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff = 18.04 cfs @ 12.04 hrs, Volume= 0.972 af, Depth= 3.15"

Routed to Pond 352P: Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 5-yr, 24-hr storm Rainfall=3.38"

_	Area	(ac)	CN	Desc	cription			
*	3.	706	98	Lead	hate Surfa	ace Water F	Pond	
	3.706 100.00% Impervious Area							
	Тс	Leng	th :	Slope	Velocity	Capacity	Description	
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)		
	0.0						Direct Entry	

#### Summary for Pond 349P: Leachate/Surface Water Pond

Inflow Area = 10.671 ac,100.00% Impervious, Inflow Depth = 3.15" for 5-yr, 24-hr storm event

Inflow = 24.41 cfs @ 12.27 hrs, Volume= 2.798 af

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs Starting Elev= 794.76' Surf.Area= 47,114 sf Storage= 75,708 cf

Peak Elev= 796.97' @ 25.15 hrs Surf.Area= 61,584 sf Storage= 197,605 cf (121,897 cf above start)

Flood Elev= 796.97' Surf.Area= 61,588 sf Storage= 197,647 cf (121,939 cf above start)

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Volume	Invert	Avail.Storage	Storage Description
#1	792.00'	405,390 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

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Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
792.00	1,051	0	0
794.00	41,126	42,177	42,177
796.00	56,885	98,011	140,188
798.00	66,581	123,466	263,654
800.00	75,155	141,736	405,390

#### Summary for Pond 350P: Leachate/Surface Water Pond

Inflow Area = 10.615 ac,100.00% Impervious, Inflow Depth = 3.15" for 5-yr, 24-hr storm event

Inflow = 24.26 cfs @ 12.27 hrs, Volume= 2.784 af

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs

Starting Elev= 794.78' Surf.Area= 47,272 sf Storage= 76,652 cf

Peak Elev= 796.97' @ 25.15 hrs Surf.Area= 61,608 sf Storage= 197,910 cf (121,257 cf above start)

Flood Elev= 796.97' Surf.Area= 61,588 sf Storage= 197,647 cf (120,995 cf above start)

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert	Avail.S	torage	Storage	Description			
#1	792.00'	92.00' 405,390 cf		Custon	Custom Stage Data (Prismatic)Listed below (Recalc)			
Elevation (feet)		.Area sq-ft)		.Store c-feet)	Cum.Store (cubic-feet)			
792.00	,	1,051	•	0	0			
794.00	4	1,126	4	2,177	42,177			
796.00	56	3,885	ç	8,011	140,188			
798.00	66	3,581	12	23,466	263,654			
800.00	7	5,155	14	1,736	405,390			

#### Summary for Pond 351P: Leachate/Surface Water Pond

Inflow Area = 11.423 ac,100.00% Impervious, Inflow Depth = 3.15" for 5-yr, 24-hr storm event

Inflow = 26.51 cfs @ 12.27 hrs, Volume= 2.995 af

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs

Starting Elev= 794.58' Surf.Area= 45,696 sf Storage= 67,355 cf

Peak Elev= 796.97' @ 25.15 hrs Surf.Area= 61,602 sf Storage= 197,834 cf (130,479 cf above start)

Flood Elev= 796.97' Surf.Area= 61,588 sf Storage= 197,647 cf (130,292 cf above start)

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

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Volume	Invert	Avail.S	Storage	Storage	e Description		
#1	792.00'	405	,390 cf	Custon	Custom Stage Data (Prismatic)Listed below (Recalc)		
Elevation (feet)		f.Area (sq-ft)		:Store c-feet)	Cum.Store (cubic-feet)		
792.00		1,051		0	0		
794.00	4	1,126	4	12,177	42,177		
796.00	5	6,885	ę	98,011	140,188		
798.00	6	6,581	12	23,466	263,654		
800.00	7	5,155	14	11,736	405,390		

#### Summary for Pond 352P: Leachate/Surface Water Pond

Inflow Area = 11.161 ac,100.00% Impervious, Inflow Depth = 3.15" for 5-yr, 24-hr storm event

Inflow = 27.07 cfs @ 12.05 hrs, Volume= 2.927 af

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs

Starting Elev= 794.64' Surf.Area= 46,169 sf Storage= 70,111 cf

Peak Elev= 796.97' @ 25.15 hrs Surf.Area= 61,584 sf Storage= 197,602 cf (127,491 cf above start)

Flood Elev= 796.97' Surf.Area= 61,588 sf Storage= 197,647 cf (127,536 cf above start)

Avail Storage Storage Description

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no outflow)

Invert

Volume

VOIGITIC	IIIVCIL	Avaii.Otorage		Otorage	Description	
#1	792.00' 40		5,390 cf	Custon	n Stage Data (Pr	ismatic)Listed below (Recalc)
Elevation (feet)		.Area sq-ft)	Inc. (cubic	Store -feet)	Cum.Store (cubic-feet)	
792.00	•	1,051		0	0	
794.00	41	1,126	4:	2,177	42,177	
796.00	56	5,885	9	8,011	140,188	
798.00	66	5,581	12	3,466	263,654	
800.00	75	5,155	14	1,736	405,390	

#### Summary for Pond 353P: Leachate/Surface Water Pond

Inflow Area = 11.489 ac,100.00% Impervious, Inflow Depth = 3.15" for 5-yr, 24-hr storm event

Inflow = 27.48 cfs @ 12.06 hrs, Volume= 3.013 af

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs

Starting Elev= 794.56' Surf.Area= 45,539 sf Storage= 66,443 cf

Peak Elev= 796.97' @ 25.15 hrs Surf.Area= 61,591 sf Storage= 197,686 cf (131,243 cf above start)

Flood Elev= 796.97' Surf.Area= 61,588 sf Storage= 197,647 cf (131,204 cf above start)

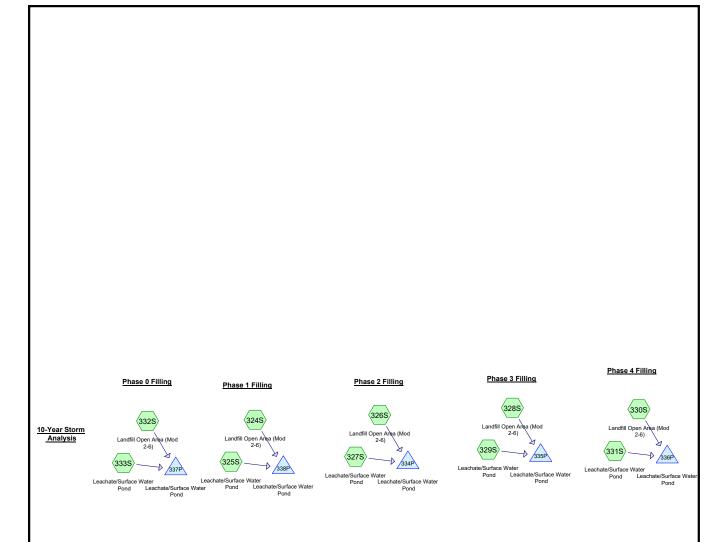
Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

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# WPL Columbia\_Leachate Pond Evaluation\_22MSE 24-hr 4 5-yr, 24-hr storm Rainfall=3.38" Prepared by SCS Engineers HydroCAD® 10.10-7a s/n 05804 © 2021 HydroCAD Software Solutions LLC Page 9

Volume	Invert	Avail.Storage	Storage Description
#1	792.00'	405,390 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

Elevation (feet)	Surf.Area (sg-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
792.00	1,051	Ó	0
794.00	41,126	42,177	42,177
796.00	56,885	98,011	140,188
798.00	66,581	123,466	263,654
800.00	75,155	141,736	405,390











Outflow=0.00 cfs 0.000 af

Time span=0.00-33.00 hrs, dt=0.05 hrs, 661 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method
Subcatchment 324S: Landfill Open Area Runoff Area=339,047 sf 100.00% Impervious Runoff Depth=3.74" Tc=20.0 min CN=98 Runoff=25.60 cfs 2.423 af
Subcatchment 325S: Leachate/Surface Runoff Area=3.706 ac 100.00% Impervious Runoff Depth=3.74" Tc=0.0 min CN=98 Runoff=21.25 cfs 1.154 af
Subcatchment 326S: Landfill Open Area Runoff Area=335,031 sf 100.00% Impervious Runoff Depth=3.74" Tc=20.0 min CN=98 Runoff=25.30 cfs 2.394 af
Subcatchment 327S: Leachate/Surface Runoff Area=2.980 ac 100.00% Impervious Runoff Depth=3.74" Tc=0.0 min CN=98 Runoff=17.09 cfs 0.928 af
Subcatchment 328S: Landfill Open Area Runoff Area=332,594 sf 100.00% Impervious Runoff Depth=3.74" Tc=20.0 min CN=98 Runoff=25.12 cfs 2.377 af
Subcatchment 329S: Leachate/Surface Runoff Area=2.980 ac 100.00% Impervious Runoff Depth=3.74" Tc=0.0 min CN=98 Runoff=17.09 cfs 0.928 af
Subcatchment 330S: Landfill Open Area Runoff Area=367,758 sf 100.00% Impervious Runoff Depth=3.74" Tc=20.0 min CN=98 Runoff=27.77 cfs 2.628 af
Subcatchment 331S: Leachate/Surface Runoff Area=2.980 ac 100.00% Impervious Runoff Depth=3.74" Tc=0.0 min CN=98 Runoff=17.09 cfs 0.928 af
Subcatchment 332S: Landfill Open Area Runoff Area=324,737 sf 100.00% Impervious Runoff Depth=3.74" Tc=20.0 min CN=98 Runoff=24.52 cfs 2.320 af
Subcatchment 333S: Leachate/Surface Runoff Area=3.706 ac 100.00% Impervious Runoff Depth=3.74" Tc=0.0 min CN=98 Runoff=21.25 cfs 1.154 af
Pond 334P: Leachate/Surface Water Pond Peak Elev=796.97' Storage=197,822 cf
Pond 335P: Leachate/Surface Water Pond Peak Elev=796.97' Storage=197,929 cf
Pond 336P: Leachate/Surface Water Pond Peak Elev=796.97' Storage=197,874 cf
Pond 337P: Leachate/SurfaceWater Pond Peak Elev=796.97' Storage=197,655 cf Outflow=31.91 cfs 3.474 af Outflow=0.00 cfs 0.000 af
Pond 338P: Leachate/SurfaceWater Pond Peak Elev=796.97' Storage=197,547 cf Inflow=32.39 cfs 3.576 af

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#### Summary for Subcatchment 324S: Landfill Open Area (Mod 2-6)

2.423 af. Depth= 3.74" Runoff 25.60 cfs @ 12.29 hrs, Volume=

Routed to Pond 338P: Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 10-yr, 24-hr storm Rainfall=3.97"

	Α	rea (sf)	CN [	Description						
*	3	39,047	98 <b>N</b>	Mod 2 - 6 Open Area						
	339,047 100.00% Impervious Are					rea				
	Тс	Length	Slope	,	Capacity	Description				
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	20.0					Direct Entry, Estimated				

#### Summary for Subcatchment 325S: Leachate/Surface Water Pond

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

21.25 cfs @ 12.04 hrs, Volume= 1.154 af, Depth= 3.74"

Routed to Pond 338P: Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 10-yr, 24-hr storm Rainfall=3.97"

	Area	(ac)	CN	Desc	cription							
*	3.	706	98	Lead	eachate Surface Water Pond							
3.706 100.00% Impervious Area							a					
	Тс	Leng	th		,		Description					
	(min)	(fee	t)	(ft/ft)	(ft/sec)	(cfs)						
	0.0						Direct Entry,					

#### **Summary for Subcatchment 326S: Landfill Open Area (Mod 2-6)**

25.30 cfs @ 12.29 hrs, Volume= 2.394 af, Depth= 3.74" Runoff Routed to Pond 334P: Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 10-yr, 24-hr storm Rainfall=3.97"

	Area (sf)	CN	Description
*	335,031	98	Mod 2 - 6 Open Area
	335,031		100.00% Impervious Area

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	Тс	Length	Slope	Velocity	Capacity	Description
(m	nin)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
2	0.0					Direct Entry, Estimated

#### Summary for Subcatchment 327S: Leachate/Surface Water Pond

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff = 17.09 cfs @ 12.04 hrs, Volume= 0.928 af, Depth= 3.74" Routed to Pond 334P : Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 10-yr, 24-hr storm Rainfall=3.97"

	Area	(ac)	CN	Desc	cription				
*	2.	2.980 98 Leachate Surface Water Pond							
	Tc (min)	Leng		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
_	0.0	(iee	:()	(11/11)	(II/Sec)	(CIS)	Direct Entry,		

#### **Summary for Subcatchment 328S: Landfill Open Area (Mod 2-6)**

Runoff = 25.12 cfs @ 12.29 hrs, Volume= 2.377 af, Depth= 3.74"

Routed to Pond 335P : Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 10-yr, 24-hr storm Rainfall=3.97"

	Α	rea (sf)	CN [	Description						
*	3	32,594	98 I	Mod 2 - 6 Open Area						
	3	32,594	,	100.00% Im	npervious A	rea				
	Tc	Length	Slope	Velocity	Capacity	Description				
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	20.0					Direct Entry, Estimated				

#### Summary for Subcatchment 329S: Leachate/Surface Water Pond

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff = 17.09 cfs @ 12.04 hrs, Volume= 0.928 af, Depth= 3.74" Routed to Pond 335P : Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 10-yr, 24-hr storm Rainfall=3.97"

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	Area	(ac)	CN	Desc	cription						
*	2.	980	98	Lead	_eachate Surface Water Pond						
	2.980 100.00% Impervious Area										
	Tc Lengt			Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
	0.0	•	•	•	•	, ,	Direct Entry,				

#### **Summary for Subcatchment 330S: Landfill Open Area (Mod 2-6)**

27.77 cfs @ 12.29 hrs, Volume= 2.628 af, Depth= 3.74" Routed to Pond 336P: Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 10-yr, 24-hr storm Rainfall=3.97"

_	Α	rea (sf)	CN I	Description					
*	3	67,758	98 I	Mod 2 - 11 Open Area					
	367,758 100.00% Impervious					rea			
	Tc	Length	Slope	,	Capacity	Description			
-	(min) 20.0	(feet)	(ft/ft)	(ft/sec)	(cfs)	Direct Entry, Estimated			

#### Summary for Subcatchment 331S: Leachate/Surface Water Pond

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

17.09 cfs @ 12.04 hrs, Volume= 0.928 af, Depth= 3.74" Runoff Routed to Pond 336P: Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 10-yr, 24-hr storm Rainfall=3.97"

Area (ac) CN Description									
*	2.	.980	98 Leachate Surface Water Pond						
	2.	.980		100.	00% Impei	rvious Area	1		
	Тс	Lengt	h S	Slope	Velocity	Capacity	Description		
_	(min)	(fee	t)	(ft/ft)	(ft/sec)	(cfs)			
	0.0						Direct Entry,		

#### Summary for Subcatchment 332S: Landfill Open Area (Mod 2-6)

Runoff 24.52 cfs @ 12.29 hrs, Volume= 2.320 af, Depth= 3.74"

Routed to Pond 337P: Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 10-yr, 24-hr storm Rainfall=3.97"

WPL Columbia\_Leachate Pond Evaluation\_2MSE 24-hr 4 10-yr, 24-hr storm Rainfall=3.97"
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_	Α	rea (sf)	CN [	Description						
*	3	24,737	98 N	Mod 2 - 6 Open Area						
	3	24,737	1	00.00% Im	pervious A	rea				
	Тс	Length	Slope	Velocity	Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	20.0					Direct Entry, Estimated				

#### Summary for Subcatchment 333S: Leachate/Surface Water Pond

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff = 21.25 cfs @ 12.04 hrs, Volume= 1.154 af, Depth= 3.74"

Routed to Pond 337P: Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 10-yr, 24-hr storm Rainfall=3.97"

	Area	(ac)	CN	Desc	cription						
*	3.	706	98	Leac	eachate Surface Water Pond						
	3.	a									
		Lengt	h S	Slope	,		Description				
	(min)	(fee	t)	(ft/ft)	(ft/sec)	(cfs)					
	0.0						Direct Entry,				

#### Summary for Pond 334P: Leachate/Surface Water Pond

Inflow Area = 10.671 ac,100.00% Impervious, Inflow Depth = 3.74" for 10-yr, 24-hr storm event

Inflow = 28.77 cfs @ 12.27 hrs, Volume= 3.322 af

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs

Starting Elev= 794.26' Surf.Area= 43,175 sf Storage= 53,136 cf

Peak Elev= 796.97' @ 25.15 hrs Surf.Area= 61,601 sf Storage= 197,822 cf (144,686 cf above start)

Flood Elev= 796.97' Surf.Area= 61,588 sf Storage= 197,647 cf (144,511 cf above start)

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Volume	Invert	Avail.Storage	Storage Description
#1	792.00'	405.390 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

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Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
792.00	1,051	0	0
794.00	41,126	42,177	42,177
796.00	56,885	98,011	140,188
798.00	66,581	123,466	263,654
800.00	75,155	141,736	405,390

#### Summary for Pond 335P: Leachate/Surface Water Pond

Inflow Area = 10.615 ac,100.00% Impervious, Inflow Depth = 3.74" for 10-yr, 24-hr storm event

Inflow = 28.58 cfs @ 12.27 hrs, Volume= 3.304 af

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs

Starting Elev= 794.28' Surf.Area= 43,332 sf Storage= 54,001 cf

Peak Elev= 796.97' @ 25.15 hrs Surf.Area= 61,610 sf Storage= 197,929 cf (143,927 cf above start)

Flood Elev= 796.97' Surf.Area= 61,588 sf Storage= 197,647 cf (143,646 cf above start)

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert Avail.Storage		Storage	Description		
#1	792.00'	405,	405,390 cf		n Stage Data (Pr	ismatic)Listed below (Recalc)
Elevation (feet)		.Area (sq-ft)		:.Store c-feet)	Cum.Store (cubic-feet)	
792.00		1,051	•	0	0	
794.00	4	1,126	4	12,177	42,177	
796.00	5	6,885	Ś	98,011	140,188	
798.00	6	6,581	12	23,466	263,654	
800.00	7	75, <sup>1</sup> 55 14		11,736	405,390	

#### Summary for Pond 336P: Leachate/Surface Water Pond

Inflow Area = 11.423 ac,100.00% Impervious, Inflow Depth = 3.74" for 10-yr, 24-hr storm event

Inflow = 31.24 cfs @ 12.27 hrs, Volume= 3.555 af

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs

Starting Elev= 794.02' Surf.Area= 41,284 sf Storage= 43,001 cf

Peak Elev= 796.97' @ 25.15 hrs Surf.Area= 61,605 sf Storage= 197,874 cf (154,873 cf above start)

Flood Elev= 796.97' Surf.Area= 61,588 sf Storage= 197,647 cf (154,646 cf above start)

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

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Volume	Invert			Storage	e Description	
#1	792.00'			Custon	$\textbf{Custom Stage Data (Prismatic)} Listed \ below \ (Recalc)$	
Elevation (feet)		f.Area (sq-ft)		:.Store c-feet)	Cum.Store (cubic-feet)	
792.00		1,051		0	0	
794.00		1,126	4	12,177	42,177	
796.00	5	6,885		98,011	140,188	
798.00	6	6,581	12	23,466	263,654	
800.00	7	5,155	14	11,736	405,390	

#### Summary for Pond 337P: Leachate/Surface Water Pond

Inflow Area = 11.161 ac,100.00% Impervious, Inflow Depth = 3.74" for 10-yr, 24-hr storm event

Inflow = 31.91 cfs @ 12.05 hrs, Volume= 3.474 af

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs

Starting Elev= 794.10' Surf.Area= 41,914 sf Storage= 46,329 cf

Peak Elev= 796.97' @ 25.15 hrs Surf.Area= 61,588 sf Storage= 197,655 cf (151,326 cf above start)

Flood Elev= 796.97' Surf.Area= 61,588 sf Storage= 197,647 cf (151,318 cf above start)

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert	Avail.Storage		Storage	e Description	
#1	792.00'	405,3	405,390 cf		n Stage Data (Pr	rismatic)Listed below (Recalc)
Elevation (feet)		.Area (sq-ft)		.Store c-feet)	Cum.Store (cubic-feet)	
792.00	•	1,051		Ó	0	
794.00	4	1,126	4	2,177	42,177	
796.00	56	56,885		8,011	140,188	
798.00	66,581 12		3,466	263,654		
800.00	75,155 14		1,736	405,390		

#### Summary for Pond 338P: Leachate/Surface Water Pond

Inflow Area = 11.489 ac,100.00% Impervious, Inflow Depth = 3.74" for 10-yr, 24-hr storm event

Inflow = 32.39 cfs @ 12.06 hrs, Volume= 3.576 af

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs

Starting Elev= 793.99' Surf.Area= 40,926 sf Storage= 41,767 cf

Peak Elev= 796.97' @ 25.15 hrs Surf.Area= 61,580 sf Storage= 197,547 cf (155,781 cf above start)

Flood Elev= 796.97' Surf.Area= 61,588 sf Storage= 197,647 cf (155,880 cf above start)

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

**COL POO Filling** 

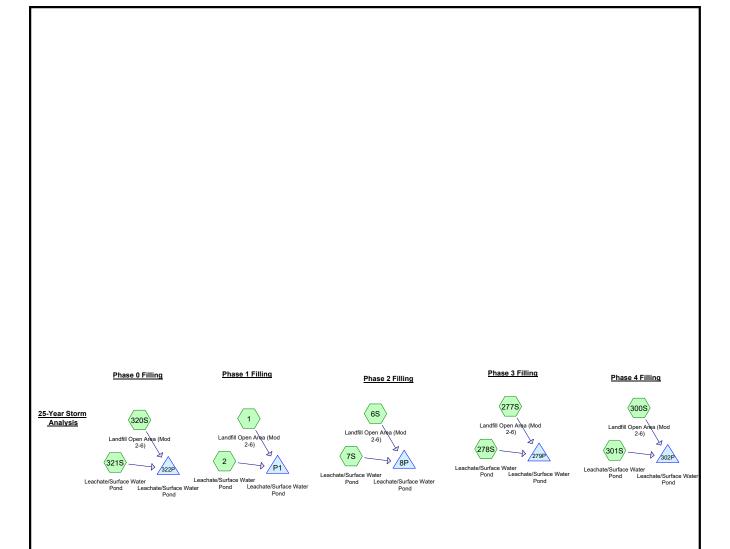
## WPL Columbia\_Leachate Pond Evaluation\_2MSE 24-hr 4 10-yr, 24-hr storm Rainfall=3.97"

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Volume	Invert	Avail.Storag	ge Storage	e Description	
#1	792.00'	405,390	cf Custor	n Stage Data (Pı	rismatic)Listed below (Recalc)
Elevation		.Area	Inc.Store	Cum.Store	
(feet)	(	sq-ft) (c	ubic-feet)	(cubic-feet)	
792.00		1,051	0	0	
794.00	4	1,126	42,177	42,177	
796.00	56	6,885	98,011	140,188	
798.00	66	3,581	123,466	263,654	
800.00	,		141,736	405,390	











Outflow=0.00 cfs 0.000 af

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Time span=0.00-33.00 hrs, dt=0.05 hrs, 661 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Runoff Area=339,047 sf 100.00% Impervious Runoff Depth=4.67" Subcatchment 1: Landfill Open Area Tc=20.0 min CN=98 Runoff=31.77 cfs 3.031 af Subcatchment2: Leachate/SurfaceWater Runoff Area=3.706 ac 100.00% Impervious Runoff Depth=4.67" Tc=0.0 min CN=98 Runoff=26.35 cfs 1.443 af Runoff Area=335,031 sf 100.00% Impervious Runoff Depth=4.67" Subcatchment 6S: Landfill Open Area Tc=20.0 min CN=98 Runoff=31.39 cfs 2.995 af Subcatchment 7S: Leachate/Surface Runoff Area=2.980 ac 100.00% Impervious Runoff Depth=4.67" Tc=0.0 min CN=98 Runoff=21.19 cfs 1.161 af Subcatchment 277S: Landfill Open Area Runoff Area = 332,594 sf 100.00% Impervious Runoff Depth = 4.67" Tc=20.0 min CN=98 Runoff=31.16 cfs 2.974 af Subcatchment 278S: Leachate/Surface Runoff Area=2.980 ac 100.00% Impervious Runoff Depth=4.67" Tc=0.0 min CN=98 Runoff=21.19 cfs 1.161 af Subcatchment 300S: Landfill Open Area Runoff Area=367,758 sf 100.00% Impervious Runoff Depth=4.67" Tc=20.0 min CN=98 Runoff=34.46 cfs 3.288 af Runoff Area=2.980 ac 100.00% Impervious Runoff Depth=4.67" Subcatchment 301S: Leachate/Surface Tc=0.0 min CN=98 Runoff=21.19 cfs 1.161 af Subcatchment 320S: Landfill Open Area Runoff Area=324,737 sf 100.00% Impervious Runoff Depth=4.67" Tc=20.0 min CN=98 Runoff=30.43 cfs 2.903 af Subcatchment 321S: Leachate/Surface Runoff Area=3.706 ac 100.00% Impervious Runoff Depth=4.67" Tc=0.0 min CN=98 Runoff=26.35 cfs 1.443 af Peak Elev=796.97' Storage=197,735 cf Inflow=35.69 cfs 4.156 af Pond 8P: Leachate/SurfaceWater Pond Outflow=0.00 cfs 0.000 af Pond 279P: Leachate/Surface Water Pond Peak Elev=796.97' Storage=197,837 cf Inflow=35.46 cfs 4.134 af Outflow=0.00 cfs 0.000 af Pond 302P: Leachate/Surface Water Pond Peak Elev=796.97' Storage=197,879 cf Inflow=38.75 cfs 4.448 af Outflow=0.00 cfs 0.000 af Pond 322P: Leachate/SurfaceWater Pond Peak Elev=796.97' Storage=197,831 cf Inflow=39.61 cfs 4.347 af Outflow=0.00 cfs 0.000 af Pond P1: Leachate/SurfaceWater Pond Peak Elev=796.97' Storage=197,936 cf Inflow=40.21 cfs 4.474 af

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#### Summary for Subcatchment 1: Landfill Open Area (Mod 2-6)

Runoff 31.77 cfs @ 12.28 hrs, Volume= Routed to Pond P1: Leachate/Surface Water Pond

3.031 af, Depth= 4.67"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 25-yr, 24-hr storm Rainfall=4.91"

	Α	rea (sf)	CN [	Description						
*	3	39,047	98 <b>N</b>	Mod 2 - 6 Open Area						
	3	39,047	_	00.00% Im	npervious A	rea				
	Тс	Length	Slope	,	Capacity	Description				
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	20.0					Direct Entry, Estimated				

#### Summary for Subcatchment 2: Leachate/Surface Water Pond

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

26.35 cfs @ 12.04 hrs, Volume=

1.443 af, Depth= 4.67"

Routed to Pond P1: Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 25-yr, 24-hr storm Rainfall=4.91"

	Area	(ac)	CN	Desc	cription							
*	3.	706	98	Lead	eachate Surface Water Pond							
	3.706 100.00% Impervious Area											
	Тс	Leng	th		,		Description					
	(min)	(fee	t)	(ft/ft)	(ft/sec)	(cfs)						
	0.0						Direct Entry,					

#### **Summary for Subcatchment 6S: Landfill Open Area (Mod 2-6)**

31.39 cfs @ 12.28 hrs, Volume= 2.995 af, Depth= 4.67" Runoff Routed to Pond 8P: Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 25-yr, 24-hr storm Rainfall=4.91"

	Area (sf)	CN	Description
*	335,031	98	Mod 2 - 6 Open Area
	335,031 100.00% Imper		100.00% Impervious Area

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Tc	•		,		Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
20.0					Direct Entry, Estimated

#### Summary for Subcatchment 7S: Leachate/Surface Water Pond

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

21.19 cfs @ 12.04 hrs, Volume= Routed to Pond 8P: Leachate/Surface Water Pond 1.161 af, Depth= 4.67"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 25-yr, 24-hr storm Rainfall=4.91"

	Area	(ac)	CN	Desc	cription				
*	2.	2.980 98 Leachate Surface Water Pond							
2.980 100.00% Impervious Area									
	Tc (min)	Leng		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
_	0.0	(iee	:()	(11/11)	(II/Sec)	(CIS)	Direct Entry,		

#### **Summary for Subcatchment 277S: Landfill Open Area (Mod 2-6)**

Runoff 31.16 cfs @ 12.28 hrs, Volume= Routed to Pond 279P: Leachate/Surface Water Pond

2.974 af, Depth= 4.67"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 25-yr, 24-hr storm Rainfall=4.91"

_	Α	rea (sf)	CN I	Description							
7	• 3	32,594	98 1	Mod 2 - 6 Open Area							
	3	32,594	•	100.00% Im	pervious A	rea					
	Tc (min)	3	Slope (ft/ft)	,	Capacity (cfs)	Description					
-	20.0	(feet)	(11/11)	(IUSEC)	(CIS)	Direct Entry, Estimated					

Direct Entry, Estimated

#### Summary for Subcatchment 278S: Leachate/Surface Water Pond

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

1.161 af, Depth= 4.67" 21.19 cfs @ 12.04 hrs, Volume= Routed to Pond 279P: Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 25-yr, 24-hr storm Rainfall=4.91"

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	Area	(ac)	CN	Desc	cription							
*	2.	980	98	Lead	eachate Surface Water Pond							
	2.980 100.00% Impervious Area						a					
	Tc (min)	Lengt (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description					
	0.0	(	-,	(1211)	(1220)	(3.5)	Direct Entry,					

#### **Summary for Subcatchment 300S: Landfill Open Area (Mod 2-6)**

Runoff = 34.46 cfs @ 12.28 hrs, Volume= 3.288 af, Depth= 4.67" Routed to Pond 302P : Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 25-yr, 24-hr storm Rainfall=4.91"

	Α	rea (sf)	CN [	Description							
*	3	67,758	98 <b>N</b>	Mod 2 - 11 Open Area							
	3	67,758	1	100.00% Im	npervious A	rea					
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description					
_	20.0	(leet)	(11/11)	(II/Sec)	(CIS)	Direct Entry, Estimated					

#### Summary for Subcatchment 301S: Leachate/Surface Water Pond

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff = 21.19 cfs @ 12.04 hrs, Volume= 1.161 af, Depth= 4.67" Routed to Pond 302P : Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 25-yr, 24-hr storm Rainfall=4.91"

	Area	(ac)	CN	Desc	cription							
*	2.	980	98	Lead	Leachate Surface Water Pond							
	2.980 100.00% Impervious Area											
	Тс	Leng	th	Slope	Velocity	Capacity	Description					
_	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)						
	0.0						Direct Entry,					

#### **Summary for Subcatchment 320S: Landfill Open Area (Mod 2-6)**

Runoff = 30.43 cfs @ 12.28 hrs, Volume= 2.903 af, Depth= 4.67" Routed to Pond 322P : Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 25-yr, 24-hr storm Rainfall=4.91"

WPL Columbia Leachate Pond Evaluation 2MSE 24-hr 4 25-yr, 24-hr storm Rainfall=4.91" Prepared by SCS Engineers Printed 5/25/2022

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	Α	rea (sf)	CN [	Description							
*	3	24,737	98 <b>N</b>	Mod 2 - 6 Open Area							
	324,737 100.00% Impervious Are				npervious A	rea					
	Тс	Length	Slope	Velocity	Capacity	Description					
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
	20.0					Direct Entry, Estimated					

#### Summary for Subcatchment 321S: Leachate/Surface Water Pond

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff 26.35 cfs @ 12.04 hrs, Volume= 1.443 af, Depth= 4.67" Routed to Pond 322P: Leachate/Surface Water Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs MSE 24-hr 4 25-yr, 24-hr storm Rainfall=4.91"

	Area	(ac)	CN	Desc	cription								
*	3.	706	98	Leac	eachate Surface Water Pond								
	3.706 100.00% Impervious Area						a						
		Lengt	h S	Slope	,	, ,	Description						
	(min)	(fee	t)	(ft/ft)	(ft/sec)	(cfs)							
	0.0						Direct Entry,						

#### Summary for Pond 8P: Leachate/Surface Water Pond

10.671 ac,100.00% Impervious, Inflow Depth = 4.67" for 25-yr, 24-hr storm event Inflow Area =

35.69 cfs @ 12.27 hrs, Volume= Inflow 4.156 af

Outflow 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs

Starting Elev= 793.24' Surf.Area= 25,898 sf Storage= 16,708 cf

Peak Elev= 796.97' @ 25.15 hrs Surf.Area= 61,594 sf Storage= 197,735 cf (181,027 cf above start)

Flood Elev= 796.97' Surf.Area= 61,588 sf Storage= 197,647 cf (180,939 cf above start)

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Volume	Invert	Avail.Storage	Storage Description
#1	792.00'	405,390 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

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Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
792.00	1,051	0	0
794.00	41,126	42,177	42,177
796.00	56,885	98,011	140,188
798.00	66,581	123,466	263,654
800.00	75,155	141,736	405,390

#### Summary for Pond 279P: Leachate/Surface Water Pond

Inflow Area = 10.615 ac,100.00% Impervious, Inflow Depth = 4.67" for 25-yr, 24-hr storm event

35.46 cfs @ 12.27 hrs, Volume= 4.134 af Inflow =

0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min Outflow

Routing by Stor-Ind method, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs

Starting Elev= 793.28' Surf.Area= 26,699 sf Storage= 17,760 cf

Peak Elev= 796.97' @ 25.15 hrs Surf.Area= 61,603 sf Storage= 197,837 cf (180,077 cf above start)

Flood Elev= 796.97' Surf.Area= 61,588 sf Storage= 197,647 cf (179,887 cf above start)

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert	Avail.Stora	age Stora	age Description	
#1	792.00'	00' 405,390 cf		tom Stage Data (P	rismatic)Listed below (Recalc)
Elevation (feet)		.Area sq-ft) (	Inc.Store		
792.00		1,051	0	0	
794.00	4	1,126	42,177	42,177	
796.00	50	6,885	98,011	140,188	
798.00	60	6,581	123,466	263,654	
800.00	7:	5,155	141,736	405,390	

#### Summary for Pond 302P: Leachate/Surface Water Pond

Inflow Area = 11.423 ac,100.00% Impervious, Inflow Depth = 4.67" for 25-yr, 24-hr storm event

Inflow 38.75 cfs @ 12.27 hrs, Volume= 4.448 af

Outflow 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs

Starting Elev= 792.59' Surf.Area= 12,873 sf Storage= 4,108 cf

Peak Elev= 796.97' @ 25.15 hrs Surf.Area= 61,606 sf Storage= 197,879 cf (193,772 cf above start)

Flood Elev= 796.97' Surf.Area= 61,588 sf Storage= 197,647 cf (193,540 cf above start)

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

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Volume	Invert	Avail.S	Storage	Storage	e Description	
#1	792.00'	792.00' 405,390 cf		Custor	n Stage Data (Pr	rismatic)Listed below (Recalc)
Elevation (feet)	Sur	f.Area (sq-ft)		:Store c-feet)	Cum.Store (cubic-feet)	
792.00		1,051		0	0	
794.00	4	1,126	4	12,177	42,177	
796.00	5	6,885	Ś	98,011	140,188	
798.00	6	6,581	12	23,466	263,654	
800.00	7	5,155	14	11,736	405,390	

#### Summary for Pond 322P: Leachate/Surface Water Pond

11.161 ac,100.00% Impervious, Inflow Depth = 4.67" for 25-yr, 24-hr storm event Inflow Area =

Inflow 39.61 cfs @ 12.05 hrs, Volume= 4.347 af

0.00 cfs @ 0.00 hrs, Volume= Outflow 0.000 af, Atten= 100%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs

Starting Elev= 792.87' Surf.Area= 18,484 sf Storage= 8,498 cf

Peak Elev= 796.97' @ 25.15 hrs Surf.Area= 61,602 sf Storage= 197,831 cf (189,333 cf above start)

Flood Elev= 796.97' Surf.Area= 61,588 sf Storage= 197,647 cf (189,150 cf above start)

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert	Avail.Stora	age S	Storage	Description	
#1	792.00'	792.00' 405,390 cf		Custom	Stage Data (Pr	ismatic)Listed below (Recalc)
Elevation		.Area		Store	Cum.Store	
(feet)	(	sq-ft)	cubic-	teet)	(cubic-feet)	
792.00	•	1,051		0	0	
794.00	4	1,126	42	2,177	42,177	
796.00	56,885		98	3,011	140,188	
798.00	60	6,581	123	3,466	263,654	
800.00	7	5,155	141	,736	405,390	

#### Summary for Pond P1: Leachate/Surface Water Pond

Inflow Area = 11.489 ac,100.00% Impervious, Inflow Depth = 4.67" for 25-yr, 24-hr storm event

Inflow 40.21 cfs @ 12.06 hrs, Volume= 4.474 af

0.00 cfs @ 0.00 hrs, Volume= Outflow 0.000 af, Atten= 100%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-33.00 hrs, dt= 0.05 hrs

Starting Elev= 792.50' Surf.Area= 11,070 sf Storage= 3,030 cf

Peak Elev= 796.97' @ 25.15 hrs Surf.Area= 61,610 sf Storage= 197,936 cf (194,906 cf above start)

Flood Elev= 796.97' Surf.Area= 61,588 sf Storage= 197,647 cf (194,617 cf above start)

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

**COL POO Filling** 

## WPL Columbia\_Leachate Pond Evaluation\_2MSE 24-hr 4 25-yr, 24-hr storm Rainfall=4.91"

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Volume	Invert	Avail.Stora	ge Storage	e Description	
#1	792.00'	405,390	cf Custor	n Stage Data (Pı	rismatic)Listed below (Recalc)
Elevation (feet)		f.Area (sq-ft) (c	Inc.Store	Cum.Store (cubic-feet)	
792.00		1,051	Ó	0	
794.00	4	1,126	42,177	42,177	
796.00	5	6,885	98,011	140,188	
798.00	6	6,581	123,466	263,654	
800.00	7	5,155	141,736	405,390	

# Appendix A3

# 2022 Module 10 and Module 11 Design and South Sediment Basin Check

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CALC. NO.			
REV. NO.			
BY	RJG	DATE 4/7/22	
CHK'D.	MRH	DATE 4/8/22	

Job No.	25220183.00	Job	Columbia Dry Ash Disposal
Client	WPL	Subject	Storm Water Management

# **Storm Water Management Calculations**

#### Purpose:

The purpose of the storm water runoff calculations is to demonstrate that the existing storm water sedimentation basin and proposed storm water management features included in the Modules 10 and 11 Plan Modification Request can accommodate and safely convey the runoff from a 25-year, 24-hour storm event during post closure conditions.

Items addressed in these calculations:

- Sedimentation Basin
- Swales
- Culverts
- Diversion Berms
- Downslope Flumes & Energy Dissipaters
- Rock Chutes
- Discharge Aprons

The proposed storm water management conditions are shown on Figure 1.

The calculations support the capacity check of the following existing storm water management feature:

Feature	Purpose	Design Method
Sedimentation Basin	To safely handle 25-year, 24-hour storm event without overtopping the 100-year, 24-hour emergency spillway.	HydroCAD runoff modeling
Swales	Convey storm water runoff from adjacent areas to Culvert C2 and offsite during post construction conditions	HydroCAD runoff modeling and Swale Calculation
Culverts	Convey storm water from the final cover perimeter swales during post construction conditions	HydroCAD runoff modeling and HY-8 Culvert Model
Diversion Berms	Reduce storm water runoff from long final cover slopes and to divert water to perimeter swales during post construction conditions	HydroCAD runoff modeling and Diversion Berm Calculations
Downslope Flumes & Energy Dissipators	Convey storm water from diversion berms down slope to discharge locations during post construction conditions	HydroCAD runoff modeling and Downslope Flume Calculations
Rock Chutes	Erosion protection and convey storm water from energy dissipators (Flume 1 and Flume 2) to existing swale during post construction conditions	HydroCAD runoff modeling and Rock Chute Calculation
Discharge Aprons	Erosion protection from culvert discharge at culverts	HydroCAD runoff modeling and Riprap Apron Calculation

#### Approach:

Hydrograph Generation

HydroCAD was used to model the storm water management system and develop the hydrographs

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Client WPL Subject Storm Water Management

using TR-20 methodologies. The model is designed to simulate the surface runoff response of a watershed to a precipitation event. Input parameters for the model include precipitation depth for the design storm events from NOAA ATLAS 14, contributing drainage areas, runoff curve numbers, and time of concentration.

#### Swale Sizing

The proposed swales were sized for the 25-year, 24-hour storm event. A spreadsheet based on Manning's equation was used to determine the depth of flow and velocity in the swales based on the swale geometry and peak flow in the swales (as determined by the Hydrograph Generation models).

#### Culvert Sizing

Culverts were sized for the 25-year, 24-hour storm event using the HY-8 computer model developed by the US Department of Transportation, Federal Highway Administration.

#### **Diversion Berms**

Diversion berms were sized for the 25-year, 24-hour storm event using the Manning's Equation to determine the depth of flow and velocity in the swale based on the swale geometry and peak flow for the storm event (as determined by the Hydrograph Generation Calculations).

#### Downslope Flumes and Energy Dissipaters Sizing

Flumes and energy dissipaters were sized for the 25-year, 24-hour storm event. Manning's equation and the orifice equation were used to size the flumes. Energy dissipaters were sized using tables from the reference book "Hydraulic Design of Energy Dissipaters for Culverts and Channels" US Department of Transportation, Federal Highway Administration, July 2006.

#### Rock Cute Sizing

Rock chutes were sized for the 25-year, 24-hour storm event. Rock Chutes were sized based on the flow to each culvert location. The Iowa NRCS Rock Chute Design spreadsheet was used to size the chute and riprap.

#### Discharge Apron Sizing

Riprap aprons were sized for the 25-year, 24-hour storm event using equations in Section 5.2 – Riprap Blanket of WisDOT FDM 13-35-5. The riprap aprons were sized based on the flow to the culvert location. The riprap sizing was used to size the riprap discharge apron.

#### Basin Sizing

Route the proposed construction and existing drainage runoff through the sedimentation basin to confirm the basin can handle the 25-year, 24-hour storm event. HydroCAD was used to model the runoff flow through the basin outfall (as determined by the Hydrograph Generation model).

#### **Key Assumptions:**

- Drainage areas and time of concentration flow paths are as shown on **Figure 1** for Post Construction Conditions.
- An MSE4 rainfall distribution was used based on NRCS Wisconsin rainfall distribution regions.
  The precipitation depth for the 25-year, 24-hour storm was assumed to be 4.91 inches, based
  on NOAA ATLAS 14 Point Precipitation Frequency Estimates (NOAA's National Weather
  Service Hydrometeorological Design Studies Center Precipitation Frequency Data Server).
- Runoff curve numbers were based on tables presented in Urban Hydrology for Small Watersheds, and were assumed as follows and as listed in the modeling.

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BY	RJG	DATE 4/7/22				
CHK'D.	MRH	DATE 4/8/22				

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Client	WPL	Subject	Storm Water Management

Cover Type	CN
Final Cover	69 – Pasture/grassland/range in good condition,
	hydrologic soil group (HSG) C/B (assumed mid value
	between each soil group)
Pasture, grassland	39 – Pasture/grassland/range, Good, HSG A
or range	
Rain Cover	98 – Rain Cover (plastic smooth material)
Pavement	98 – impervious HSG A
Gravel	96 – Gravel, HSG A

- Type A soil group for non-disturbed areas outside the landfill as soils are loamy sand.
- Other assumptions are included with the calculations attached to this appendix.

#### Results:

#### Hydrograph Generation

The hydrograph modeling results for the 25-year and 100-year, 24-hour storm events are included in the Post Construction Conditions Hydrograph Generation section.

#### Basin Sizing

The existing sedimentation basin has the capacity to safely contain the 25-year, 24-hour storm event and safely pass the 100-year, 24-hour storm event through the emergency spillway. Refer to the Basin Sizing section.

#### Swale Sizing

The proposed swales will be constructed as shown on the Drawings. The swales have the capacity to safely convey the both the 25-year, 24-hour storm events and maintain a minimum 0.5 foot of freeboard. Refer to the Swale Sizing section.

Appropriate erosion control product was selected based on the velocities and shear stress in the swales. Refer to the Swale Sizing section below for the evaluation.

#### Culvert Sizing

Culverts will be as shown in the Drawings. The culverts have the capacity to safely convey the 25-year, 24-hour storm event. Refer to the Culvert Sizing Section for the detailed calculations.

#### Diversion Berm Sizing

The proposed final berms will be constructed as shown on the Drawings. The diversion berms will contain the runoff from the 25-year, 24-hour storm event. Refer to the Diversion Berm Design section.

#### Downslope Flume and Energy Dissipater Sizing

The downslope flumes and energy dissipaters will be constructed as shown on the Drawings. The downslope flumes are designed to contain the runoff from the 25-year, 24-hour storm event. Energy dissipaters at the bottom of the downslope flumes have been designed to handle the peak velocities. Refer to the Downslope Flume and Energy Dissipater Sizing section below for detailed calculations.

#### Rock Chute Sizing

The proposed rock chutes will be constructed as shown in the Drawings. The rock chutes will accommodate the runoff from the 25-year, 24-hour storm event. Refer to the Rock Chute Sizing section.

Job

Subject

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BY	RJG	DATE 4/7/22	_
CHK'D	MRH	DATE 4/8/22	

## \_\_\_\_

Job No. 25220183.00

WPL

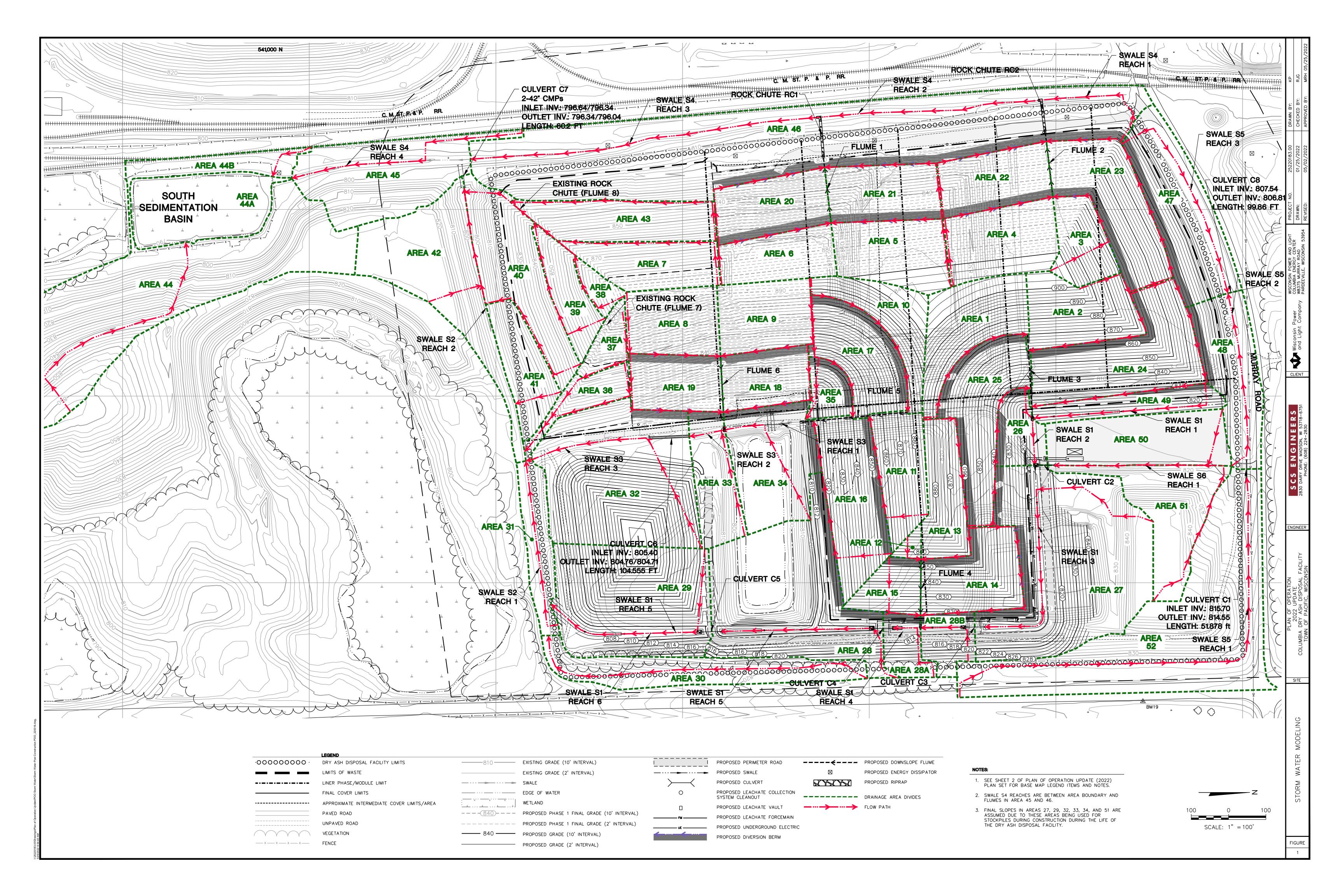
Client

<u>Discharge Apron Sizing</u>
The proposed riprap aprons will be constructed as shown in the Drawings. The aprons will accommodate the runoff from the 25-year, 24-hour storm event. Refer to Discharge Apron Sizing for design calculations.

Columbia Dry Ash Disposal

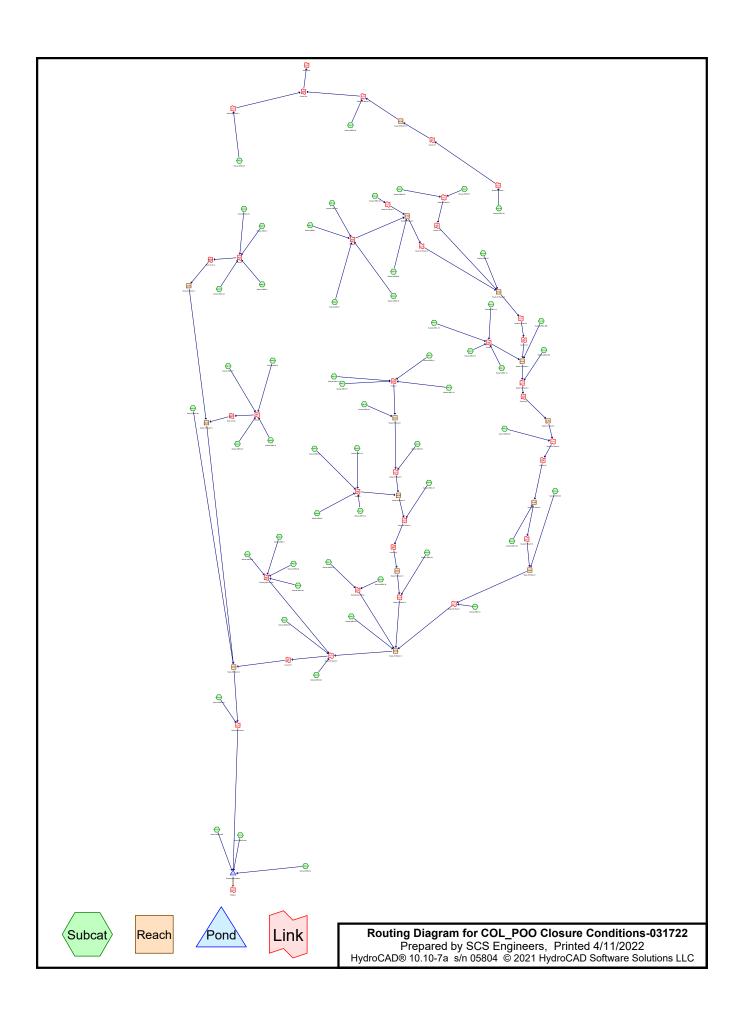
Storm Water Management

 $I:\ 25220183.00\ Data\ and\ Calculations\ Stormwater\ Landfill\ Sed\ Basin\ Size\ Check\ SWM\ Calcs\_Writeup\_Sed\ Basin\_Draft.doc$ 



# Post Construction Conditions Hydrograph Generation

- 25-year, 24-hour Storm Event
- 100-year, 24-hour Storm Event



# COL POO FINAL CONDITIONS MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

# **COL\_POO Closure Conditions-031722**

Subcatchment AREA 23: Subcat AREA 23

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Time span=0.00-40.00 hrs, dt=0.01 hrs, 4001 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method
Subcatchment AREA 1: Subcat AREA 1  Runoff Area=1.288 ac 0.00% Impervious Runoff Depth=1.89" Flow Length=408' Tc=2.6 min CN=69 Runoff=4.58 cfs 0.203 af
Subcatchment AREA 10: Subcat AREA 10 Runoff Area=0.914 ac 0.00% Impervious Runoff Depth=1.89" Flow Length=500' Tc=3.2 min CN=69 Runoff=3.17 cfs 0.144 af
Subcatchment AREA 11: Subcat AREA 11 Runoff Area=0.949 ac 0.00% Impervious Runoff Depth=1.89" Flow Length=391' Tc=4.6 min CN=69 Runoff=3.10 cfs 0.150 af
Subcatchment AREA 12: Subcat AREA 12  Runoff Area=0.098 ac 0.00% Impervious Runoff Depth=1.89" Flow Length=92' Tc=2.5 min CN=69 Runoff=0.35 cfs 0.015 af
Subcatchment AREA 13: Subcat AREA 13 Runoff Area=0.890 ac 0.00% Impervious Runoff Depth=1.89" Flow Length=590' Tc=4.6 min CN=69 Runoff=2.91 cfs 0.140 af
Subcatchment AREA 14: Subcat AREA 14 Runoff Area=1.145 ac 0.00% Impervious Runoff Depth=1.89" Flow Length=625' Tc=5.1 min CN=69 Runoff=3.66 cfs 0.181 af
Subcatchment AREA 15: Subcat AREA 15 Runoff Area=0.512 ac 0.00% Impervious Runoff Depth=1.89" Flow Length=235' Tc=4.2 min CN=69 Runoff=1.71 cfs 0.081 af
Subcatchment AREA 16: Subcat AREA 16 Runoff Area=1.510 ac 0.00% Impervious Runoff Depth=1.89" Flow Length=522' Tc=4.9 min CN=69 Runoff=4.89 cfs 0.238 af
Subcatchment AREA 17: Subcat AREA 17 Runoff Area=1.228 ac 0.00% Impervious Runoff Depth=1.89" Flow Length=386' Tc=4.7 min CN=69 Runoff=4.00 cfs 0.194 af
Subcatchment AREA 18: Subcat AREA 18 Runoff Area=0.813 ac 0.00% Impervious Runoff Depth=1.89" Flow Length=383' Tc=4.6 min CN=69 Runoff=2.66 cfs 0.128 af
Subcatchment AREA 19: Subcat AREA 19 Runoff Area=0.847 ac 0.00% Impervious Runoff Depth=1.89" Flow Length=394' Tc=4.6 min CN=69 Runoff=2.77 cfs 0.134 af
Subcatchment AREA 2: Subcat AREA 2  Runoff Area=1.167 ac 0.00% Impervious Runoff Depth=1.89" Flow Length=613' Tc=5.1 min CN=69 Runoff=3.73 cfs 0.184 af
Subcatchment AREA 20: Subcat AREA 20 Runoff Area=1.054 ac 0.00% Impervious Runoff Depth=1.89" Flow Length=453' Tc=4.7 min CN=69 Runoff=3.43 cfs 0.166 af
Subcatchment AREA 21: Subcat AREA 21  Runoff Area=1.030 ac 0.00% Impervious Runoff Depth=1.89" Flow Length=448' Tc=4.7 min CN=69 Runoff=3.35 cfs 0.162 af
Subcatchment AREA 22: Subcat AREA 22 Runoff Area=1.030 ac 0.00% Impervious Runoff Depth=1.89"

Flow Length=448' Tc=4.7 min CN=69 Runoff=3.35 cfs 0.162 af

Flow Length=715' Tc=5.4 min CN=69 Runoff=4.89 cfs 0.244 af

Runoff Area=1.548 ac 0.00% Impervious Runoff Depth=1.89"

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- Runoff Area=1.952 ac 0.00% Impervious Runoff Depth=1.89" Subcatchment AREA 24: Subcat AREA 24 Flow Length=889' Tc=5.8 min CN=69 Runoff=6.05 cfs 0.308 af
- Runoff Area=1.515 ac 0.00% Impervious Runoff Depth=1.89" Subcatchment AREA 25: Subcat AREA 25 Flow Length=495' Tc=3.9 min CN=69 Runoff=5.13 cfs 0.239 af
- Runoff Area=0.518 ac 0.00% Impervious Runoff Depth=1.74" Subcatchment AREA 26: Subcat AREA 26 Flow Length=216' Tc=4.1 min CN=67 Runoff=1.59 cfs 0.075 af
- Subcatchment AREA 27: Subcat AREA 27 Runoff Area=4.140 ac 0.00% Impervious Runoff Depth=0.55" Flow Length=864' Tc=12.0 min CN=48 Runoff=1.68 cfs 0.191 af
- Subcatchment AREA 28: Subcat AREA 28 Runoff Area=142,960 sf 0.00% Impervious Runoff Depth=0.66" Flow Length=573' Tc=9.1 min CN=50 Runoff=2.08 cfs 0.179 af
- Subcatchment AREA 28A: Subcat AREA 28A Runoff Area=0.423 ac 0.00% Impervious Runoff Depth=0.60" Flow Length=234' Tc=9.1 min CN=49 Runoff=0.23 cfs 0.021 af
- Subcatchment AREA 28B: Subcat AREA 28B Runoff Area=0.476 ac 0.00% Impervious Runoff Depth=0.71" Flow Length=211' Tc=4.5 min CN=51 Runoff=0.47 cfs 0.028 af
- Runoff Area=2.792 ac 0.00% Impervious Runoff Depth=0.22" Subcatchment AREA 29: Subcat AREA 29 Flow Length=463' Tc=14.8 min CN=40 Runoff=0.16 cfs 0.050 af
- Runoff Area=0.717 ac 0.00% Impervious Runoff Depth=1.89" Subcatchment AREA 3: Subcat AREA 3 Flow Length=409' Tc=6.3 min CN=69 Runoff=2.17 cfs 0.113 af
- Runoff Area=1.415 ac 0.00% Impervious Runoff Depth=0.18" Subcatchment AREA 30: Subcat AREA 30 Flow Length=941' Slope=0.0260 '/' Tc=22.0 min CN=39 Runoff=0.06 cfs 0.021 af
- Subcatchment AREA 31: Subcat AREA 31 Runoff Area=0.698 ac 0.00% Impervious Runoff Depth=0.18" Flow Length=481' Tc=4.4 min CN=39 Runoff=0.03 cfs 0.011 af
- Runoff Area=3.353 ac 0.00% Impervious Runoff Depth=0.46" Subcatchment AREA 32: Subcat AREA 32 Flow Length=663' Tc=17.3 min CN=46 Runoff=0.81 cfs 0.128 af
- Subcatchment AREA 33: Subcat AREA 33 Runoff Area=38,914 sf 0.00% Impervious Runoff Depth=0.60" Flow Length=377' Tc=16.0 min CN=49 Runoff=0.37 cfs 0.045 af
- Runoff Area=68,484 sf 0.00% Impervious Runoff Depth=0.37" Subcatchment AREA 34: Subcat AREA 34 Flow Length=488' Tc=16.2 min CN=44 Runoff=0.25 cfs 0.049 af
- Subcatchment AREA 35: Subcat AREA 35 Runoff Area=0.375 ac 0.00% Impervious Runoff Depth=1.89" Slope=0.2500 '/' Tc=4.2 min CN=69 Runoff=1.25 cfs 0.059 af Flow Length=174'
- Runoff Area=0.487 ac 0.00% Impervious Runoff Depth=1.82" Subcatchment AREA 36: Subcat AREA 36 Flow Length=425' Tc=4.4 min CN=68 Runoff=1.54 cfs 0.074 af
- Runoff Area=0.344 ac 0.00% Impervious Runoff Depth=1.89" Subcatchment AREA 37: Subcat AREA 37 Flow Length=510' Tc=4.6 min CN=69 Runoff=1.12 cfs 0.054 af

- Subcatchment AREA 38: Subcat AREA 38 Runoff Area=0.223 ac 0.00% Impervious Runoff Depth=1.89" Flow Length=590' Tc=4.1 min CN=69 Runoff=0.75 cfs 0.035 af
- Subcatchment AREA 39: Subcat AREA 39

  Runoff Area=0.656 ac 0.00% Impervious Runoff Depth=1.89"

  Flow Length=642' Tc=5.3 min CN=69 Runoff=2.08 cfs 0.103 af
- Subcatchment AREA 4: Subcat AREA 4

  Runoff Area=1.247 ac 0.00% Impervious Runoff Depth=1.89"
  Flow Length=478' Tc=6.6 min CN=69 Runoff=3.74 cfs 0.197 af
- Subcatchment AREA 40: Subcat AREA 40 Runoff Area=1.618 ac 0.00% Impervious Runoff Depth=1.18" Flow Length=699' Tc=5.2 min CN=59 Runoff=3.05 cfs 0.160 af
- Subcatchment AREA 41: Subcat AREA 41 Runoff Area=0.826 ac 0.00% Impervious Runoff Depth=1.12" Flow Length=722' Tc=5.9 min CN=58 Runoff=1.40 cfs 0.077 af
- Subcatchment AREA 42: Subcat AREA 42 Runoff Area=2.177 ac 0.00% Impervious Runoff Depth=0.18" Flow Length=415' Tc=9.1 min CN=39 Runoff=0.09 cfs 0.033 af
- Subcatchment AREA 43: Subcat AREA 43 Runoff Area=1.228 ac 0.00% Impervious Runoff Depth=1.89" Flow Length=778' Tc=5.9 min CN=69 Runoff=3.79 cfs 0.194 af
- Subcatchment AREA 44: Subcat AREA 44

  Runoff Area=5.227 ac 0.00% Impervious Runoff Depth=0.18"

  Flow Length=701' Tc=7.9 min CN=39 Runoff=0.22 cfs 0.079 af
- Subcatchment AREA 44A: Subcat AREA Runoff Area=1.508 ac 100.00% Impervious Runoff Depth=4.67" Tc=0.0 min CN=98 Runoff=10.70 cfs 0.587 af
- Subcatchment AREA 44B: Subcat AREA 44B Runoff Area=0.594 ac 0.00% Impervious Runoff Depth=0.66" Flow Length=147' Slope=0.0544 '/' Tc=7.6 min CN=50 Runoff=0.41 cfs 0.032 af
- Subcatchment AREA 45: Subcat AREA 45 Runoff Area=2.001 ac 0.00% Impervious Runoff Depth=0.33" Flow Length=681' Tc=21.9 min CN=43 Runoff=0.24 cfs 0.055 af
- Subcatchment AREA 46: Subcat AREA 46 Runoff Area=7.367 ac 0.36% Impervious Runoff Depth=1.18" Flow Length=1,904' Tc=9.2 min CN=59 Runoff=11.31 cfs 0.727 af
- Subcatchment AREA 47: Subcat AREA 47 Runoff Area=79,132 sf 8.81% Impervious Runoff Depth=1.52" Flow Length=582' Tc=9.1 min CN=64 Runoff=3.79 cfs 0.230 af
- Subcatchment AREA 48: Subcat AREA 48 Runoff Area=57,540 sf 11.76% Impervious Runoff Depth=1.32" Flow Length=489' Tc=5.4 min CN=61 Runoff=2.79 cfs 0.145 af
- Subcatchment AREA 49: Subcat AREA 49 Runoff Area=0.691 ac 0.00% Impervious Runoff Depth=1.18" Flow Length=522' Tc=4.3 min CN=59 Runoff=1.37 cfs 0.068 af
- Subcatchment AREA 5: Subcat AREA 5

  Runoff Area=1.195 ac 0.00% Impervious Runoff Depth=1.89"
  Flow Length=482' Tc=6.6 min CN=69 Runoff=3.58 cfs 0.188 af
- Subcatchment AREA 50: Subcat AREA 50 Runoff Area=1.482 ac 0.00% Impervious Runoff Depth=4.00" Flow Length=570' Tc=3.4 min CN=92 Runoff=9.68 cfs 0.494 af

- Subcatchment AREA 51: Subcat AREA 51 Runoff Area=1.417 ac 0.00% Impervious Runoff Depth=0.22" Flow Length=884' Tc=12.2 min CN=40 Runoff=0.08 cfs 0.025 af
- Subcatchment AREA 52: Subcat AREA 52 Runoff Area=197,330 sf 13.14% Impervious Runoff Depth=0.51" Flow Length=1,294' Tc=6.3 min CN=47 Runoff=2.06 cfs 0.191 af
- Subcatchment AREA 6: Subcat AREA 6

  Runoff Area=0.892 ac 0.00% Impervious Runoff Depth=1.89"
  Flow Length=415' Tc=4.6 min CN=69 Runoff=2.92 cfs 0.141 af
- Subcatchment AREA 7: Subcat AREA 7

  Runoff Area=1.017 ac 0.00% Impervious Runoff Depth=1.89"
  Flow Length=833' Tc=5.8 min CN=69 Runoff=3.15 cfs 0.160 af
- Subcatchment AREA 8: Subcat AREA 8

  Runoff Area=1.009 ac 0.00% Impervious Runoff Depth=1.89"
  Flow Length=409' Tc=4.7 min CN=69 Runoff=3.29 cfs 0.159 af
- Subcatchment AREA 9: Subcat AREA 9

  Runoff Area=1.047 ac 0.00% Impervious Runoff Depth=1.89"

  Flow Length=426' Tc=4.8 min CN=69 Runoff=3.40 cfs 0.165 af
- **Reach S1 R2: Swale S1 Reach 2** Avg. Flow Depth=0.76' Max Vel=2.58 fps Inflow=22.03 cfs 1.077 af n=0.030 L=127.0' S=0.0055 '/' Capacity=140.64 cfs Outflow=21.68 cfs 1.077 af
- **Reach S1 R3: Swale S1 Reach 3** Avg. Flow Depth=0.88' Max Vel=2.69 fps Inflow=31.44 cfs 1.788 af n=0.030 L=578.0' S=0.0051 '/' Capacity=135.10 cfs Outflow=27.38 cfs 1.788 af
- **Reach S1 R4: Swale S1 Reach 4** Avg. Flow Depth=0.94' Max Vel=3.19 fps Inflow=35.79 cfs 2.233 af n=0.030 L=195.8' S=0.0066'/ Capacity=154.36 cfs Outflow=35.20 cfs 2.233 af
- **Reach S1 R5: Swale S1 Reach 5** Avg. Flow Depth=0.97' Max Vel=2.89 fps Inflow=35.39 cfs 2.255 af n=0.030 L=411.6' S=0.0053 '/' Capacity=137.86 cfs Outflow=33.17 cfs 2.255 af
- **Reach S1 R6: Swale S1 Reach 6** Avg. Flow Depth=0.97' Max Vel=2.87 fps Inflow=35.21 cfs 2.484 af n=0.030 L=430.9' S=0.0052 '/' Capacity=136.28 cfs Outflow=33.18 cfs 2.484 af
- **Reach S2 R1: Swale S2 Reach 1** Avg. Flow Depth=1.18' Max Vel=1.99 fps Inflow=33.19 cfs 2.506 af n=0.030 L=472.0' S=0.0020'/' Capacity=84.99 cfs Outflow=29.93 cfs 2.506 af
- **Reach S2 R2: Swale S2 Reach 2** Avg. Flow Depth=0.98' Max Vel=3.41 fps Inflow=48.80 cfs 4.314 af n=0.030 L=751.0' S=0.0069 '/' Capacity=182.04 cfs Outflow=46.24 cfs 4.314 af
- **Reach S3 R1: Swale S3 Reach 1** Avg. Flow Depth=0.63' Max Vel=2.73 fps Inflow=16.31 cfs 0.785 af n=0.030 L=215.0' S=0.0070 '/' Capacity=125.24 cfs Outflow=15.87 cfs 0.785 af
- **Reach S3 R2: Swale S3 Reach 2** Avg. Flow Depth=1.75' Max Vel=3.61 fps Inflow=27.94 cfs 1.419 af n=0.030 L=97.0' S=0.0070 '/' Capacity=71.57 cfs Outflow=27.78 cfs 1.419 af
- **Reach S3 R3: Swale S3 Reach 3** Avg. Flow Depth=0.73' Max Vel=3.34 fps Inflow=27.86 cfs 1.464 af n=0.030 L=353.0' S=0.0097 '/' Capacity=186.19 cfs Outflow=26.59 cfs 1.464 af
- **Reach S4 R2: Swale S4 Reach 2** Avg. Flow Depth=0.46' Max Vel=2.23 fps Inflow=14.04 cfs 0.716 af n=0.030 L=601.0' S=0.0069 '/' Capacity=174.20 cfs Outflow=11.87 cfs 0.716 af

#### **COL POO FINAL CONDITIONS**

#### **COL POO Closure Conditions-031722**

MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

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Reach S4 R3: Swale S4 Reach 3	Avg.	Flow Depth=0	.63'	Max Vel=2.42 fps	Inflow=23.93 cfs	1.374 af
n=0.030	L=946.0'	S=0.0056 '/'	Cap	acity=156.53 cfs	Outflow=18.66 cfs	1.374 af

Avg. Flow Depth=1.27' Max Vel=4.35 fps Inflow=81.28 cfs 7.099 af Reach S4 R4: Swale S4 Reach 4 n=0.030 L=483.0' S=0.0082 '/' Capacity=427.66 cfs Outflow=80.05 cfs 7.099 af

Inflow=2.06 cfs 0.191 af Reach S5 R2: Swale S5 Reach 2 Outflow=2.06 cfs 0.191 af

af s 5.880 af af

	Outliow-2.06 cis 0.191 al
<b>Pond Sed Pond: Sedimentation Basin</b> Peak Elev Primary=9.42 cfs 1.973 af Secondary=0.00 cfs 0.000 af	r=791.59' Storage=137,326 cf Inflow=82.78 cfs 7.853 af Tertiary=0.00 cfs 0.000 af Outflow=14.75 cfs 7.854 af
Link C1: Culvert C1	Inflow=2.06 cfs 0.191 af Primary=2.06 cfs 0.191 af
Link C2: Culvert C2	Inflow=9.68 cfs 0.520 af Primary=9.68 cfs 0.520 af
Link C3: Culvert C3	Inflow=27.38 cfs 1.788 af Primary=27.38 cfs 1.788 af
Link C4: Culvert C4	Inflow=35.39 cfs 2.255 af Primary=35.39 cfs 2.255 af
Link C5: Culvert C5	Inflow=35.21 cfs 2.434 af Primary=35.21 cfs 2.434 af
Link C6: Culvert C6	Inflow=27.86 cfs 1.464 af Primary=27.86 cfs 1.464 af
Link C7: Culvert C7	Inflow=52.15 cfs 4.999 af Primary=52.15 cfs 4.999 af
Link C8: Culvert C8	Inflow=8.32 cfs 0.566 af Primary=8.32 cfs 0.566 af
Link F1: Flume 1	Inflow=13.17 cfs 0.658 af

Inflow=13.17 cfs 0.658 af Link F1: Flume 1 Primary=13.17 cfs 0.658 af

Link F2: Flume 2 Inflow=14.04 cfs 0.716 af Primary=14.04 cfs 0.716 af

Inflow=19.08 cfs 0.934 af Link F3: Flume 3 Primary=19.08 cfs 0.934 af

Link F4: Flume 4 Inflow=8.58 cfs 0.417 af Primary=8.58 cfs 0.417 af

Inflow=15.06 cfs 0.725 af Link F5: Flume 5

Primary=15.06 cfs 0.725 af

#### **COL POO FINAL CONDITIONS**

MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

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injurios/ibs for a sim coost o Est myaros/ib conward conditions EES	r ugo r
Link F6: Flume 6	Inflow=12.11 cfs 0.586 af
	Primary=12.11 cfs 0.586 af
Link F7: Existing East Flume	Inflow=2.66 cfs 0.128 af
Link F7. Existing East Fluine	Primary=2.66 cfs 0.128 af
Link F8: Existing West Flume	Inflow=9.73 cfs 0.492 af
	Primary=9.73 cfs 0.492 af
Link North Area: North Area	Inflow=8.32 cfs 0.566 af
LIIK NOI (II Alea. NOI (II Alea	Primary=8.32 cfs 0.566 af
Link RC1: Rock Chute 1	Inflow=13.17 cfs 0.658 af
	Primary=13.17 cfs 0.658 af
Link RC2: Rock Chute 2	Inflow=14.04 cfs 0.716 af
LIIIK NOZ. NOCK CHUIE Z	Primary=14.04 cfs 0.716 af
Link Swale 1 R6: Swale S1 Reach 6	Inflow=33.18 cfs 2.484 af
	Primary=33.18 cfs 2.484 af
Link Swale S1 R1: Swale S1 Reach 1	Inflow=1.37 cfs 0.068 af
Lilik Swale ST KT. Swale ST Reacit T	Primary=1.37 cfs 0.068 af
	,,
Link Swale S1 R2: Swale S1 Reach 2	Inflow=21.68 cfs 1.077 af
	Primary=21.68 cfs 1.077 af
Link Swale S1 R3: Swale S1 Reach 3	Inflow=27.38 cfs 1.788 af
Link Owale of No. Owale of Neach o	Primary=27.38 cfs 1.788 af
	•
Link Swale S1 R4: Swale S1 Reach 4	Inflow=35.39 cfs 2.255 af
	Primary=35.39 cfs 2.255 af
Link Swale S1 R5: Swale S1 Reach 5	Inflow=35.21 cfs 2.434 af
	Primary=35.21 cfs 2.434 af
	•
Link Swale S2 R1: Swale S2 Reach 1	Inflow=29.95 cfs 2.516 af
	Primary=29.95 cfs 2.516 af
Link Swale S2 R2: Swale S2 Reach 2	Inflow=52.15 cfs 4.999 af
	Primary=52.15 cfs 4.999 af
	•
Link Swale S3 R1: Swale S3 Reach 1	Inflow=15.88 cfs 0.833 af
	Primary=15.88 cfs 0.833 af
Link Swale S3 R2: Swale S3 Reach 2	Inflow=27.86 cfs 1.464 af
	Primary=27.86 cfs 1.464 af
	•
Link Swale S3 R3: Swale S3 Reach 3	Inflow=26.70 cfs 1.592 af
	Primary=26.70 cfs 1.592 af

**COL POO FINAL CONDITIONS** 

# **COL\_POO Closure Conditions-031722**

MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

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Link Swale S4 R4: Swale S4 Reach 4	Inflow=80.09 cfs 7.154 af
	Primary=80.09 cfs 7.154 af
Link Swale CE D4: Cwale CE Decah 4	Inflow=2.06 cfs 0.191 af
Link Swale S5 R1: Swale S5 Reach 1	Primary=2.06 cfs 0.191 af
	1 mary 2.00 dia 0.101 di
Link Swale S5 R2: Swale S5 Reach 2	Inflow=4.68 cfs 0.336 af
	Primary=4.68 cfs 0.336 af

Link Swale S5 R3: Swale S5 Reach 3 Inflow=3.79 cfs 0.230 af Primary=3.79 cfs 0.230 af

Link Swale S6 R1: Swale S6 Reach 1 Inflow=9.68 cfs 0.520 af Primary=9.68 cfs 0.520 af

Link Wetland: Wetland Inflow=9.42 cfs 1.973 af Primary=9.42 cfs 1.973 af

Total Runoff Area = 82.060 ac Runoff Volume = 8.419 af Average Runoff Depth = 1.23" 97.02% Pervious = 79.615 ac 2.98% Impervious = 2.446 ac

MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

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# **Summary for Subcatchment AREA 1: Subcat AREA 1**

Runoff = 4.58 cfs @ 12.11 hrs, Volume= 0.203 af, Depth= 1.89"

Routed to Link F3: Flume 3

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

	Area	(ac) C	N Desc	cription		
	1.	.288 6	9 Past	ure/grassla	and/range,	Fair, HSG B
	1.	288	100.	00% Pervi	ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	1.7	37	0.2500	0.36		Sheet Flow,
_	0.9	371	0.0200	6.74	80.87	Grass: Short n= 0.150 P2= 2.77"  Trap/Vee/Rect Channel Flow, Diversion Berm  Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00' n= 0.030 Earth, grassed & winding
_	2.6	408	Total			

# **Summary for Subcatchment AREA 10: Subcat AREA 10**

Runoff = 3.17 cfs @ 12.11 hrs, Volume= 0.144 af, Depth= 1.89"

Routed to Link F5: Flume 5

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

_		914 6	9 Past			Fair, HSG B
	0.	914	100.	00% Pervi	ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	2.1	46	0.2500	0.37		Sheet Flow,
_	1.1	454	0.0200	6.74	80.87	Grass: Short n= 0.150 P2= 2.77"  Trap/Vee/Rect Channel Flow, Diversion Berm  Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00' n= 0.030 Earth, grassed & winding
	3.2	500	Total			

# **Summary for Subcatchment AREA 11: Subcat AREA 11**

Runoff = 3.10 cfs @ 12.12 hrs, Volume= 0.150 af, Depth= 1.89"

Routed to Link F5: Flume 5

MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

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	Area	(ac) C	N Desc	cription				
0.949 69 Pasture/grassland/range, Fair, HSG B								
0.949 100.00% Pervious Area								
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
	3.8	100	0.2500	0.43		Sheet Flow,		
	0.1	14	0.2500	3.50		Grass: Short n= 0.150 P2= 2.77"  Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps		
	0.7	277	0.0200	6.74	80.87	Trap/Vee/Rect Channel Flow, Diversion Berm Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00' n= 0.030 Earth, grassed & winding		
	4.6	391	Total					

# **Summary for Subcatchment AREA 12: Subcat AREA 12**

Runoff = 0.35 cfs @ 12.11 hrs, Volume= 0.015 af, Depth= 1.89"

Routed to Link F4: Flume 4

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

	Area	(ac) C	N Desc	cription		
	0.	098 6	Fair, HSG B			
	0.	098	100.	00% Pervi	ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	2.4	56	0.2500	0.39		Sheet Flow,
	0.1	36	0.0200	6.74	80.87	Grass: Short n= 0.150 P2= 2.77"  Trap/Vee/Rect Channel Flow, Diversion Berm  Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00' n= 0.030 Earth, grassed & winding
_	2.5	92	Total			

# **Summary for Subcatchment AREA 13: Subcat AREA 13**

Runoff = 2.91 cfs @ 12.12 hrs, Volume= 0.140 af, Depth= 1.89" Routed to Link F4 : Flume 4

MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

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_	Area	(ac) C	N Desc	cription		
	0.	890 6	9 Past	ure/grassla	and/range,	Fair, HSG B
	0.	890	100.	00% Pervi	ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	3.4	87	0.2500	0.42		Sheet Flow,
	1.2	503	0.0200	6.74	80.87	Grass: Short n= 0.150 P2= 2.77"  Trap/Vee/Rect Channel Flow, Diversion Berm  Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00' n= 0.030 Earth, grassed & winding
	4.6	590	Total			

# **Summary for Subcatchment AREA 14: Subcat AREA 14**

Runoff = 3.66 cfs @ 12.13 hrs, Volume=

0.181 af, Depth= 1.89"

Routed to Link F4: Flume 4

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

_	Area	(ac) C	N Desc	cription					
1.145 69 Pasture/grassland/range, Fair, HSG B									
1.145 100.00% Pervious Area									
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
	3.8	100	0.2500	0.43		Sheet Flow,			
	0.1	27	0.2500	3.50		Grass: Short n= 0.150 P2= 2.77"  Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps			
	1.2	498	0.0200	6.74	80.87	Trap/Vee/Rect Channel Flow, Diversion Berm Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00' n= 0.030 Earth, grassed & winding			
	5.1	625	Total						

# **Summary for Subcatchment AREA 15: Subcat AREA 15**

Runoff = 1.71 cfs @ 12.12 hrs, Volume= 0.081 af, Depth= 1.89"

Routed to Link F4: Flume 4

_	Area (ac)	CN	Description
	0.512	69	Pasture/grassland/range, Fair, HSG B
	0.512		100.00% Pervious Area

MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	3.8	100	0.2500	0.43		Sheet Flow,
	0.2	50	0.2500	3.50		Grass: Short n= 0.150 P2= 2.77"  Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
	0.2	85	0.0200	6.74	80.87	Trap/Vee/Rect Channel Flow, Diversion Berm Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00'
_						n= 0.030 Earth, grassed & winding
_	4.2	235	Total	•		

# **Summary for Subcatchment AREA 16: Subcat AREA 16**

Runoff = 4.89 cfs @ 12.13 hrs, Volume= 0.238 af, Depth= 1.89"

Routed to Link F5: Flume 5

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

_	Area	(ac) C	N Desc	cription					
1.510 69 Pasture/grassland/range, Fair, HSG B									
	1.	510	100.	00% Pervi	ous Area				
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
	3.8	100	0.2500	0.43		Sheet Flow,			
	0.2	50	0.2500	3.50		Grass: Short n= 0.150 P2= 2.77"  Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps			
	0.9	372	0.0200	6.74	80.87	Trap/Vee/Rect Channel Flow, Diversion Berm			
						Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00' n= 0.030 Earth, grassed & winding			
_	4.9	522	Total						

# **Summary for Subcatchment AREA 17: Subcat AREA 17**

Runoff = 4.00 cfs @ 12.12 hrs, Volume= 0.194 af, Depth= 1.89"

Routed to Link F5: Flume 5

_	Area (ac)	CN	Description
	1.228	69	Pasture/grassland/range, Fair, HSG B
Ī	1.228		100.00% Pervious Area

MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	3.8	100	0.2500	0.43		Sheet Flow,
	0.3	63	0.2500	3.50		Grass: Short n= 0.150 P2= 2.77"  Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
	0.6	223	0.0200	6.74	80.87	Trap/Vee/Rect Channel Flow, Diversion Berm Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00'
_						n= 0.030 Earth, grassed & winding
	4.7	386	Total			

# **Summary for Subcatchment AREA 18: Subcat AREA 18**

Runoff = 2.66 cfs @ 12.12 hrs, Volume= 0.128 af, Depth= 1.89"

Routed to Link F6: Flume 6

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

_	Area	(ac) C	N Desc	cription		
0.813 69 Pasture/grassland/range, Fair, HSG B						
	0.	813	100.	00% Pervi	ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	3.8	100	0.2500	0.43		Sheet Flow,
	0.2	48	0.2500	3.50		Grass: Short n= 0.150 P2= 2.77"  Shallow Concentrated Flow,
	0.6	235	0.0200	6.74	80.87	Short Grass Pasture Kv= 7.0 fps <b>Trap/Vee/Rect Channel Flow, Diversion Berm</b> Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00' n= 0.030 Earth, grassed & winding
_	4.6	383	Total			, <u>, , , , , , , , , , , , , , , , , , </u>

# **Summary for Subcatchment AREA 19: Subcat AREA 19**

Runoff = 2.77 cfs @ 12.12 hrs, Volume= 0.134 af, Depth= 1.89"

Routed to Link F6: Flume 6

	Area (ac)	CN	Description
	0.847	69	Pasture/grassland/range, Fair, HSG B
Ī	0.847		100.00% Pervious Area

MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	3.8	100	0.2500	0.43		Sheet Flow,
	0.2	50	0.2500	3.50		Grass: Short n= 0.150 P2= 2.77"  Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
	0.6	244	0.0200	6.74	80.87	Trap/Vee/Rect Channel Flow, Diversion Berm Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00'
_						n= 0.030 Earth, grassed & winding
_	4.6	394	Total	•		

# **Summary for Subcatchment AREA 2: Subcat AREA 2**

Runoff = 3.73 cfs @ 12.13 hrs, Volume= 0.184 af, Depth= 1.89"

Routed to Link F3: Flume 3

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

_	Area	(ac) C	N Desc	cription			
1.167 69 Pasture/grassland/range, Fair, HSG B							
	1.	167	100.	00% Pervi	ous Area		
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
	3.8	100	0.2500	0.43		Sheet Flow,	
	0.1	18	0.2500	3.50		Grass: Short n= 0.150 P2= 2.77"  Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps	
	1.2	495	0.0200	6.74	80.87	Trap/Vee/Rect Channel Flow, Diversion Berm	
_						Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00' n= 0.030 Earth, grassed & winding	
	5.1	613	Total				

# **Summary for Subcatchment AREA 20: Subcat AREA 20**

Runoff = 3.43 cfs @ 12.12 hrs, Volume= 0.166 af, Depth= 1.89"

Routed to Link F1: Flume 1

_	Area (ac)	CN	Description
	1.054	69	Pasture/grassland/range, Fair, HSG B
Ī	1.054		100.00% Pervious Area

MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	3.8	100	0.2500	0.43		Sheet Flow, Grass: Short n= 0.150 P2= 2.77"
	0.2	50	0.2500	3.50		Shallow Concentrated Flow,
	0.7	303	0.0200	6.74	80.87	Short Grass Pasture Kv= 7.0 fps  Trap/Vee/Rect Channel Flow, Diversion Berm
						Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00' n= 0.030 Earth, grassed & winding
•	4.7	453	Total			, ,

# **Summary for Subcatchment AREA 21: Subcat AREA 21**

Runoff = 3.35 cfs @ 12.12 hrs, Volume= 0.162 af,

0.162 af, Depth= 1.89"

Routed to Link F1: Flume 1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

_	Area	(ac) C	N Desc	cription			
1.030 69 Pasture/grassland/range, Fair, HSG B							
	1.	.030	100.	00% Pervi	ous Area		
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
	3.8	100	0.2500	0.43		Sheet Flow,	
	0.2	50	0.2500	3.50		Grass: Short n= 0.150 P2= 2.77" <b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps	
	0.7	298	0.0200	6.74	80.87	Trap/Vee/Rect Channel Flow, Diversion Berm Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00' n= 0.030 Earth, grassed & winding	
	4.7	448	Total			11 0.000 Earth, grassou & Winding	

# **Summary for Subcatchment AREA 22: Subcat AREA 22**

Runoff = 3.35 cfs @ 12.12 hrs, Volume= 0.162 af, Depth= 1.89"

Routed to Link F2: Flume 2

_	Area (ac)	CN	Description
	1.030	69	Pasture/grassland/range, Fair, HSG B
Ī	1.030		100.00% Pervious Area

MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	3.8	100	0.2500	0.43		Sheet Flow,
	0.2	50	0.2500	3.50		Grass: Short n= 0.150 P2= 2.77"  Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
	0.7	298	0.0200	6.74	80.87	Trap/Vee/Rect Channel Flow, Diversion Berm Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00'
_						n= 0.030 Earth, grassed & winding
_	4.7	448	Total	•		

# **Summary for Subcatchment AREA 23: Subcat AREA 23**

Runoff = 4.89 cfs @ 12.13 hrs, Volume= 0.244 af, Depth= 1.89"

Routed to Link F2: Flume 2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

	Area	(ac) C	N Desc	cription				
1.548 69 Pasture/grassland/range, Fair, HSG B								
	1.	548	100.	00% Pervi	ous Area			
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
_	3.8	100	0.2500	0.43		Sheet Flow,		
	0.1	24	0.2500	3.50		Grass: Short n= 0.150 P2= 2.77"  Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps		
	1.5	591	0.0200	6.74	80.87	Trap/Vee/Rect Channel Flow, Diversion Berm Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00' n= 0.030 Earth, grassed & winding		
	5.4	715	Total	·				

# **Summary for Subcatchment AREA 24: Subcat AREA 24**

Runoff = 6.05 cfs @ 12.13 hrs, Volume= 0.308 af, Depth= 1.89"

Routed to Link F3: Flume 3

	Area (ac)	CN	Description
	1.952	69	Pasture/grassland/range, Fair, HSG B
_	1.952		100.00% Pervious Area

MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	3.8	100	0.2500	0.43		Sheet Flow, Grass: Short n= 0.150 P2= 2.77"
	0.1	24	0.2500	3.50		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
	1.9	765	0.0200	6.74	80.87	Trap/Vee/Rect Channel Flow, Diversion Berm Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00'
_						n= 0.030 Earth, grassed & winding
	5.8	889	Total			

# **Summary for Subcatchment AREA 25: Subcat AREA 25**

Runoff = 5.13 cfs @ 12.12 hrs, Volume= 0.239 af, Depth= 1.89"

Routed to Link F3: Flume 3

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

_	Area	(ac) C	N Desc	cription		
	1.	515 6	9 Past	ure/grassla	and/range,	Fair, HSG B
	1.	515	100.	00% Pervi	ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	2.8	67	0.2500	0.40		Sheet Flow,
	1.1	428	0.0200	6.74	80.87	Grass: Short n= 0.150 P2= 2.77" <b>Trap/Vee/Rect Channel Flow,</b> Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00' n= 0.030 Earth, grassed & winding
_	3.9	495	Total			

# **Summary for Subcatchment AREA 26: Subcat AREA 26**

Runoff = 1.59 cfs @ 12.12 hrs, Volume= 0.075 af, Depth= 1.74"

Routed to Reach S1 R2 : Swale S1 Reach 2

	Area (ac)	CN	Description			
	0.396	69	Pasture/grassland/range, Fair, HSG B			
	0.072	39	Pasture/grassland/range, Good, HSG A			
	0.049	96	Gravel surface, HSG A			
*	0.000	0	Pasture/grassland/range, Fair			
	0.518	67	Weighted Average			
	0.518		100.00% Pervious Area			

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	Tc	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	3.6	93	0.2500	0.43		Sheet Flow,
						Grass: Short n= 0.150 P2= 2.77"
	0.5	123	0.0055	4.39	140.49	Trap/Vee/Rect Channel Flow, Swale 1 Reach 2
						Bot.W=8.00' D=2.00' Z= 4.0 '/' Top.W=24.00'
_						n= 0.030 Earth, grassed & winding
	4.1	216	Total			

# **Summary for Subcatchment AREA 27: Subcat AREA 27**

Runoff = 1.68 cfs @ 12.25 hrs, Volume=

0.191 af, Depth= 0.55"

Routed to Reach S1 R3: Swale S1 Reach 3

	Area	(ac)	CN	Desc	cription		
	0.	651	69	Past	ure/grassla	and/range,	Fair, HSG B
	2.	758	39	Past	ure/grassla	and/range,	Good, HSG A
	0.	010	96	Grav	el surface	, HSG Å	
		295	96		el surface	,	
		426	39	Past	ure/grassla	and/range,	Good, HSG A
*		000	0				
*		000	0				
*		000	0	, HS			
*		000	0	, HS			
*		000	0	, HS			
*		000	0	, HS		d /	Cood
_		000	0			and/range,	<u>G000</u>
		140	48		hted Aver	0	
	4.	140		100.0	00% Pervi	ous Area	
	Тс	Lengt	h	Slope	Velocity	Capacity	Description
	(min)	(feet		(ft/ft)	(ft/sec)	(cfs)	Description
_	7.3	10		0.0500	0.23	(013)	Sheet Flow,
	7.5	10	0 0	.0300	0.23		Grass: Short n= 0.150 P2= 2.77"
	2.3	21	7 0	.0500	1.57		Shallow Concentrated Flow,
	2.0		. 0	.0000	1.07		Short Grass Pasture Kv= 7.0 fps
	0.3	2	0 0	.0050	1.14		Shallow Concentrated Flow,
							Unpaved Kv= 16.1 fps
	0.1	1	4 0	.2500	3.50		Shallow Concentrated Flow,
							Short Grass Pasture Kv= 7.0 fps
	2.0	51	3 0	.0051	4.23	135.28	Trap/Vee/Rect Channel Flow, Swale 1 Reach 3
							Bot.W=8.00' D=2.00' Z= 4.0 '/' Top.W=24.00'
_							n= 0.030 Earth, grassed & winding
	12.0	86	4 T	otal			

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## Summary for Subcatchment AREA 28: Subcat AREA 28

Runoff = 2.08 cfs @ 12.19 hrs, Volume=

0.179 af, Depth= 0.66"

Routed to Link Swale S1 R5 : Swale S1 Reach 5

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

	Α	rea (sf)	CN D	escription			
*	1	30,267 00,859 11,834		ge, Fair, HSG B ge, Good, HSG A			
		42,960 42,960	50 Weighted Average 100.00% Pervious Area				
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
	5.9	78	0.0526	0.22		Sheet Flow,	
	1.1	22	0.2500	0.32		Grass: Short n= 0.150 P2= 2.77" <b>Sheet Flow,</b> Grass: Short n= 0.150 P2= 2.77"	
	0.1	24	0.2500	3.50		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps	
	0.3	23	0.0050	1.14		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps	
	0.1	16	0.2500	3.50		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps	
	1.6	410	0.0053	4.31	137.91	Trap/Vee/Rect Channel Flow, Swale 1 Reach Bot.W=8.00' D=2.00' Z= 4.0 '/' Top.W=24.00' n= 0.030 Earth, grassed & winding	
	9.1	573	Total				

# Summary for Subcatchment AREA 28A: Subcat AREA 28A

Runoff = 0.23 cfs @ 12.20 hrs, Volume= 0.021 af, Depth= 0.60" Routed to Link Swale S1 R4 : Swale S1 Reach 4

 Area (ac)	CN	Description
0.035	69	Pasture/grassland/range, Fair, HSG B
0.257	Pasture/grassland/range, Good, HSG A	
0.075	39	Pasture/grassland/range, Good, HSG A
0.010	96	Gravel surface, HSG A
 0.046	96	Gravel surface, HSG A
 0.423	49	Weighted Average
0.423		100.00% Pervious Area

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.3	82	0.0334	0.19	, ,	Sheet Flow,
					Grass: Short n= 0.150 P2= 2.77"
1.0	18	0.2500	0.31		Sheet Flow,
					Grass: Short n= 0.150 P2= 2.77"
0.2	34	0.2500	3.50		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
0.3	20	0.0050	1.14		Shallow Concentrated Flow,
					Unpaved Kv= 16.1 fps
0.1	13	0.2500	3.50		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
0.2	67	0.0069	4.92	157.36	Trap/Vee/Rect Channel Flow,
					Bot.W=8.00' D=2.00' Z= 4.0 '/' Top.W=24.00'
					n= 0.030 Earth, grassed & winding
9.1	234	Total			

# Summary for Subcatchment AREA 28B: Subcat AREA 28B

Runoff = 0.47 cfs @ 12.13 hrs, Volume=

0.028 af, Depth= 0.71"

Routed to Reach S1 R4 : Swale S1 Reach 4

	Area	(ac) C	N Des	cription					
	0.	050	69 Past	Pasture/grassland/range, Fair, HSG B					
	0.	110	39 Past	Pasture/grassland/range, Good, HSG A					
	0.	240	39 Past	ure/grassla	and/range,	Good, HSG A			
	0.	009	96 Grav	el surface	, HSG Å				
_	0.	067	96 Grav	/el surface	, HSG A				
	0.	476	51 Wei	ghted Aver	age				
	0.	476	100.	00% Pervi	ous Area				
	Тс	Length	Slope	Velocity	Capacity	Description			
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	2.5	58	0.2500	0.39		Sheet Flow,			
						Grass: Short n= 0.150 P2= 2.77"			
	0.6	20	0.0050	0.53		Sheet Flow,			
						Smooth surfaces n= 0.011 P2= 2.77"			
	1.0	18	0.2500	0.31		Sheet Flow,			
	0.4	445		4.00	4.40.40	Grass: Short n= 0.150 P2= 2.77"			
	0.4	115	0.0055	4.39	140.49	Trap/Vee/Rect Channel Flow,			
						Bot.W=8.00' D=2.00' Z= 4.0 '/' Top.W=24.00'			
_						n= 0.030 Earth, grassed & winding			
	4.5	211	Total						

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## **Summary for Subcatchment AREA 29: Subcat AREA 29**

Runoff = 0.16 cfs @ 12.58 hrs, Volume=

0.050 af, Depth= 0.22"

Routed to Reach S1 R6: Swale S1 Reach 6

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

	Area	(ac) C	N Desc	cription					
				el surface		Good, HSG A			
*		000		el surface	•	C000, 1100 / C			
_				Weighted Average					
	2.	792	100.	00% Pervi	ous Area				
	Тс	Length	Slope	Velocity	Capacity	Description			
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	'			
	11.8	100	0.0150	0.14		Sheet Flow,			
						Grass: Short n= 0.150 P2= 2.77"			
	1.9	100	0.0150	0.86		Shallow Concentrated Flow,			
	0.4	40	0.0500	0.50		Short Grass Pasture Kv= 7.0 fps			
	0.1	16	0.2500	3.50		Shallow Concentrated Flow,			
	1.0	247	0.0052	4.27	136.60	Short Grass Pasture Kv= 7.0 fps  Trap/Vee/Rect Channel Flow, Swale S1 Reach 5  Bot.W=8.00' D=2.00' Z= 4.0 '/' Top.W=24.00'			
						n= 0.030 Earth, grassed & winding			
	14.8	463	Total						

# **Summary for Subcatchment AREA 3: Subcat AREA 3**

Runoff = 2.17 cfs @ 12.14 hrs, Volume= 0.113 af, Depth= 1.89"

Routed to Link F2: Flume 2

	Area (ac)	CN	Description				
	0.717	69	Pasture/grassland/range, Fair, HSG B				
0.717 100.00% Pervious Area		100.00% Pervious Area					

MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91" Printed 4/11/2022

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.9	44	0.1000	0.26	, ,	Sheet Flow,
					Grass: Short n= 0.150 P2= 2.77"
2.4	56	0.2500	0.39		Sheet Flow,
					Grass: Short n= 0.150 P2= 2.77"
0.4	76	0.2500	3.50		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
0.6	233	0.0200	6.74	80.87	Trap/Vee/Rect Channel Flow, Diversion Berm
					Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00'
					n= 0.030 Earth, grassed & winding
6.3	409	Total			

# **Summary for Subcatchment AREA 30: Subcat AREA 30**

Runoff = 0.06 cfs @ 13.18 hrs, Volume= 0.021 a

0.021 af, Depth= 0.18"

Routed to Reach S2 R1: Swale S2 Reach 1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

_	Area	(ac) C	N Desc	cription		
	1.	415 3	39 Past	ure/grassla	and/range,	Good, HSG A
	1.	415	100.	00% Pervi	ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	9.5	100	0.0260	0.18		Sheet Flow,
	2.9	194	0.0260	1.13		Grass: Short n= 0.150 P2= 2.77"  Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
_	9.6	647	0.0260	1.13		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
	22.0	941	Total			

# **Summary for Subcatchment AREA 31: Subcat AREA 31**

Runoff = 0.03 cfs @ 12.44 hrs, Volume= 0.011 af, Depth= 0.18"

Routed to Link Swale S2 R1: Swale S2 Reach 1

_	Area (ac)	CN	Description
Ī	0.698	39	Pasture/grassland/range, Good, HSG A
-	0.698		100.00% Pervious Area

MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

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	Tc	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	1.6	34	0.2500	0.35		Sheet Flow,
						Grass: Short n= 0.150 P2= 2.77"
	2.8	447	0.0020	2.65	84.72	
						Bot.W=8.00' D=2.00' Z= 4.0 '/' Top.W=24.00'
_						n= 0.030 Earth, grassed & winding
	44	481	Total			

# **Summary for Subcatchment AREA 32: Subcat AREA 32**

Runoff = 0.81 cfs @ 12.38 hrs, Volume= 0.128 af, Depth= 0.46"

Routed to Link Swale S3 R3: Swale S3 Reach 3

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

Area	(ac) C	N Desc	cription					
0.	567 6	9 Past	Pasture/grassland/range, Fair, HSG B					
2.	413 3	39 Past	Pasture/grassland/range, Good, HSG A					
0.								
0.274 39 Pasture/grassland/range, Good, HSG A								
3.353 46 Weighted Average								
3.	353	100.	00% Pervi	ous Area				
Tc	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
12.1	100	0.0140	0.14		Sheet Flow,			
					Grass: Short n= 0.150 P2= 2.77"			
4.2	211	0.0140	0.83		Shallow Concentrated Flow,			
					Short Grass Pasture Kv= 7.0 fps			
0.1	23	0.1740	2.92		Shallow Concentrated Flow,			
					Short Grass Pasture Kv= 7.0 fps			
0.9	329	0.0097	5.83	186.57	Trap/Vee/Rect Channel Flow, Swale 3 Reach 3			
					Bot.W=8.00' D=2.00' Z= 4.0 '/' Top.W=24.00'			
					n= 0.030 Earth, grassed & winding			
17.3	663	Total						

# **Summary for Subcatchment AREA 33: Subcat AREA 33**

Runoff = 0.37 cfs @ 12.32 hrs, Volume= 0.045 af, Depth= 0.60"

Routed to Link Swale S3 R2 : Swale S3 Reach 2

MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

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	Α	rea (sf)	CN E	Description							
		4,079	96 (	96 Gravel surface, HSG A							
		1,422	96 C	96 Gravel surface, HSG A							
		30,707	39 F	Pasture/gra	ssland/rang	ge, Good, HSG A					
*		2,706				ge, Fair, HSG A					
_		38,914	49 V	Veighted A	verage						
		38,914		0	ervious Are	a					
			•								
	Tc	Length	Slope	Velocity	Capacity	Description					
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	'					
_	12.1	100	0.0140	0.14	` ,	Sheet Flow,					
						Grass: Short n= 0.150 P2= 2.77"					
	3.6	178	0.0140	0.83		Shallow Concentrated Flow,					
						Short Grass Pasture Kv= 7.0 fps					
	0.0	12	0.4000	4.43		Shallow Concentrated Flow,					
						Short Grass Pasture Kv= 7.0 fps					
	0.3	87	0.0070	5.23	125.44	Trap/Vee/Rect Channel Flow, Swale 3 Reach 2					
						Bot.W=8.00' D=2.00' Z= 2.0 '/' Top.W=16.00'					
						n= 0.030 Earth, grassed & winding					
	16.0	377	Total								

# Summary for Subcatchment AREA 34: Subcat AREA 34

Runoff = 0.25 cfs @ 12.43 hrs, Volume=

0.049 af, Depth= 0.37"

Routed to Link Swale S3 R1: Swale S3 Reach 1

			O				
	A	rea (sf)	CN D	escription)			
	5,695 69 Pasture/grassland/range, Fair, HSG B						
		3,470	96	Gravel surfa	ace, HSG A	Ä	
59,319 39 Pasture/grassland/range, Good, HSG A							
		68,484		Veighted A		,	
		68,484			ervious Are	а	
		00, 10 1		00.00701	J. 110 do 7 11 0	<b>-</b>	
	Тс	Length	Slope	Velocity	Capacity	Description	
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	2 · · · · · · · · · · · · · · · ·	
	12.1	100	0.0140	0.14	` '	Sheet Flow,	
						Grass: Short n= 0.150 P2= 2.77"	
	3.4	170	0.0140	0.83		Shallow Concentrated Flow,	
						Short Grass Pasture Kv= 7.0 fps	
	0.1	15	0.4000	4.43		Shallow Concentrated Flow,	
	0	.0	0.1000			Short Grass Pasture Kv= 7.0 fps	
	0.6	203	0.0070	5.23	125.44	Trap/Vee/Rect Channel Flow, Swale 3 Reach 1	
	0.0	200	0.0070	0.20	120.11	Bot.W=8.00' D=2.00' Z= 2.0 '/' Top.W=16.00'	
						n= 0.030 Earth, grassed & winding	
_	16.2	488	Total			c.ccca.a., g.accca c. Williamg	

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# **Summary for Subcatchment AREA 35: Subcat AREA 35**

Runoff = 1.25 cfs @ 12.12 hrs, Volume=

0.059 af, Depth= 1.89"

Routed to Reach S3 R1: Swale S3 Reach 1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

	Area	(ac) C	N Desc	cription				
	0.375 69 Pasture/grassland/range, Fair, HSG B							
0.375 100.00% Pervious Area								
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
-	3.8	100	0.2500	0.43	, ,	Sheet Flow,		
	0.4	74	0.2500	3.50		Grass: Short n= 0.150 P2= 2.77"  Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps		
	4.2	174	Total	-	_			

## **Summary for Subcatchment AREA 36: Subcat AREA 36**

Runoff = 1.54 cfs @ 12.12 hrs, Volume=

0.074 af, Depth= 1.82"

Routed to Link F7: Existing East Flume

	Area	(ac) C	N Desc	cription			
0.470 69 Pasture/grassland/range, Fair, HSG B							
	0.	016	39 Past	ure/grassl	and/range,	Good, HSG A	
*	0.	000	0 Past	ure/grassl	and/range,	Good	
	0.	487	68 Weig	ghted Aver	age		
	0.	487	100.	00% Pervi	ous Area		
	Тс	Length	Slope	Velocity	Capacity	Description	
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
	3.5	90	0.2500	0.43		Sheet Flow,	
						Grass: Short n= 0.150 P2= 2.77"	
	0.7	201	0.0200	4.80	23.38	·	
						Bot.W=0.00' D=1.18' Z= 4.0 & 3.0 '/' Top.W=8.26'	
						n= 0.030 Earth, grassed & winding	
	0.2	134	0.2500	12.26	441.43	Trap/Vee/Rect Channel Flow, Riprap Flume	
						Bot.W=12.00' D=2.00' Z= 3.0 '/' Top.W=24.00'	
_						n= 0.078 Riprap, 12-inch	
	44	425	Total				

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# **Summary for Subcatchment AREA 37: Subcat AREA 37**

Runoff = 1.12 cfs @ 12.12 hrs, Volume=

0.054 af, Depth= 1.89"

Routed to Link F7: Existing East Flume

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

	Area	(ac) C	N Des	cription		
	0.	344 6	9 Past	ture/grassl	and/range,	Fair, HSG B
_	0.344 100.00% Pervious Area					
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	3.8	100	0.2500	0.43	•	Sheet Flow,
						Grass: Short n= 0.150 P2= 2.77"
	0.1	30	0.2500	3.50		Shallow Concentrated Flow,
	0.4	126	0.0200	4.80	23.38	Short Grass Pasture Kv= 7.0 fps <b>Trap/Vee/Rect Channel Flow, Existing Diversion Berm</b> Bot.W=0.00' D=1.18' Z= 4.0 & 3.0 '/' Top.W=8.26' n= 0.030 Earth, grassed & winding
	0.3	254	0.2500	12.26	441.43	Trap/Vee/Rect Channel Flow, Riprap Flume Bot.W=12.00' D=2.00' Z= 3.0 '/' Top.W=24.00' n= 0.078 Riprap, 12-inch
_	4.6	510	Total			

## **Summary for Subcatchment AREA 38: Subcat AREA 38**

Runoff = 0.75 cfs @ 12.12 hrs, Volume=

0.035 af, Depth= 1.89"

Routed to Link F8: Existing West Flume

	Area	(ac) C	N Desc	cription		
	0.	223 6	9 Past	ure/grassla	and/range,	Fair, HSG B
	0.	0.223 69 Pasture/grassland/ 0.223 100.00% Pervious c Length Slope Velocity Ca ) (feet) (ft/ft) (ft/sec) 1 77 0.2500 0.41 5 156 0.0200 4.80				
	Tc (min)			,	Capacity (cfs)	Description
	3.1	77	0.2500	0.41		Sheet Flow,
						Grass: Short n= 0.150 P2= 2.77"
	0.5	156	0.0200	4.80	23.38	Trap/Vee/Rect Channel Flow, Existing Diversion Berm
						Bot.W=0.00' D=1.18' Z= 4.0 & 3.0 '/' Top.W=8.26' n= 0.030 Earth, grassed & winding
	0.5	357	0.2500	12.26	441.43	Trap/Vee/Rect Channel Flow, Riprap Flume
						Bot.W=12.00' D=2.00' Z= 3.0 '/' Top.W=24.00'
_						n= 0.078 Riprap, 12-inch
	4.1	590	Total			

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# **Summary for Subcatchment AREA 39: Subcat AREA 39**

Runoff = 2.08 cfs @ 12.13 hrs, Volume=

0.103 af, Depth= 1.89"

Routed to Link F8 : Existing West Flume

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

	Area	(ac) C	N Des	cription		
_		<u>, , , , , , , , , , , , , , , , , , , </u>			and/range,	Fair, HSG B
	0.	656		00% Pervi		
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	3.8	100	0.2500	0.43		Sheet Flow,
	0.1	11	0.2500	3.50		Grass: Short n= 0.150 P2= 2.77"  Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
	1.1	314	0.0200	4.80	23.38	Trap/Vee/Rect Channel Flow, Existing Diversion Berm Bot.W=0.00' D=1.18' Z= 4.0 & 3.0 '/' Top.W=8.26' n= 0.030 Earth, grassed & winding
	0.3	217	0.2500	12.26	441.43	Trap/Vee/Rect Channel Flow, Riprap Flume Bot.W=12.00' D=2.00' Z= 3.0 '/' Top.W=24.00' n= 0.078 Riprap, 12-inch
_	5.3	642	Total			

# **Summary for Subcatchment AREA 4: Subcat AREA 4**

Runoff = 3.74 cfs @ 12.14 hrs, Volume= 0.197 af, Depth= 1.89"

Routed to Link F2: Flume 2

	<u>Area</u>	(ac) C	N Des	cription		
	1.	247 6	9 Past	ure/grassla	and/range,	Fair, HSG B
	1.	247	100.	00% Pervi	ous Area	
(1	Tc min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	3.5	57	0.1000	0.27		Sheet Flow,
						Grass: Short n= 0.150 P2= 2.77"
	2.0	43	0.2500	0.37		Sheet Flow, Grass: Short n= 0.150 P2= 2.77"
	0.4	83	0.2500	3.50		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
	0.7	295	0.0200	6.74	80.87	Trap/Vee/Rect Channel Flow, Diversion Berm Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00' n= 0.030 Earth, grassed & winding
	6.6	478	Total			· · · · · · · · · · · · · · · · · · ·

MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91" Printed 4/11/2022

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# **Summary for Subcatchment AREA 40: Subcat AREA 40**

Runoff = 3.05 cfs @ 12.13 hrs, Volume=

0.160 af, Depth= 1.18"

Routed to Link Swale S2 R2 : Swale S2 Reach 2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

	Area	(ac) C	N Desc	cription		
	1.079 69 Pasture/grassland/range, F					Fair, HSG B
	0.	539	39 Past	ure/grassla	and/range,	Good, HSG A
*	0.	000	0 Past	ure/grassla	and/range,	Good
	1.	618 5	59 Weig	ghted Aver	age	
1.618			100.	00% Pervi	ous Area	
	-		01		0 "	D
	Tc	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	3.1	77	0.2500	0.41		Sheet Flow,
						Grass: Short n= 0.150 P2= 2.77"
	8.0	237	0.0200	4.80	23.38	
						Bot.W=0.00' D=1.18' Z= 4.0 & 3.0 '/' Top.W=8.26'
						n= 0.030 Earth, grassed & winding
	0.3	70	0.2500	3.50		Shallow Concentrated Flow,
						Short Grass Pasture Kv= 7.0 fps
	1.0	315	0.0069	5.05	181.72	Trap/Vee/Rect Channel Flow, Swale S2 Reach 2
						Bot.W=10.00' D=2.00' Z= 4.0 '/' Top.W=26.00'
						n= 0.030 Earth, grassed & winding
	5.2	699	Total			

# Summary for Subcatchment AREA 41: Subcat AREA 41

Runoff = 1.40 cfs @ 12.14 hrs, Volume= 0.077 af, Depth= 1.12"

Routed to Reach S2 R2 : Swale S2 Reach 2

Area (ac)	CN	Description
0.520	69	Pasture/grassland/range, Fair, HSG B
0.306	39	Pasture/grassland/range, Good, HSG A
0.826	58	Weighted Average
0.826		100.00% Pervious Area

MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	3.8	100	0.2500	0.43		Sheet Flow,
	0.1	26	0.2500	3.50		Grass: Short n= 0.150 P2= 2.77"  Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
	2.0	596	0.0069	5.05	181.72	Trap/Vee/Rect Channel Flow, Swale S2 Reach 2 Bot.W=10.00' D=2.00' Z= 4.0 '/' Top.W=26.00' n= 0.030 Earth, grassed & winding
-	5.9	722	Total			5.555 Earth, grassea a milang

# **Summary for Subcatchment AREA 42: Subcat AREA 42**

Runoff = 0.09 cfs @ 12.55 hrs, Volume= 0.033 af,

0.033 af, Depth= 0.18"

Routed to Link Swale S2 R2: Swale S2 Reach 2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

_	Area	(ac) C	N Des	cription		
2.177 39 Pasture/gr					and/range,	Good, HSG A
_	2.	177	100.	00% Pervi	ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	6.4	66	0.0303	0.17		Sheet Flow,
						Grass: Short n= 0.150 P2= 2.77"
	1.6	34	0.2500	0.35		Sheet Flow,
	0.0	40	0.0500	0.50		Grass: Short n= 0.150 P2= 2.77"
	0.2	49	0.2500	3.50		Shallow Concentrated Flow,
_	0.9	266	0.0069	5.05	181.72	Short Grass Pasture Kv= 7.0 fps <b>Trap/Vee/Rect Channel Flow, Swale S2 Reach 2</b> Bot.W=10.00' D=2.00' Z= 4.0 '/' Top.W=26.00' n= 0.030 Earth, grassed & winding
	9 1	415	Total			

# **Summary for Subcatchment AREA 43: Subcat AREA 43**

Runoff = 3.79 cfs @ 12.14 hrs, Volume= 0.194 af, Depth= 1.89"

Routed to Link F8: Existing West Flume

Area (ac)	CN	Description
1.228	69	Pasture/grassland/range, Fair, HSG B
1.228	1	100.00% Pervious Area

MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

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Тс	Length	Slope	Velocity	Capacity	Description
 (min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
3.8	100	0.2500	0.43		Sheet Flow,
					Grass: Short n= 0.150 P2= 2.77"
0.0	6	0.2500	3.50		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
1.9	541	0.0200	4.80	23.38	Trap/Vee/Rect Channel Flow, Existing Diversion Berm
					Bot.W=0.00' D=1.18' Z= 4.0 & 3.0 '/' Top.W=8.26'
					n= 0.030 Earth, grassed & winding
0.2	131	0.2500	12.26	441.43	Trap/Vee/Rect Channel Flow, Riprap Flume
					Bot.W=12.00' D=2.00' Z= 3.0 '/' Top.W=24.00'
					n= 0.078 Riprap, 12-inch
5.9	778	Total			

### Summary for Subcatchment AREA 44: Subcat AREA 44

Runoff = 0.22 cfs @ 12.54 hrs, Volume=

0.079 af, Depth= 0.18"

Routed to Pond Sed Pond : Sedimentation Basin

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

Area	(ac) C	N Desc	cription		
5.	227 3	89 Past	ure/grassla	and/range,	Good, HSG A
5.	227	100.	00% Pervi	ous Area	
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
4.5	75	0.0933	0.28		Sheet Flow,
1.3	25	0.2500	0.33		Grass: Short n= 0.150 P2= 2.77" <b>Sheet Flow,</b> Grass: Short n= 0.150 P2= 2.77"
0.0	10	0.2500	3.50		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
0.8	381	0.0265	7.85	109.92	Trap/Vee/Rect Channel Flow, Bot.W=0.00' D=2.00' Z= 4.0 & 3.0 '/' Top.W=14.00'
0.8	162	0.2500	3.50		n= 0.030 Earth, grassed & winding  Shallow Concentrated Flow,  Short Grass Pasture Kv= 7.0 fps
0.5	48	0.0500	1.57		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
7.9	701	Total			

### Summary for Subcatchment AREA 44A: Subcat AREA 44A

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff = 10.70 cfs @ 12.09 hrs, Volume= Routed to Pond Sed Pond : Sedimentation Basin 0.587 af, Depth= 4.67"

MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

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Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

_	Area	(ac)	CN				
_	1.	508	98	Water Surface, HSG A			
1.508 100.00% Impervious Area						rvious Area	a .
	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	0.0				•		Direct Entry,

### Summary for Subcatchment AREA 44B: Subcat AREA 44B

Runoff = 0.41 cfs @ 12.17 hrs, Volume=

0.032 af, Depth= 0.66"

Routed to Pond Sed Pond : Sedimentation Basin

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

_	Area	(ac) C	N Des	cription				
	0.	479 3	39 Past	ure/grassl	and/range,	Good, HSG A		
	0.	115	96 Grav	el surface/	, HSG Å			
*	0.	000	0 , HS	G A				
*	0.	000	0 , HS	G A				
	0.594 50 Weighted Average							
0.594 100.00% Pervious Area								
	Tc	Length	Slope	Velocity	Capacity	Description		
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
	7.1	100	0.0544	0.24		Sheet Flow,		
						Grass: Short n= 0.150 P2= 2.77"		
	0.5	47	0.0544	1.63		Shallow Concentrated Flow,		
						Short Grass Pasture Kv= 7.0 fps		
	7.6	147	Total					

### **Summary for Subcatchment AREA 45: Subcat AREA 45**

Runoff = 0.24 cfs @ 12.57 hrs, Volume= 0 Routed to Link Swale S4 R4 : Swale S4 Reach 4

0.055 af, Depth= 0.33"

rodica to Ellik Gwale G4 1(4 : Gwale G4 1(cdolf 4

MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

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_	Area	(ac)	CN	Desc	ription							
*	0.	000	0	, HS	HSG A							
	1.	870	39	Pastı	ure/grassla	and/range,	Good, HSG A					
	0.	000	96	Grav	el surface	, HSG A						
_	0.	130	96	Grav	el surface	, HSG A						
2.001 43 Weighted Average												
	2.	001		100.0	00% Pervi	ous Area						
	Тс	Length	າ S	Slope	Velocity	Capacity	Description					
_	(min)	(feet	)	(ft/ft)	(ft/sec)	(cfs)						
	15.7	100	0.	0074	0.11		Sheet Flow,					
								0 4 = 0		~ <b></b> "		

				,	- 1	•
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	15.7	100	0.0074	0.11		Sheet Flow,
						Grass: Short n= 0.150 P2= 2.77"
	4.7	169	0.0074	0.60		Shallow Concentrated Flow,
						Short Grass Pasture Kv= 7.0 fps
	0.4	49	0.0800	1.98		Shallow Concentrated Flow,
						Short Grass Pasture Kv= 7.0 fps
	1.1	363	0.0082	5.42	162.67	Trap/Vee/Rect Channel Flow, Swale S4 Reach 2
						Bot.W=8.00' D=2.00' Z= 4.0 & 3.0 '/' Top.W=22.00'
_						n= 0.030 Earth, grassed & winding
	21.9	681	Total			

### Summary for Subcatchment AREA 46: Subcat AREA 46

0.727 af, Depth= 1.18" Runoff 11.31 cfs @ 12.18 hrs, Volume= Routed to Reach S4 R4: Swale S4 Reach 4

	Area (ac)	CN	Description
	3.081	69	Pasture/grassland/range, Fair, HSG B
	0.590	96	Gravel surface, HSG B
	3.264	39	Pasture/grassland/range, Good, HSG A
	0.017	98	Paved parking, HSG A
	0.009	98	Paved parking, HSG A
	0.378	96	Gravel surface, HSG A
	0.001	96	Gravel surface, HSG A
	0.026	96	Gravel surface, HSG A
*	0.000	0	, HSG A
*	0.000	0	, HSG A
*	0.000	0	, HSG A
*	0.000	0	, HSG A
*	0.000	0	, HSG A
*	0.000	0	, HSG A
*	0.000	0	Pasture/grassland/range, Fair
	7.367	59	Weighted Average
	7.340		99.64% Pervious Area
	0.027		0.36% Impervious Area

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To	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
2.2	51	0.2500	0.38		Sheet Flow,
					Grass: Short n= 0.150 P2= 2.77"
0.1	16	0.2500	2.44		Sheet Flow,
					Smooth surfaces n= 0.011 P2= 2.77"
0.9	31	0.0050	0.58		Sheet Flow,
					Smooth surfaces n= 0.011 P2= 2.77"
0.4	47	0.0650	1.78		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
5.6	1,759	0.0073	5.26	178.68	Trap/Vee/Rect Channel Flow, Swale S4 Reach 1
					Bot.W=10.00' D=2.00' Z= 3.0 & 4.0 '/' Top.W=24.00'
					n= 0.030 Earth, grassed & winding
9.2	1,904	Total			

### **Summary for Subcatchment AREA 47: Subcat AREA 47**

Runoff = 3.79 cfs @ 12.17 hrs, Volume=

0.230 af, Depth= 1.52"

Routed to Link Swale S5 R3 : Swale S5 Reach 3

_	Α	rea (sf)	CN E	Description					
		49,617	69 F	Pasture/gra	ssland/rang	ge, Fair, HSG B			
		6,971	98 F	Paved park	ing, HSG A	- \			
		1,619	96 C	Gravel surface, HSG A					
_		20,925	39 F	Pasture/gra	ssland/rang	ge, Good, HSG A			
		79,132	64 V	Veighted A	verage				
		72,161	g	1.19% Per	vious Area				
		6,971	8	3.81% Impe	ervious Area	a			
	Тс	Length	Slope	Velocity	Capacity	Description			
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	2.0	43	0.2500	0.37		Sheet Flow,			
						Grass: Short n= 0.150 P2= 2.77"			
	0.1	11	0.1111	1.63		Sheet Flow,			
						Smooth surfaces n= 0.011 P2= 2.77"			
	0.7	12	0.2500	0.28		Sheet Flow,			
						Grass: Short n= 0.150 P2= 2.77"			
	2.9	28	0.0393	0.16		Sheet Flow,			
						Grass: Short n= 0.150 P2= 2.77"			
	3.4	488	0.0024	2.40	52.81	• •			
						Bot.W=0.00' D=2.00' Z= 5.0 & 6.0 '/' Top.W=22.00'			
_						n= 0.030 Earth, grassed & winding			
	9.1	582	Total						

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### **Summary for Subcatchment AREA 48: Subcat AREA 48**

Runoff = 2.79 cfs @ 12.13 hrs, Volume=

0.145 af, Depth= 1.32"

Routed to Link Swale S5 R2 : Swale S5 Reach 2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

A	rea (sf)	CN E	escription				
	24,597 69 Pasture/grassland/range, Fair, HSG B						
	24,117	39 F	asture/gra	ssland/rang	ge, Good, HSG A		
	2,057	96 G	Gravel surfa	ace, HSG A	À		
	6,769	98 F	aved park	ing, HSG A	· ·		
	57,540	61 V	Veighted A	verage			
	50,771	8	8.24% Per	vious Area			
	6,769	1	1.76% Imp	pervious Are	ea		
Tc	Length	Slope	Velocity	Capacity	Description		
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
0.6	19	0.0050	0.53		Sheet Flow,		
					Smooth surfaces n= 0.011 P2= 2.77"		
1.7	29	0.1667	0.29		Sheet Flow,		
					Grass: Short n= 0.150 P2= 2.77"		
3.1	441	0.0024	2.38	40.39	- I		
					Bot.W=0.00' D=2.00' Z= 2.5 & 6.0 '/' Top.W=17.00'		
					n= 0.030 Earth, grassed & winding		
5.4	489	Total					

### **Summary for Subcatchment AREA 49: Subcat AREA 49**

Runoff = 1.37 cfs @ 12.12 hrs, Volume= Routed to Link Swale S1 R1 : Swale S1 Reach 1 0.068 af, Depth= 1.18"

_	Area	(ac) (	CN Des	N Description							
	0.	439	Fair, HSG B								
0.246 39 Pasture/grassland/range, G						Good, HSG A					
0.006 96 Gravel surface, HSG A											
	0.691 59 Weighted Average										
	0.	691	100.	00% Pervi	ous Area						
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description					
	2.5	59	0.2500	0.39		Sheet Flow,					
	1.8	463	0.0053	4.31	137.91	Grass: Short n= 0.150 P2= 2.77"  Trap/Vee/Rect Channel Flow, Swale S1 Reach 1  Bot.W=8.00' D=2.00' Z= 4.0 '/' Top.W=24.00' n= 0.030 Earth, grassed & winding					

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4.3 522 Total

### **Summary for Subcatchment AREA 5: Subcat AREA 5**

Runoff = 3.58 cfs @ 12.14 hrs, Volume= 0.188 af, Depth= 1.89"

Routed to Link F1: Flume 1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

_	Area	(ac) C	N Desc	cription		
	1.	195 6	9 Past	ure/grassla	and/range,	Fair, HSG B
	1.	195	100.	00% Pervi	ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	3.6	59	0.1000	0.27		Sheet Flow,
						Grass: Short n= 0.150 P2= 2.77"
	1.9	41	0.2500	0.36		Sheet Flow,
						Grass: Short n= 0.150 P2= 2.77"
	0.4	85	0.2500	3.50		Shallow Concentrated Flow,
						Short Grass Pasture Kv= 7.0 fps
	0.7	297	0.0200	6.74	80.87	Trap/Vee/Rect Channel Flow, Diversion Berm
						Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00'
_						n= 0.030 Earth, grassed & winding
	6.6	482	Total			

#### 2 10101

### **Summary for Subcatchment AREA 50: Subcat AREA 50**

Runoff = 9.68 cfs @ 12.11 hrs, Volume= 0.494 af, Depth= 4.00" Routed to Link Swale S6 R1 : Swale S6 Reach 1

 Area (ac)	CN	Description			
 0.100	39	Pasture/grassland/range, Good, HSG A			
0.001	39	Pasture/grassland/range, Good, HSG A			
 1.382	96	Gravel surface, HSG A			
1.482	92	Weighted Average			
1.482		100.00% Pervious Area			

MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	1.6	100	0.0119	1.04	(010)	Sheet Flow,
						Smooth surfaces n= 0.011 P2= 2.77"
	0.4	47	0.0119	1.76		Shallow Concentrated Flow,
	0.0	10	0.5000	4.95		Unpaved Kv= 16.1 fps Shallow Concentrated Flow,
	0.0	10	0.0000	4.50		Short Grass Pasture Kv= 7.0 fps
	1.4	413	0.0066	5.00	130.01	Trap/Vee/Rect Channel Flow, Swale S6 Reach 1
						Bot.W=8.00' D=2.00' Z= 2.5 '/' Top.W=18.00'
_						n= 0.030 Earth, grassed & winding
	3.4	570	Total			

### **Summary for Subcatchment AREA 51: Subcat AREA 51**

Runoff = 0.08 cfs @ 12.54 hrs, Volume=

0.025 af, Depth= 0.22"

Routed to Link Swale S6 R1 : Swale S6 Reach 1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

	Area	(ac) C	N Desc	cription		
_	1.	.396 3	Good, HSG A			
0.020 96 Gravel surface, HSG A 1.417 40 Weighted Average 1.417 100.00% Pervious Area						
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	7.3	100	0.0500	0.23		Sheet Flow,
	3.2	302	0.0500	1.57		Grass: Short n= 0.150 P2= 2.77"  Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
	0.3	53	0.0313	2.85		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
	1.4	429	0.0066	5.00	130.01	Trap/Vee/Rect Channel Flow, Swale S6 Reach 1 Bot.W=8.00' D=2.00' Z= 2.5 '/' Top.W=18.00' n= 0.030 Earth, grassed & winding
_	12.2	884	Total			, 0

### **Summary for Subcatchment AREA 52: Subcat AREA 52**

Runoff = 2.06 cfs @ 12.16 hrs, Volume= 0.19

0.191 af, Depth= 0.51"

Routed to Link Swale S5 R1: Swale S5 Reach 1

MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

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A	rea (sf)	CN D	escription				
1	169,213 39 Pasture/grassland/range, Good, HSG A						
	25,933	98 P	aved park	ing, HSG A	,		
	2,184	96 G	ravel surfa	ace, HSG A	1		
1	97,330	47 V	/eighted A	verage			
1	71,397	8	6.86% Per	vious Area			
	25,933	1	3.14% Imp	ervious Are	ea		
			·				
Tc	Length	Slope	Velocity	Capacity	Description		
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
0.6	18	0.0050	0.52		Sheet Flow,		
					Smooth surfaces n= 0.011 P2= 2.77"		
1.4	21	0.1333	0.25		Sheet Flow,		
					Grass: Short n= 0.150 P2= 2.77"		
4.3	1,255	0.0096	4.82	125.20	· • · · · · · · · · · · · · · · · · · ·		
					Bot.W=0.00' D=2.00' Z= 6.0 & 7.0 '/' Top.W=26.00'		
					n= 0.030 Earth, grassed & winding		
6.3	1,294	Total					

### **Summary for Subcatchment AREA 6: Subcat AREA 6**

Runoff = 2.92 cfs @ 12.12 hrs, Volume= 0.141 af, Depth= 1.89"

Routed to Link F1: Flume 1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

	Area	(ac) C	N Des	cription		
	0.	892 6	9 Past	ure/grassl	and/range,	Fair, HSG B
	0.	892				
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	3.8	100	0.2500	0.43		Sheet Flow,
	0.0	7	0.2500	3.50		Grass: Short n= 0.150 P2= 2.77"  Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
	0.8	308	0.0200	6.74	80.87	Trap/Vee/Rect Channel Flow, Diversion Berm Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00' n= 0.030 Earth, grassed & winding
-	4.6	415	Total			

### **Summary for Subcatchment AREA 7: Subcat AREA 7**

Runoff = 3.15 cfs @ 12.13 hrs, Volume= 0.160 af, Depth= 1.89"

Routed to Link F8: Existing West Flume

MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

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P	ad	e	3

_	Area	(ac) C	N Des	cription		
	1.	017 6	9 Past	ure/grassla	and/range,	Fair, HSG B
	1.	017	100.	00% Pervi	ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	3.8	100	0.2500	0.43		Sheet Flow,
	0.1	18	0.2500	3.50		Grass: Short n= 0.150 P2= 2.77"  Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
	1.5	419	0.0200	4.80	23.38	Trap/Vee/Rect Channel Flow, Existing Diversion Berm Bot.W=0.00' D=1.18' Z= 4.0 & 3.0 '/' Top.W=8.26'
	0.4	296	0.2500	12.26	441.43	n= 0.030 Earth, grassed & winding  Trap/Vee/Rect Channel Flow,  Bot.W=12.00' D=2.00' Z= 3.0 '/' Top.W=24.00' n= 0.078 Riprap, 12-inch
_	5.8	833	Total			

### **Summary for Subcatchment AREA 8: Subcat AREA 8**

Runoff = 3.29 cfs @ 12.12 hrs, Volume= 0.159 af, Depth= 1.89"

Routed to Link F6: Flume 6

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

	Area	(ac) C	N Desc	cription		
	1.	009 6	89 Past	ure/grassla	and/range,	Fair, HSG B
	1.	009	100.	00% Pervi	ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	3.8	100	0.2500	0.43		Sheet Flow,
	0.3	66	0.2500	3.50		Grass: Short n= 0.150 P2= 2.77"  Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
	0.6	243	0.0200	6.74	80.87	Trap/Vee/Rect Channel Flow, Diversion Berm Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00' n= 0.030 Earth, grassed & winding
_	4.7	409	Total			

## **Summary for Subcatchment AREA 9: Subcat AREA 9**

Runoff = 3.40 cfs @ 12.13 hrs, Volume= 0.165 af, Depth= 1.89"

Routed to Link F6: Flume 6

MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

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_	Area	(ac) C	N Desc	cription		
	1.	047 6	9 Past	ure/grassl	and/range,	Fair, HSG B
	1.	047	100.	00% Pervi	ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	3.8	100	0.2500	0.43		Sheet Flow,
	0.4	76	0.2500	3.50		Grass: Short n= 0.150 P2= 2.77"  Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
	0.6	250	0.0200	6.74	80.87	Trap/Vee/Rect Channel Flow, Diversion Berm Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00'
_						n= 0.030 Earth, grassed & winding
	4.8	426	Total			

### Summary for Reach S1 R2: Swale S1 Reach 2

Inflow Area = 7.131 ac, 0.00% Impervious, Inflow Depth = 1.81" for 25-yr, 24-hr event

22.03 cfs @ 12.12 hrs, Volume= Inflow 1.077 af

21.68 cfs @ 12.13 hrs, Volume= Outflow 1.077 af, Atten= 2%, Lag= 0.5 min

Routed to Link Swale S1 R2 : Swale S1 Reach 2

Routing by Dyn-Stor-Ind method, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

Max. Velocity= 2.58 fps, Min. Travel Time= 0.8 min

Avg. Velocity = 0.69 fps, Avg. Travel Time= 3.1 min

Peak Storage= 1,066 cf @ 12.13 hrs

Average Depth at Peak Storage= 0.76', Surface Width= 14.08' Bank-Full Depth= 2.00' Flow Area= 32.0 sf, Capacity= 140.64 cfs

8.00' x 2.00' deep channel, n= 0.030 Earth, grassed & winding

Side Slope Z-value= 4.0 '/' Top Width= 24.00'

Length= 127.0' Slope= 0.0055 '/'

Inlet Invert= 814.81', Outlet Invert= 814.11'



### Summary for Reach S1 R3: Swale S1 Reach 3

14.170 ac, 0.00% Impervious, Inflow Depth = 1.51" for 25-yr, 24-hr event 31.44 cfs @ 12.12 hrs, Volume= 1.788 af Inflow Area =

Inflow

27.38 cfs @ 12.15 hrs, Volume= Outflow 1.788 af, Atten= 13%, Lag= 1.6 min

Routed to Link Swale S1 R3 : Swale S1 Reach 3

MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs Max. Velocity= 2.69 fps, Min. Travel Time= 3.6 min Avg. Velocity = 0.61 fps, Avg. Travel Time= 15.9 min

Peak Storage= 5,875 cf @ 12.15 hrs Average Depth at Peak Storage= 0.88', Surface Width= 15.05' Bank-Full Depth= 2.00' Flow Area= 32.0 sf, Capacity= 135.10 cfs

8.00' x 2.00' deep channel, n= 0.030 Earth, grassed & winding Side Slope Z-value= 4.0 '/' Top Width= 24.00' Length= 578.0' Slope= 0.0051 '/' Inlet Invert= 814.11', Outlet Invert= 811.17'



### Summary for Reach S1 R4: Swale S1 Reach 4

Inflow Area = 17.292 ac, 0.00% Impervious, Inflow Depth = 1.55" for 25-yr, 24-hr event

Inflow = 35.79 cfs @ 12.14 hrs, Volume= 2.233 af

Outflow = 35.20 cfs @ 12.15 hrs, Volume= 2.233 af, Atten= 2%, Lag= 0.7 min

Routed to Link Swale S1 R4: Swale S1 Reach 4

Routing by Dyn-Stor-Ind method, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs Max. Velocity= 3.19 fps, Min. Travel Time= 1.0 min Avg. Velocity = 0.70 fps, Avg. Travel Time= 4.6 min

Peak Storage= 2,163 cf @ 12.15 hrs Average Depth at Peak Storage= 0.94', Surface Width= 15.52' Bank-Full Depth= 2.00' Flow Area= 32.0 sf, Capacity= 154.36 cfs

8.00' x 2.00' deep channel, n= 0.030 Earth, grassed & winding Side Slope Z-value= 4.0 '/' Top Width= 24.00' Length= 195.8' Slope= 0.0066 '/' Inlet Invert= 811.17', Outlet Invert= 809.87'



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MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91" Printed 4/11/2022

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### Summary for Reach S1 R5: Swale S1 Reach 5

Inflow Area = 0.00% Impervious, Inflow Depth = 1.53" for 25-yr, 24-hr event 17.714 ac.

35.39 cfs @ 12.15 hrs, Volume= Inflow 2.255 af

2.255 af, Atten= 6%, Lag= 1.6 min 33.17 cfs @ 12.18 hrs, Volume= Outflow

Routed to Link Swale S1 R5 : Swale S1 Reach 5

Routing by Dyn-Stor-Ind method, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

Max. Velocity= 2.89 fps, Min. Travel Time= 2.4 min Avg. Velocity = 0.64 fps, Avg. Travel Time= 10.7 min

Peak Storage= 4,722 cf @ 12.18 hrs

Average Depth at Peak Storage= 0.97', Surface Width= 15.73'

Bank-Full Depth= 2.00' Flow Area= 32.0 sf, Capacity= 137.86 cfs

8.00' x 2.00' deep channel, n= 0.030 Earth, grassed & winding

Side Slope Z-value= 4.0 '/' Top Width= 24.00'

Length= 411.6' Slope= 0.0053 '/'

Inlet Invert= 809.77', Outlet Invert= 807.59'



### Summary for Reach S1 R6: Swale S1 Reach 6

23.788 ac, 0.00% Impervious, Inflow Depth = 1.25" for 25-yr, 24-hr event Inflow Area =

Inflow 35.21 cfs @ 12.18 hrs, Volume= 2.484 af

33.18 cfs @ 12.21 hrs, Volume= 2.484 af, Atten= 6%, Lag= 1.8 min Outflow

Routed to Link Swale 1 R6: Swale S1 Reach 6

Routing by Dyn-Stor-Ind method. Time Span= 0.00-40.00 hrs. dt= 0.01 hrs.

Max. Velocity= 2.87 fps, Min. Travel Time= 2.5 min

Avg. Velocity = 0.65 fps, Avg. Travel Time= 11.0 min

Peak Storage= 4,986 cf @ 12.21 hrs

Average Depth at Peak Storage= 0.97', Surface Width= 15.78'

Bank-Full Depth= 2.00' Flow Area= 32.0 sf, Capacity= 136.28 cfs

8.00' x 2.00' deep channel, n= 0.030 Earth, grassed & winding

Side Slope Z-value= 4.0 '/' Top Width= 24.00'

Length= 430.9' Slope= 0.0052 '/'

Inlet Invert= 807.15', Outlet Invert= 804.92'

MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

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#### Summary for Reach S2 R1: Swale S2 Reach 1

Inflow Area = 25.203 ac, 0.00% Impervious, Inflow Depth = 1.19" for 25-yr, 24-hr event

Inflow = 33.19 cfs @ 12.21 hrs, Volume= 2.506 af

Outflow = 29.93 cfs @ 12.26 hrs, Volume= 2.506 af, Atten= 10%, Lag= 3.0 min

Routed to Link Swale S2 R1: Swale S2 Reach 1

Routing by Dyn-Stor-Ind method, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

Max. Velocity= 1.99 fps, Min. Travel Time= 4.0 min Avg. Velocity = 0.45 fps, Avg. Travel Time= 17.6 min

Peak Storage= 7,099 cf @ 12.26 hrs

Average Depth at Peak Storage= 1.18', Surface Width= 17.45' Bank-Full Depth= 2.00' Flow Area= 32.0 sf, Capacity= 84.99 cfs

8.00' x 2.00' deep channel, n= 0.030 Earth, grassed & winding

Side Slope Z-value= 4.0 '/' Top Width= 24.00'

Length= 472.0' Slope= 0.0020 '/'

Inlet Invert= 802.25', Outlet Invert= 801.30'



### Summary for Reach S2 R2: Swale S2 Reach 2

Inflow Area = 42.068 ac, 0.00% Impervious, Inflow Depth = 1.23" for 25-yr, 24-hr event

Inflow = 48.80 cfs @ 12.18 hrs, Volume= 4.314 af

Outflow = 46.24 cfs @ 12.25 hrs, Volume= 4.314 af, Atten= 5%, Lag= 4.2 min

Routed to Link Swale S2 R2: Swale S2 Reach 2

Routing by Dyn-Stor-Ind method, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

Max. Velocity= 3.41 fps, Min. Travel Time= 3.7 min

Avg. Velocity = 0.75 fps, Avg. Travel Time= 16.7 min

Peak Storage= 10,190 cf @ 12.25 hrs

Average Depth at Peak Storage= 0.98', Surface Width= 17.81'

Bank-Full Depth= 2.00' Flow Area= 36.0 sf, Capacity= 182.04 cfs

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10.00' x 2.00' deep channel, n= 0.030 Earth, grassed & winding Side Slope Z-value= 4.0 '/' Top Width= 26.00' Length= 751.0' Slope= 0.0069 '/' Inlet Invert= 801.30', Outlet Invert= 796.10'



### Summary for Reach S3 R1: Swale S3 Reach 1

Inflow Area = 4.976 ac, 0.00% Impervious, Inflow Depth = 1.89" for 25-yr, 24-hr event

Inflow = 16.31 cfs @ 12.12 hrs, Volume= 0.785 af

Outflow = 15.87 cfs @ 12.13 hrs, Volume= 0.785 af, Atten= 3%, Lag= 0.7 min

Routed to Link Swale S3 R1: Swale S3 Reach 1

Routing by Dyn-Stor-Ind method, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

Max. Velocity= 2.73 fps, Min. Travel Time= 1.3 min Avg. Velocity = 0.67 fps, Avg. Travel Time= 5.4 min

Peak Storage= 1,248 cf @ 12.13 hrs

Average Depth at Peak Storage= 0.63', Surface Width= 10.51' Bank-Full Depth= 2.00' Flow Area= 24.0 sf, Capacity= 125.24 cfs

8.00' x 2.00' deep channel, n= 0.030 Earth, grassed & winding

Side Slope Z-value= 2.0 '/' Top Width= 16.00'

Length= 215.0' Slope= 0.0070 '/'

Inlet Invert= 807.58', Outlet Invert= 806.08'



### Summary for Reach S3 R2: Swale S3 Reach 2

Inflow Area = 10.265 ac, 0.00% Impervious, Inflow Depth = 1.66" for 25-yr, 24-hr event

Inflow = 27.94 cfs @ 12.13 hrs, Volume= 1.419 af

Outflow = 27.78 cfs @ 12.13 hrs, Volume= 1.419 af, Atten= 1%, Lag= 0.3 min

Routed to Link Swale S3 R2: Swale S3 Reach 2

Routing by Dyn-Stor-Ind method, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

Max. Velocity= 3.61 fps, Min. Travel Time= 0.4 min

Avg. Velocity = 1.31 fps, Avg. Travel Time= 1.2 min

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Peak Storage= 745 cf @ 12.13 hrs Average Depth at Peak Storage= 1.75', Surface Width= 8.77'

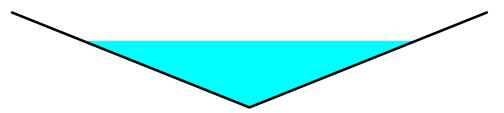
Bank-Full Depth= 2.50' Flow Area= 15.6 sf, Capacity= 71.57 cfs

0.00' x 2.50' deep channel, n= 0.030 Earth, grassed & winding

Side Slope Z-value= 2.5 '/' Top Width= 12.50'

Length= 97.0' Slope= 0.0070 '/'

Inlet Invert= 806.08', Outlet Invert= 805.40'



### Summary for Reach S3 R3: Swale S3 Reach 3

Inflow Area = 11.158 ac, 0.00% Impervious, Inflow Depth = 1.57" for 25-yr, 24-hr event

Inflow = 27.86 cfs @ 12.13 hrs, Volume= 1.464 af

Outflow = 26.59 cfs @ 12.15 hrs, Volume= 1.464 af, Atten= 5%, Lag= 1.0 min

Routed to Link Swale S3 R3 : Swale S3 Reach 3

Routing by Dyn-Stor-Ind method, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

Max. Velocity = 3.34 fps, Min. Travel Time = 1.8 min Avg. Velocity = 0.88 fps, Avg. Travel Time = 6.7 min

Peak Storage= 2,810 cf @ 12.15 hrs

Average Depth at Peak Storage= 0.73', Surface Width= 13.83' Bank-Full Depth= 2.00' Flow Area= 32.0 sf, Capacity= 186.19 cfs

8.00' x 2.00' deep channel, n= 0.030 Earth, grassed & winding

Side Slope Z-value= 4.0 '/' Top Width= 24.00'

Length= 353.0' Slope= 0.0097 '/'

Inlet Invert= 804.71', Outlet Invert= 801.30'



#### Summary for Reach S4 R2: Swale S4 Reach 2

Inflow Area = 4.541 ac, 0.00% Impervious, Inflow Depth = 1.89" for 25-yr, 24-hr event

Inflow = 14.04 cfs @ 12.13 hrs, Volume= 0.716 af

Outflow = 11.87 cfs @ 12.17 hrs, Volume= 0.716 af, Atten= 15%, Lag= 2.1 min

Routed to Reach S4 R3: Swale S4 Reach 3

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs Max. Velocity= 2.23 fps, Min. Travel Time= 4.5 min Avg. Velocity = 0.55 fps, Avg. Travel Time= 18.3 min

Peak Storage= 3,193 cf @ 12.17 hrs Average Depth at Peak Storage= 0.46', Surface Width= 13.21' Bank-Full Depth= 2.00' Flow Area= 34.0 sf, Capacity= 174.20 cfs

10.00' x 2.00' deep channel, n= 0.030 Earth, grassed & winding Side Slope Z-value= 4.0 3.0 '/' Top Width= 24.00' Length= 601.0' Slope= 0.0069 '/' Inlet Invert= 806.43', Outlet Invert= 802.26'



### Summary for Reach S4 R3: Swale S4 Reach 3

[62] Hint: Exceeded Reach S4 R2 OUTLET depth by 0.23' @ 12.28 hrs

Inflow Area = 8.711 ac, 0.00% Impervious, Inflow Depth = 1.89" for 25-yr, 24-hr event

Inflow = 23.93 cfs @ 12.14 hrs, Volume= 1.374 af

Outflow = 18.66 cfs @ 12.20 hrs, Volume= 1.374 af, Atten= 22%, Lag= 3.4 min

Routed to Reach S4 R4: Swale S4 Reach 4

Routing by Dyn-Stor-Ind method, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs Max. Velocity= 2.42 fps, Min. Travel Time= 6.5 min Avg. Velocity = 0.57 fps, Avg. Travel Time= 27.9 min

Peak Storage= 7,289 cf @ 12.20 hrs Average Depth at Peak Storage= 0.63', Surface Width= 14.42' Bank-Full Depth= 2.00' Flow Area= 34.0 sf, Capacity= 156.53 cfs

10.00' x 2.00' deep channel, n= 0.030 Earth, grassed & winding Side Slope Z-value= 3.0 4.0 '/' Top Width= 24.00' Length= 946.0' Slope= 0.0056 '/' Inlet Invert= 802.26', Outlet Invert= 796.96'



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### Summary for Reach S4 R4: Swale S4 Reach 4

[62] Hint: Exceeded Reach S4 R3 OUTLET depth by 0.67' @ 12.27 hrs

Inflow Area = 65.063 ac, 0.04% Impervious, Inflow Depth = 1.31" for 25-yr, 24-hr event

Inflow = 81.28 cfs @ 12.20 hrs, Volume= 7.099 af

Outflow = 80.05 cfs @ 12.23 hrs, Volume= 7.099 af, Atten= 2%, Lag= 1.7 min

Routed to Link Swale S4 R4: Swale S4 Reach 4

Routing by Dyn-Stor-Ind method, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

Max. Velocity= 4.35 fps, Min. Travel Time= 1.9 min Avg. Velocity = 0.97 fps, Avg. Travel Time= 8.3 min

Peak Storage= 8,890 cf @ 12.23 hrs

Average Depth at Peak Storage= 1.27', Surface Width= 18.91'

Bank-Full Depth= 3.00' Flow Area= 61.5 sf, Capacity= 427.66 cfs

10.00' x 3.00' deep channel, n= 0.030 Earth, grassed & winding

Side Slope Z-value= 3.0 4.0 '/' Top Width= 31.00'

Length= 483.0' Slope= 0.0082 '/'

Inlet Invert= 796.96', Outlet Invert= 793.00'



#### Summary for Reach S5 R2: Swale S5 Reach 2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 4.530 ac, 13.14% Impervious, Inflow Depth = 0.51" for 25-yr, 24-hr event

Inflow = 2.06 cfs @ 12.16 hrs, Volume= 0.191 af

Outflow = 2.06 cfs @ 12.16 hrs, Volume= 0.191 af, Atten= 0%, Lag= 0.0 min

Routed to Link Swale S5 R2: Swale S5 Reach 2

Routing by Dyn-Stor-Ind method, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### **Summary for Pond Sed Pond: Sedimentation Basin**

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=42)

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Inflow Area =	74.393 ac,	2.06% Impervious, Inflow I	Depth = 1.27" for 25-yr, 24-hr event
Inflow =	82.78 cfs @	12.23 hrs, Volume=	7.853 af
Outflow =	14.75 cfs @	13.29 hrs, Volume=	7.854 af, Atten= 82%, Lag= 64.1 min
Discarded =	5.33 cfs @	13.29 hrs, Volume=	5.880 af
Primary =	9.42 cfs @	13.29 hrs, Volume=	1.973 af
Routed to Link	: Wetland : We	etland	
Secondary =	0.00 cfs @	0.00 hrs, Volume=	0.000 af
Routed to Link	: Wetland : We	etland	
Tertiary =	0.00 cfs @	0.00 hrs, Volume=	0.000 af
Routed to Link	: Wetland : We	etland	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs Peak Elev= 791.59' @ 13.29 hrs Surf.Area= 63,986 sf Storage= 137,326 cf Flood Elev= 794.00' Surf.Area= 75,797 sf Storage= 304,443 cf

Avail.Storage Storage Description

Plug-Flow detention time= (not calculated: outflow precedes inflow)

Center-of-Mass det. time= 184.8 min ( 1,043.0 - 858.2 )

Invert

VOIGITIC	HIVCH	7 (Vall.Oto	rage Clorage i	Description			
#1	789.00'	304,44	43 cf Custom	Stage Data (P	rismatic)Listed below (Recalc)		
Elevation		.Area	Inc.Store	Cum.Store			
(fee	et) (	sq-ft)	(cubic-feet)	(cubic-feet)			
789.0	00 27	7,325	0	0			
790.0		5,972	41,649	41,649			
791.0		1,532	58,752	100,401			
792.0		5,703	63,618	164,018			
793.0		9,675	67,689	231,707			
794.0	00 7	5,797	72,736	304,443			
Device	Routing	Invert	Outlet Devices	i			
#1	Primary	787.70'	15.0" Round	Culvert			
	•		L= 40.0' RCP	, mitered to cor	nform to fill, Ke= 0.700		
			Inlet / Outlet Invert= 787.70' / 787.50' S= 0.0050 '/' Cc= 0.900				
			n= 0.011 Con	crete pipe, stra	ight & clean, Flow Area= 1.23 sf		
#2	Device 1	791.00'	30.0" Horiz. O	rifice/Grate (	C= 0.600		
				flow at low hea			
#3	Device 1	790.50'	0.8" Vert. Orif				
				flow at low hea			
#4	Device 1	790.00'	0.8" Vert. Orif				
			Limited to weir				
#5	Device 1	789.00'	0.5" Vert. Orif				
				6.0" cc spacing			
	0 1	700 501		flow at low hea			
#6	Secondary	792.50'			road-Crested Rectangular Weir		
					0.80 1.00 1.20 1.40 1.60		
ш <del>-</del>	T	700.001	٠ ,	,	70 2.69 2.68 2.69 2.67 2.64		
#7	Tertiary	793.00'			Broad-Crested Rectangular Weir		
					0.80 1.00 1.20 1.40 1.60		
40	Diogardad	700 001		) 2.49  2.56  2. <b>filtration over</b>	70 2.69 2.68 2.69 2.67 2.64		
#8	Discarded	789.00'	3.000 III/III EX	illuation over	Surface area		

MSE 24-hr 4 25-vr. 24-hr Rainfall=4.91"

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Discarded OutFlow Max=5.33 cfs @ 13.29 hrs HW=791.59' (Free Discharge) **-8=Exfiltration** (Exfiltration Controls 5.33 cfs)

Primary OutFlow Max=9.42 cfs @ 13.29 hrs HW=791.59' TW=0.00' (Dynamic Tailwater)

-1=Culvert (Inlet Controls 9.42 cfs @ 7.67 fps)

**2=Orifice/Grate** (Passes < 11.59 cfs potential flow)

-3=Orifice/Grate (Passes < 0.07 cfs potential flow)

**-4=Orifice/Grate** (Passes < 0.08 cfs potential flow)

-5=Orifice/Grate (Passes < 0.58 cfs potential flow)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=789.00' TW=0.00' (Dynamic Tailwater) -6=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Tertiary OutFlow Max=0.00 cfs @ 0.00 hrs HW=789.00' TW=0.00' (Dynamic Tailwater) 7=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

### Summary for Link C1: Culvert C1

4.530 ac, 13.14% Impervious, Inflow Depth = 0.51" for 25-yr, 24-hr event Inflow Area =

Inflow 2.06 cfs @ 12.16 hrs, Volume= 0.191 af

2.06 cfs @ 12.16 hrs, Volume= 0.191 af, Atten= 0%, Lag= 0.0 min

Routed to Reach S5 R2: Swale S5 Reach 2

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### Summary for Link C2: Culvert C2

Inflow Area = 2.899 ac, 0.00% Impervious, Inflow Depth = 2.15" for 25-yr, 24-hr event

Inflow 9.68 cfs @ 12.11 hrs, Volume= 0.520 af

9.68 cfs @ 12.11 hrs, Volume= 0.520 af, Atten= 0%, Lag= 0.0 min Primary

Routed to Reach S1 R3: Swale S1 Reach 3

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### Summary for Link C3: Culvert C3

14.170 ac, 0.00% Impervious, Inflow Depth = 1.51" for 25-yr, 24-hr event Inflow Area =

27.38 cfs @ 12.15 hrs, Volume= Inflow 1.788 af

27.38 cfs @ 12.15 hrs, Volume= 1.788 af, Atten= 0%, Lag= 0.0 min Primary

Routed to Reach S1 R4: Swale S1 Reach 4

MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

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### **Summary for Link C4: Culvert C4**

Inflow Area = 17.714 ac, 0.00% Impervious, Inflow Depth = 1.53" for 25-yr, 24-hr event

Inflow = 35.39 cfs @ 12.15 hrs, Volume= 2.255 af

Primary = 35.39 cfs @ 12.15 hrs, Volume= 2.255 af, Atten= 0%, Lag= 0.0 min

Routed to Reach S1 R5: Swale S1 Reach 5

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### Summary for Link C5: Culvert C5

Inflow Area = 20.996 ac, 0.00% Impervious, Inflow Depth = 1.39" for 25-yr, 24-hr event

Inflow = 35.21 cfs @ 12.18 hrs, Volume= 2.434 af

Primary = 35.21 cfs @ 12.18 hrs, Volume= 2.434 af, Atten= 0%, Lag= 0.0 min

Routed to Reach S1 R6: Swale S1 Reach 6

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### **Summary for Link C6: Culvert C6**

Inflow Area = 11.158 ac, 0.00% Impervious, Inflow Depth = 1.57" for 25-yr, 24-hr event

Inflow = 27.86 cfs @ 12.13 hrs, Volume= 1.464 af

Primary = 27.86 cfs @ 12.13 hrs, Volume= 1.464 af, Atten= 0%, Lag= 0.0 min

Routed to Reach S3 R3: Swale S3 Reach 3

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### **Summary for Link C7: Culvert C7**

Inflow Area = 48.985 ac, 0.00% Impervious, Inflow Depth = 1.22" for 25-yr, 24-hr event

Inflow = 52.15 cfs @ 12.23 hrs, Volume= 4.999 af

Primary = 52.15 cfs @ 12.23 hrs, Volume= 4.999 af, Atten= 0%, Lag= 0.0 min

Routed to Reach S4 R4: Swale S4 Reach 4

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### **Summary for Link C8: Culvert C8**

Inflow Area = 7.668 ac, 11.88% Impervious, Inflow Depth = 0.89" for 25-yr, 24-hr event

Inflow = 8.32 cfs @ 12.15 hrs, Volume= 0.566 af

Primary = 8.32 cfs @ 12.15 hrs, Volume= 0.566 af, Atten= 0%, Lag= 0.0 min

Routed to Link North Area: North Area

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### **Summary for Link F1: Flume 1**

Inflow Area = 4.170 ac, 0.00% Impervious, Inflow Depth = 1.89" for 25-yr, 24-hr event

Inflow = 13.17 cfs @ 12.13 hrs, Volume= 0.658 af

Primary = 13.17 cfs @ 12.13 hrs, Volume= 0.658 af, Atten= 0%, Lag= 0.0 min

Routed to Link RC1: Rock Chute 1

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### **Summary for Link F2: Flume 2**

Inflow Area = 4.541 ac, 0.00% Impervious, Inflow Depth = 1.89" for 25-yr, 24-hr event

Inflow = 14.04 cfs @ 12.13 hrs, Volume= 0.716 af

Primary = 14.04 cfs @ 12.13 hrs, Volume= 0.716 af, Atten= 0%, Lag= 0.0 min

Routed to Link RC2: Rock Chute 2

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### **Summary for Link F3: Flume 3**

Inflow Area = 5.923 ac, 0.00% Impervious, Inflow Depth = 1.89" for 25-yr, 24-hr event

Inflow = 19.08 cfs @ 12.12 hrs, Volume= 0.934 af

Primary = 19.08 cfs @ 12.12 hrs, Volume= 0.934 af, Atten= 0%, Lag= 0.0 min

Routed to Reach S1 R2: Swale S1 Reach 2

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### **Summary for Link F4: Flume 4**

Inflow Area = 2.645 ac, 0.00% Impervious, Inflow Depth = 1.89" for 25-yr, 24-hr event

Inflow = 8.58 cfs @ 12.12 hrs, Volume= 0.417 af

Primary = 8.58 cfs @ 12.12 hrs, Volume= 0.417 af, Atten= 0%, Lag= 0.0 min

Routed to Reach S1 R4: Swale S1 Reach 4

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### **Summary for Link F5: Flume 5**

Inflow Area = 4.601 ac, 0.00% Impervious, Inflow Depth = 1.89" for 25-yr, 24-hr event

Inflow = 15.06 cfs @ 12.12 hrs, Volume= 0.725 af

Primary = 15.06 cfs @ 12.12 hrs, Volume= 0.725 af, Atten= 0%, Lag= 0.0 min

Routed to Reach S3 R1: Swale S3 Reach 1

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### **Summary for Link F6: Flume 6**

Inflow Area = 3.717 ac, 0.00% Impervious, Inflow Depth = 1.89" for 25-yr, 24-hr event

Inflow = 12.11 cfs @ 12.12 hrs, Volume= 0.586 af

Primary = 12.11 cfs @ 12.12 hrs, Volume= 0.586 af, Atten= 0%, Lag= 0.0 min

Routed to Reach S3 R2 : Swale S3 Reach 2

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### **Summary for Link F7: Existing East Flume**

Inflow Area = 0.830 ac, 0.00% Impervious, Inflow Depth = 1.85" for 25-yr, 24-hr event

Inflow = 2.66 cfs @ 12.12 hrs, Volume= 0.128 af

Primary = 2.66 cfs @ 12.12 hrs, Volume= 0.128 af, Atten= 0%, Lag= 0.0 min

Routed to Reach S2 R2: Swale S2 Reach 2

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### **Summary for Link F8: Existing West Flume**

Inflow Area = 3.122 ac, 0.00% Impervious, Inflow Depth = 1.89" for 25-yr, 24-hr event

Inflow = 9.73 cfs @ 12.13 hrs, Volume= 0.492 af

Primary = 9.73 cfs @ 12.13 hrs, Volume= 0.492 af, Atten= 0%, Lag= 0.0 min

Routed to Link Swale S2 R2 : Swale S2 Reach 2

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### **Summary for Link North Area: North Area**

Inflow Area = 7.668 ac, 11.88% Impervious, Inflow Depth = 0.89" for 25-yr, 24-hr event

Inflow = 8.32 cfs @ 12.15 hrs, Volume= 0.566 af

Primary = 8.32 cfs @ 12.15 hrs, Volume= 0.566 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### **Summary for Link RC1: Rock Chute 1**

Inflow Area = 4.170 ac, 0.00% Impervious, Inflow Depth = 1.89" for 25-yr, 24-hr event

Inflow = 13.17 cfs @ 12.13 hrs, Volume= 0.658 af

Primary = 13.17 cfs @ 12.13 hrs, Volume= 0.658 af, Atten= 0%, Lag= 0.0 min

Routed to Reach S4 R3: Swale S4 Reach 3

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### Summary for Link RC2: Rock Chute 2

Inflow Area = 4.541 ac, 0.00% Impervious, Inflow Depth = 1.89" for 25-yr, 24-hr event

Inflow = 14.04 cfs @ 12.13 hrs, Volume= 0.716 af

Primary = 14.04 cfs @ 12.13 hrs, Volume= 0.716 af, Atten= 0%, Lag= 0.0 min

Routed to Reach S4 R2 : Swale S4 Reach 2

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### Summary for Link Swale 1 R6: Swale S1 Reach 6

Inflow Area = 23.788 ac, 0.00% Impervious, Inflow Depth = 1.25" for 25-yr, 24-hr event

Inflow = 33.18 cfs @ 12.21 hrs, Volume= 2.484 af

Primary = 33.18 cfs @ 12.21 hrs, Volume= 2.484 af, Atten= 0%, Lag= 0.0 min

Routed to Reach S2 R1: Swale S2 Reach 1

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### Summary for Link Swale S1 R1: Swale S1 Reach 1

Inflow Area = 0.691 ac, 0.00% Impervious, Inflow Depth = 1.18" for 25-yr, 24-hr event

Inflow = 1.37 cfs @ 12.12 hrs, Volume= 0.068 af

Primary = 1.37 cfs @ 12.12 hrs, Volume= 0.068 af, Atten= 0%, Lag= 0.0 min

Routed to Reach S1 R2: Swale S1 Reach 2

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### Summary for Link Swale S1 R2: Swale S1 Reach 2

Inflow Area = 7.131 ac, 0.00% Impervious, Inflow Depth = 1.81" for 25-yr, 24-hr event

Inflow = 21.68 cfs @ 12.13 hrs, Volume= 1.077 af

Primary = 21.68 cfs @ 12.13 hrs, Volume= 1.077 af, Atten= 0%, Lag= 0.0 min

Routed to Reach S1 R3: Swale S1 Reach 3

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### Summary for Link Swale S1 R3: Swale S1 Reach 3

Inflow Area = 14.170 ac, 0.00% Impervious, Inflow Depth = 1.51" for 25-yr, 24-hr event

Inflow = 27.38 cfs @ 12.15 hrs, Volume= 1.788 af

Primary = 27.38 cfs @ 12.15 hrs, Volume= 1.788 af, Atten= 0%, Lag= 0.0 min

Routed to Link C3: Culvert C3

MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

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### Summary for Link Swale S1 R4: Swale S1 Reach 4

Inflow Area = 17.714 ac, 0.00% Impervious, Inflow Depth = 1.53" for 25-yr, 24-hr event

Inflow = 35.39 cfs @ 12.15 hrs, Volume= 2.255 af

Primary = 35.39 cfs @ 12.15 hrs, Volume= 2.255 af, Atten= 0%, Lag= 0.0 min

Routed to Link C4: Culvert C4

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### Summary for Link Swale S1 R5: Swale S1 Reach 5

Inflow Area = 20.996 ac, 0.00% Impervious, Inflow Depth = 1.39" for 25-yr, 24-hr event

Inflow = 35.21 cfs @ 12.18 hrs, Volume= 2.434 af

Primary = 35.21 cfs @ 12.18 hrs, Volume= 2.434 af, Atten= 0%, Lag= 0.0 min

Routed to Link C5: Culvert C5

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### Summary for Link Swale S2 R1: Swale S2 Reach 1

Inflow Area = 25.901 ac, 0.00% Impervious, Inflow Depth = 1.17" for 25-yr, 24-hr event

Inflow = 29.95 cfs @ 12.26 hrs, Volume= 2.516 af

Primary = 29.95 cfs @ 12.26 hrs, Volume= 2.516 af, Atten= 0%, Lag= 0.0 min

Routed to Reach S2 R2: Swale S2 Reach 2

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### Summary for Link Swale S2 R2: Swale S2 Reach 2

Inflow Area = 48.985 ac, 0.00% Impervious, Inflow Depth = 1.22" for 25-yr, 24-hr event

Inflow = 52.15 cfs @ 12.23 hrs, Volume= 4.999 af

Primary = 52.15 cfs @ 12.23 hrs, Volume= 4.999 af, Atten= 0%, Lag= 0.0 min

Routed to Link C7: Culvert C7

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### Summary for Link Swale S3 R1: Swale S3 Reach 1

Inflow Area = 6.548 ac, 0.00% Impervious, Inflow Depth = 1.53" for 25-yr, 24-hr event

Inflow = 15.88 cfs @ 12.13 hrs, Volume= 0.833 af

Primary = 15.88 cfs @ 12.13 hrs, Volume= 0.833 af, Atten= 0%, Lag= 0.0 min

Routed to Reach S3 R2: Swale S3 Reach 2

MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

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### Summary for Link Swale S3 R2: Swale S3 Reach 2

Inflow Area = 11.158 ac, 0.00% Impervious, Inflow Depth = 1.57" for 25-yr, 24-hr event

Inflow = 27.86 cfs @ 12.13 hrs, Volume= 1.464 af

Primary = 27.86 cfs @ 12.13 hrs, Volume= 1.464 af, Atten= 0%, Lag= 0.0 min

Routed to Link C6: Culvert C6

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### Summary for Link Swale S3 R3: Swale S3 Reach 3

Inflow Area = 14.511 ac, 0.00% Impervious, Inflow Depth = 1.32" for 25-yr, 24-hr event

Inflow = 26.70 cfs @ 12.15 hrs, Volume= 1.592 af

Primary = 26.70 cfs @ 12.15 hrs, Volume= 1.592 af, Atten= 0%, Lag= 0.0 min

Routed to Reach S2 R2: Swale S2 Reach 2

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### Summary for Link Swale S4 R4: Swale S4 Reach 4

Inflow Area = 67.064 ac, 0.04% Impervious, Inflow Depth = 1.28" for 25-yr, 24-hr event

Inflow = 80.09 cfs @ 12.23 hrs, Volume= 7.154 af

Primary = 80.09 cfs @ 12.23 hrs, Volume= 7.154 af, Atten= 0%, Lag= 0.0 min

Routed to Pond Sed Pond : Sedimentation Basin

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### Summary for Link Swale S5 R1: Swale S5 Reach 1

Inflow Area = 4.530 ac, 13.14% Impervious, Inflow Depth = 0.51" for 25-yr, 24-hr event

Inflow = 2.06 cfs @ 12.16 hrs, Volume= 0.191 af

Primary = 2.06 cfs @ 12.16 hrs, Volume= 0.191 af, Atten= 0%, Lag= 0.0 min

Routed to Link C1: Culvert C1

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### Summary for Link Swale S5 R2: Swale S5 Reach 2

Inflow Area = 5.851 ac, 12.83% Impervious, Inflow Depth = 0.69" for 25-yr, 24-hr event

Inflow = 4.68 cfs @ 12.15 hrs, Volume= 0.336 af

Primary = 4.68 cfs @ 12.15 hrs, Volume= 0.336 af, Atten= 0%, Lag= 0.0 min

Routed to Link C8: Culvert C8

MSE 24-hr 4 25-yr, 24-hr Rainfall=4.91"

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### Summary for Link Swale S5 R3: Swale S5 Reach 3

Inflow Area = 1.817 ac, 8.81% Impervious, Inflow Depth = 1.52" for 25-yr, 24-hr event

Inflow = 3.79 cfs @ 12.17 hrs, Volume= 0.230 af

Primary = 3.79 cfs @ 12.17 hrs, Volume= 0.230 af, Atten= 0%, Lag= 0.0 min

Routed to Link C8: Culvert C8

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### Summary for Link Swale S6 R1: Swale S6 Reach 1

Inflow Area = 2.899 ac, 0.00% Impervious, Inflow Depth = 2.15" for 25-yr, 24-hr event

Inflow = 9.68 cfs @ 12.11 hrs, Volume= 0.520 af

Primary = 9.68 cfs @ 12.11 hrs, Volume= 0.520 af, Atten= 0%, Lag= 0.0 min

Routed to Link C2: Culvert C2

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### **Summary for Link Wetland: Wetland**

Inflow Area = 74.393 ac, 2.06% Impervious, Inflow Depth = 0.32" for 25-yr, 24-hr event

Inflow = 9.42 cfs @ 13.29 hrs, Volume= 1.973 af

Primary = 9.42 cfs @ 13.29 hrs, Volume= 1.973 af, Atten= 0%, Lag= 0.0 min

# COL POO FINAL CONDITIONS MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

### **COL\_POO Closure Conditions-031722**

Subcatchment AREA 23: Subcat AREA 23

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Time span=0.00-40.00 hrs, dt=0.01 hrs, 4001 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method
Subcatchment AREA 1: Subcat AREA 1  Runoff Area=1.288 ac 0.00% Impervious Runoff Depth=3.18" Flow Length=408' Tc=2.6 min CN=69 Runoff=7.63 cfs 0.342 af
Subcatchment AREA 10: Subcat AREA 10 Runoff Area=0.914 ac 0.00% Impervious Runoff Depth=3.18" Flow Length=500' Tc=3.2 min CN=69 Runoff=5.29 cfs 0.242 af
Subcatchment AREA 11: Subcat AREA 11 Runoff Area=0.949 ac 0.00% Impervious Runoff Depth=3.18" Flow Length=391' Tc=4.6 min CN=69 Runoff=5.21 cfs 0.251 af
Subcatchment AREA 12: Subcat AREA 12  Runoff Area=0.098 ac 0.00% Impervious Runoff Depth=3.18" Flow Length=92' Tc=2.5 min CN=69 Runoff=0.58 cfs 0.026 af
Subcatchment AREA 13: Subcat AREA 13 Runoff Area=0.890 ac 0.00% Impervious Runoff Depth=3.18" Flow Length=590' Tc=4.6 min CN=69 Runoff=4.89 cfs 0.236 af
Subcatchment AREA 14: Subcat AREA 14 Runoff Area=1.145 ac 0.00% Impervious Runoff Depth=3.18" Flow Length=625' Tc=5.1 min CN=69 Runoff=6.17 cfs 0.303 af
Subcatchment AREA 15: Subcat AREA 15 Runoff Area=0.512 ac 0.00% Impervious Runoff Depth=3.18" Flow Length=235' Tc=4.2 min CN=69 Runoff=2.86 cfs 0.136 af
Subcatchment AREA 16: Subcat AREA 16 Runoff Area=1.510 ac 0.00% Impervious Runoff Depth=3.18" Flow Length=522' Tc=4.9 min CN=69 Runoff=8.20 cfs 0.400 af
Subcatchment AREA 17: Subcat AREA 17 Runoff Area=1.228 ac 0.00% Impervious Runoff Depth=3.18" Flow Length=386' Tc=4.7 min CN=69 Runoff=6.72 cfs 0.326 af
Subcatchment AREA 18: Subcat AREA 18 Runoff Area=0.813 ac 0.00% Impervious Runoff Depth=3.18" Flow Length=383' Tc=4.6 min CN=69 Runoff=4.47 cfs 0.215 af
Subcatchment AREA 19: Subcat AREA 19 Runoff Area=0.847 ac 0.00% Impervious Runoff Depth=3.18" Flow Length=394' Tc=4.6 min CN=69 Runoff=4.66 cfs 0.225 af
Subcatchment AREA 2: Subcat AREA 2  Runoff Area=1.167 ac 0.00% Impervious Runoff Depth=3.18" Flow Length=613' Tc=5.1 min CN=69 Runoff=6.28 cfs 0.309 af
Subcatchment AREA 20: Subcat AREA 20 Runoff Area=1.054 ac 0.00% Impervious Runoff Depth=3.18" Flow Length=453' Tc=4.7 min CN=69 Runoff=5.77 cfs 0.279 af
Subcatchment AREA 21: Subcat AREA 21  Runoff Area=1.030 ac 0.00% Impervious Runoff Depth=3.18" Flow Length=448' Tc=4.7 min CN=69 Runoff=5.64 cfs 0.273 af
Subcatchment AREA 22: Subcat AREA 22 Runoff Area=1.030 ac 0.00% Impervious Runoff Depth=3.18"

Flow Length=448' Tc=4.7 min CN=69 Runoff=5.64 cfs 0.273 af

Flow Length=715' Tc=5.4 min CN=69 Runoff=8.23 cfs 0.410 af

Runoff Area=1.548 ac 0.00% Impervious Runoff Depth=3.18"

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- Subcatchment AREA 24: Subcat AREA 24 Runoff Area=1.952 ac 0.00% Impervious Runoff Depth=3.18" Flow Length=889' Tc=5.8 min CN=69 Runoff=10.20 cfs 0.517 af
- Subcatchment AREA 25: Subcat AREA 25

  Runoff Area=1.515 ac 0.00% Impervious Runoff Depth=3.18"

  Flow Length=495' Tc=3.9 min CN=69 Runoff=8.59 cfs 0.402 af
- Subcatchment AREA 26: Subcat AREA 26 Runoff Area=0.518 ac 0.00% Impervious Runoff Depth=2.98" Flow Length=216' Tc=4.1 min CN=67 Runoff=2.74 cfs 0.129 af
- Subcatchment AREA 27: Subcat AREA 27 Runoff Area=4.140 ac 0.00% Impervious Runoff Depth=1.28" Flow Length=864' Tc=12.0 min CN=48 Runoff=5.63 cfs 0.442 af
- Subcatchment AREA 28: Subcat AREA 28 Runoff Area=142,960 sf 0.00% Impervious Runoff Depth=1.44" Flow Length=573' Tc=9.1 min CN=50 Runoff=5.98 cfs 0.395 af
- Subcatchment AREA 28A: Subcat AREA 28A Runoff Area=0.423 ac 0.00% Impervious Runoff Depth=1.36" Flow Length=234' Tc=9.1 min CN=49 Runoff=0.71 cfs 0.048 af
- Subcatchment AREA 28B: Subcat AREA 28B Runoff Area=0.476 ac 0.00% Impervious Runoff Depth=1.53" Flow Length=211' Tc=4.5 min CN=51 Runoff=1.20 cfs 0.061 af
- Subcatchment AREA 29: Subcat AREA 29 Runoff Area=2.792 ac 0.00% Impervious Runoff Depth=0.69" Flow Length=463' Tc=14.8 min CN=40 Runoff=1.21 cfs 0.161 af
- Subcatchment AREA 3: Subcat AREA 3

  Runoff Area=0.717 ac 0.00% Impervious Runoff Depth=3.18"
  Flow Length=409' Tc=6.3 min CN=69 Runoff=3.66 cfs 0.190 af
- Subcatchment AREA 30: Subcat AREA 30 Runoff Area=1.415 ac 0.00% Impervious Runoff Depth=0.63" Flow Length=941' Slope=0.0260 '/' Tc=22.0 min CN=39 Runoff=0.43 cfs 0.074 af
- Subcatchment AREA 31: Subcat AREA 31 Runoff Area=0.698 ac 0.00% Impervious Runoff Depth=0.63" Flow Length=481' Tc=4.4 min CN=39 Runoff=0.42 cfs 0.036 af
- Subcatchment AREA 32: Subcat AREA 32 Runoff Area=3.353 ac 0.00% Impervious Runoff Depth=1.13" Flow Length=663' Tc=17.3 min CN=46 Runoff=3.11 cfs 0.315 af
- Subcatchment AREA 33: Subcat AREA 33 Runoff Area=38,914 sf 0.00% Impervious Runoff Depth=1.36" Flow Length=377' Tc=16.0 min CN=49 Runoff=1.14 cfs 0.101 af
- Subcatchment AREA 34: Subcat AREA 34 Runoff Area=68,484 sf 0.00% Impervious Runoff Depth=0.98" Flow Length=488' Tc=16.2 min CN=44 Runoff=1.20 cfs 0.128 af
- Subcatchment AREA 35: Subcat AREA 35

  Runoff Area=0.375 ac 0.00% Impervious Runoff Depth=3.18"

  Flow Length=174' Slope=0.2500 '/' Tc=4.2 min CN=69 Runoff=2.10 cfs 0.099 af
- Subcatchment AREA 36: Subcat AREA 36

  Runoff Area=0.487 ac 0.00% Impervious Runoff Depth=3.08"

  Flow Length=425' Tc=4.4 min CN=68 Runoff=2.62 cfs 0.125 af
- Subcatchment AREA 37: Subcat AREA 37 Runoff Area=0.344 ac 0.00% Impervious Runoff Depth=3.18" Flow Length=510' Tc=4.6 min CN=69 Runoff=1.89 cfs 0.091 af

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Subcatchment AREA 38: Subcat AREA 38 Runoff Area=0.223 ac 0.00% Impervious Runoff Depth=3.18" Flow Length=590' Tc=4.1 min CN=69 Runoff=1.25 cfs 0.059 af

Subcatchment AREA 39: Subcat AREA 39

Runoff Area=0.656 ac 0.00% Impervious Runoff Depth=3.18"

Flow Length=642' Tc=5.3 min CN=69 Runoff=3.50 cfs 0.174 af

Subcatchment AREA 4: Subcat AREA 4

Runoff Area=1.247 ac 0.00% Impervious Runoff Depth=3.18"

Flow Length=478' Tc=6.6 min CN=69 Runoff=6.31 cfs 0.331 af

Subcatchment AREA 40: Subcat AREA 40 Runoff Area=1.618 ac 0.00% Impervious Runoff Depth=2.23" Flow Length=699' Tc=5.2 min CN=59 Runoff=6.03 cfs 0.300 af

Subcatchment AREA 41: Subcat AREA 41 Runoff Area=0.826 ac 0.00% Impervious Runoff Depth=2.13" Flow Length=722' Tc=5.9 min CN=58 Runoff=2.84 cfs 0.147 af

Subcatchment AREA 42: Subcat AREA 42 Runoff Area=2.177 ac 0.00% Impervious Runoff Depth=0.63" Flow Length=415' Tc=9.1 min CN=39 Runoff=0.93 cfs 0.114 af

Subcatchment AREA 43: Subcat AREA 43 Runoff Area=1.228 ac 0.00% Impervious Runoff Depth=3.18" Flow Length=778' Tc=5.9 min CN=69 Runoff=6.39 cfs 0.325 af

Subcatchment AREA 44: Subcat AREA 44 Runoff Area=5.227 ac 0.00% Impervious Runoff Depth=0.63" Flow Length=701' Tc=7.9 min CN=39 Runoff=2.38 cfs 0.273 af

Subcatchment AREA 44A: Subcat AREA Runoff Area=1.508 ac 100.00% Impervious Runoff Depth=6.35" Tc=0.0 min CN=98 Runoff=14.38 cfs 0.798 af

Subcatchment AREA 44B: Subcat AREA 44B Runoff Area=0.594 ac 0.00% Impervious Runoff Depth=1.44" Flow Length=147' Slope=0.0544 '/' Tc=7.6 min CN=50 Runoff=1.17 cfs 0.071 af

Subcatchment AREA 45: Subcat AREA 45 Runoff Area=2.001 ac 0.00% Impervious Runoff Depth=0.90" Flow Length=681' Tc=21.9 min CN=43 Runoff=1.16 cfs 0.150 af

Subcatchment AREA 46: Subcat AREA 46 Runoff Area=7.367 ac 0.36% Impervious Runoff Depth=2.23" Flow Length=1,904' Tc=9.2 min CN=59 Runoff=22.74 cfs 1.366 af

Subcatchment AREA 47: Subcat AREA 47 Runoff Area=79,132 sf 8.81% Impervious Runoff Depth=2.69" Flow Length=582' Tc=9.1 min CN=64 Runoff=6.90 cfs 0.408 af

Subcatchment AREA 48: Subcat AREA 48 Runoff Area=57,540 sf 11.76% Impervious Runoff Depth=2.41" Flow Length=489' Tc=5.4 min CN=61 Runoff=5.30 cfs 0.265 af

Subcatchment AREA 49: Subcat AREA 49 Runoff Area=0.691 ac 0.00% Impervious Runoff Depth=2.23" Flow Length=522' Tc=4.3 min CN=59 Runoff=2.68 cfs 0.128 af

Subcatchment AREA 5: Subcat AREA 5

Runoff Area=1.195 ac 0.00% Impervious Runoff Depth=3.18"

Flow Length=482' Tc=6.6 min CN=69 Runoff=6.05 cfs 0.317 af

Subcatchment AREA 50: Subcat AREA 50 Runoff Area=1.482 ac 0.00% Impervious Runoff Depth=5.65" Flow Length=570' Tc=3.4 min CN=92 Runoff=13.35 cfs 0.698 af

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- Subcatchment AREA 51: Subcat AREA 51 Runoff Area=1.417 ac 0.00% Impervious Runoff Depth=0.69" Flow Length=884' Tc=12.2 min CN=40 Runoff=0.67 cfs 0.082 af
- Subcatchment AREA 52: Subcat AREA 52 Runoff Area=197,330 sf 13.14% Impervious Runoff Depth=1.20" Flow Length=1,294' Tc=6.3 min CN=47 Runoff=7.48 cfs 0.454 af
- Subcatchment AREA 6: Subcat AREA 6

  Runoff Area=0.892 ac 0.00% Impervious Runoff Depth=3.18"

  Flow Length=415' Tc=4.6 min CN=69 Runoff=4.90 cfs 0.236 af
- Subcatchment AREA 7: Subcat AREA 7

  Runoff Area=1.017 ac 0.00% Impervious Runoff Depth=3.18"
  Flow Length=833' Tc=5.8 min CN=69 Runoff=5.31 cfs 0.269 af
- Subcatchment AREA 8: Subcat AREA 8

  Runoff Area=1.009 ac 0.00% Impervious Runoff Depth=3.18"

  Flow Length=409' Tc=4.7 min CN=69 Runoff=5.52 cfs 0.268 af
- Subcatchment AREA 9: Subcat AREA 9

  Runoff Area=1.047 ac 0.00% Impervious Runoff Depth=3.18"

  Flow Length=426' Tc=4.8 min CN=69 Runoff=5.71 cfs 0.278 af
- **Reach S1 R2: Swale S1 Reach 2** Avg. Flow Depth=1.01' Max Vel=3.03 fps Inflow=37.51 cfs 1.827 af n=0.030 L=127.0' S=0.0055 '/' Capacity=140.64 cfs Outflow=37.05 cfs 1.827 af
- Reach S1 R3: Swale S1 Reach 3 Avg. Flow Depth=1.18' Max Vel=3.17 fps Inflow=53.22 cfs 3.049 af n=0.030 L=578.0' S=0.0051 '/' Capacity=135.10 cfs Outflow=47.76 cfs 3.049 af
- **Reach S1 R4: Swale S1 Reach 4** Avg. Flow Depth=1.26' Max Vel=3.74 fps Inflow=62.37 cfs 3.811 af n=0.030 L=195.8' S=0.0066 '/' Capacity=154.36 cfs Outflow=61.58 cfs 3.811 af
- **Reach S1 R5: Swale S1 Reach 5** Avg. Flow Depth=1.31' Max Vel=3.42 fps Inflow=62.23 cfs 3.859 af n=0.030 L=411.6' S=0.0053'/ Capacity=137.86 cfs Outflow=59.21 cfs 3.859 af
- **Reach S1 R6: Swale S1 Reach 6** Avg. Flow Depth=1.36' Max Vel=3.44 fps Inflow=65.66 cfs 4.415 af n=0.030 L=430.9' S=0.0052 '/' Capacity=136.28 cfs Outflow=62.73 cfs 4.415 af
- **Reach S2 R1: Swale S2 Reach 1** Avg. Flow Depth=1.65' Max Vel=2.39 fps Inflow=62.82 cfs 4.489 af n=0.030 L=472.0' S=0.0020'/' Capacity=84.99 cfs Outflow=57.87 cfs 4.489 af
- **Reach S2 R2: Swale S2 Reach 2** Avg. Flow Depth=1.40' Max Vel=4.16 fps Inflow=95.28 cfs 7.736 af n=0.030 L=751.0' S=0.0069 '/' Capacity=182.04 cfs Outflow=90.88 cfs 7.736 af
- **Reach S3 R1: Swale S3 Reach 1** Avg. Flow Depth=0.85' Max Vel=3.26 fps Inflow=27.41 cfs 1.319 af n=0.030 L=215.0' S=0.0070 '/' Capacity=125.24 cfs Outflow=26.88 cfs 1.319 af
- **Reach S3 R2: Swale S3 Reach 2** Avg. Flow Depth=2.14' Max Vel=4.13 fps Inflow=47.52 cfs 2.432 af n=0.030 L=97.0' S=0.0070 '/' Capacity=71.57 cfs Outflow=47.32 cfs 2.432 af
- **Reach S3 R3: Swale S3 Reach 3** Avg. Flow Depth=0.98' Max Vel=3.94 fps Inflow=47.83 cfs 2.533 af n=0.030 L=353.0' S=0.0097 '/' Capacity=186.19 cfs Outflow=46.22 cfs 2.533 af
- **Reach S4 R2: Swale S4 Reach 2** Avg. Flow Depth=0.63' Max Vel=2.70 fps Inflow=23.68 cfs 1.204 af n=0.030 L=601.0' S=0.0069 '/' Capacity=174.20 cfs Outflow=20.91 cfs 1.204 af

#### **COL POO FINAL CONDITIONS**

#### **COL POO Closure Conditions-031722**

MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

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**Reach S4 R3: Swale S4 Reach 3** Avg. Flow Depth=0.89' Max Vel=2.94 fps Inflow=41.60 cfs 2.309 af n=0.030 L=946.0' S=0.0056 '/' Capacity=156.53 cfs Outflow=34.31 cfs 2.309 af

**Reach S4 R4: Swale S4 Reach 4** Avg. Flow Depth=1.82' Max Vel=5.29 fps Inflow=159.67 cfs 12.653 af n=0.030 L=483.0' S=0.0082 '/' Capacity=427.66 cfs Outflow=157.44 cfs 12.653 af

Reach S5 R2: Swale S5 Reach 2 Inflow=7.48 cfs 0.454 af Outflow=7.48 cfs 0.454 af

Pond Sed Pond: Sedimentation Basin Peak Elev=793.06' Storage=236,005 cf Inflow=164.77 cfs 13.946 af .167 af Primary=11.35 cfs 4.914 af Secondary=22.50 cfs 1.762 af Tertiary=6.00 cfs 0.104 af Outflow=45.68 cfs 13.947 af

Link C1: Culvert C1	Inflow=7.48 cfs 0.454 af Primary=7.48 cfs 0.454 af
Link C2: Culvert C2	Inflow=13.45 cfs 0.780 af Primary=13.45 cfs 0.780 af
Link C3: Culvert C3	Inflow=47.76 cfs 3.049 af
Link C4: Culvert C4	Primary=47.76 cfs 3.049 af  Inflow=62.23 cfs 3.859 af
Link C5: Culvert C5	Primary=62.23 cfs 3.859 af  Inflow=65.15 cfs 4.254 af
Link C6: Culvert C6	Primary=65.15 cfs 4.254 af  Inflow=47.83 cfs 2.533 af
Link C7: Culvert C7	Primary=47.83 cfs 2.533 af  Inflow=103.37 cfs 8.978 af
Link C8: Culvert C8	Primary=103.37 cfs 8.978 af  Inflow=19.20 cfs 1.127 af
Link F1: Flume 1	Primary=19.20 cfs 1.127 af Inflow=22.19 cfs 1.105 af
Link F2: Flume 2	Primary=22.19 cfs 1.105 af Inflow=23.68 cfs 1.204 af
Link F3: Flume 3	Primary=23.68 cfs 1.204 af Inflow=32.10 cfs 1.570 af
Link F4: Flume 4	Primary=32.10 cfs 1.570 af Inflow=14.43 cfs 0.701 af
Link F5: Flume 5	Primary=14.43 cfs 0.701 af Inflow=25.31 cfs 1.219 af
	Primary=25.31 cfs 1.219 af

MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

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Link F6: Flume 6	Inflow=20.36 cfs 0.985 af Primary=20.36 cfs 0.985 af
Link F7: Existing East Flume	Inflow=4.50 cfs 0.216 af Primary=4.50 cfs 0.216 af
Link F8: Existing West Flume	Inflow=16.40 cfs 0.828 af Primary=16.40 cfs 0.828 af
Link North Area: North Area	Inflow=19.20 cfs 1.127 af Primary=19.20 cfs 1.127 af
Link RC1: Rock Chute 1	Inflow=22.19 cfs 1.105 af Primary=22.19 cfs 1.105 af
Link RC2: Rock Chute 2	Inflow=23.68 cfs 1.204 af Primary=23.68 cfs 1.204 af
Link Swale 1 R6: Swale S1 Reach 6	Inflow=62.73 cfs 4.415 af Primary=62.73 cfs 4.415 af
Link Swale S1 R1: Swale S1 Reach 1	Inflow=2.68 cfs 0.128 af Primary=2.68 cfs 0.128 af
Link Swale S1 R2: Swale S1 Reach 2	Inflow=37.05 cfs 1.827 af Primary=37.05 cfs 1.827 af
Link Swale S1 R3: Swale S1 Reach 3	Inflow=47.76 cfs 3.049 af Primary=47.76 cfs 3.049 af
Link Swale S1 R4: Swale S1 Reach 4	Inflow=62.23 cfs 3.859 af Primary=62.23 cfs 3.859 af
Link Swale S1 R5: Swale S1 Reach 5	Inflow=65.15 cfs 4.254 af Primary=65.15 cfs 4.254 af
Link Swale S2 R1: Swale S2 Reach 1	Inflow=58.13 cfs 4.525 af Primary=58.13 cfs 4.525 af
Link Swale S2 R2: Swale S2 Reach 2	Inflow=103.37 cfs 8.978 af Primary=103.37 cfs 8.978 af
Link Swale S3 R1: Swale S3 Reach 1	Inflow=27.22 cfs 1.447 af Primary=27.22 cfs 1.447 af
Link Swale S3 R2: Swale S3 Reach 2	Inflow=47.83 cfs 2.533 af Primary=47.83 cfs 2.533 af
Link Swale S3 R3: Swale S3 Reach 3	Inflow=47.45 cfs 2.848 af Primary=47.45 cfs 2.848 af

**COL POO FINAL CONDITIONS** 

Inflow=39.85 cfs 6.780 af Primary=39.85 cfs 6.780 af

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Link Swale S4 R4: Swale S4 Reach 4	Inflow=157.92 cfs 12.803 af Primary=157.92 cfs 12.803 af
Link Swale S5 R1: Swale S5 Reach 1	Inflow=7.48 cfs 0.454 af Primary=7.48 cfs 0.454 af
Link Swale S5 R2: Swale S5 Reach 2	Inflow=12.65 cfs 0.720 af Primary=12.65 cfs 0.720 af
Link Swale S5 R3: Swale S5 Reach 3	Inflow=6.90 cfs 0.408 af Primary=6.90 cfs 0.408 af
Link Swale S6 R1: Swale S6 Reach 1	Inflow=13.45 cfs 0.780 af Primary=13.45 cfs 0.780 af

**Link Wetland: Wetland** 

Total Runoff Area = 82.060 ac Runoff Volume = 15.074 af Average Runoff Depth = 2.20" 97.02% Pervious = 79.615 ac 2.98% Impervious = 2.446 ac Prepared by SCS Engineers

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### **Summary for Subcatchment AREA 1: Subcat AREA 1**

Runoff = 7.63 cfs @ 12.11 hrs, Volume= 0.342 af, Depth= 3.18"

Routed to Link F3: Flume 3

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

	Area	(ac) C	N Desc	cription		
	1.	.288 6	9 Past	ure/grassla	and/range,	Fair, HSG B
	1.	.288	100.	00% Pervi	ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	1.7	37	0.2500	0.36		Sheet Flow,
_	0.9	371	0.0200	6.74	80.87	Grass: Short n= 0.150 P2= 2.77"  Trap/Vee/Rect Channel Flow, Diversion Berm  Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00' n= 0.030 Earth, grassed & winding
	2.6	408	Total			

### **Summary for Subcatchment AREA 10: Subcat AREA 10**

Runoff = 5.29 cfs @ 12.11 hrs, Volume= 0.242 af, Depth= 3.18"

Routed to Link F5 : Flume 5

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

	Area	(ac) C	N Desc	cription		
	0.	914 6	9 Past	ure/grassla	and/range,	Fair, HSG B
_	0.	914	100.	00% Pervi	ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	2.1	46	0.2500	0.37		Sheet Flow,
	1.1	454	0.0200	6.74	80.87	Grass: Short n= 0.150 P2= 2.77"  Trap/Vee/Rect Channel Flow, Diversion Berm  Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00' n= 0.030 Earth, grassed & winding
	3.2	500	Total			

### **Summary for Subcatchment AREA 11: Subcat AREA 11**

Runoff = 5.21 cfs @ 12.12 hrs, Volume= 0.251 af, Depth= 3.18"

Routed to Link F5: Flume 5

MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

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_	Area	(ac) C	N Desc	cription		
	0.	949 6	9 Past	ure/grassl	and/range,	Fair, HSG B
	0.	949	100.	00% Pervi	ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	3.8	100	0.2500	0.43		Sheet Flow,
	0.1	14	0.2500	3.50		Grass: Short n= 0.150 P2= 2.77"  Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
	0.7	277	0.0200	6.74	80.87	Trap/Vee/Rect Channel Flow, Diversion Berm Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00' n= 0.030 Earth, grassed & winding
	4.6	391	Total			

### **Summary for Subcatchment AREA 12: Subcat AREA 12**

Runoff = 0.58 cfs @ 12.11 hrs, Volume= 0.026 af, Depth= 3.18"

Routed to Link F4: Flume 4

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

Area	(ac) C	N Desc	cription		
0.	.098 6	9 Past	ure/grassla	and/range,	Fair, HSG B
0.	.098	100.	00% Pervi	ous Area	
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.4	56	0.2500	0.39	, ,	Sheet Flow,
0.1	36	0.0200	6.74	80.87	Grass: Short n= 0.150 P2= 2.77"  Trap/Vee/Rect Channel Flow, Diversion Berm  Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00' n= 0.030 Earth, grassed & winding
2.5	92	Total			

### **Summary for Subcatchment AREA 13: Subcat AREA 13**

Runoff = 4.89 cfs @ 12.12 hrs, Volume= 0.236 af, Depth= 3.18" Routed to Link F4 : Flume 4

MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

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	Area	(ac) C	N Desc	cription					
0.890 69 Pasture/grassland/range, Fair, HSG B									
	0.	.890	100.	00% Pervi	ous Area				
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
_	3.4	87	0.2500	0.42		Sheet Flow,			
	1.2	503	0.0200	6.74	80.87	Grass: Short n= 0.150 P2= 2.77"  Trap/Vee/Rect Channel Flow, Diversion Berm  Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00' n= 0.030 Earth, grassed & winding			
	4.6	590	Total						

### **Summary for Subcatchment AREA 14: Subcat AREA 14**

Runoff = 6.17 cfs @ 12.13 hrs, Volume=

0.303 af, Depth= 3.18"

Routed to Link F4: Flume 4

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

	Area	(ac) C	N Des	cription						
	1.145 69 Pasture/grassland/range, Fair, HSG B									
1.145 100.00% Pervious Area										
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
	3.8	100	0.2500	0.43		Sheet Flow,				
	0.1	27	0.2500	3.50		Grass: Short n= 0.150 P2= 2.77"  Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps				
	1.2	498	0.0200	6.74	80.87	Trap/Vee/Rect Channel Flow, Diversion Berm Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00' n= 0.030 Earth, grassed & winding				
_	5 1	625	Total							

### **Summary for Subcatchment AREA 15: Subcat AREA 15**

Runoff = 2.86 cfs @ 12.12 hrs, Volume= 0.136 af, Depth= 3.18"

Routed to Link F4: Flume 4

_	Area (ac)	CN	Description
_	0.512	69	Pasture/grassland/range, Fair, HSG B
	0.512		100.00% Pervious Area

MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	3.8	100	0.2500	0.43	, ,	Sheet Flow,
	0.2	50	0.2500	3.50		Grass: Short n= 0.150 P2= 2.77"  Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
	0.2	85	0.0200	6.74	80.87	Trap/Vee/Rect Channel Flow, Diversion Berm Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00'
_						n= 0.030 Earth, grassed & winding
	4.2	235	Total			

#### **Summary for Subcatchment AREA 16: Subcat AREA 16**

Runoff = 8.20 cfs @ 12.12 hrs, Volume= 0.400 af, Depth= 3.18"

Routed to Link F5: Flume 5

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

_	Area	(ac) C	N Desc	cription		
	1.	Fair, HSG B				
1.510 100.00% Pervious Area						
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	3.8	100	0.2500	0.43		Sheet Flow,
	0.2	50	0.2500	3.50		Grass: Short n= 0.150 P2= 2.77"  Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
	0.9	372	0.0200	6.74	80.87	Trap/Vee/Rect Channel Flow, Diversion Berm Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00' n= 0.030 Earth, grassed & winding
-	4.9	522	Total			o.oo za.a., g.aood a Willamg

# **Summary for Subcatchment AREA 17: Subcat AREA 17**

Runoff = 6.72 cfs @ 12.12 hrs, Volume= 0.326 af, Depth= 3.18"

Routed to Link F5: Flume 5

_	Area (ac)	CN	Description
	1.228	69	Pasture/grassland/range, Fair, HSG B
Ī	1.228		100.00% Pervious Area

MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.8	100	0.2500	0.43		Sheet Flow,
0.3	63	0.2500	3.50		Grass: Short n= 0.150 P2= 2.77"  Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
0.6	223	0.0200	6.74	80.87	Trap/Vee/Rect Channel Flow, Diversion Berm Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00' n= 0.030 Earth, grassed & winding
4.7	386	Total			

#### **Summary for Subcatchment AREA 18: Subcat AREA 18**

Runoff = 4.47 cfs @ 12.12 hrs, Volume= 0.215

0.215 af, Depth= 3.18"

Routed to Link F6: Flume 6

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

_	Area	(ac) C	N Desc	cription		
	0.	Fair, HSG B				
_	0.	813	100.	00% Pervi	ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	3.8	100	0.2500	0.43		Sheet Flow,
	0.2	48	0.2500	3.50		Grass: Short n= 0.150 P2= 2.77"  Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
	0.6	235	0.0200	6.74	80.87	Trap/Vee/Rect Channel Flow, Diversion Berm Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00'
_						n= 0.030 Earth, grassed & winding
	4.6	383	Total			

# **Summary for Subcatchment AREA 19: Subcat AREA 19**

Runoff = 4.66 cfs @ 12.12 hrs, Volume= 0.225 af, Depth= 3.18"

Routed to Link F6: Flume 6

_	Area (ac)	CN	Description
	0.847	69	Pasture/grassland/range, Fair, HSG B
	0.847		100.00% Pervious Area

MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
-	3.8	100	0.2500	0.43		Sheet Flow,
	0.2	50	0.2500	3.50		Grass: Short n= 0.150 P2= 2.77"  Shallow Concentrated Flow,
	0.6	244	0.0200	6.74	80.87	Short Grass Pasture Kv= 7.0 fps  Trap/Vee/Rect Channel Flow, Diversion Berm
						Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00' n= 0.030 Earth, grassed & winding
_	4.6	394	Total			

#### **Summary for Subcatchment AREA 2: Subcat AREA 2**

Runoff = 6.28 cfs @ 12.13 hrs, Volume= 0.309 af, Depth= 3.18"

Routed to Link F3: Flume 3

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

_	Area	(ac) C	N Desc	cription		
	Fair, HSG B					
	1.	167	100.	00% Pervi	ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	3.8	100	0.2500	0.43		Sheet Flow,
	0.1	18	0.2500	3.50		Grass: Short n= 0.150 P2= 2.77"  Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
	1.2	495	0.0200	6.74	80.87	Trap/Vee/Rect Channel Flow, Diversion Berm
						Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00'
_						n= 0.030 Earth, grassed & winding
	5.1	613	Total			

# **Summary for Subcatchment AREA 20: Subcat AREA 20**

Runoff = 5.77 cfs @ 12.12 hrs, Volume= 0.279 af, Depth= 3.18"

Routed to Link F1: Flume 1

	Area (ac)	CN	Description
	1.054	69	Pasture/grassland/range, Fair, HSG B
Ī	1.054		100.00% Pervious Area

MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	3.8	100	0.2500	0.43		Sheet Flow,
			0.0500	0.50		Grass: Short n= 0.150 P2= 2.77"
	0.2	50	0.2500	3.50		Shallow Concentrated Flow,
	0.7	202	0.0200	6.74	90.97	Short Grass Pasture Kv= 7.0 fps
	0.7	303	0.0200	6.74	80.87	Trap/Vee/Rect Channel Flow, Diversion Berm Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00'
						n= 0.030 Earth, grassed & winding
_	4.7	453	Total			c.ccca, g.accca a. milanig

#### **Summary for Subcatchment AREA 21: Subcat AREA 21**

Runoff = 5.64 cfs @ 12.12 hrs, Volume= 0.273 af, Depth= 3.18"

Routed to Link F1: Flume 1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

	Area	(ac) C	N Desc	cription		
	Fair, HSG B					
	1.	.030	100.	00% Pervi	ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	3.8	100	0.2500	0.43		Sheet Flow,
	0.2	50	0.2500	3.50		Grass: Short n= 0.150 P2= 2.77"  Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
	0.7	298	0.0200	6.74	80.87	Trap/Vee/Rect Channel Flow, Diversion Berm
_						Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00' n= 0.030 Earth, grassed & winding
	4.7	448	Total			

# **Summary for Subcatchment AREA 22: Subcat AREA 22**

Runoff = 5.64 cfs @ 12.12 hrs, Volume= 0.273 af, Depth= 3.18"

Routed to Link F2: Flume 2

_	Area (ac)	CN	Description
	1.030	69	Pasture/grassland/range, Fair, HSG B
Ī	1.030		100.00% Pervious Area

MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	3.8	100	0.2500	0.43		Sheet Flow, Grass: Short n= 0.150 P2= 2.77"
	0.2	50	0.2500	3.50		Shallow Concentrated Flow,
	0.7	298	0.0200	6.74	80.87	Short Grass Pasture Kv= 7.0 fps Trap/Vee/Rect Channel Flow, Diversion Berm
						Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00' n= 0.030 Earth, grassed & winding
-	4.7	448	Total			11- 0.000 Larai, grassea & winding

#### **Summary for Subcatchment AREA 23: Subcat AREA 23**

Runoff = 8.23 cfs @ 12.13 hrs, Volume= 0.410 af, Depth= 3.18"

Routed to Link F2: Flume 2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

_	Area	(ac) C	N Desc	cription				
1.548 69 Pasture/grassland/range, Fair, HSG B								
	1.	.548	100.	00% Pervi	ous Area			
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
	3.8	100	0.2500	0.43		Sheet Flow,		
	0.1	24	0.2500	3.50		Grass: Short n= 0.150 P2= 2.77"  Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps		
	1.5	591	0.0200	6.74	80.87	Trap/Vee/Rect Channel Flow, Diversion Berm Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00' n= 0.030 Earth, grassed & winding		
	5.4	715	Total					

# **Summary for Subcatchment AREA 24: Subcat AREA 24**

Runoff = 10.20 cfs @ 12.13 hrs, Volume= 0.517 af, Depth= 3.18"

Routed to Link F3: Flume 3

Area (ac)	CN	Description
1.952	69	Pasture/grassland/range, Fair, HSG B
1.952		100.00% Pervious Area

MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	3.8	100	0.2500	0.43	, , ,	Sheet Flow, Grass: Short n= 0.150 P2= 2.77"
	0.1	24	0.2500	3.50		Shallow Concentrated Flow,
	1.9	765	0.0200	6.74	80.87	Short Grass Pasture Kv= 7.0 fps  Trap/Vee/Rect Channel Flow, Diversion Berm
						Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00' n= 0.030 Earth, grassed & winding
-	5.8	889	Total			

# **Summary for Subcatchment AREA 25: Subcat AREA 25**

Runoff = 8.59 cfs @ 12.12 hrs, Volume= 0.402 af, Depth= 3.18"

Routed to Link F3: Flume 3

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

_	Area	(ac) C	N Desc	cription		
	1.	Fair, HSG B				
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	2.8	67	0.2500	0.40		Sheet Flow,
	1.1	428	0.0200	6.74	80.87	Grass: Short n= 0.150 P2= 2.77" <b>Trap/Vee/Rect Channel Flow,</b> Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00' n= 0.030 Earth, grassed & winding
_	3.9	495	Total			

# **Summary for Subcatchment AREA 26: Subcat AREA 26**

Runoff = 2.74 cfs @ 12.12 hrs, Volume= 0.129 af, Depth= 2.98"

Routed to Reach S1 R2 : Swale S1 Reach 2

	Area (ac)	CN	Description		
	0.396	0.396 69 Pasture/grassland/range, Fair, HSG B			
	0.072 39 Pasture/grassland/range, Good, HSG A				
	0.049	96	Gravel surface, HSG A		
*	0.000	0	Pasture/grassland/range, Fair		
	0.518	67	Weighted Average		
	0.518		100.00% Pervious Area		

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	3.6	93	0.2500	0.43		Sheet Flow,
_	0.5	123	0.0055	4.39	140.49	Grass: Short n= 0.150 P2= 2.77"  Trap/Vee/Rect Channel Flow, Swale 1 Reach 2  Bot.W=8.00' D=2.00' Z= 4.0 '/' Top.W=24.00'  n= 0.030 Earth, grassed & winding
	4.1	216	Total			

#### **Summary for Subcatchment AREA 27: Subcat AREA 27**

Runoff = 5.63 cfs @ 12.22 hrs, Volume= 0.442 af, Depth= 1.28"

Routed to Reach S1 R3: Swale S1 Reach 3

_	Area	(ac)	CN	Desc	cription							
	0.	651	69	Past	ure/grassla	and/range,	Fair, HSG B					
		758	39				Good, HSG A					
		010	96		Gravel surface, HSG A							
		295	96		Gravel surface, HSG A							
		426	39	Past	ure/grassla	and/range,	Good, HSG A					
*		000	0									
*	_	000	0									
*		000	0	, HS								
*		000	0	, HS								
*		000	0	, HS								
*		000	0	, HS			Cand					
_		000	0			and/range,	G000					
		140	48		hted Aver							
	4.140 100.00% Pervious Area					ous Area						
	Тс	Lengtl	h .	Slope	Velocity	Capacity	Description					
	(min)	(feet		(ft/ft)	(ft/sec)	(cfs)	Boompton					
_	7.3	100		.0500	0.23	(===)	Sheet Flow,					
				.0000	0.20		Grass: Short n= 0.150 P2= 2.77"					
	2.3	21	7 0	.0500	1.57		Shallow Concentrated Flow,					
							Short Grass Pasture Kv= 7.0 fps					
	0.3	20	0 0	.0050	1.14		Shallow Concentrated Flow,					
							Unpaved Kv= 16.1 fps					
	0.1	14	4 0	.2500	3.50		Shallow Concentrated Flow,					
							Short Grass Pasture Kv= 7.0 fps					
	2.0	513	3 0	.0051	4.23	135.28	Trap/Vee/Rect Channel Flow, Swale 1 Reach 3					
							Bot.W=8.00' D=2.00' Z= 4.0 '/' Top.W=24.00'					
_							n= 0.030 Earth, grassed & winding					
	12.0	864	4 T	otal								

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#### Summary for Subcatchment AREA 28: Subcat AREA 28

Runoff = 5.98 cfs @ 12.18 hrs, Volume=

0.395 af, Depth= 1.44"

Routed to Link Swale S1 R5 : Swale S1 Reach 5

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

	Α	rea (sf)	CN D	escription				
30,267 69 Pasture/grassland/range, Fair, HSG B 100,859 39 Pasture/grassland/range, Good, HSG A * 11,834 96 Gravel surface								
		42,960 42,960	50 Weighted Average 100.00% Pervious Area					
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
	5.9	78	0.0526	0.22		Sheet Flow,		
	1.1	22	0.2500	0.32		Grass: Short n= 0.150 P2= 2.77" <b>Sheet Flow,</b> Grass: Short n= 0.150 P2= 2.77"		
	0.1	24	0.2500	3.50		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps		
	0.3	23	0.0050	1.14		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps		
	0.1	16	0.2500	3.50		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps		
	1.6	410	0.0053	4.31	137.91	Trap/Vee/Rect Channel Flow, Swale 1 Reach Bot.W=8.00' D=2.00' Z= 4.0 '/' Top.W=24.00' n= 0.030 Earth, grassed & winding		
	9.1	573	Total					

# Summary for Subcatchment AREA 28A: Subcat AREA 28A

Runoff = 0.71 cfs @ 12.18 hrs, Volume= 0.048 af, Depth= 1.36" Routed to Link Swale S1 R4 : Swale S1 Reach 4

Area (ac)	CN	Description					
0.035	69	Pasture/grassland/range, Fair, HSG B					
0.257	39	Pasture/grassland/range, Good, HSG A					
0.075	39	Pasture/grassland/range, Good, HSG A					
0.010	96	Gravel surface, HSG A					
0.046	96	Gravel surface, HSG A					
0.423	49	Weighted Average					
0.423		100.00% Pervious Area					

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.3	82	0.0334	0.19	, ,	Sheet Flow,
					Grass: Short n= 0.150 P2= 2.77"
1.0	18	0.2500	0.31		Sheet Flow,
					Grass: Short n= 0.150 P2= 2.77"
0.2	34	0.2500	3.50		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
0.3	20	0.0050	1.14		Shallow Concentrated Flow,
					Unpaved Kv= 16.1 fps
0.1	13	0.2500	3.50		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
0.2	67	0.0069	4.92	157.36	Trap/Vee/Rect Channel Flow,
					Bot.W=8.00' D=2.00' Z= 4.0 '/' Top.W=24.00'
					n= 0.030 Earth, grassed & winding
9.1	234	Total			

# Summary for Subcatchment AREA 28B: Subcat AREA 28B

Runoff = 1.20 cfs @ 12.13 hrs, Volume=

0.061 af, Depth= 1.53"

Routed to Reach S1 R4: Swale S1 Reach 4

Area	(ac) (	N Des	cription					
0.	050	69 Pas	Pasture/grassland/range, Fair, HSG B					
0.	110				Good, HSG A			
_					Good, HSG A			
			vel surface	•				
0.			vel surface	<u>, HSG A</u>				
_			ghted Aver					
0.	476	100	.00% Pervi	ous Area				
т.	ما في مرد م	Clana	\/alaaitu	Conneitu	Decembelian			
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
(min)				(618)	01 4 51			
2.5	58	0.2500	0.39		Sheet Flow,			
0.6	20	0.0050	0.50		Grass: Short n= 0.150 P2= 2.77"			
0.6	20	0.0050	0.53		Sheet Flow,			
1.0	10	0.2500	0.31		Smooth surfaces n= 0.011 P2= 2.77"			
1.0	18	0.2300	0.31		Sheet Flow, Grass: Short n= 0.150 P2= 2.77"			
0.4	115	0.0055	4.39	140.49	Trap/Vee/Rect Channel Flow,			
0.4	115	0.0055	4.39	140.49	Bot.W=8.00' D=2.00' Z= 4.0 '/' Top.W=24.00'			
					n= 0.030 Earth, grassed & winding			
4.5	211	Total			11 0.000 Earth, grassed a winding			
4.5	211	าบเลเ						

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## **Summary for Subcatchment AREA 29: Subcat AREA 29**

Runoff = 1.21 cfs @ 12.31 hrs, Volume=

0.161 af, Depth= 0.69"

Routed to Reach S1 R6: Swale S1 Reach 6

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

	Area	(ac) (	CN Des	cription		
				el surface	•	Good, HSG A
*		000		.ure/grassi /el surface	0 /	G000, FISG A
_			<u> </u>			
		792 792	•	ghted Aver 00% Pervi		
	۷.	192	100.	00 /0 F CIVI	ous Alea	
	Тс	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	·
	11.8	100	0.0150	0.14		Sheet Flow,
						Grass: Short n= 0.150 P2= 2.77"
	1.9	100	0.0150	0.86		Shallow Concentrated Flow,
						Short Grass Pasture Kv= 7.0 fps
	0.1	16	0.2500	3.50		Shallow Concentrated Flow,
						Short Grass Pasture Kv= 7.0 fps
	1.0	247	0.0052	4.27	136.60	Trap/Vee/Rect Channel Flow, Swale S1 Reach 5
						Bot.W=8.00' D=2.00' Z= 4.0 '/' Top.W=24.00'
_						n= 0.030 Earth, grassed & winding
	14.8	463	Total			

# **Summary for Subcatchment AREA 3: Subcat AREA 3**

Runoff = 3.66 cfs @ 12.14 hrs, Volume= 0.190 af, Depth= 3.18"

Routed to Link F2: Flume 2

_	Area (ac)	CN	Description
	0.717	69	Pasture/grassland/range, Fair, HSG B
	0.717		100.00% Pervious Area

MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	2.9	44	0.1000	0.26	(013)	Sheet Flow,
	2.9	44	0.1000	0.20		Grass: Short n= 0.150 P2= 2.77"
	2.4	56	0.2500	0.39		Sheet Flow,
		00	0.2000	0.00		Grass: Short n= 0.150 P2= 2.77"
	0.4	76	0.2500	3.50		Shallow Concentrated Flow,
						Short Grass Pasture Kv= 7.0 fps
	0.6	233	0.0200	6.74	80.87	Trap/Vee/Rect Channel Flow, Diversion Berm
						Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00'
_						n= 0.030 Earth, grassed & winding
	6.3	409	Total			

# **Summary for Subcatchment AREA 30: Subcat AREA 30**

Runoff = 0.43 cfs @ 12.46 hrs, Volume=

0.074 af, Depth= 0.63"

Routed to Reach S2 R1: Swale S2 Reach 1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

	Area	(ac) C	N Desc	cription		
	1.	415 3	39 Past	ure/grassla	and/range,	Good, HSG A
	1.	415	100.	00% Pervi	ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	9.5	100	0.0260	0.18		Sheet Flow,
	2.9	194	0.0260	1.13		Grass: Short n= 0.150 P2= 2.77"  Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
_	9.6	647	0.0260	1.13		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
	22.0	941	Total			

# **Summary for Subcatchment AREA 31: Subcat AREA 31**

Runoff = 0.42 cfs @ 12.14 hrs, Volume= 0.036 af, Depth= 0.63"

Routed to Link Swale S2 R1 : Swale S2 Reach 1

_	Area (ac)	CN	Description
Ī	0.698	39	Pasture/grassland/range, Good, HSG A
-	0.698		100.00% Pervious Area

MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.6	34	0.2500	0.35	•	Sheet Flow,
2.8	447	0.0020	2.65	84.72	Grass: Short n= 0.150 P2= 2.77"  Trap/Vee/Rect Channel Flow, Swale 2 Reach 1  Bot.W=8.00' D=2.00' Z= 4.0 '/' Top.W=24.00'  n= 0.030 Earth, grassed & winding
4.4	481	Total			

#### **Summary for Subcatchment AREA 32: Subcat AREA 32**

Runoff = 3.11 cfs @ 12.31 hrs, Volume= 0.315 af, Depth= 1.13"

Routed to Link Swale S3 R3: Swale S3 Reach 3

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

Area	(ac) C	N Desc	cription						
0.	.567 6	69 Past	Pasture/grassland/range, Fair, HSG B						
2.	413	39 Past	Pasture/grassland/range, Good, HSG A						
0.	.099 9		el surface	•					
0	274	39 Past	ure/grassla	and/range,	Good, HSG A				
3.	.353 4		Weighted Average						
3.	.353	100.	00% Pervi	ous Area					
Tc	Length	Slope	Velocity	Capacity	Description				
(min)_	(feet)	(ft/ft)	(ft/sec)	(cfs)					
12.1	100	0.0140	0.14		Sheet Flow,				
					Grass: Short n= 0.150 P2= 2.77"				
4.2	211	0.0140	0.83		Shallow Concentrated Flow,				
					Short Grass Pasture Kv= 7.0 fps				
0.1	23	0.1740	2.92		Shallow Concentrated Flow,				
0.0	000	0.0007	5.00	400.57	Short Grass Pasture Kv= 7.0 fps				
0.9	329	0.0097	5.83	186.57	Trap/Vee/Rect Channel Flow, Swale 3 Reach 3				
					Bot.W=8.00' D=2.00' Z= 4.0 '/' Top.W=24.00'				
					n= 0.030 Earth, grassed & winding				
17.3	663	Total							

# **Summary for Subcatchment AREA 33: Subcat AREA 33**

Runoff = 1.14 cfs @ 12.28 hrs, Volume= 0.101 af, Depth= 1.36" Routed to Link Swale S3 R2 : Swale S3 Reach 2

MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

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	Area (sf)	CN [	Description		
	4,079	96 (	Gravel surfa	ace, HSG A	4
	1,422			ace, HSG A	
	30,707				ge, Good, HSG A
*	2,706	69 F	Pasture/gra	ssland/rang	ge, Fair, HSG A
	38,914	49 \	Veighted A	verage	
	38,914			ervious Are	a
	,				
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	·
12.1	100	0.0140	0.14		Sheet Flow,
					Grass: Short n= 0.150 P2= 2.77"
3.6	178	0.0140	0.83		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
0.0	12	0.4000	4.43		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
0.3	87	0.0070	5.23	125.44	Trap/Vee/Rect Channel Flow, Swale 3 Reach 2
					Bot.W=8.00' D=2.00' Z= 2.0 '/' Top.W=16.00'
					n= 0.030 Earth, grassed & winding
16.0	377	Total			

# Summary for Subcatchment AREA 34: Subcat AREA 34

Runoff = 1.20 cfs @ 12.30 hrs, Volume= 0.128 af, Depth= 0.98"

Routed to Link Swale S3 R1: Swale S3 Reach 1

	Area (sf)	CN [	Description					
5,695 69 Pasture/grassland/range				ssland/ran	ge, Fair, HSG B			
	3,470	96 (	Gravel surfa	ace, HSG A	Ä			
	59,319	39 F	Pasture/grassland/range, Good, HSG A					
	68,484	44 V	Veighted A	verage				
	68,484	1	00.00% Pe	ervious Are	a			
Tc	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
12.1	100	0.0140	0.14		Sheet Flow,			
					Grass: Short n= 0.150 P2= 2.77"			
3.4	170	0.0140	0.83		Shallow Concentrated Flow,			
					Short Grass Pasture Kv= 7.0 fps			
0.1	15	0.4000	4.43		Shallow Concentrated Flow,			
					Short Grass Pasture Kv= 7.0 fps			
0.6	203	0.0070	5.23	125.44	- I			
					Bot.W=8.00' D=2.00' Z= 2.0 '/' Top.W=16.00'			
					n= 0.030 Earth, grassed & winding			
16.2	488	Total						

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#### **Summary for Subcatchment AREA 35: Subcat AREA 35**

Runoff = 2.10 cfs @ 12.12 hrs, Volume=

0.099 af, Depth= 3.18"

Routed to Reach S3 R1: Swale S3 Reach 1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

Area	(ac) C	N Des	cription		
0.	375 6	9 Past	ure/grassla	and/range,	Fair, HSG B
0.	375	100.	00% Pervi	ous Area	
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.8	100	0.2500	0.43		Sheet Flow,
0.4	74	0.2500	3.50		Grass: Short n= 0.150 P2= 2.77"  Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
4.2	174	Total			

#### **Summary for Subcatchment AREA 36: Subcat AREA 36**

Runoff = 2.62 cfs @ 12.12 hrs, Volume=

0.125 af, Depth= 3.08"

Routed to Link F7: Existing East Flume

	Area	(ac) C	N Des	cription		
	0.	470	69 Past	ure/grassla	and/range,	Fair, HSG B
	0.	016	39 Past	ure/grassla	and/range,	Good, HSG A
*	0.	000	0 Past	ure/grassla	and/range,	Good
	0.	487	68 Wei	hted Aver	age	
	0.	487		, 00% Pervi		
	Tc	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	<u> </u>
	3.5	90	0.2500	0.43		Sheet Flow,
						Grass: Short n= 0.150 P2= 2.77"
	0.7	201	0.0200	4.80	23.38	Trap/Vee/Rect Channel Flow,
						Bot.W=0.00' D=1.18' Z= 4.0 & 3.0 '/' Top.W=8.26'
						n= 0.030 Earth, grassed & winding
	0.2	134	0.2500	12.26	441.43	Trap/Vee/Rect Channel Flow, Riprap Flume
						Bot.W=12.00' D=2.00' Z= 3.0 '/' Top.W=24.00'
_						n= 0.078 Riprap, 12-inch
	4.4	425	Total			

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# **Summary for Subcatchment AREA 37: Subcat AREA 37**

Runoff = 1.89 cfs @ 12.12 hrs, Volume=

0.091 af, Depth= 3.18"

Routed to Link F7: Existing East Flume

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

_	Area	(ac) C	N Des	cription		
	0.	344 6	9 Past	ure/grassla	and/range,	Fair, HSG B
	0.	344	100.	00% Pervi	ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	3.8	100	0.2500	0.43	, ,	Sheet Flow,
	0.1	30	0.2500	3.50		Grass: Short n= 0.150 P2= 2.77"  Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
	0.4	126	0.0200	4.80	23.38	Trap/Vee/Rect Channel Flow, Existing Diversion Berm Bot.W=0.00' D=1.18' Z= 4.0 & 3.0 '/' Top.W=8.26'
	0.3	254	0.2500	12.26	441.43	n= 0.030 Earth, grassed & winding  Trap/Vee/Rect Channel Flow, Riprap Flume  Bot.W=12.00' D=2.00' Z= 3.0 '/' Top.W=24.00' n= 0.078 Riprap, 12-inch
	4.6	510	Total			

# **Summary for Subcatchment AREA 38: Subcat AREA 38**

Runoff = 1.25 cfs @ 12.12 hrs, Volume=

0.059 af, Depth= 3.18"

Routed to Link F8: Existing West Flume

	Area	(ac) C	N Desc	cription		
	0.	223 6	9 Past	ure/grassla	and/range,	Fair, HSG B
	0.	223	100.	00% Pervi	ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	3.1	77	0.2500	0.41		Sheet Flow,
						Grass: Short n= 0.150 P2= 2.77"
	0.5	156	0.0200	4.80	23.38	Trap/Vee/Rect Channel Flow, Existing Diversion Berm
						Bot.W=0.00' D=1.18' Z= 4.0 & 3.0 '/' Top.W=8.26' n= 0.030 Earth, grassed & winding
	0.5	357	0.2500	12.26	441.43	Trap/Vee/Rect Channel Flow, Riprap Flume
						Bot.W=12.00' D=2.00' Z= 3.0 '/' Top.W=24.00'
_						n= 0.078 Riprap, 12-inch
	4.1	590	Total			

MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

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# **Summary for Subcatchment AREA 39: Subcat AREA 39**

Runoff = 3.50 cfs @ 12.13 hrs, Volume=

0.174 af, Depth= 3.18"

Routed to Link F8: Existing West Flume

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

	Area	(ac) C	N Des	cription		
_	0.	Fair, HSG B				
	0.	656		00% Pervi		
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	3.8	100	0.2500	0.43		Sheet Flow,
	0.1	11	0.2500	3.50		Grass: Short n= 0.150 P2= 2.77"  Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
	1.1	314	0.0200	4.80	23.38	Trap/Vee/Rect Channel Flow, Existing Diversion Berm Bot.W=0.00' D=1.18' Z= 4.0 & 3.0 '/' Top.W=8.26' n= 0.030 Earth, grassed & winding
	0.3	217	0.2500	12.26	441.43	Trap/Vee/Rect Channel Flow, Riprap Flume Bot.W=12.00' D=2.00' Z= 3.0 '/' Top.W=24.00' n= 0.078 Riprap, 12-inch
_	5.3	642	Total			

# **Summary for Subcatchment AREA 4: Subcat AREA 4**

Runoff = 6.31 cfs @ 12.14 hrs, Volume= 0.331 af, Depth= 3.18"

Routed to Link F2: Flume 2

	Area (ac) CN Description								
1.247 69 Pasture/grassland/range, Fair, HSG B									
1.247 100.00% Pervious Area					ous Area				
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
	3.5	57	0.1000	0.27	, ,	Sheet Flow,			
						Grass: Short n= 0.150 P2= 2.77"			
	2.0	43	0.2500	0.37		Sheet Flow,			
						Grass: Short n= 0.150 P2= 2.77"			
	0.4	83	0.2500	3.50		Shallow Concentrated Flow,			
						Short Grass Pasture Kv= 7.0 fps			
	0.7	295	0.0200	6.74	80.87	Trap/Vee/Rect Channel Flow, Diversion Berm			
						Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00'			
						n= 0.030 Earth, grassed & winding			
	6.6	478	Total						

MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

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## **Summary for Subcatchment AREA 40: Subcat AREA 40**

Runoff = 6.03 cfs @ 12.13 hrs, Volume=

0.300 af, Depth= 2.23"

Routed to Link Swale S2 R2: Swale S2 Reach 2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

	Area	(ac) C	N Desc	cription		
	1.	.079 6	9 Past	ure/grassl	and/range,	Fair, HSG B
	0.	.539 3	39 Past	:ure/grassl	and/range,	Good, HSG A
*	0.	.000	0 Past	ure/grassl	and/range,	Good
	1.	.618 5	59 Weig	ghted Aver	age	
	1.	.618	100.	00% Pervi	ous Area	
	Тс	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	3.1	77	0.2500	0.41		Sheet Flow,
						Grass: Short n= 0.150 P2= 2.77"
	8.0	237	0.0200	4.80	23.38	, , , , , , , , , , , , , , , , , , ,
						Bot.W=0.00' D=1.18' Z= 4.0 & 3.0 '/' Top.W=8.26'
						n= 0.030 Earth, grassed & winding
	0.3	70	0.2500	3.50		Shallow Concentrated Flow,
	4.0	0.45		- 0-	404 70	Short Grass Pasture Kv= 7.0 fps
	1.0	315	0.0069	5.05	181.72	Trap/Vee/Rect Channel Flow, Swale S2 Reach 2
						Bot.W=10.00' D=2.00' Z= 4.0 '/' Top.W=26.00'
_						n= 0.030 Earth, grassed & winding
	5.2	699	Total			

# **Summary for Subcatchment AREA 41: Subcat AREA 41**

Runoff = 2.84 cfs @ 12.14 hrs, Volume=

0.147 af, Depth= 2.13"

Routed to Reach S2 R2 : Swale S2 Reach 2

Area (ac)	CN	Description				
0.520 69 Pasture/grassland/range, Fair, HSG B						
0.306	39	Pasture/grassland/range, Good, HSG A				
0.826	58	Weighted Average				
0.826		100.00% Pervious Area				

MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	3.8	100	0.2500	0.43		Sheet Flow,
	0.1	26	0.2500	3.50		Grass: Short n= 0.150 P2= 2.77"  Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
	2.0	596	0.0069	5.05	181.72	Trap/Vee/Rect Channel Flow, Swale S2 Reach 2 Bot.W=10.00' D=2.00' Z= 4.0 '/' Top.W=26.00' n= 0.030 Earth, grassed & winding
-	5.9	722	Total			11 0.000 Earth, gradoud & Wilding

#### **Summary for Subcatchment AREA 42: Subcat AREA 42**

Runoff = 0.93 cfs @ 12.22 hrs, Volume= 0.5

0.114 af, Depth= 0.63"

Routed to Link Swale S2 R2 : Swale S2 Reach 2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

_	Area	(ac) C	N Desc	cription				
2.177 39 Pasture/grassland/range, Good, HSG A								
	2.177 100.00% Pervious Area							
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
	6.4	66	0.0303	0.17		Sheet Flow,		
	1.6	34	0.2500	0.35		Grass: Short n= 0.150 P2= 2.77"  Sheet Flow,		
	1.0	0.	0.2000	0.00		Grass: Short n= 0.150 P2= 2.77"		
	0.2	49	0.2500	3.50		Shallow Concentrated Flow,		
		000		- 0-	404 70	Short Grass Pasture Kv= 7.0 fps		
	0.9	266	0.0069	5.05	181.72	Trap/Vee/Rect Channel Flow, Swale S2 Reach 2 Bot.W=10.00' D=2.00' Z= 4.0 '/' Top.W=26.00'		
						n= 0.030 Earth, grassed & winding		
_	9.1	415	Total					

# **Summary for Subcatchment AREA 43: Subcat AREA 43**

Runoff = 6.39 cfs @ 12.13 hrs, Volume= 0.325 af, Depth= 3.18"

Routed to Link F8: Existing West Flume

_	Area (ac)	CN	Description
	1.228	69	Pasture/grassland/range, Fair, HSG B
1.228			100.00% Pervious Area

MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59" Printed 4/11/2022

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.8	100	0.2500	0.43		Sheet Flow,
					Grass: Short n= 0.150 P2= 2.77"
0.0	6	0.2500	3.50		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
1.9	541	0.0200	4.80	23.38	Trap/Vee/Rect Channel Flow, Existing Diversion Berm
					Bot.W=0.00' D=1.18' Z= 4.0 & 3.0 '/' Top.W=8.26'
					n= 0.030 Earth, grassed & winding
0.2	131	0.2500	12.26	441.43	Trap/Vee/Rect Channel Flow, Riprap Flume
					Bot.W=12.00' D=2.00' Z= 3.0 '/' Top.W=24.00'
					n= 0.078 Riprap, 12-inch
5.9	778	Total			

#### Summary for Subcatchment AREA 44: Subcat AREA 44

Runoff = 2.38 cfs @ 12.19 hrs, Volume=

0.273 af, Depth= 0.63"

Routed to Pond Sed Pond: Sedimentation Basin

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

Area	(ac) C	N Desc	cription		
5.	227 3	9 Past	ure/grassla	and/range,	Good, HSG A
5.	227	100.	00% Pervi	ous Area	
Тс	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
4.5	75	0.0933	0.28		Sheet Flow,
					Grass: Short n= 0.150 P2= 2.77"
1.3	25	0.2500	0.33		Sheet Flow,
					Grass: Short n= 0.150 P2= 2.77"
0.0	10	0.2500	3.50		Shallow Concentrated Flow,
0.0	004	0.0005	7.05	400.00	Short Grass Pasture Kv= 7.0 fps
8.0	381	0.0265	7.85	109.92	Trap/Vee/Rect Channel Flow,
					Bot.W=0.00' D=2.00' Z= 4.0 & 3.0 '/' Top.W=14.00' n= 0.030 Earth, grassed & winding
0.8	162	0.2500	3.50		Shallow Concentrated Flow,
0.0	102	0.2000	0.00		Short Grass Pasture Kv= 7.0 fps
0.5	48	0.0500	1.57		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
7.9	701	Total			·

# Summary for Subcatchment AREA 44A: Subcat AREA 44A

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff = 14.38 cfs @ 12.09 hrs, Volume= Routed to Pond Sed Pond : Sedimentation Basin 0.798 af, Depth= 6.35"

MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

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Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

Area (ac) CN Description							
_	1.	508	98	Wate	er Surface,	, HSG A	
1.508 100.00% Impervious Area							à
_	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	0.0						Direct Entry,

#### Summary for Subcatchment AREA 44B: Subcat AREA 44B

Runoff = 1.17 cfs @ 12.16 hrs, Volume=

0.071 af, Depth= 1.44"

Routed to Pond Sed Pond : Sedimentation Basin

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

	Area	(ac) (	N Des	cription		
	0.	479	39 Past	ture/grassl	and/range,	Good, HSG A
0.115 96 Gravel surface, HSG A						
* 0.000 0 , HSG A						
*	0.	000	0 , HS	G A		
	0.	594	50 Wei	ghted Aver	age	
	0.	594	100.	00% Pervi	ous Area	
	Тс	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	7.1	100	0.0544	0.24		Sheet Flow,
						Grass: Short n= 0.150 P2= 2.77"
	0.5	47	0.0544	1.63		Shallow Concentrated Flow,
_						Short Grass Pasture Kv= 7.0 fps
	76	147	Total			

#### Summary for Subcatchment AREA 45: Subcat AREA 45

Runoff = 1.16 cfs @ 12.41 hrs, Volume= Routed to Link Swale S4 R4 : Swale S4 Reach 4 0.150 af, Depth= 0.90"

MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

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	Area	(ac) (	CN Des	cription		
*	0.	000	0 , HS	G A		
	1.870		39 Pas	ture/grassla	and/range,	Good, HSG A
	0.	000	96 Gra	vel surface	, HSG A	
_	0.	130	96 Gra	vel surface	, HSG A	
	2.	001	43 Wei	ghted Aver	age	
	2.	001	100	00% Pervi	ous Area	
	_					
	Tc	Length	•	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	15.7	100	0.0074	0.11		Sheet Flow,
						Grass: Short n= 0.150 P2= 2.77"
	4.7	169	0.0074	0.60		Shallow Concentrated Flow,
						Short Grass Pasture Kv= 7.0 fps
	0.4	49	0.0800	1.98		Shallow Concentrated Flow,
						Short Grass Pasture Kv= 7.0 fps
	1.1	363	0.0082	5.42	162.67	Trap/Vee/Rect Channel Flow, Swale S4 Reach 2
						Bot.W=8.00' D=2.00' Z= 4.0 & 3.0 '/' Top.W=22.00'
_						n= 0.030 Earth, grassed & winding
	21.9	681	Total			

# **Summary for Subcatchment AREA 46: Subcat AREA 46**

Runoff = 22.74 cfs @ 12.17 hrs, Volume= 1.366 af, Depth= 2.23"

Routed to Reach S4 R4: Swale S4 Reach 4

	Area (ac)	CN	Description
	3.081	69	Pasture/grassland/range, Fair, HSG B
	0.590	96	Gravel surface, HSG B
	3.264	39	Pasture/grassland/range, Good, HSG A
	0.017	98	Paved parking, HSG A
	0.009	98	Paved parking, HSG A
	0.378	96	Gravel surface, HSG A
	0.001	96	Gravel surface, HSG A
	0.026	96	Gravel surface, HSG A
*	0.000	0	, HSG A
*	0.000	0	, HSG A
*	0.000	0	, HSG A
*	0.000	0	, HSG A
*	0.000	0	, HSG A
*	0.000	0	, HSG A
*	0.000	0	Pasture/grassland/range, Fair
	7.367	59	Weighted Average
	7.340		99.64% Pervious Area
	0.027		0.36% Impervious Area

MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59" Prepared by SCS Engineers Printed 4/11/2022

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.2	51	0.2500	0.38	(0.0)	Sheet Flow,
					Grass: Short n= 0.150 P2= 2.77"
0.1	16	0.2500	2.44		Sheet Flow,
					Smooth surfaces n= 0.011 P2= 2.77"
0.9	31	0.0050	0.58		Sheet Flow,
					Smooth surfaces n= 0.011 P2= 2.77"
0.4	47	0.0650	1.78		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
5.6	1,759	0.0073	5.26	178.68	Trap/Vee/Rect Channel Flow, Swale S4 Reach 1
					Bot.W=10.00' D=2.00' Z= 3.0 & 4.0 '/' Top.W=24.00'
					n= 0.030 Earth, grassed & winding
9.2	1,904	Total			

# **Summary for Subcatchment AREA 47: Subcat AREA 47**

Runoff 6.90 cfs @ 12.17 hrs, Volume= 0.408 af, Depth= 2.69"

Routed to Link Swale S5 R3 : Swale S5 Reach 3

_	Α	rea (sf)	CN E	<b>Description</b>				
49,617 69 Pasture/grassland/range, Fair, HSG B								
		6,971	98 F	Paved park	ing, HSG A	- L		
		1,619	96	Gravel surface, HSG A				
_		20,925	39 F	<sup>p</sup> asture/gra	ssland/rang	ge, Good, HSG A		
		79,132	64 V	Veighted A	verage			
		72,161	9	1.19% Per	vious Area			
		6,971	8	.81% Impe	ervious Area	a		
	Тс	Length	Slope	Velocity		Description		
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
	2.0	43	0.2500	0.37		Sheet Flow,		
						Grass: Short n= 0.150 P2= 2.77"		
	0.1	11	0.1111	1.63		Sheet Flow,		
						Smooth surfaces n= 0.011 P2= 2.77"		
	0.7	12	0.2500	0.28		Sheet Flow,		
						Grass: Short n= 0.150 P2= 2.77"		
	2.9	28	0.0393	0.16		Sheet Flow,		
						Grass: Short n= 0.150 P2= 2.77"		
	3.4	488	0.0024	2.40	52.81	•		
						Bot.W=0.00' D=2.00' Z= 5.0 & 6.0 '/' Top.W=22.00'		
_						n= 0.030 Earth, grassed & winding		
	9.1	582	Total					

MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59" Printed 4/11/2022

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#### **Summary for Subcatchment AREA 48: Subcat AREA 48**

Runoff = 5.30 cfs @ 12.13 hrs, Volume=

0.265 af, Depth= 2.41"

Routed to Link Swale S5 R2 : Swale S5 Reach 2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

A	rea (sf)	CN E	escription			
	24,597 69 Pasture/grassland/range, Fair, HSG B					
24,117 39 Pasture/grassland/range, Good, HSG A						
	2,057	96 G	Gravel surfa	ace, HSG A	À	
	6,769	98 F	aved park	ing, HSG A	· ·	
	57,540	61 V	Veighted A	verage		
	50,771	8	8.24% Per	vious Area		
	6,769	1	1.76% Imp	pervious Are	ea	
Tc	Length	Slope	Velocity	Capacity	Description	
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
0.6	19	0.0050	0.53		Sheet Flow,	
					Smooth surfaces n= 0.011 P2= 2.77"	
1.7	29	0.1667	0.29		Sheet Flow,	
					Grass: Short n= 0.150 P2= 2.77"	
3.1	441	0.0024	2.38	40.39	- I	
					Bot.W=0.00' D=2.00' Z= 2.5 & 6.0 '/' Top.W=17.00'	
					n= 0.030 Earth, grassed & winding	
5.4	489	Total				

## **Summary for Subcatchment AREA 49: Subcat AREA 49**

Runoff = 2.68 cfs @ 12.12 hrs, Volume= 0.1 Routed to Link Swale S1 R1 : Swale S1 Reach 1

0.128 af, Depth= 2.23"

Dura # hu COC TD 00 marth and 1111-COC Wainlife d CN Time Consu

	Area	(ac) (	CN Des	cription			
0.439 69 Pasture/grassland/range, Fair, HSG B							
	0.	246	39 Past	ure/grassla	and/range,	Good, HSG A	
	0.	006	96 Gra\	∕el surface	, HSG A		
	0.	691	59 Weig	ghted Aver	age		
	0.	691	100.	00% Pervi	ous Area		
	Тс	Length	Slope	Velocity	Capacity	Description	
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
	2.5	59	0.2500	0.39		Sheet Flow,	
						Grass: Short n= 0.150 P2= 2.77"	
	1.8	463	0.0053	4.31	137.91	Trap/Vee/Rect Channel Flow, Swale S1 Reach 1	
						Bot.W=8.00' D=2.00' Z= 4.0 '/' Top.W=24.00'	
						n= 0.030 Earth, grassed & winding	

MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

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4.3 522 Total

#### **Summary for Subcatchment AREA 5: Subcat AREA 5**

Runoff = 6.05 cfs @ 12.14 hrs, Volume= 0.317 af, Depth= 3.18"

Routed to Link F1: Flume 1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

_	Area	(ac) C	N Desc	cription		
	1.	195 6	9 Past	ure/grassla	and/range,	Fair, HSG B
_	1.	195	100.	00% Pervi	ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	3.6	59	0.1000	0.27		Sheet Flow,
	1.9	41	0.2500	0.36		Grass: Short n= 0.150 P2= 2.77"  Sheet Flow,
	0.4	85	0.2500	3.50		Grass: Short n= 0.150 P2= 2.77"  Shallow Concentrated Flow, Short Grass Posture, Ky= 7.0 fps
	0.7	297	0.0200	6.74	80.87	Short Grass Pasture Kv= 7.0 fps <b>Trap/Vee/Rect Channel Flow, Diversion Berm</b> Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00' n= 0.030 Earth, grassed & winding
-	6.6	482	Total			II- 0.030 ⊑aitii, grassed & Willding

#### **Summary for Subcatchment AREA 50: Subcat AREA 50**

Runoff = 13.35 cfs @ 12.11 hrs, Volume= 0.698 af, Depth= 5.65" Routed to Link Swale S6 R1 : Swale S6 Reach 1

 Area (ac)	CN	Description
0.100	39	Pasture/grassland/range, Good, HSG A
0.001	39	Pasture/grassland/range, Good, HSG A
 1.382	96	Gravel surface, HSG A
1.482	92	Weighted Average
1.482		100.00% Pervious Area

MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	1.6	100	0.0119	1.04		Sheet Flow,
						Smooth surfaces n= 0.011 P2= 2.77"
	0.4	47	0.0119	1.76		Shallow Concentrated Flow,
						Unpaved Kv= 16.1 fps
	0.0	10	0.5000	4.95		Shallow Concentrated Flow,
						Short Grass Pasture Kv= 7.0 fps
	1.4	413	0.0066	5.00	130.01	Trap/Vee/Rect Channel Flow, Swale S6 Reach 1
						Bot.W=8.00' D=2.00' Z= 2.5 '/' Top.W=18.00'
_						n= 0.030 Earth, grassed & winding
	3.4	570	Total			

#### **Summary for Subcatchment AREA 51: Subcat AREA 51**

Runoff = 0.67 cfs @ 12.27 hrs, Volume=

0.082 af, Depth= 0.69"

Routed to Link Swale S6 R1 : Swale S6 Reach 1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

_	Area	(ac) C	N Desc	cription				
1.396 39 Pasture/grassland/range, Good, HSG A								
0.020 96 Gravel surface, HSG A								
	1.	417 4	10 Weig	hted Aver	age			
	1.	417	100.	00% Pervi	ous Area			
	То	Longth	Clana	Valacity	Consoity	Description		
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
_			, ,	, ,	(615)			
	7.3	100	0.0500	0.23		Sheet Flow,		
						Grass: Short n= 0.150 P2= 2.77"		
	3.2	302	0.0500	1.57		Shallow Concentrated Flow,		
						Short Grass Pasture Kv= 7.0 fps		
	0.3	53	0.0313	2.85		Shallow Concentrated Flow,		
						Unpaved Kv= 16.1 fps		
	1.4	429	0.0066	5.00	130.01	Trap/Vee/Rect Channel Flow, Swale S6 Reach 1		
						Bot.W=8.00' D=2.00' Z= 2.5 '/' Top.W=18.00'		
						n= 0.030 Earth, grassed & winding		
_	12.2	884	Total		•			

# **Summary for Subcatchment AREA 52: Subcat AREA 52**

Runoff = 7.48 cfs @ 12.15 hrs, Volume= Routed to Link Swale S5 R1 : Swale S5 Reach 1 0.454 af, Depth= 1.20"

MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

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A	rea (sf)	CN D	escription		
1	69,213	39 P	asture/gra	ssland/rang	ge, Good, HSG A
	25,933	98 P	aved park	ing, HSG A	
	2,184	96 G	ravel surfa	ace, HSG A	1
1	97,330	47 V	Veighted A	verage	
1	71,397	8	6.86% Per	vious Area	
	25,933	1	3.14% Imp	ervious Are	ea
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
0.6	18	0.0050	0.52		Sheet Flow,
					Smooth surfaces n= 0.011 P2= 2.77"
1.4	21	0.1333	0.25		Sheet Flow,
					Grass: Short n= 0.150 P2= 2.77"
4.3	1,255	0.0096	4.82	125.20	Trap/Vee/Rect Channel Flow, Swale S5 Reach 1
					Bot.W=0.00' D=2.00' Z= 6.0 & 7.0 '/' Top.W=26.00'
					n= 0.030 Earth, grassed & winding
6.3	1,294	Total			

# **Summary for Subcatchment AREA 6: Subcat AREA 6**

Runoff = 4.90 cfs @ 12.12 hrs, Volume= 0.236 af, Depth= 3.18"

Routed to Link F1: Flume 1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

_	Area	(ac) C	N Desc	cription		
	0.	892 6	9 Past	ure/grassl	and/range,	Fair, HSG B
	0.	892	100.	00% Pervi	ous Area	
_	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	3.8	100	0.2500	0.43		Sheet Flow,
	0.0	7	0.2500	3.50		Grass: Short n= 0.150 P2= 2.77"  Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
	8.0	308	0.0200	6.74	80.87	Trap/Vee/Rect Channel Flow, Diversion Berm Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00' n= 0.030 Earth, grassed & winding
-	4.6	415	Total			

## **Summary for Subcatchment AREA 7: Subcat AREA 7**

Runoff = 5.31 cfs @ 12.13 hrs, Volume= 0.269 af, Depth= 3.18"

Routed to Link F8: Existing West Flume

MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

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12.26

Area	(ac) C	N Des	cription		
1.	017 6	9 Past	ture/grassl	and/range,	Fair, HSG B
1.	017	100.	00% Pervi	ous Area	
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.8	100	0.2500	0.43		Sheet Flow,
0.1	18	0.2500	3.50		Grass: Short n= 0.150 P2= 2.77"  Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
1.5	419	0.0200	4.80	23.38	Trap/Vee/Rect Channel Flow, Existing Diversion Berm Bot.W=0.00' D=1.18' Z= 4.0 & 3.0 '/' Top.W=8.26' n= 0.030 Earth, grassed & winding

5.8 833 Total

296 0.2500

0.4

# **Summary for Subcatchment AREA 8: Subcat AREA 8**

Trap/Vee/Rect Channel Flow,

n= 0.078 Riprap, 12-inch

Bot.W=12.00' D=2.00' Z= 3.0'/' Top.W=24.00'

Runoff = 5.52 cfs @ 12.12 hrs, Volume= 0.268 af, Depth= 3.18"

441.43

Routed to Link F6: Flume 6

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

_	Area	(ac) C	N Desc	cription		
	1.	009 6	9 Past	ure/grassl	and/range,	Fair, HSG B
	1.	009	100.	00% Pervi	ous Area	
	Tc (min)	Length Slope (feet) (ft/ft)		Velocity (ft/sec)	Capacity (cfs)	Description
	3.8	100	0.2500	0.43		Sheet Flow,
	0.3	66	0.2500	3.50		Grass: Short n= 0.150 P2= 2.77"  Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
	0.6	243	0.0200	6.74	80.87	Trap/Vee/Rect Channel Flow, Diversion Berm Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00' n= 0.030 Earth, grassed & winding
	4.7	409	Total			

# **Summary for Subcatchment AREA 9: Subcat AREA 9**

Runoff = 5.71 cfs @ 12.12 hrs, Volume= 0.278 af, Depth= 3.18"

Routed to Link F6: Flume 6

MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

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_	Area	(ac) C	N Desc	cription		
	1.	047 6	9 Past	ure/grassl	and/range,	Fair, HSG B
1.047 100.00% Pervious						
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	3.8	100	0.2500	0.43		Sheet Flow,
	0.4	76	0.2500	3.50		Grass: Short n= 0.150 P2= 2.77"  Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
	0.6	250	0.0200	6.74	80.87	Trap/Vee/Rect Channel Flow, Diversion Berm Bot.W=0.00' D=2.00' Z= 4.0 & 2.0 '/' Top.W=12.00' n= 0.030 Earth, grassed & winding
_	4.8	426	Total			<u>-</u>

#### Summary for Reach S1 R2: Swale S1 Reach 2

Inflow Area = 7.131 ac, 0.00% Impervious, Inflow Depth = 3.07" for 100-yr, 24-hr event

37.51 cfs @ 12.12 hrs, Volume= Inflow 1.827 af

37.05 cfs @ 12.12 hrs, Volume= Outflow 1.827 af, Atten= 1%, Lag= 0.4 min

Routed to Link Swale S1 R2 : Swale S1 Reach 2

Routing by Dyn-Stor-Ind method, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

Max. Velocity= 3.03 fps, Min. Travel Time= 0.7 min

Avg. Velocity = 0.80 fps, Avg. Travel Time= 2.7 min

Peak Storage= 1,553 cf @ 12.12 hrs

Average Depth at Peak Storage= 1.01', Surface Width= 16.12' Bank-Full Depth= 2.00' Flow Area= 32.0 sf, Capacity= 140.64 cfs

8.00' x 2.00' deep channel, n= 0.030 Earth, grassed & winding

Side Slope Z-value= 4.0 '/' Top Width= 24.00'

Length= 127.0' Slope= 0.0055 '/'

Inlet Invert= 814.81', Outlet Invert= 814.11'



# Summary for Reach S1 R3: Swale S1 Reach 3

14.170 ac, 0.00% Impervious, Inflow Depth = 2.58" for 100-yr, 24-hr event 53.22 cfs @ 12.12 hrs, Volume= 3.049 af Inflow Area =

Inflow

47.76 cfs @ 12.15 hrs, Volume= 3.049 af, Atten= 10%, Lag= 1.5 min Outflow

Routed to Link Swale S1 R3 : Swale S1 Reach 3

MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

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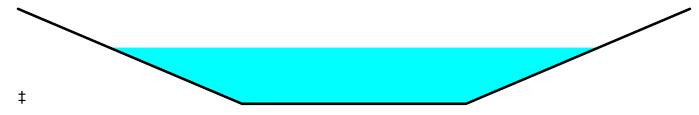
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Routing by Dyn-Stor-Ind method, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs Max. Velocity= 3.17 fps, Min. Travel Time= 3.0 min Avg. Velocity = 0.70 fps, Avg. Travel Time= 13.8 min

Peak Storage= 8,716 cf @ 12.15 hrs Average Depth at Peak Storage= 1.18', Surface Width= 17.47' Bank-Full Depth= 2.00' Flow Area= 32.0 sf, Capacity= 135.10 cfs

8.00' x 2.00' deep channel, n= 0.030 Earth, grassed & winding Side Slope Z-value= 4.0 '/' Top Width= 24.00' Length= 578.0' Slope= 0.0051 '/' Inlet Invert= 814.11', Outlet Invert= 811.17'



# Summary for Reach S1 R4: Swale S1 Reach 4

Inflow Area = 17.292 ac, 0.00% Impervious, Inflow Depth = 2.64" for 100-yr, 24-hr event

Inflow = 62.37 cfs @ 12.14 hrs, Volume= 3.811 af

Outflow = 61.58 cfs @ 12.15 hrs, Volume= 3.811 af, Atten= 1%, Lag= 0.6 min

Routed to Link Swale S1 R4: Swale S1 Reach 4

Routing by Dyn-Stor-Ind method, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs Max. Velocity= 3.74 fps, Min. Travel Time= 0.9 min Avg. Velocity = 0.81 fps, Avg. Travel Time= 4.0 min

Peak Storage= 3,220 cf @ 12.15 hrs Average Depth at Peak Storage= 1.26', Surface Width= 18.09' Bank-Full Depth= 2.00' Flow Area= 32.0 sf, Capacity= 154.36 cfs

8.00' x 2.00' deep channel, n= 0.030 Earth, grassed & winding Side Slope Z-value= 4.0 '/' Top Width= 24.00' Length= 195.8' Slope= 0.0066 '/' Inlet Invert= 811.17', Outlet Invert= 809.87'



MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

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# Summary for Reach S1 R5: Swale S1 Reach 5

Inflow Area = 17.714 ac, 0.00% Impervious, Inflow Depth = 2.61" for 100-yr, 24-hr event

Inflow = 62.23 cfs @ 12.15 hrs, Volume= 3.859 af

Outflow = 59.21 cfs @ 12.17 hrs, Volume= 3.859 af, Atten= 5%, Lag= 1.3 min

Routed to Link Swale S1 R5: Swale S1 Reach 5

Routing by Dyn-Stor-Ind method, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

Max. Velocity= 3.42 fps, Min. Travel Time= 2.0 min

Avg. Velocity = 0.74 fps, Avg. Travel Time= 9.2 min

Peak Storage= 7,135 cf @ 12.17 hrs

Average Depth at Peak Storage= 1.31', Surface Width= 18.48'

Bank-Full Depth= 2.00' Flow Area= 32.0 sf, Capacity= 137.86 cfs

8.00' x 2.00' deep channel, n= 0.030 Earth, grassed & winding

Side Slope Z-value= 4.0 '/' Top Width= 24.00'

Length= 411.6' Slope= 0.0053 '/'

Inlet Invert= 809.77', Outlet Invert= 807.59'

‡

# Summary for Reach S1 R6: Swale S1 Reach 6

Inflow Area = 23.788 ac, 0.00% Impervious, Inflow Depth = 2.23" for 100-yr, 24-hr event

Inflow = 65.66 cfs @ 12.17 hrs, Volume= 4.415 af

Outflow = 62.73 cfs @ 12.20 hrs, Volume= 4.415 af, Atten= 4%, Lag= 1.5 min

Routed to Link Swale 1 R6: Swale S1 Reach 6

Routing by Dyn-Stor-Ind method, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

Max. Velocity= 3.44 fps, Min. Travel Time= 2.1 min

Avg. Velocity = 0.76 fps, Avg. Travel Time= 9.4 min

Peak Storage= 7,852 cf @ 12.20 hrs

Average Depth at Peak Storage= 1.36', Surface Width= 18.86'

Bank-Full Depth= 2.00' Flow Area= 32.0 sf, Capacity= 136.28 cfs

8.00' x 2.00' deep channel, n= 0.030 Earth, grassed & winding

Side Slope Z-value= 4.0 '/' Top Width= 24.00'

Length= 430.9' Slope= 0.0052 '/'

Inlet Invert= 807.15', Outlet Invert= 804.92'

MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59" Printed 4/11/2022

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#### Summary for Reach S2 R1: Swale S2 Reach 1

Inflow Area = 25.203 ac, 0.00% Impervious, Inflow Depth = 2.14" for 100-yr, 24-hr event

Inflow = 62.82 cfs @ 12.20 hrs, Volume= 4.489 af

Outflow = 57.87 cfs @ 12.24 hrs, Volume= 4.489 af, Atten= 8%, Lag= 2.5 min

Routed to Link Swale S2 R1 : Swale S2 Reach 1

Routing by Dyn-Stor-Ind method, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

Max. Velocity= 2.39 fps, Min. Travel Time= 3.3 min Avg. Velocity = 0.52 fps, Avg. Travel Time= 15.1 min

Peak Storage= 11,415 cf @ 12.24 hrs

Average Depth at Peak Storage= 1.65', Surface Width= 21.24' Bank-Full Depth= 2.00' Flow Area= 32.0 sf, Capacity= 84.99 cfs

8.00' x 2.00' deep channel, n= 0.030 Earth, grassed & winding

Side Slope Z-value= 4.0 '/' Top Width= 24.00'

Length= 472.0' Slope= 0.0020 '/'

Inlet Invert= 802.25', Outlet Invert= 801.30'



# Summary for Reach S2 R2: Swale S2 Reach 2

Inflow Area = 42.068 ac, 0.00% Impervious, Inflow Depth = 2.21" for 100-yr, 24-hr event

Inflow = 95.28 cfs @ 12.17 hrs, Volume= 7.736 af

Outflow = 90.88 cfs @ 12.23 hrs, Volume= 7.736 af, Atten= 5%, Lag= 3.1 min

Routed to Link Swale S2 R2 : Swale S2 Reach 2

Routing by Dyn-Stor-Ind method, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

Max. Velocity= 4.16 fps, Min. Travel Time= 3.0 min

Avg. Velocity = 0.88 fps, Avg. Travel Time= 14.3 min

Peak Storage= 16,407 cf @ 12.23 hrs

Average Depth at Peak Storage= 1.40', Surface Width= 21.20'

Bank-Full Depth= 2.00' Flow Area= 36.0 sf, Capacity= 182.04 cfs

MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

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10.00' x 2.00' deep channel, n= 0.030 Earth, grassed & winding Side Slope Z-value= 4.0 '/' Top Width= 26.00' Length= 751.0' Slope= 0.0069 '/' Inlet Invert= 801.30', Outlet Invert= 796.10'



#### Summary for Reach S3 R1: Swale S3 Reach 1

Inflow Area = 4.976 ac, 0.00% Impervious, Inflow Depth = 3.18" for 100-yr, 24-hr event

Inflow = 27.41 cfs @ 12.12 hrs, Volume= 1.319 af

Outflow = 26.88 cfs @ 12.13 hrs, Volume= 1.319 af, Atten= 2%, Lag= 0.6 min

Routed to Link Swale S3 R1: Swale S3 Reach 1

Routing by Dyn-Stor-Ind method, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

Max. Velocity= 3.26 fps, Min. Travel Time= 1.1 min Avg. Velocity = 0.77 fps, Avg. Travel Time= 4.7 min

Peak Storage= 1,774 cf @ 12.13 hrs

Average Depth at Peak Storage= 0.85', Surface Width= 11.40' Bank-Full Depth= 2.00' Flow Area= 24.0 sf, Capacity= 125.24 cfs

8.00' x 2.00' deep channel, n= 0.030 Earth, grassed & winding

Side Slope Z-value= 2.0 '/' Top Width= 16.00'

Length= 215.0' Slope= 0.0070 '/'

Inlet Invert= 807.58', Outlet Invert= 806.08'



# Summary for Reach S3 R2: Swale S3 Reach 2

Inflow Area = 10.265 ac, 0.00% Impervious, Inflow Depth = 2.84" for 100-yr, 24-hr event

Inflow = 47.52 cfs @ 12.13 hrs, Volume= 2.432 af

Outflow = 47.32 cfs @ 12.13 hrs, Volume= 2.432 af, Atten= 0%, Lag= 0.3 min

Routed to Link Swale S3 R2: Swale S3 Reach 2

Routing by Dyn-Stor-Ind method, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs Max. Velocity= 4.13 fps, Min. Travel Time= 0.4 min

Avg. Velocity = 1.45 fps, Avg. Travel Time= 1.1 min

MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

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Peak Storage= 1,111 cf @ 12.13 hrs

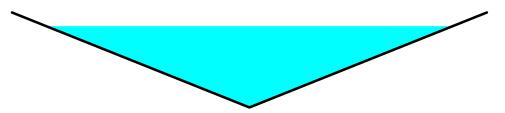
Average Depth at Peak Storage= 2.14', Surface Width= 10.70' Bank-Full Depth= 2.50' Flow Area= 15.6 sf, Capacity= 71.57 cfs

0.00' x 2.50' deep channel, n= 0.030 Earth, grassed & winding

Side Slope Z-value= 2.5 '/' Top Width= 12.50'

Length= 97.0' Slope= 0.0070 '/'

Inlet Invert= 806.08', Outlet Invert= 805.40'



#### Summary for Reach S3 R3: Swale S3 Reach 3

Inflow Area = 11.158 ac, 0.00% Impervious, Inflow Depth = 2.72" for 100-yr, 24-hr event

47.83 cfs @ 12.13 hrs, Volume= 2.533 af Inflow

Outflow 46.22 cfs @ 12.15 hrs, Volume= 2.533 af, Atten= 3%, Lag= 0.9 min

Routed to Link Swale S3 R3: Swale S3 Reach 3

Routing by Dyn-Stor-Ind method, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

Max. Velocity= 3.94 fps, Min. Travel Time= 1.5 min

Avg. Velocity = 1.02 fps, Avg. Travel Time= 5.8 min

Peak Storage= 4,140 cf @ 12.15 hrs

Average Depth at Peak Storage= 0.98', Surface Width= 15.86' Bank-Full Depth= 2.00' Flow Area= 32.0 sf, Capacity= 186.19 cfs

8.00' x 2.00' deep channel, n= 0.030 Earth, grassed & winding

Side Slope Z-value= 4.0 '/' Top Width= 24.00'

Length= 353.0' Slope= 0.0097 '/'

Inlet Invert= 804.71', Outlet Invert= 801.30'



#### Summary for Reach S4 R2: Swale S4 Reach 2

4.541 ac. 0.00% Impervious, Inflow Depth = 3.18" for 100-yr, 24-hr event Inflow Area =

23.68 cfs @ 12.13 hrs, Volume= Inflow 1.204 af

20.91 cfs @ 12.16 hrs. Volume= 1.204 af, Atten= 12%, Lag= 1.8 min Outflow

Routed to Reach S4 R3: Swale S4 Reach 3

MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs Max. Velocity= 2.70 fps, Min. Travel Time= 3.7 min Avg. Velocity = 0.63 fps, Avg. Travel Time= 16.0 min

Peak Storage= 4,652 cf @ 12.16 hrs Average Depth at Peak Storage= 0.63', Surface Width= 14.44' Bank-Full Depth= 2.00' Flow Area= 34.0 sf, Capacity= 174.20 cfs

10.00' x 2.00' deep channel, n= 0.030 Earth, grassed & winding Side Slope Z-value= 4.0 3.0 '/' Top Width= 24.00' Length= 601.0' Slope= 0.0069 '/' Inlet Invert= 806.43', Outlet Invert= 802.26'



#### Summary for Reach S4 R3: Swale S4 Reach 3

[62] Hint: Exceeded Reach S4 R2 OUTLET depth by 0.32' @ 12.25 hrs

Inflow Area = 8.711 ac, 0.00% Impervious, Inflow Depth = 3.18" for 100-yr, 24-hr event

Inflow = 41.60 cfs @ 12.14 hrs, Volume= 2.309 af

Outflow = 34.31 cfs @ 12.18 hrs, Volume= 2.309 af, Atten= 18%, Lag= 2.7 min

Routed to Reach S4 R4: Swale S4 Reach 4

Routing by Dyn-Stor-Ind method, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs Max. Velocity= 2.94 fps, Min. Travel Time= 5.4 min Avg. Velocity = 0.64 fps, Avg. Travel Time= 24.5 min

Peak Storage= 11,027 cf @ 12.18 hrs Average Depth at Peak Storage= 0.89', Surface Width= 16.22' Bank-Full Depth= 2.00' Flow Area= 34.0 sf, Capacity= 156.53 cfs

10.00' x 2.00' deep channel, n= 0.030 Earth, grassed & winding Side Slope Z-value= 3.0 4.0 '/' Top Width= 24.00' Length= 946.0' Slope= 0.0056 '/' Inlet Invert= 802.26', Outlet Invert= 796.96'



MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

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#### Summary for Reach S4 R4: Swale S4 Reach 4

[62] Hint: Exceeded Reach S4 R3 OUTLET depth by 0.96' @ 12.25 hrs

Inflow Area = 65.063 ac, 0.04% Impervious, Inflow Depth = 2.33" for 100-yr, 24-hr event

Inflow = 159.67 cfs @ 12.19 hrs, Volume= 12.653 af

Outflow = 157.44 cfs @ 12.21 hrs, Volume= 12.653 af, Atten= 1%, Lag= 1.3 min

Routed to Link Swale S4 R4: Swale S4 Reach 4

Routing by Dyn-Stor-Ind method, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

Max. Velocity= 5.29 fps, Min. Travel Time= 1.5 min Avg. Velocity = 1.12 fps, Avg. Travel Time= 7.2 min

Peak Storage= 14,379 cf @ 12.21 hrs

Average Depth at Peak Storage= 1.82', Surface Width= 22.73' Bank-Full Depth= 3.00' Flow Area= 61.5 sf, Capacity= 427.66 cfs

10.00' x 3.00' deep channel, n= 0.030 Earth, grassed & winding

Side Slope Z-value= 3.0 4.0 '/' Top Width= 31.00'

Length= 483.0' Slope= 0.0082 '/'

Inlet Invert= 796.96', Outlet Invert= 793.00'



#### Summary for Reach S5 R2: Swale S5 Reach 2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 4.530 ac, 13.14% Impervious, Inflow Depth = 1.20" for 100-yr, 24-hr event

Inflow = 7.48 cfs @ 12.15 hrs, Volume= 0.454 af

Outflow = 7.48 cfs @ 12.15 hrs, Volume= 0.454 af, Atten= 0%, Lag= 0.0 min

Routed to Link Swale S5 R2: Swale S5 Reach 2

Routing by Dyn-Stor-Ind method, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

**Summary for Pond Sed Pond: Sedimentation Basin** 

MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

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Inflow Area =	74.393 ac,	2.06% Impervious, Inflow	/ Depth = 2.25"	for 100-yr, 24-hr event
Inflow =	164.77 cfs @	12.20 hrs, Volume=	13.946 af	
Outflow =	45.68 cfs @	12.70 hrs, Volume=	13.947 af, Atte	en= 72%, Lag= 30.2 min
Discarded =	5.84 cfs @	12.70 hrs, Volume=	7.167 af	_
Primary =	11.35 cfs @	12.70 hrs, Volume=	4.914 af	
Routed to Lir	nk Wetland : We	etland		
Secondary =	22.50 cfs @	12.70 hrs, Volume=	1.762 af	
Routed to Lir	nk Wetland : We	etland		
Tertiary =	6.00 cfs @	12.70 hrs, Volume=	0.104 af	
Routed to Lir	nk Wetland : We	etland		

Routing by Dyn-Stor-Ind method, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs Peak Elev= 793.06' @ 12.70 hrs Surf.Area= 70,052 sf Storage= 236,005 cf Flood Elev= 794.00' Surf.Area= 75,797 sf Storage= 304,443 cf

Avail.Storage Storage Description

Plug-Flow detention time= (not calculated: outflow precedes inflow)

Center-of-Mass det. time= 169.7 min ( 1,014.6 - 845.0 )

Invert

#1	789.00'	304,44	13 cf Custom	Stage Data (P	rismatic)Listed below (Recalc)
Elevation	on Surf.	Surf.Area		Cum.Store	
(fee	et) (:	sq-ft)	(cubic-feet)	(cubic-feet)	
789.0	00 27	7,325	0	0	
790.0	00 55	5,972	41,649	41,649	
791.0	00 61	1,532	58,752	100,401	
792.0		5,703	63,618	164,018	
793.0		9,675	67,689	231,707	
794.0	00 75	5,797	72,736	304,443	
Device	Routing	Invert	Outlet Devices	<b>S</b>	
#1	Primary	787.70'	15.0" Round	Culvert	
	•		L= 40.0' RCP	, mitered to co	nform to fill, Ke= 0.700
			Inlet / Outlet In	vert= 787.70' /	787.50' S= 0.0050 '/' Cc= 0.900
					ight & clean, Flow Area= 1.23 sf
#2	Device 1	791.00'			
				flow at low hea	
#3	Device 1	790.50'		ice/Grate X 4.0	
11.4	D : 4	700 001		flow at low hea	
#4 Device 1 790.00'			fice/Grate X 4.0		
μг	Davisa 1	700 001		flow at low hea	
#5	Device 1	789.00'		<b>fice/Grate X 14</b> 6.0" cc spacing	
				flow at low hea	
#6	Secondary	792.50'			Broad-Crested Rectangular Weir
#0	Occordary	192.50			0.80 1.00 1.20 1.40 1.60
					.70 2.69 2.68 2.69 2.67 2.64
#7	Tertiary	793.00'			Broad-Crested Rectangular Weir
	. G. tidi y				0.80 1.00 1.20 1.40 1.60
					.70 2.69 2.68 2.69 2.67 2.64
#8	Discarded	789.00'		filtration over	

MSE 24-hr 4 100-yr, 24-hr Rainfall=6.59"

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Discarded OutFlow Max=5.84 cfs @ 12.70 hrs HW=793.06' (Free Discharge) **-8=Exfiltration** (Exfiltration Controls 5.84 cfs)

Primary OutFlow Max=11.35 cfs @ 12.70 hrs HW=793.06' TW=0.00' (Dynamic Tailwater)

-1=Culvert (Inlet Controls 11.35 cfs @ 9.25 fps)

**2=Orifice/Grate** (Passes < 33.94 cfs potential flow)

-3=Orifice/Grate (Passes < 0.11 cfs potential flow)

**-4=Orifice/Grate** (Passes < 0.12 cfs potential flow)

-5=Orifice/Grate (Passes < 0.91 cfs potential flow)

Secondary OutFlow Max=22.49 cfs @ 12.70 hrs HW=793.06' TW=0.00' (Dynamic Tailwater) -6=Broad-Crested Rectangular Weir (Weir Controls 22.49 cfs @ 2.00 fps)

Tertiary OutFlow Max=5.99 cfs @ 12.70 hrs HW=793.06' TW=0.00' (Dynamic Tailwater) 7=Broad-Crested Rectangular Weir (Weir Controls 5.99 cfs @ 0.62 fps)

### Summary for Link C1: Culvert C1

4.530 ac, 13.14% Impervious, Inflow Depth = 1.20" for 100-yr, 24-hr event Inflow Area =

Inflow 7.48 cfs @ 12.15 hrs, Volume= 0.454 af

7.48 cfs @ 12.15 hrs, Volume= 0.454 af, Atten= 0%, Lag= 0.0 min

Routed to Reach S5 R2 : Swale S5 Reach 2

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

## Summary for Link C2: Culvert C2

Inflow Area = 2.899 ac, 0.00% Impervious, Inflow Depth = 3.23" for 100-yr, 24-hr event

13.45 cfs @ 12.11 hrs, Volume= Inflow 0.780 af

13.45 cfs @ 12.11 hrs, Volume= 0.780 af, Atten= 0%, Lag= 0.0 min Primary

Routed to Reach S1 R3: Swale S1 Reach 3

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

## Summary for Link C3: Culvert C3

14.170 ac, 0.00% Impervious, Inflow Depth = 2.58" for 100-yr, 24-hr event Inflow Area =

47.76 cfs @ 12.15 hrs, Volume= Inflow 3.049 af

47.76 cfs @ 12.15 hrs, Volume= 3.049 af, Atten= 0%, Lag= 0.0 min Primary

Routed to Reach S1 R4: Swale S1 Reach 4

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### **Summary for Link C4: Culvert C4**

Inflow Area = 17.714 ac, 0.00% Impervious, Inflow Depth = 2.61" for 100-yr, 24-hr event

Inflow = 62.23 cfs @ 12.15 hrs, Volume= 3.859 af

Primary = 62.23 cfs @ 12.15 hrs, Volume= 3.859 af, Atten= 0%, Lag= 0.0 min

Routed to Reach S1 R5 : Swale S1 Reach 5

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### Summary for Link C5: Culvert C5

Inflow Area = 20.996 ac, 0.00% Impervious, Inflow Depth = 2.43" for 100-yr, 24-hr event

Inflow = 65.15 cfs @ 12.17 hrs, Volume= 4.254 af

Primary = 65.15 cfs @ 12.17 hrs, Volume= 4.254 af, Atten= 0%, Lag= 0.0 min

Routed to Reach S1 R6: Swale S1 Reach 6

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### **Summary for Link C6: Culvert C6**

Inflow Area = 11.158 ac, 0.00% Impervious, Inflow Depth = 2.72" for 100-yr, 24-hr event

Inflow = 47.83 cfs @ 12.13 hrs, Volume= 2.533 af

Primary = 47.83 cfs @ 12.13 hrs, Volume= 2.533 af, Atten= 0%, Lag= 0.0 min

Routed to Reach S3 R3: Swale S3 Reach 3

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

## **Summary for Link C7: Culvert C7**

Inflow Area = 48.985 ac, 0.00% Impervious, Inflow Depth = 2.20" for 100-yr, 24-hr event

Inflow = 103.37 cfs @ 12.20 hrs, Volume= 8.978 af

Primary = 103.37 cfs @ 12.20 hrs, Volume= 8.978 af, Atten= 0%, Lag= 0.0 min

Routed to Reach S4 R4: Swale S4 Reach 4

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

## **Summary for Link C8: Culvert C8**

Inflow Area = 7.668 ac, 11.88% Impervious, Inflow Depth = 1.76" for 100-yr, 24-hr event

Inflow = 19.20 cfs @ 12.15 hrs, Volume= 1.127 af

Primary = 19.20 cfs @ 12.15 hrs, Volume= 1.127 af, Atten= 0%, Lag= 0.0 min

Routed to Link North Area: North Area

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## **Summary for Link F1: Flume 1**

Inflow Area = 4.170 ac, 0.00% Impervious, Inflow Depth = 3.18" for 100-yr, 24-hr event

Inflow = 22.19 cfs @ 12.13 hrs, Volume= 1.105 af

Primary = 22.19 cfs @ 12.13 hrs, Volume= 1.105 af, Atten= 0%, Lag= 0.0 min

Routed to Link RC1: Rock Chute 1

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### **Summary for Link F2: Flume 2**

Inflow Area = 4.541 ac, 0.00% Impervious, Inflow Depth = 3.18" for 100-yr, 24-hr event

Inflow = 23.68 cfs @ 12.13 hrs, Volume= 1.204 af

Primary = 23.68 cfs @ 12.13 hrs, Volume= 1.204 af, Atten= 0%, Lag= 0.0 min

Routed to Link RC2: Rock Chute 2

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### **Summary for Link F3: Flume 3**

Inflow Area = 5.923 ac, 0.00% Impervious, Inflow Depth = 3.18" for 100-yr, 24-hr event

Inflow = 32.10 cfs @ 12.12 hrs, Volume= 1.570 af

Primary = 32.10 cfs @ 12.12 hrs, Volume= 1.570 af, Atten= 0%, Lag= 0.0 min

Routed to Reach S1 R2: Swale S1 Reach 2

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

## **Summary for Link F4: Flume 4**

Inflow Area = 2.645 ac, 0.00% Impervious, Inflow Depth = 3.18" for 100-yr, 24-hr event

Inflow = 14.43 cfs @ 12.12 hrs, Volume= 0.701 af

Primary = 14.43 cfs @ 12.12 hrs, Volume= 0.701 af, Atten= 0%, Lag= 0.0 min

Routed to Reach S1 R4: Swale S1 Reach 4

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

## **Summary for Link F5: Flume 5**

Inflow Area = 4.601 ac, 0.00% Impervious, Inflow Depth = 3.18" for 100-yr, 24-hr event

Inflow = 25.31 cfs @ 12.12 hrs, Volume= 1.219 af

Primary = 25.31 cfs @ 12.12 hrs, Volume= 1.219 af, Atten= 0%, Lag= 0.0 min

Routed to Reach S3 R1: Swale S3 Reach 1

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### **Summary for Link F6: Flume 6**

Inflow Area = 3.717 ac, 0.00% Impervious, Inflow Depth = 3.18" for 100-yr, 24-hr event

Inflow = 20.36 cfs @ 12.12 hrs, Volume= 0.985 af

Primary = 20.36 cfs @ 12.12 hrs, Volume= 0.985 af, Atten= 0%, Lag= 0.0 min

Routed to Reach S3 R2 : Swale S3 Reach 2

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### **Summary for Link F7: Existing East Flume**

Inflow Area = 0.830 ac, 0.00% Impervious, Inflow Depth = 3.12" for 100-yr, 24-hr event

Inflow = 4.50 cfs @ 12.12 hrs, Volume= 0.216 af

Primary = 4.50 cfs @ 12.12 hrs, Volume= 0.216 af, Atten= 0%, Lag= 0.0 min

Routed to Reach S2 R2: Swale S2 Reach 2

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### **Summary for Link F8: Existing West Flume**

Inflow Area = 3.122 ac, 0.00% Impervious, Inflow Depth = 3.18" for 100-yr, 24-hr event

Inflow = 16.40 cfs @ 12.13 hrs, Volume= 0.828 af

Primary = 16.40 cfs @ 12.13 hrs, Volume= 0.828 af, Atten= 0%, Lag= 0.0 min

Routed to Link Swale S2 R2 : Swale S2 Reach 2

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

## **Summary for Link North Area: North Area**

Inflow Area = 7.668 ac, 11.88% Impervious, Inflow Depth = 1.76" for 100-yr, 24-hr event

Inflow = 19.20 cfs @ 12.15 hrs, Volume= 1.127 af

Primary = 19.20 cfs @ 12.15 hrs, Volume= 1.127 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

## **Summary for Link RC1: Rock Chute 1**

Inflow Area = 4.170 ac, 0.00% Impervious, Inflow Depth = 3.18" for 100-yr, 24-hr event

Inflow = 22.19 cfs @ 12.13 hrs, Volume= 1.105 af

Primary = 22.19 cfs @ 12.13 hrs, Volume= 1.105 af, Atten= 0%, Lag= 0.0 min

Routed to Reach S4 R3: Swale S4 Reach 3

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## Summary for Link RC2: Rock Chute 2

Inflow Area = 4.541 ac, 0.00% Impervious, Inflow Depth = 3.18" for 100-yr, 24-hr event

Inflow = 23.68 cfs @ 12.13 hrs, Volume= 1.204 af

Primary = 23.68 cfs @ 12.13 hrs, Volume= 1.204 af, Atten= 0%, Lag= 0.0 min

Routed to Reach S4 R2 : Swale S4 Reach 2

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### Summary for Link Swale 1 R6: Swale S1 Reach 6

Inflow Area = 23.788 ac, 0.00% Impervious, Inflow Depth = 2.23" for 100-yr, 24-hr event

Inflow = 62.73 cfs @ 12.20 hrs, Volume= 4.415 af

Primary = 62.73 cfs @ 12.20 hrs, Volume= 4.415 af, Atten= 0%, Lag= 0.0 min

Routed to Reach S2 R1: Swale S2 Reach 1

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### Summary for Link Swale S1 R1: Swale S1 Reach 1

Inflow Area = 0.691 ac, 0.00% Impervious, Inflow Depth = 2.23" for 100-yr, 24-hr event

Inflow = 2.68 cfs @ 12.12 hrs, Volume= 0.128 af

Primary = 2.68 cfs @ 12.12 hrs, Volume= 0.128 af, Atten= 0%, Lag= 0.0 min

Routed to Reach S1 R2 : Swale S1 Reach 2

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

## Summary for Link Swale S1 R2: Swale S1 Reach 2

Inflow Area = 7.131 ac, 0.00% Impervious, Inflow Depth = 3.07" for 100-yr, 24-hr event

Inflow = 37.05 cfs @ 12.12 hrs, Volume= 1.827 af

Primary = 37.05 cfs @ 12.12 hrs, Volume= 1.827 af, Atten= 0%, Lag= 0.0 min

Routed to Reach S1 R3: Swale S1 Reach 3

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

## Summary for Link Swale S1 R3: Swale S1 Reach 3

Inflow Area = 14.170 ac, 0.00% Impervious, Inflow Depth = 2.58" for 100-yr, 24-hr event

Inflow = 47.76 cfs @ 12.15 hrs, Volume= 3.049 af

Primary = 47.76 cfs @ 12.15 hrs, Volume= 3.049 af, Atten= 0%, Lag= 0.0 min

Routed to Link C3: Culvert C3

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## Summary for Link Swale S1 R4: Swale S1 Reach 4

Inflow Area = 17.714 ac, 0.00% Impervious, Inflow Depth = 2.61" for 100-yr, 24-hr event

Inflow = 62.23 cfs @ 12.15 hrs, Volume= 3.859 af

Primary = 62.23 cfs @ 12.15 hrs, Volume= 3.859 af, Atten= 0%, Lag= 0.0 min

Routed to Link C4: Culvert C4

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### Summary for Link Swale S1 R5: Swale S1 Reach 5

Inflow Area = 20.996 ac, 0.00% Impervious, Inflow Depth = 2.43" for 100-yr, 24-hr event

Inflow = 65.15 cfs @ 12.17 hrs, Volume= 4.254 af

Primary = 65.15 cfs @ 12.17 hrs, Volume= 4.254 af, Atten= 0%, Lag= 0.0 min

Routed to Link C5: Culvert C5

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### Summary for Link Swale S2 R1: Swale S2 Reach 1

Inflow Area = 25.901 ac, 0.00% Impervious, Inflow Depth = 2.10" for 100-yr, 24-hr event

Inflow = 58.13 cfs @ 12.24 hrs, Volume= 4.525 af

Primary = 58.13 cfs @ 12.24 hrs, Volume= 4.525 af, Atten= 0%, Lag= 0.0 min

Routed to Reach S2 R2: Swale S2 Reach 2

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

## Summary for Link Swale S2 R2: Swale S2 Reach 2

Inflow Area = 48.985 ac, 0.00% Impervious, Inflow Depth = 2.20" for 100-yr, 24-hr event

Inflow = 103.37 cfs @ 12.20 hrs, Volume= 8.978 af

Primary = 103.37 cfs @ 12.20 hrs, Volume= 8.978 af, Atten= 0%, Lag= 0.0 min

Routed to Link C7: Culvert C7

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

## Summary for Link Swale S3 R1: Swale S3 Reach 1

Inflow Area = 6.548 ac, 0.00% Impervious, Inflow Depth = 2.65" for 100-yr, 24-hr event

Inflow = 27.22 cfs @ 12.13 hrs, Volume= 1.447 af

Primary = 27.22 cfs @ 12.13 hrs, Volume= 1.447 af, Atten= 0%, Lag= 0.0 min

Routed to Reach S3 R2: Swale S3 Reach 2

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## Summary for Link Swale S3 R2: Swale S3 Reach 2

Inflow Area = 11.158 ac, 0.00% Impervious, Inflow Depth = 2.72" for 100-yr, 24-hr event

Inflow = 47.83 cfs @ 12.13 hrs, Volume= 2.533 af

Primary = 47.83 cfs @ 12.13 hrs, Volume= 2.533 af, Atten= 0%, Lag= 0.0 min

Routed to Link C6: Culvert C6

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### Summary for Link Swale S3 R3: Swale S3 Reach 3

Inflow Area = 14.511 ac, 0.00% Impervious, Inflow Depth = 2.36" for 100-yr, 24-hr event

Inflow = 47.45 cfs @ 12.15 hrs, Volume= 2.848 af

Primary = 47.45 cfs @ 12.15 hrs, Volume= 2.848 af, Atten= 0%, Lag= 0.0 min

Routed to Reach S2 R2 : Swale S2 Reach 2

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### Summary for Link Swale S4 R4: Swale S4 Reach 4

Inflow Area = 67.064 ac, 0.04% Impervious, Inflow Depth = 2.29" for 100-yr, 24-hr event

Inflow = 157.92 cfs @ 12.21 hrs, Volume= 12.803 af

Primary = 157.92 cfs @ 12.21 hrs, Volume= 12.803 af, Atten= 0%, Lag= 0.0 min

Routed to Pond Sed Pond : Sedimentation Basin

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

## Summary for Link Swale S5 R1: Swale S5 Reach 1

Inflow Area = 4.530 ac, 13.14% Impervious, Inflow Depth = 1.20" for 100-yr, 24-hr event

Inflow = 7.48 cfs @ 12.15 hrs, Volume= 0.454 af

Primary = 7.48 cfs @ 12.15 hrs, Volume= 0.454 af, Atten= 0%, Lag= 0.0 min

Routed to Link C1: Culvert C1

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

## Summary for Link Swale S5 R2: Swale S5 Reach 2

Inflow Area = 5.851 ac, 12.83% Impervious, Inflow Depth = 1.48" for 100-yr, 24-hr event

Inflow = 12.65 cfs @ 12.14 hrs, Volume= 0.720 af

Primary = 12.65 cfs @ 12.14 hrs, Volume= 0.720 af, Atten= 0%, Lag= 0.0 min

Routed to Link C8: Culvert C8

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### Summary for Link Swale S5 R3: Swale S5 Reach 3

Inflow Area = 1.817 ac, 8.81% Impervious, Inflow Depth = 2.69" for 100-yr, 24-hr event

Inflow = 6.90 cfs @ 12.17 hrs, Volume= 0.408 af

Primary = 6.90 cfs @ 12.17 hrs, Volume= 0.408 af, Atten= 0%, Lag= 0.0 min

Routed to Link C8 : Culvert C8

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### Summary for Link Swale S6 R1: Swale S6 Reach 1

Inflow Area = 2.899 ac, 0.00% Impervious, Inflow Depth = 3.23" for 100-yr, 24-hr event

Inflow = 13.45 cfs @ 12.11 hrs, Volume= 0.780 af

Primary = 13.45 cfs @ 12.11 hrs, Volume= 0.780 af, Atten= 0%, Lag= 0.0 min

Routed to Link C2: Culvert C2

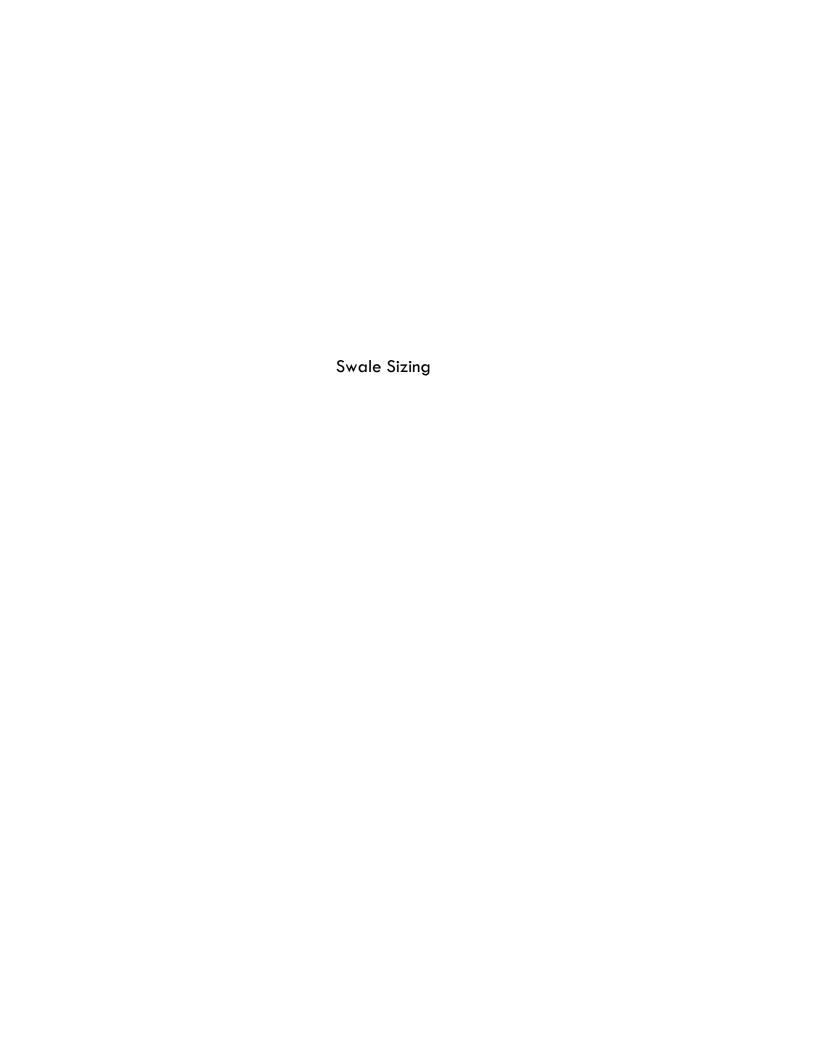
Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.01 hrs

### **Summary for Link Wetland: Wetland**

Inflow Area = 74.393 ac, 2.06% Impervious, Inflow Depth = 1.09" for 100-yr, 24-hr event

Inflow = 39.85 cfs @ 12.70 hrs, Volume= 6.780 af

Primary = 39.85 cfs @ 12.70 hrs, Volume= 6.780 af, Atten= 0%, Lag= 0.0 min



SCS ENGINE	ERS	Sheet No:	1 of 2
		Calc. No.	
		Rev. No.	0
Job No. 25220183.00	Job: Columbia Energy Center POO Landfill Closure	By: RJG	Date: 2/23/22
Client: WPL	Subject: Swale Sizing	Chk'd: MJT	Date: 4/5/22

#### Purpose:

To size the proposed swale along Module 10 and 11 to accommodate the 25-year, 24-hour storm event and determine required rolled erosion control product. To confirm capacity of existing swale during closure condition.

#### References:

- 1. WisDOT Facilities Development Manual Chapter 13, Section 30-15 Grass Lined Channels.
- 2. Design of Roadside Channels with Flexible Linings, HEC-15, USDOT FHWA.
- 3. HydroCAD Report\_POO Landfill Closure
- 4. Table 7E-5.01: Typical Rolled Erosion Control Product Properties and Uses, lowa SUDAS Design and Specifications Manual.

#### Approach:

Use the HydroCAD Model results to obtain the peak flow during a 25-year, 24-hour storm event.

Use Grass Lined Channel Design WisDOT Spreadsheet, FDM 13-30 Attachment 15.2 (from Reference #1) to size the swale for each design swale cross section. The WisDOT spreadsheet incorporates the design guidelines and equations described in "Design of Roadside Channels with Flexible Linings", HEC-15, USDOT FHWA (Reference #2).

Confirm the swale is stable and has enough capacity for the design flow rate.

Use Table 7E-5.01 (see Reference #4) to select appropriate erosion control mat based on shear stress and application.

#### Assumptions:

- 1. Swales geometry shown on the drawing set.
- 2. Assume the following parameters per Section 15.2 Grass Lining Properties from Reference #1:

Vegetation Retardance Class = C for Swales

Vegetation Condition = Good

Vegetation Growth Form = Turf

3. Assume cohesive soil type with ASTM Soil Class SC and a Plasticity Index (PI) of 16.

#### Calculations:

From the HydroCAD Report, the 25-year, 24-hour peak discharge rates in the swales are

Swales:	25-year		25-year		25-year
Swale \$1 Reach 1=	1.37 cfs	Swale S2 Reach 2=	52.2 cfs	Swale S4 Reach 4=	80.1 cfs
Swale \$1 Reach 2=	21.7 cfs	Swale S3 Reach 1=	15.9 cfs	Swale S5 Reach 1=	2.1 cfs
Swale \$1 Reach 3=	27.4 cfs	Swale S3 Reach 2=	27.9 cfs	Swale S5 Reach 2=	4.7 cfs
Swale \$1 Reach 4=	35.4 cfs	Swale S3 Reach 3=	26.7 cfs	Swale S5 Reach 3=	3.8 cfs
Swale \$1 Reach 5=	35.2 cfs	Swale S4 Reach 1*=	cfs	Swale S6 Reach 1=	9.7 cfs
Swale \$1 Reach 6=	33.2 cfs	Swale S4 Reach 2*=	cfs		
Swale S2 Reach 1=	30.0 cfs	Swale S4 Reach 3*=	cfs		

Use max. flow from Swale S1 reaches to confirm swale works since slope is constant.

Use the WisDOT Grass Swale Design Spreadsheet (Page 2) to determine the flow depth, velocity and shear stress in the swales.

#### Results:

The swales are adequately designed to accommodate the flows from the 25-year, 24-hour storm event.

The swales are stable at the design flow rates.

Use Class I, Type B erosion mat.

<sup>\*</sup>Use full Swale S4 Reach 4 for swale flow in Swale S4 reaches.

### SCS ENGINEERS SCS ENGINEERS

| Sheet No: | Calc. No. | Rev. No. | By: RJG | Date: 2/23/22 | Chk'd: MJT | Date: 4/5/22 | Job: Columbia Energy Center POO Landfill Closure Subject: Swale Sizing Job No. 25220183.00 Client: WPL

Channel/Ditch Geometry	Swale S1	Swale S1 Reach 1	Swale S1 Reach 2	Swale S1 Reach 3	Swale S1 Reach 4	Swale S1 Reach 5	Swale S1 Reach 6	Swale S2 Reach 1	Swale S2 Reach 2	Swale S3 Reach 1	Swale S3 Reach 2	Swale S3 Reach 3	Swale S4 Reach 1	Swale S4 Reach 2	Swale S4 Reach 3	Swale S4 Reach 4	Swale S5 Reach 1	Swale S5 Reach 2	Swale S5 Reach 3	Swale S6 Reach 1
Channel Slope, S <sub>o</sub> (ft/ft)	0.0055	0.0053	0.0055	0.0051	0.0069	0.0053	0.0084	0.0020	0.0069	0.0070	0.0070	0.0097	0.0155	0.0069	0.0056	0.0082	0.0096	0.0024	0.0024	0.0066
Channel Bottom Width, B (ft)	8	8	8	8	8	8	8	8	10	8	8	0	10	10	10	10	0	0	0	8
Channel Side Slope, z	4	4	4	4	4	4	4	4	4	2	2	4	4	4	4	4	6	6	6	2.5
Channel Side Slope, z <sub>2</sub>	4	4	4	4	4	4	4	4	4	2	2	4	3	3	3	3	7	2.5	2.5	2.5
Flow Depth, d (ft) Solve iteratively	1.59	0.37	1.30	1.47	1.46	1.61	1.32	2.18	1.61	1.07	1.39	1.81	1.42	1.97	2.13	1.85	0.67	1.51	1.41	0.85
Safety Factor, SF	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
Vegetation/Soil Parameters																				
Vegetation Retardance Class	С	С	С	С	С	С	С	С	С	С	С	С	С	С	С	С	С	С	С	С
Vegetation Condition	good	good	good	good	good	good	good	good	good	good	good	good	good	good	good	good	good	good	good	good
Vegetation Growth Form	turf	turf	turf	turf	turf	turf	turf	turf	turf	turf	turf	turf	turf	turf	turf	turf	turf	turf	turf	turf
Soil Type	cohesive	cohesive	cohesive	cohesive	cohesive	cohesive	cohesive	cohesive	cohesive	cohesive	cohesive	cohesive	cohesive	cohesive	cohesive	cohesive	cohesive	cohesive	cohesive	cohesive
D <sub>75</sub> (in) (Set at 0.00 for cohesive soils)																				
ASTM Soil Class	SC	sc	SC	sc	sc	SC	SC	SC	SC	SC	SC	SC	SC	SC	SC	SC	SC	SC	SC	SC
Plasticity Index, Pl	16	16	16	16	16	16	16	16	16	16	16	16	16	16	16	16	16	16	16	16
Results Summary																				
Design Q (ft <sup>3</sup> /s)	35.4	1.4	21.7	27.4	35.4	35.2	33.2	30.0	52.2	15.9	27.9	26.7	80.1	80.1	80.1	80.1	2.1	4.7	3.8	9.7
<ol> <li>Swales geometry shown on the drawing set.</li> </ol>	35.4	1.4	22.1	27.4	35.4	35.2	33.5	29.8	52.5	16.0	28.0	27.1	79.6	80.5	79.5	81.6	2.1	4.7	3.8	9.6
Difference Between Design & Calc. Flow (%)	0.2%	0.2%	1.9%	0.0%	0.1%	0.0%	1.0%	-0.4%	0.6%	0.5%	0.6%	1.6%	-0.6%	0.5%	-0.7%	1.8%	0.0%	-0.3%	0.2%	-0.5%
Stable (Yes or No)	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES
Channel Parameters																				
Vegetation Height, h (ft)	0.67	0.67	0.67	0.67	0.67	0.67	0.67	0.67	0.67	0.67	0.67	0.67	0.67	0.67	0.67	0.67	0.67	0.67	0.67	0.67
Grass Roughness Coefficient, Ch	0.238	0.238	0.238	0.238	0.238	0.238	0.238	0.238	0.238	0.238	0.238	0.238	0.238	0.238	0.238	0.238	0.238	0.238	0.238	0.238
Cover Factor, C <sub>f</sub>	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90
Noncohesive Soil																				1
Soil Grain Roughness, n	0.016	0.016	0.016	0.016	0.016	0.016	0.016	0.016	0.016	0.016	0.016	0.016	0.016	0.016	0.016	0.016	0.016	0.016	0.016	0.016
Permissible Soil Shear Stress, τ <sub>p</sub> (lb/ft²)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Cohesive Soil																				
Porosity, e	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35
Soil Coefficient 1, c <sub>1</sub>	1.0700	1.0700	1.0700	1.0700	1.0700	1.0700	1.0700	1.0700	1.0700	1.0700	1.0700	1.0700	1.0700	1.0700	1.0700	1.0700	1.0700	1.0700	1.0700	1.0700
Soil Coefficient 2, c <sub>2</sub>	14.30	14.30	14.30	14.30	14.30	14.30	14.30	14.30	14.30	14.30	14.30	14.30	14.30	14.30	14.30	14.30	14.30	14.30	14.30	14.30
Soil Coefficient 3, c <sub>3</sub>	47.700	47.700	47.700	47.700	47.700	47.700	47.700	47.700	47.700	47.700	47.700	47.700	47.700	47.700	47.700	47.700	47.700	47.700	47.700	47.700
Soil Coefficient 4, c <sub>4</sub>	1.42	1.42	1.42	1.42	1.42	1.42	1.42	1.42	1.42	1.42	1.42	1.42	1.42	1.42	1.42	1.42	1.42	1.42	1.42	1.42
Soil Coefficient 5, c <sub>5</sub>	-0.61	-0.61	-0.61	-0.61	-0.61	-0.61	-0.61	-0.61	-0.61	-0.61	-0.61	-0.61	-0.61	-0.61	-0.61	-0.61	-0.61	-0.61	-0.61	-0.61
Soil Coefficient 6, c <sub>6</sub>	0.00010	0.00010	0.00010	0.00010	0.00010	0.00010	0.00010	0.00010	0.00010	0.00010	0.00010	0.00010	0.00010	0.00010	0.00010	0.00010	0.00010	0.00010	0.00010	0.00010
Permissible Soil Shear Stress, τ <sub>p</sub> (lb/ft²)	0.080	0.080	0.080	0.080	0.080	0.080	0.080	0.080	0.080	0.080	0.080	0.080	0.080	0.080	0.080	0.080	0.080	0.080	0.080	0.080
Total Permissible Shear Stress, τ <sub>p</sub> (lb/ft²)	0.080	0.080	0.080	0.080	0.080	0.080	0.080	0.080	0.080	0.080	0.080	0.080	0.080	0.080	0.080	0.080	0.080	0.080	0.080	0.080
Cross Sectional Area, A (ff)	22.832	3.453	17.160	20.404	20.206	23.248	17.530	36.450	26.468	10.850	14.984	13.104	21.257	33.283	37.179	30.479	2.874	9.690	8.449	8.606
Wetted Perimeter, P (ft)	21.11	11.01	18.72	20.12	20.04	21.28	18.88	25.98	23.28	12.79	14.22	14.93	20.35	24.35	25.52	23.48	8.75	13.25	12.37	12.58
Hydraulic Radius, R (ft)	1.082	0.314	0.917	1.014	1.008	1.093	0.928	1.403	1.137	0.849	1.054	0.878	1.045	1.367	1.457	1.298	0.329	0.731	0.683	0.684
Top Width, T (ft)	20.72	10.92	18.40	19.76	19.68	20.88	18.56	25.44	22.88	12.28	13.56	14.48	19.94	23.79	24.91	22.95	8.65	12.84	11.99	12.25
Hydraulic Depth, D (ft)	1.102 0.261	0.316 0.125	0.933 0.235	1.033 0.233	1.027 0.305	1.113 0.253	0.944 0.347	1.433 0.121	1.157 0.325	0.884 0.276	1.105 0.314	0.905	1.066 0.639	1.399 0.360	1.493 0.309	1.328 0.409	0.333 0.219	0.755 0.098	0.705 0.094	0.703 0.235
Froude Number (Q design)	0.261	0.125	0.235	0.233	0.305	0.253	0.347	0.121	0.325	0.276	0.314	0.383	1.01	0.360	0.309	0.409	0.219	0.098	0.094	0.235
Channel Shear Stress, τ <sub>o</sub> (lb/ft²)																				
Actual Sheer Stress, τ <sub>d</sub> (lb/ft²)	0.55	0.12 0.126	0.45	0.47	0.63	0.53	0.69	0.27 0.102	0.69	0.47 0.076	0.61	1.10 0.065	1.37 0.051	0.85	0.74	0.95	0.40	0.23	0.21	0.35
Mannings n							0.000											0.123	****	
Average Velocity, V (ft/s)  Calculated Flow, Q (ft <sup>3</sup> /s)	1.55 35.4	0.40 1.4	1.26 22.1	1.34 27.4	1.75 35.4	1.51 35.2	1.89 33.5	0.82 29.8	1.97 52.5	1.46 16.0	1.86 28.0	2.04 27.1	3.77 79.6	2.41 80.5	2.15 79.5	2.63 81.6	0.72 2.1	0.48 4.7	0.45 3.8	1.12 9.6
7 7	0.2%	0.2%	1.9%	0.0%	0.1%	0.0%	1.0%	-0.4%	0.6%	0.5%	0.6%	1.6%	-0.6%	0.5%	79.5 -0.7%	1.8%	0.0%	-0.3%	0.2%	-0.5%
Difference Between Design & Calc. Flow (%)	0.2%	0.000	0.002	0.002	0.1%	0.0%	0.004	0.001	0.004	0.5%	0.6%	0.007	0.014	0.5%	0.004	0.007	0.0%	0.000	0.2%	0.001
Effective Shear on Soil Surface, $\tau_e$ (lb/ft²)  Total Permissible Shear on Veq., $\tau_{none}$ (lb/ft²)	17.60	49.69	20.53	20.03	15.78	18.08	14.47	32.56	14.47	18.08	14.90	13.22	8.14	12.42	14.05	11.27	29.45	47.35	49.69	22.08
Stable (Y or N)	YES	49.69 YES	20.53 YES	YES	15.78 YES	YES	YES	32.56 YES	YES	18.08 YES	14.90 YES	13.22 YES	YES	YES	14.05 YES	11.27 YES	29.45 YES	47.35 YES	49.69 YES	22.08 YES
Stable (1 of N)	165	150	155	155	159	155	159	155	159	150	159	155	1E5	155	159	150	159	155	159	159

Source: Grass Lined Channel Design WisDOT Spreadsheet, FDM 13-30 Attachment 15.2

### SCS ENGINEERS

 Calc. No.

 Rev. No.
 0

 Job No. 25220183.00
 Job: Col Job: Columbia Energy Center
 By: RJG
 Date: 2/23/22

 Client: WPL
 Subject: Subject: Swale Sizing
 Chk'd: MJT
 Date: 4/5/22

#### **Non-Channel Erosion Mat**

(1052)

Wisconsin Department of Natural Resources Conservation Practice Standard

To differentiate applications Erosion mats are organized into three Classes of mats, which are further broken down into various Types.

- A. Class I: A short-term duration (minimum of 6 months), light duty, organic mat with photodegradable plastic or biodegradable netting.
  - Type A Use on erodible slopes 2.5:1 or flatter.
  - Type B Double netted product for use on erodible slopes 2:1 or flatter.
- B. Class I, Urban: A short-term duration (minimum of 6 months), light duty, organic erosion control mat for areas where mowing may be accomplished within two weeks after installation.
  - Urban, Type A Use on erodible soils with slopes 4:1 or flatter.
  - Urban, Type B A double netted product for use on slopes 2.5:1 or flatter.
- C. Class II: A long-term duration (three years or greater), organic erosion control revegetative mat.
  - Type A Jute fiber only for use on slopes 2:1 or flatter for sod reinforcement.
  - Type B For use on slopes 2:1 or greater made with plastic or biodegradable net.
  - Type C A woven mat of 100% organic fibers for use on slopes 2:1 or flatter and in environmentally and biologically sensitive areas where plastic netting is inappropriate.
- D. Class III: A permanent 100% synthetic ECRM or TRM. Either a soil stabilizer Type A or Class I, Type A or B erosion mat must be placed over the soil filled TRM.
  - Type A An ECRM for use on slopes 2:1 or flatter.
  - Type B or C A TRM for use on slopes 2:1 or flatter.
  - Type D A TRM for use on slopes 1:1 or flatter.

#### **Channel Erosion Mat**

Sheet No:

4 of 4

(1053)

Wisconsin Department of Natural Resources Conservation Practice Standard

To differentiate applications WisDOT organizes erosion mats into three classes of mats, which are further broken down into various Types.

- A. Class I: A short-term duration (minimum of 6 months), light duty, organic ECRM with plastic or biodegradable netting.
  - Type A Only suitable for slope applications, not channel applications.
  - Type B Double netted product for use in channels where the calculated (design) shear stress is 1.5 lbs/ft<sup>2</sup> or less.
- Class II: A long-term duration (three years or greater), organic ECRM.
  - Type A Jute fiber only for use in channels to reinforce sod.
  - Type B For use in channels where the calculated (design) shear stress is 2.0 lbs/ft² or less. Made with plastic or biodegradable mat.
  - Type C A woven mat of 100% organic material for use in channels where the calculated (design) shear stress is 2.0 lbs/ft<sup>2</sup> or less. Applicable

for use in environmentally sensitive areas where plastic netting is inappropriate.

- C. Class III: A permanent 100% synthetic ECRM or TRM. Class I, Type B erosion mat or Class II, Type B or C erosion mat must be placed over a soil filled TRM.
  - Type A An ECRM for use in channels where the calculated (design) shear stress of 2.0 lbs/ft<sup>2</sup> or less.
  - Type B A TRM for use in channels where the calculated (design) shear stress of 2.0 lbs/ft<sup>2</sup> or less.
  - Type C A TRM for use in channels where the calculated (design) shear stress of 3.5 lbs/ft² or less.
  - Type D A TRM for use in channels where the calculated (design) shear stress of 5.0 lbs/ft<sup>2</sup> or less.



SCS ENG	INEERS	Sheet No: 1/7				
		Calc. No.				
		Rev. No.				
Job No. 25220183.00	Job: COL - POO	By: RJG	Date: 4/7/22			
Client: WPL	Subject: Culvert Sizing	Chk'd: MJT	Date:			

#### Purpose:

To size the post closure culverts to accommodate the 25-year, 24-hour storm event.

#### References:

- 1. HY-8 7.40 Computer Model
- 2. HydroCAD Report\_Post Construction and HydroCAD Report\_Post Construction Temporary Culvert
- 3. Figure 1 Storm Water Post Construction

#### Approach:

- 1. Create culvert crossing in HY-8 and input data from Reference #2 and #3.
- 2. Adjust diameter size and number of culverts in model until design flow does not over top berm/road crossing.

#### **Assumptions:**

- 1. Assume the tailwater channel data is a based on discharge swale or rock chute geometry (Reference #2).
- 2. Culverts are circular, PE Pipe with smooth interior, and with square edge with headwall.
- 3. Culvert elevatons, lengths, and slopes based on Figure 1 (Reference #3).
- 4. Roadwa data for crossing based on Figure 1 (Reference #3).
- 5. Discharge flows from HydroCAD report (Refence #2).

#### Calculations:

See attached HY-8 Model output reports.

#### Results:

The culverts are adequately designed to accommodate the flows from the 25-year, 24-hour storm event.

Culvert	Dia. (ft)	# of Barrels	Upstream Invert (ft)	Downstream Invert (ft)	Slope (%)	Length (ft)
C1	2	1	815.70	814.55	2.22	52
C2	1.5	2	814.40	814.20	0.49	41
C3	2.5	2	811.17	811.16	0.02	50
C4	2.5	2	809.87	809.74	0.26	50
C5	2.5	2	807.57	807.15	0.84	50
C6	2	2	805.40	804.76	0.61	105
C7	3.5	2	796.64	796.34	0.50	60
C8	2	1	807.54	806.81	0.73	100

#### Site Data - Culvert C1

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft

Inlet Elevation: 815.70 ft
Outlet Station: 51.88 ft
Outlet Elevation: 814.55 ft

Number of Barrels: 1

## **Culvert Data Summary - Culvert C1**

Barrel Shape: Circular
Barrel Diameter: 2.00 ft

Barrel Material: Smooth HDPE

Embedment: 0.00 in

Barrel Manning's n: 0.0120

Culvert Type: Straight

Inlet Configuration: Square Edge with Headwall

Inlet Depression: None

### **Crossing Discharge Data**

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 2.06 cfs
Design Flow: 2.06 cfs
Maximum Flow: 7.48 cfs

#### Tailwater Channel Data - Culvert C1

Tailwater Channel Option: Triangular Channel

Side Slope (H:V): 6.00 (\_:1) Channel Slope: 0.0300

------

Channel Manning's n: 0.0300

Channel Invert Elevation: 815.32 ft

Table 1 - Culvert Summary Table: Culvert C1

Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
2.06	2.06	816.37	0.670	0.0*	1-JS1t	0.321	0.498	1.127	0.357	1.129	2.695
2.60	2.60	816.46	0.758	0.031	1-JS1t	0.361	0.562	1.160	0.390	1.378	2.857
3.14	3.14	816.54	0.838	0.070	1-JS1t	0.396	0.619	1.188	0.418	1.616	2.995
3.69	3.69	816.61	0.912	0.108	1-JS1t	0.428	0.672	1.214	0.444	1.847	3.117
4.23	4.23	816.68	0.982	0.145	1-JS1t	0.459	0.722	1.237	0.467	2.072	3.226
4.77	4.77	816.76	1.058	0.182	1-S2n	0.487	0.768	0.503	0.489	7.698	3.324
5.31	5.31	816.83	1.134	0.220	1-S2n	0.515	0.813	0.533	0.509	7.895	3.415
5.85	5.85	816.91	1.206	0.258	1-S2n	0.541	0.855	0.562	0.528	8.081	3.499
6.40	6.40	816.98	1.275	0.298	1-S2n	0.566	0.895	0.590	0.546	8.262	3.577
6.94	6.94	817.04	1.342	0.338	1-S2n	0.590	0.934	0.617	0.563	8.416	3.651
7.48	7.48	817.11	1.406	0.379	1-S2n	0.614	0.972	0.643	0.579	8.566	3.720

<sup>\*</sup> Full Flow Headwater elevation is below inlet invert.

#### Straight Culvert

Inlet Elevation (invert): 815.70 ft, Outlet Elevation (invert): 814.55 ft

Culvert Length: 51.89 ft, Culvert Slope: 0.0222

Table 2 - Summary of Culvert Flows at Crossing: Culvert C1

Headwater Elevation (ft)	Total Discharge (cfs)	Culvert C1 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
816.37	2.06	2.06	0.00	1
816.46	2.60	2.60	0.00	1
816.54	3.14	3.14	0.00	1
816.61	3.69	3.69	0.00	1
816.68	4.23	4.23	0.00	1
816.76	4.77	4.77	0.00	1
816.83	5.31	5.31	0.00	1
816.91	5.85	5.85	0.00	1
816.98	6.40	6.40	0.00	1
817.04	6.94	6.94	0.00	1
817.11	7.48	7.48	0.00	1
819.06	22.61	22.61	0.00	Overtopping

#### Site Data - C2

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft

Inlet Elevation: 814.40 ft
Outlet Station: 41.00 ft
Outlet Elevation: 814.20 ft

Number of Barrels: 2

### **Culvert Data Summary - C2**

Barrel Shape: Circular Barrel Diameter: 1.50 ft

Barrel Material: Smooth HDPE

Embedment: 0.00 in

Barrel Manning's n: 0.0120

Culvert Type: Straight

Inlet Configuration: Square Edge with Headwall

Inlet Depression: None

#### **Tailwater Channel Data - Culvert C2**

Tailwater Channel Option: Trapezoidal Channel

Bottom Width: 8.00 ft

Side Slope (H:V): 4.00 (\_:1)

Channel Slope: 0.0050

Channel Manning's n: 0.0300

Channel Invert Elevation: 814.10 ft

### **Crossing Discharge Data**

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 9.68 cfs
Design Flow: 9.68 cfs
Maximum Flow: 13.45 cfs

Table 1 - Culvert Summary Table: C2

Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
9.68	9.68	815.67	1.271	0.199	1-S2n	0.767	0.842	0.767	0.499	4.728	1.939
10.06	10.06	815.70	1.302	0.926	1-S2n	0.786	0.858	0.786	0.510	4.769	1.963
10.43	10.43	815.73	1.333	0.966	1-S2n	0.805	0.877	0.805	0.521	4.807	1.987
10.81	10.81	815.76	1.364	1.003	1-S2n	0.824	0.893	0.824	0.531	4.842	2.010
11.19	11.19	815.79	1.395	1.041	1-S2n	0.843	0.909	0.843	0.542	4.871	2.032
11.57	11.57	815.83	1.426	1.079	1-S2n	0.863	0.924	0.863	0.552	4.899	2.053
11.94	11.94	815.86	1.457	1.117	1-S2n	0.882	0.939	0.882	0.562	4.943	2.074
12.32	12.32	815.89	1.489	1.156	1-S2n	0.902	0.954	0.902	0.572	4.973	2.095
12.70	12.70	815.92	1.521	1.196	5-S2n	0.921	0.968	0.921	0.581	5.001	2.115
13.07	13.07	815.95	1.553	1.240	5-S2n	0.941	0.987	0.941	0.591	5.028	2.134
13.45	13.45	815.99	1.586	1.281	5-S2n	0.962	1.001	0.962	0.600	5.048	2.153

\*

#### Straight Culvert

Inlet Elevation (invert): 814.40 ft,  $\,$   $\,$  Outlet Elevation (invert): 814.20 ft

Culvert Length: 41.00 ft, Culvert Slope: 0.0049

Table 2 - Summary of Culvert Flows at Crossing: Culvert C2

Headwater Elevation (ft)	Total Discharge (cfs)	C2 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
815.67	9.68	9.68	0.00	1
815.70	10.06	10.06	0.00	1
815.73	10.43	10.43	0.00	1
815.76	10.81	10.81	0.00	1
815.79	11.19	11.19	0.00	1
815.83	11.57	11.57	0.00	1
815.86	11.94	11.94	0.00	1
815.89	12.32	12.32	0.00	1
815.92	12.70	12.70	0.00	1
815.95	13.07	13.07	0.00	1
815.99	13.45	13.45	0.00	1
816.90	21.79	21.79	0.00	Overtopping

#### Site Data - C3

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft

Inlet Elevation: 811.17 ft
Outlet Station: 50.00 ft
Outlet Elevation: 811.16 ft

Number of Barrels: 2

### **Culvert Data Summary - C3**

Barrel Shape: Circular Barrel Diameter: 2.50 ft

Barrel Material: Smooth HDPE

Embedment: 0.00 in

Barrel Manning's n: 0.0120

Culvert Type: Straight

Inlet Configuration: Square Edge with Headwall

Inlet Depression: None

#### **Tailwater Channel Data - Culvert C3**

Tailwater Channel Option: Trapezoidal Channel

Bottom Width: 8.00 ft

Side Slope (H:V): 4.00 (\_:1) Channel Slope: 0.0050

Chariner Slope. 0.0030

Channel Manning's n: 0.0300

Channel Invert Elevation: 811.17 ft

### **Crossing Discharge Data**

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 27.38 cfs
Design Flow: 27.38 cfs
Maximum Flow: 47.76 cfs

**Table 1 - Culvert Summary Table: C3** 

Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
27.38	27.38	813.15	1.836	1.981	7-H2c	-1.000	1.245	1.245	0.886	5.607	2.677
29.42	29.42	813.23	1.918	2.064	7-H2c	-1.000	1.292	1.292	0.921	5.745	2.735
31.46	31.46	813.32	1.998	2.147	7-H2c	-1.000	1.339	1.339	0.954	5.878	2.789
33.49	33.49	813.40	2.077	2.228	7-H2c	-1.000	1.383	1.383	0.987	6.009	2.841
35.53	35.53	813.48	2.155	2.308	7-H2c	-1.000	1.427	1.427	1.018	6.137	2.891
37.57	37.46	813.55	2.229	2.384	7-H2c	-1.000	1.467	1.467	1.049	6.257	2.938
39.61	38.68	813.60	2.276	2.431	7-H2c	-1.000	1.492	1.492	1.078	6.332	2.983
41.65	39.64	813.64	2.312	2.468	7-H2c	-1.000	1.511	1.511	1.107	6.391	3.027
43.68	40.50	813.67	2.345	2.502	7-H2c	-1.000	1.528	1.528	1.135	6.443	3.068
45.72	41.26	813.70	2.374	2.531	7-H2c	-1.000	1.543	1.543	1.163	6.490	3.109
47.76	42.00	813.73	2.403	2.559	7-H2c	-1.000	1.557	1.557	1.189	6.534	3.148

### Straight Culvert

Inlet Elevation (invert): 811.17 ft, Outlet Elevation (invert): 811.16 ft

Culvert Length: 50.00 ft, Culvert Slope: 0.0002

Table 2 - Summary of Culvert Flows at Crossing: Culvert C3

Headwater Elevation (ft)	Total Discharge (cfs)	C3 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
813.15	27.38	27.38	0.00	1
813.23	29.42	29.42	0.00	1
813.32	31.46	31.46	0.00	1
813.40	33.49	33.49	0.00	1
813.48	35.53	35.53	0.00	1
813.55	37.57	37.46	0.02	10
813.60	39.61	38.68	0.85	6
813.64	41.65	39.64	1.94	5
813.67	43.68	40.50	3.15	5
813.70	45.72	41.26	4.38	4
813.73	47.76	42.00	5.71	4
813.55	37.37	37.37	0.00	Overtopping

#### Site Data - C4

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft

Inlet Elevation: 809.87 ft
Outlet Station: 50.00 ft
Outlet Elevation: 809.74 ft

Number of Barrels: 2

### **Culvert Data Summary - C4**

Barrel Shape: Circular
Barrel Diameter: 2.50 ft

Barrel Material: Smooth HDPE

Embedment: 0.00 in

Barrel Manning's n: 0.0120

Culvert Type: Straight

Inlet Configuration: Square Edge with Headwall

Inlet Depression: None

### Tailwater Channel Data - Culvert C4

Tailwater Channel Option: Trapezoidal Channel

Bottom Width: 8.00 ft

Side Slope (H:V): 4.00 (\_:1)

Channel Slope: 0.0070

Channel Manning's n: 0.0300

Channel Invert Elevation: 809.87 ft

#### **Crossing Discharge Data**

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 35.39 cfs
Design Flow: 35.39 cfs
Maximum Flow: 62.23 cfs

Table 1 - Culvert Summary Table: C4

Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
35.39	35.39	812.13	2.147	2.263	2-M2c	1.660	1.424	1.424	0.929	6.128	3.252
38.07	38.07	812.24	2.249	2.365	2-M2c	1.752	1.479	1.479	0.966	6.295	3.322
40.76	40.41	812.32	2.338	2.454	2-M2c	1.837	1.526	1.526	1.002	6.438	3.389
43.44	41.81	812.38	2.392	2.507	7-M2c	1.891	1.553	1.553	1.036	6.523	3.453
46.13	42.96	812.42	2.437	2.550	7-M2c	1.938	1.575	1.575	1.069	6.593	3.513
48.81	44.01	812.46	2.478	2.589	7-M2c	1.983	1.595	1.595	1.102	6.656	3.571
51.49	44.95	812.49	2.515	2.624	7-M2c	2.027	1.613	1.613	1.133	6.713	3.627
54.18	45.85	812.53	2.550	2.658	7-M2c	2.073	1.629	1.629	1.163	6.767	3.680
56.86	46.71	812.56	2.585	2.691	7-M2c	2.121	1.645	1.645	1.193	6.819	3.731
59.55	47.53	812.59	2.617	2.721	7-M2c	2.174	1.660	1.660	1.222	6.868	3.781
62.23	48.31	812.62	2.649	2.751	7-M2c	2.500	1.674	1.674	1.250	6.915	3.828

\*

### Straight Culvert

Inlet Elevation (invert): 809.87 ft, Outlet Elevation (invert): 809.74 ft

Culvert Length: 50.00 ft, Culvert Slope: 0.0026

Table 2 - Summary of Culvert Flows at Crossing: Culvert C4

Headwater Elevation (ft)	Total Discharge (cfs)	C4 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
812.13	35.39	35.39	0.00	1
812.24	38.07	38.07	0.00	1
812.32	40.76	40.41	0.26	9
812.38	43.44	41.81	1.56	6
812.42	46.13	42.96	3.08	5
812.46	48.81	44.01	4.75	5
812.49	51.49	44.95	6.46	4
812.53	54.18	45.85	8.25	4
812.56	56.86	46.71	10.10	4
812.59	59.55	47.53	11.98	4
812.62	62.23	48.31	13.89	4
812.30	39.78	39.78	0.00	Overtopping

#### Site Data - C5

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft

Inlet Elevation: 807.57 ft
Outlet Station: 50.00 ft
Outlet Elevation: 807.15 ft

Number of Barrels: 2

### **Culvert Data Summary - C5**

Barrel Shape: Circular
Barrel Diameter: 2.50 ft

Barrel Material: Smooth HDPE

Embedment: 0.00 in

Barrel Manning's n: 0.0120

Culvert Type: Straight

Inlet Configuration: Square Edge with Headwall

Inlet Depression: None

### **Tailwater Channel Data - Culvert C5**

Tailwater Channel Option: Trapezoidal Channel

Bottom Width: 8.00 ft

Side Slope (H:V): 4.00 (\_:1)

Channel Slope: 0.0050

Channel Manning's n: 0.0300

Channel Invert Elevation: 807.59 ft

#### **Crossing Discharge Data**

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 35.21 cfs
Design Flow: 35.21 cfs
Maximum Flow: 65.15 cfs

**Table 1 - Culvert Summary Table: C5** 

Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
35.21	35.21	809.70	2.133	1.411	1-S2n	1.148	1.420	1.190	1.013	7.642	2.883
38.20	38.20	809.82	2.247	1.523	1-S2n	1.203	1.482	1.248	1.058	7.801	2.952
41.20	41.20	809.93	2.362	1.638	1-S2n	1.257	1.541	1.305	1.101	7.950	3.017
44.19	44.19	810.05	2.478	1.773	1-S2n	1.311	1.598	1.360	1.142	8.093	3.079
47.19	47.19	810.17	2.596	1.912	5-S2n	1.364	1.654	1.415	1.182	8.230	3.137
50.18	50.18	810.29	2.719	2.054	5-S2n	1.417	1.707	1.470	1.220	8.362	3.193
53.17	53.17	810.42	2.846	2.199	5-S2n	1.470	1.758	1.523	1.257	8.490	3.246
56.17	55.74	810.53	2.959	2.326	5-S2n	1.516	1.800	1.569	1.294	8.595	3.296
59.16	57.10	810.59	3.021	2.395	5-S2n	1.541	1.822	1.593	1.329	8.650	3.345
62.16	58.20	810.64	3.072	2.451	5-S2n	1.561	1.839	1.613	1.363	8.693	3.391
65.15	59.19	810.69	3.118	2.501	5-S2n	1.578	1.854	1.630	1.396	8.732	3.436

### Straight Culvert

Inlet Elevation (invert): 807.57 ft, Outlet Elevation (invert): 807.15 ft

Culvert Length: 50.00 ft, Culvert Slope: 0.0084

\*

Table 24 - Summary of Culvert Flows at Crossing: Culvert C5

Headwater Elevation (ft)	Total Discharge (cfs)	C5 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
809.70	35.21	35.21	0.00	1
809.82	38.20	38.20	0.00	1
809.93	41.20	41.20	0.00	1
810.05	44.19	44.19	0.00	1
810.17	47.19	47.19	0.00	1
810.29	50.18	50.18	0.00	1
810.42	53.17	53.17	0.00	1
810.53	56.17	55.74	0.36	10
810.59	59.16	57.10	1.98	6
810.64	62.16	58.20	3.88	5
810.69	65.15	59.19	5.92	5
810.50	55.08	55.08	0.00	Overtopping

#### Site Data - C6

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft

Inlet Elevation: 805.40 ft
Outlet Station: 104.56 ft
Outlet Elevation: 804.76 ft

Number of Barrels: 2

### **Culvert Data Summary - C6**

Barrel Shape: Circular Barrel Diameter: 2.00 ft

Barrel Material: Smooth HDPE

Embedment: 0.00 in

Barrel Manning's n: 0.0120

Culvert Type: Straight

Inlet Configuration: Mitered to Conform to Slope

Inlet Depression: None

### **Crossing Discharge Data**

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 27.86 cfs
Design Flow: 27.86 cfs
Maximum Flow: 47.83 cfs

## **Tailwater Channel Data - Culvert C6**

Tailwater Channel Option: Trapezoidal Channel

Bottom Width: 10.00 ft Side Slope (H:V): 2.00 (\_:1) Channel Slope: 0.0070

Channel Manning's n: 0.0300

Channel Invert Elevation: 804.56 ft

Table 1 - Culvert Summary Table: C6

Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
27.86	27.86	807.61	2.214	1.559	5-S2n	1.263	1.344	1.263	0.769	6.666	3.141
29.86	29.86	807.76	2.362	1.734	5-S2n	1.325	1.392	1.325	0.800	6.758	3.216
31.85	31.85	807.92	2.520	1.916	5-S2n	1.390	1.439	1.391	0.831	6.829	3.287
33.85	33.85	808.09	2.689	2.105	5-S2n	1.458	1.483	1.458	0.861	6.901	3.355
35.85	35.85	808.27	2.869	2.806	7-M2c	1.531	1.525	1.525	0.890	6.973	3.420
37.84	37.84	808.46	3.061	2.896	7-M2c	1.613	1.565	1.565	0.918	7.174	3.483
39.84	39.00	808.58	3.176	2.950	7-M2c	1.669	1.587	1.587	0.946	7.293	3.543
41.84	39.67	808.64	3.245	2.982	7-M2c	1.705	1.600	1.600	0.973	7.363	3.601
43.84	40.22	808.70	3.302	3.010	7-M2c	1.740	1.610	1.610	0.999	7.421	3.656
45.83	40.73	808.76	3.356	3.038	7-M2c	1.780	1.619	1.619	1.025	7.474	3.710
47.83	41.19	808.80	3.404	3.064	7-M2c	2.000	1.627	1.627	1.051	7.523	3.762

\*

### Straight Culvert

Inlet Elevation (invert): 805.40 ft, Outlet Elevation (invert): 804.76 ft

Culvert Length: 104.56 ft, Culvert Slope: 0.0061

\*

Table 2 - Summary of Culvert Flows at Crossing: Culvert C6

Headwater Elevation (ft)	Total Discharge (cfs)	C6 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
807.61	27.86	27.86	0.00	1
807.76	29.86	29.86	0.00	1
807.92	31.85	31.85	0.00	1
808.09	33.85	33.85	0.00	1
808.27	35.85	35.85	0.00	1
808.46	37.84	37.84	0.00	1
808.58	39.84	39.00	0.80	8
808.64	41.84	39.67	2.13	6
808.70	43.84	40.22	3.56	5
808.76	45.83	40.73	5.07	5
808.80	47.83	41.19	6.62	5
808.50	38.24	38.24	0.00	Overtopping

#### Site Data - C7

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft

Inlet Elevation: 796.64 ft
Outlet Station: 60.20 ft
Outlet Elevation: 796.34 ft

Number of Barrels: 2

### **Culvert Data Summary - C7**

Barrel Shape: Circular Barrel Diameter: 3.50 ft

Barrel Material: Corrugated Steel

Embedment: 0.00 in

Barrel Manning's n: 0.0240

Culvert Type: Straight

Inlet Configuration: Square Edge with Headwall

Inlet Depression: None

### **Tailwater Channel Data - Culvert C7**

Tailwater Channel Option: Trapezoidal Channel

Bottom Width: 10.00 ft

Side Slope (H:V): 4.00 (:1)

Channel Slope: 0.0100

Channel Manning's n: 0.0300

Channel Invert Elevation: 795.60 ft

#### **Crossing Discharge Data**

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 52.15 cfs
Design Flow: 52.15 cfs
Maximum Flow: 103.37 cfs

Table 1 - Culvert Summary Table: C7

Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
52.15	52.15	799.12	2.228	2.484	2-M2c	2.109	1.572	1.572	0.943	6.224	4.017
57.27	57.27	799.26	2.356	2.622	2-M2c	2.247	1.651	1.651	0.992	6.414	4.133
62.39	62.39	799.40	2.481	2.756	2-M2c	2.389	1.727	1.727	1.039	6.596	4.241
67.52	67.52	799.53	2.604	2.889	2-M2c	2.539	1.800	1.800	1.084	6.773	4.342
72.64	72.64	799.66	2.725	3.019	2-M2c	2.703	1.870	1.870	1.128	6.945	4.438
77.76	77.76	799.79	2.846	3.148	2-M2c	2.898	1.938	1.938	1.170	7.112	4.528
82.88	82.88	799.92	2.966	3.277	2-M2c	3.500	2.004	2.004	1.210	7.277	4.614
88.00	88.00	800.04	3.086	3.405	2-M2c	3.500	2.067	2.067	1.250	7.439	4.696
93.13	93.13	800.17	3.207	3.534	7-M2c	3.500	2.129	2.129	1.288	7.599	4.774
98.25	98.25	800.30	3.330	3.663	7-M2c	3.500	2.189	2.189	1.324	7.758	4.849
103.37	103.37	800.43	3.454	3.794	7-M2c	3.500	2.248	2.248	1.360	7.916	4.921

\*

### Straight Culvert

Inlet Elevation (invert): 796.64 ft, Outlet Elevation (invert): 796.34 ft

Culvert Length: 60.20 ft, Culvert Slope: 0.0050

\*

Table 15 - Summary of Culvert Flows at Crossing: Culvert C7

Headwater Elevation (ft)	Total Discharge (cfs)	C7 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
799.12	52.15	52.15	0.00	1
799.26	57.27	57.27	0.00	1
799.40	62.39	62.39	0.00	1
799.53	67.52	67.52	0.00	1
799.66	72.64	72.64	0.00	1
799.79	77.76	77.76	0.00	1
799.92	82.88	82.88	0.00	1
800.04	88.00	88.00	0.00	1
800.17	93.13	93.13	0.00	1
800.30	98.25	98.25	0.00	1
800.43	103.37	103.37	0.00	1
802.50	162.85	162.85	0.00	Overtopping

#### Site Data - C8

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft

Inlet Elevation: 807.54 ft
Outlet Station: 99.86 ft
Outlet Elevation: 806.81 ft

Number of Barrels: 1

### **Culvert Data Summary - C8**

Barrel Shape: Circular Barrel Diameter: 2.00 ft

Barrel Material: Corrugated Steel

Embedment: 0.00 in

Barrel Manning's n: 0.0240

Culvert Type: Straight

Inlet Configuration: Thin Edge Projecting

Inlet Depression: None

### **Tailwater Channel Data - Culvert C8**

Tailwater Channel Option: Trapezoidal Channel

Bottom Width: 12.00 ft

Side Slope (H:V): 4.00 (\_:1)

Channel Slope: 0.0560

Channel Manning's n: 0.0450

Channel Invert Elevation: 807.44 ft

#### **Crossing Discharge Data**

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 8.32 cfs
Design Flow: 8.32 cfs
Maximum Flow: 19.2 cfs

**Table 1 - Culvert Summary Table: C8** 

Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
8.32	8.32	809.29	1.614	1.747	2-M2c	1.344	1.028	1.028	0.230	5.117	2.797
9.41	9.41	809.43	1.751	1.891	2-M2c	1.478	1.096	1.096	0.248	5.339	2.926
10.50	10.50	809.58	1.890	2.038	7-M2c	1.639	1.160	1.160	0.264	5.553	3.045
11.58	11.58	809.74	2.033	2.199	7-M2c	2.000	1.222	1.222	0.280	5.762	3.156
12.67	12.67	809.92	2.182	2.381	7-M2c	2.000	1.280	1.280	0.295	5.968	3.260
13.76	13.76	810.22	2.338	2.679	7-M2c	2.000	1.336	1.336	0.310	6.173	3.357
14.85	14.85	810.57	2.504	3.026	7-M2c	2.000	1.389	1.389	0.324	6.378	3.451
15.94	15.94	810.93	2.679	3.391	7-M2c	2.000	1.439	1.439	0.337	6.585	3.538
17.02	17.02	811.32	2.866	3.776	7-M2c	2.000	1.487	1.487	0.351	6.796	3.622
18.11	18.11	811.72	3.066	4.183	7-M2c	2.000	1.533	1.533	0.364	7.011	3.703
19.20	19.20	812.15	3.279	4.611	7-M2c	2.000	1.576	1.576	0.376	7.231	3.780

\*

### Straight Culvert

Inlet Elevation (invert): 807.54 ft, Outlet Elevation (invert): 806.81 ft

Culvert Length: 99.86 ft, Culvert Slope: 0.0073

\*

Table 2 - Summary of Culvert Flows at Crossing: Culvert C8

Headwater Elevation (ft)	Total Discharge (cfs)	C8 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
809.29	8.32	8.32	0.00	1
809.43	9.41	9.41	0.00	1
809.58	10.50	10.50	0.00	1
809.74	809.74 11.58		0.00	1
809.92	12.67	12.67	0.00	1
810.22	13.76	13.76 0.00		1
810.57	810.57 14.85		0.00	1
810.93	810.93 15.94		0.00	1
811.32	17.02	17.02	0.00	1
811.72	18.11	18.11	0.00	1
812.15	19.20	19.20	0.00	1
812.40	812.40 19.87 19.87 0.00		0.00	Overtopping



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Determine the spacing between diversion berms on the landfill final cover, with the goal of maintaining ≤ 3 ton/acre of soil loss along the final cover.

#### References

1. "Predicting Rainfall Erosion Losses," USDA Agriculture Handbook Number 537, 1978.

(Figure 1 on Sheet 2 and Tables 10 and 13 on Sheet 4).

2. Erosion and Sediment Control Handbook," Goldman, Jackson, & Bursztynsky, 1986.

(Table 5.5 on Sheet 5).

- 3. Rainfed retention probabilities computed for different cropping tillage systems. Agricultural Water Management, A.W. Mills & G.W. Thomas, 1985. Table 5.10 on Sheet 3)
- 4. Colombia Energy Center POO Update Drawings

#### Approach:

Use the Universal Soil Loss Equation (USLE) to determine diversion berm spacing. Longest flow length is 401 feet.

**USLE Equation:** A = R \* K \* LS \* C \* Pwhere: A = Average annual soil loss, tons/acre R = Rainfall and runoff erosivity index K = Soil erodibility factor, tons/acreLS = Slope length and steepness factor C = Cover management factor P = Practice factor

or LS = \_\_\_\_A

#### Assumptions:

A =tons/acre 3 R =145 see Figure 1 on Sheet 2 (Reference #1) see Table 5.10 on Sheet 3 for Loamy Very Fine Sand (Reference #3) K = 0.38 0.0064 see Table 10 on Sheet 4, assuming 90% cover (Reference #1) P =1.0 assume no support practice used

#### Calculation:

$$LS = A = 3 = 8.51$$
  
 $R \times K \times C \times P = 145 \times 0.38 \times 0.0064 \times 1.0$ 

From the LS Values Table (Sheet 5), based on the 4:1 final cover slope, the slope distance is between 200 and 250 feet.

Use linear interpolation between the LS values for 200 and 250 feet to determine the slope length value for the 4:1 slope.

8.33 Slope Length @ 200 ft LS= LS= 9.31 Slope Length @ 250 ft

Slope length for the calculate LS factor = 209 ft

#### Results:

The maximum distance between diversion berms along the final cover to maintain less than 3 tons/acre soil loss is

209 ft.

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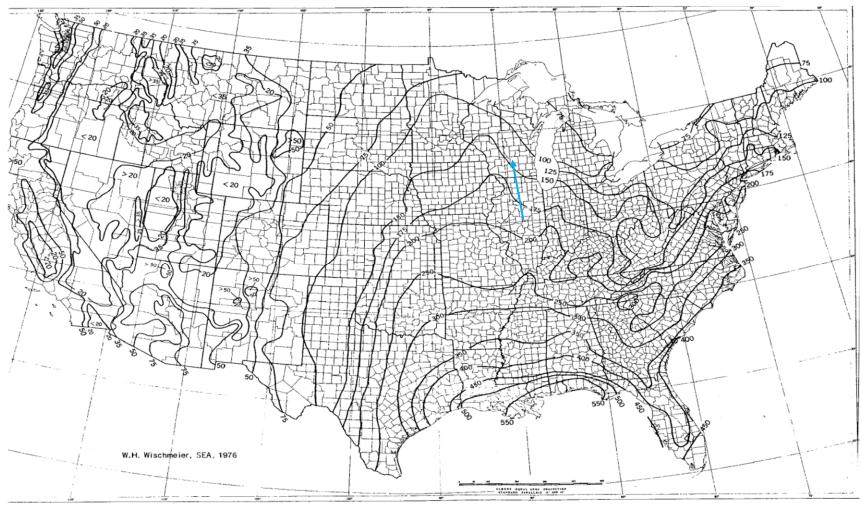


FIGURE 1.—Average annual values of the rainfall erosion index

Source: "Predicting Rainfall Erosion Losses," USDA Agriculture Handbook Number 537, 1978.

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Table 5.10. Soil Erodibility Factor  $K_{fact}$  (after Stewart et al. 1975)<sup>(a)</sup>

	P <sub>om</sub> (%)		
Textural Class	<0.5	2	4
Sand	0.05	0.03	0.02
Fine sand	0.16	0.14	0.10
Very finesand	0.42	0.36	0.28
Loamy sand	0.12	0.10	0.08
Loamy finesand	0.24	0.20	0.16
Loamy veryfine sand	0.44	0.38	0.30
Sandy loam	0.27	0.24	0.19
Fine sandyloam	0.35	0.30	0.24
Very fine sandy loam	0.47	0.41	0.33
Loam	0.38	0.34	0.29
Silt loam	0.48	0.42	0.33
Silt	0.60	0.52	0.42
Sandy clayloam	0.27	0.25	0.21
Clay loam	0.28	0.25	0.21
Silty clayloam	0.37	0.32	0.26
Sandy clay	0.14	0.13	0.12
Silty clay	0.25	0.23	0.19
Clay		0.13- 0.2	

(a) The values shown are estimated averages of broad ranges of specific soil values. When a texture is near the border line of two texture classes, use the average of the two K<sub>fact</sub> values. In addition, the values shown are commensurate with the English units used in the cited reference (and as used in the source-term module input files). To obtain analagous values in the metric units used in this report, the above values should be multiplied by 1.292.

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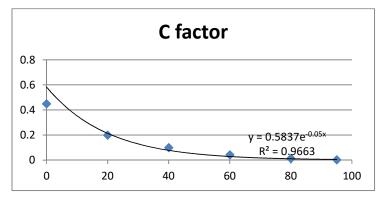
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TABLE 10.—Factor C for permanent pasture, range, and idle land<sup>1</sup>

Vegetative cano	py	Cover that contacts the soil surface									
	ercent			Pe	rcent	ground	cover				
height <sup>2</sup>	cover3	Type <sup>4</sup>	0	20	40	60	80	95+			
No appreciable		G	0.45	0.20	0.10	0.042	0.013	0.003			
canopy		w	.45	.24	.15	.091	.043	.011			
Tall weeds or	25	G	.36	.17	.09	.038	.013	.003			
short brush with average		W	.36	.20	.13	.083	.041	.011			
drop fall height	50	G	.26	.13	.07	.035	.012	.003			
of 20 in		w	.26	.16	.11	.076	.039	.011			
	75	G	.17	.10	.06	.032	.011	.003			
		W	.17	.12	.09	860.	.038	.011			
Appreciable brush	25	G	.40	.18	.09	.040	.013	.003			
or bushes, with average drop fal	II	W	.40	.22	.14	.087	.042	.011			
height of 61/2 ft	50	G	.34	.16	.08	.038	.012	.003			
		w	.34	.19	.13	.082	.041	.011			
	75	G	.28	.14	.08	.036	.012	.003			
		W	.28	.17	.12	.078	.040	.011			
Trees, but no	25	G	.42	.19	.10	.041	.013	.003			
appreciable low brush. Average		W	.42	.23	.14	.089	.042	.011			
drop fall height	50	G	.39	.18	.09	.040	.013	.003			
of 13 ft		w	.39	.21	.14	.087	.042	.011			
	75	G	.36	.17	.09	.039	.012	.003			
		w	.36	.20	.13	.084	.041	.011			

<sup>&</sup>lt;sup>1</sup> The listed C values assume that the vegetation and mulch are randomly distributed over the entire area.

Source: "Predicting Rainfall Erosion Losses," USDA Agriculture Handbook Number 537, 1978.



90 % cover = 0.0065

<sup>\*\*</sup>Canopy height is measured as the average fall height of water drops falling from the canopy to the ground. Canopy effect is inversely proportional to drop fall height and is negligible if fall height exceeds 33 ft.

<sup>&</sup>lt;sup>3</sup> Portion of total-area surface that would be hidden from view by canopy in a vertical projection (a bird's-eye view).

<sup>&</sup>lt;sup>4</sup>G: cover at surface is grass, grasslike plants, decaying compacted duff, or litter at least 2 in deep.

W: cover at surface is mostly broadleaf herbaceous plants (as weeds with little lateral-root network near the surface) or undecayed residues or both.

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TABLE 5.5 LS Values\* (10)

	Slope			LS va	lues for	followir	ng slope	lengths	<i>l</i> , ft (m	1)		LS values for following slope lengths $l$ , ft (m)												
Slope	gradient	10	20	30	40	50	60	70	80	90	100	150	200	250	300	350	400	450	500	600	700	800	900	1000
ratio	s, %	(3.0)	(6.1)	(9.1)	(12.2)	(15.2)	(18.3)	(21.3)	(24.4)	(27.4)	(30.5)	(46)	(61)	(76)				(137)		(183)	(213)	(244)	(274)	(305)
	0.5	0.06	0.07	0.07	0.08	0.08	0.09	0.09	0.09	0.09	0.10	0.10	0.11	0.11	0.12	0.12	0.13	0.13	0.13	0.14	0.14	0.14	0.15	0.15
100:1	1	0.08	0.09	0.10	0.10	0.11	0.11	0.12	0.12	0.12	0.12	0.14	0.14	0.15	0.16	0.16	0.16	0.17	0.17	0.18	0.18	0.19	0.19	0.20
	2	0.10			0.15	0.16	0.17	0.18	0.19	0.19	0.20	0.23	0.25	0.26	0.28	0.29	0.30	0.32	0.33	0.34	0.36	0.37	0.39	0.40
	3	0.14	0.18	0.20	0.22	0.23	0.25	0.26	0.27	0.28	0.29	0.32	0.35	0.38	0.40	0.42	0.43	0.45	0.46	0.49	0.51	0.54	0.55	0.57
	4	0.16	0.21	0.25	0.28	0.30	0.33	0.35	0.37	0.38	0.40	0.47	0.53	0.58	0.62	0.66	0.70	0.73	0.76	0.82	0.87	0.92	0.96	1.00
20:1	5	0.17		0.29	0.34	0.38	0.41	0.45	0.48	0.51	0.53	0.66	0.76	0.85	0.93	1.00	1.07	1.13	1.20	1.31	1.42	1.51	1.60	1.69
	6	0.21	0.30	0.37	0.43	0.48	0.52	0.56	0.60	0.64	0.67	0.82	0.95	1.06	1.16	1.26	1.34	1.43	1.50	1.65	1.78	1.90	2.02	2.13
	7	0.26	0.37	0.45	0.52	0.58	0.64	0.69	0.74	0.78	0.82	1.01	1.17	1.30	1.43	1.54	1.65	1.75	1.84	2.02	2.18	2.33	2.47	2.61
12%:1	8	0.31	0.44	0.54	0.63	0.70	0.77	0.83	0.89	0.94	0.99	1.21	1.40	1.57	1.72	1.85	1.98	2.10	2.22	2.43	2.62	2.80	2.97	3.13
	9	0.37	0.52	0.64	0.74	0.83	0.91	0.98	1.05	1.11	1.17	1.44	1.66	1.85	2.03	2.19	2.35	2.49	2.62	2.87	3.10	3.32	3.52	3.71
10:1	10	0.43	0.61	0.75	0.87	0.97	1.06	1.15	1.22	1.30	1.37	1.68	1.94	2.16	2.37	2.56	2.74	2.90	3.06	3.35	3.62	3.87	4.11	4.33
	11	0.50	0.71	0.86	1.00	1.12	1.22	1.32	1.41	1.50	1.58	1.93	2.23	2.50	2.74	2.95	3.16	3.35	3.53	3.87	4.18	4.47	4.74	4.99
8:1	12.5	0.61	0.86	1.05	1.22	1.36	1.49	1.61	1.72	1.82	1.92	2.35	2.72	3.04	3.33	3.59	3.84	4.08	4.30	4.71	5.08	5.43	5.76	6.08
	15	0.81	1.14	1.40	1.62	1.81	1.98	2.14	2.29	2.43	2.56	3.13	3.62	4.05	4.43	4.79	5.12	5.43	5.72	6.27	6.77	7.24	7.68	8.09
6:1	16.7	0.96	1.36	1.67	1.92	2.15	2.36	2.54	2.72	2.88	3.04	3.72	4.30	4.81	5.27	5.69	6.08	6.45	6.80	7.45	8.04	8.60	9.12	9.62
5:1	20	1.29	1.82	2.23	2.58	2.88	3.16	3.41	3.65	3.87	4.08	5.00	5.77	6.45	7.06	7.63	8.16	8.65	9.12	9.99	10.79	11.54	12.24	12.90
4%:1	22	1.51	2.13	2.61	3.02	3.37	3.69	3.99	4.27	4.53	4.77	5.84	6.75	7.54	8.26	8.92	9.54	10.12	10.67	11.68	12.62	13.49	14.31	15.08
4:1	25	1.86	2.63	3.23	3.73	4.16	4.56	4.93	5.27	· 5.59	5.89	7.21	8.33	9.31	10.20	11.02	11.78	12.49	13.17	14.43	15.58	16.66	17.67	18.63
	30	2.51	3.56	4.36	5.03	5.62	6.16	6.65	7.11	7.54	7.95			12.57						19.48	21.04	22.49	23.86	25.15
3:1	33.3	2.98	4.22	5.17	5.96	6.67	7.30	7.89	8.43	8.95	9.43	11.55	13.34	14.91	16.33	17.64	18.86	20.00	21.09	23.10	24.95	26.67	28.29	29.82
	35	3.23	4.57	5.60	6.46	7.23	7.92	8.55	9.14	9.70	10.22	12.52	14.46	16.16	17.70	19.12	20.44	21.68	22.86	25.04	27.04	28.91	30.67	32.32
2%:1	40	4.00	5.66	6.93	8.00	8.95	9.80	10.59	11.32	12.00	12.65	15.50	17.89	20.01	21.91	23.67	25.30	26.84	28.29	30.99	33.48	35.79	37.96	40.01
_	45	4.81	6.80	8.33	9.61	10.75	11.77	12.72	13.60	14.42	15.20	18.62	21.50	24.03	26.33	28.44	30.40	32.24	33.99	37.23	40.22	42.99	45.60	48.07
2:1	50	5.64	7.97	9.76	11.27	12.60		14.91	15.94	16.91	17.82	21.83	25.21	28.18	30.87	33.34	35.65	37.81	39.85	43.66	47.16	50.41	53.47	56.36
	55	6.48	9.16	11.22	12.96	14.48	15.87	17.14	18.32	19.43	20.48	25.09	28.97	32.39	35.48	38.32	40.97	43.45	45.80	50.18	54.20	57.94	61.45	64.78
1%:1	57	6.82	9.64	11.80	13.63	15.24	16.69	18.03	19.28	20.45	21.55	26.40	30.48	34.08	37.33	40.32	43.10	45.72	48.19	52.79	57.02	60.96	64.66	68.15
	60	7.32	10.35	12.68	14.64	16.37	17.93	19.37	20.71	21.96	23.15			36.60						56.71	61.25	65.48	69.45	73.21
1%:1	66.7			14.61	16.88	18.87			23.87	25.31	26.68			42.19						65.36	70.60	75.47	80.05	84.38
	70			15.55		20.08			25.39	26.93	28.39			44.89						69.54	75.12	80.30	85.17	89.78
	75	9.78	13.83	16.94	19.56	21.87	23.95	25.87	27.66	29.34	30.92	37.87								75.75	81.82	87.46	92.77	
1%:1		10.55			21.11		25.85	27.93	29.85	31.66	33.38	40.88	47.20	52.77	57.81	62.44	66.75	70.80	74.63	81.76	88.31	94.41	100.13	105.55
			15.98		22.61		27.69	29.90	31.97		35.74			56.51						87.55		101.09		
				20.82		26.88			34.00	36.06	38.01								84.99			107.51		
		12.71			25.41		31.12	33.62	35.94	38.12	40.18								89.84			113.64		
1:1	100	13.36	18.89	23.14	26.72	29.87	32.72	35.34				51.74	59.74	66.79	73.17	79.03	84.49	89.61	94.46	103.48	111.77	119.48	126.73	133.59

<sup>\*</sup>Calculated from

LS = 
$$\left(\frac{65.41 \times s^2}{s^2 + 10,000} + \frac{4.56 \times s}{\sqrt{s^2 + 10,000}} + 0.065\right) \left(\frac{t}{72.5}\right)^n$$

FROM "EROSION & SEAMENT COUTECL HANDBOOK", Goldman, Jackson, + Bors Ztynsky, 1986

 $<sup>\</sup>begin{array}{ll} \text{LS} = \text{topographic factor} \\ l = \text{slope length, ft (m} \times 0.3048) \\ s = \text{slope steepness,} \\ m = \text{exponent dependent upon slope steep} \\ \text{(0.2 for slopes} < 1\%, 0.3 for slopes 1 : \\ 0.4 for slopes 3.5 to 4.5\%, and \\ 0.5 for slopes > 5\%) \\ \end{array}$ 

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To size the post closure diversion berms on the final cover to accommodate the 25-year, 24-hour storm event.

#### References:

- 1. WisDOT Facilities Development Manual Chapter 13, Section 30-15 Grass Lined Channels.
- 2. Design of Roadside Channels with Flexible Linings, HEC-15, USDOT FHWA.
- 3. HydroCAD Report\_Post Construction

#### Approach:

Use the Post Closure HydroCAD Model results to obtain the peak flow during a 25-year, 24-hour storm event along the diversion berms.

Use Grass Lined Channel Design WisDOT Spreadsheet, FDM 13-30 Attachment 15.2 (from Reference #1) to size the swale for each design swale cross section. The WisDOT spreadsheet incorporates the design guidelines and equations described in "Design of Roadside Channels with Flexible Linings", HEC-15, USDOT FHWA (Reference #2). Confirm the swale is stable and has enough capacity for the design flow rate.

#### **Assumptions:**

- 1. Assume the channel geometry is a v-notch swale with one sideslope at 4:1 and one sideslope at 2:1 and a depth of 2.0 ft.
- 2. Assume 2.0% slope along the flowpath of the diversion swale.
- 3. Assume the following parameters per Section 15.2 Grass Lining Properties from Reference #1: Vegetation Retardance Class = C for Swales

Vegetation Condition = Good

Vegetation Growth Form = Turf

4. Assume cohesive soil type with ASTM Soil Class SC and a Plasticity Index (PI) of 16.

#### Calculations:

From the HydroCAD Report, the peak flow rate along the diversion berms are as follows:

<u>Areas</u>			<u>Areas</u>			<u>Areas</u>			<u>Areas</u>		
1	4.58	cfs	8	3.29	cfs	14	3.66 cfs	5	20	3.43	cfs
2	3.73	cfs	9	3.40	cfs	15	1.71 cfs	5	21	3.35	cfs
3	2.17	cfs	10	3.17	cfs	16	4.89 cfs	5	22	3.35	cfs
4	3.74	cfs	11	3.10	cfs	17	4.00 cf:	3	23	4.89	cfs
5	3.58	cfs	12	0.35	cfs	18	2.66 cfs	5	24	6.05	cfs
6	2.92	cfs	13	2.91	cfs	19	2.77 cfs	5	25	5.13	cfs

Use highest flow to confirm diversion berm functions.

Use the Grass Swale Design Spreadsheet (Page 2) to determine the flow depth, velocity and shear stress in the swales.

#### Results:

The diversion berms are adequately designed to accommodate the flows from the 25-year, 24-hour storm event. The diversion berms are stable at the design flow rates. The design flow depth of 2.0 feet maintains at least 0.5 ft of freeboard during the 25-year, 24-hour storm event.

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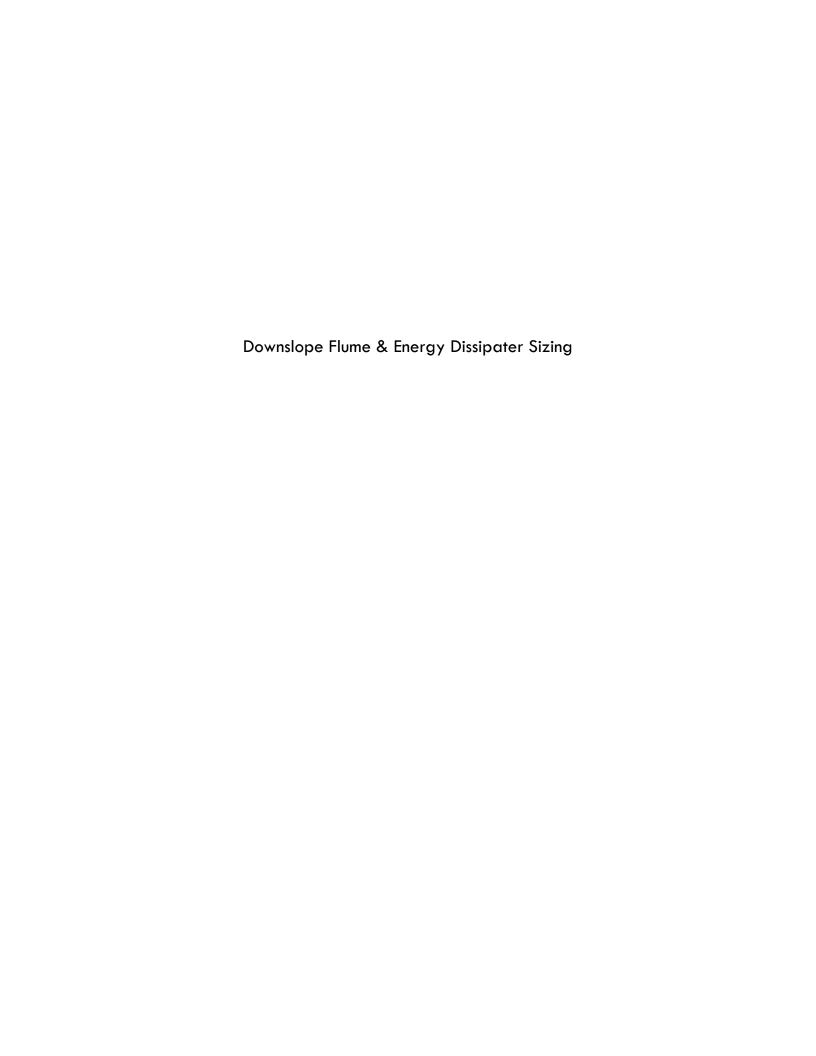
 By: RJG
 Date: 2/23/22

 Chk'd: MJT
 Date: 4/1/22

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Channel/Ditch Geometry	Area 24
Channel Slope, S <sub>o</sub> (ft/ft)	0.02
Channel Bottom Width, B (ft)	0
Channel Side Slope, z <sub>1</sub>	4
Channel Side Slope, z <sub>2</sub>	2
Flow Depth, d (ft) Solve iteratively	1.00
Safety Factor, SF	1.0
Vegetation/Soil Parameters	
Vegetation Retardance Class	С
Vegetation Condition	good
Vegetation Growth Form	turf
Soil Type	cohesive
D <sub>75</sub> (in) (Set at 0.00 for cohesive soils)	
ASTM Soil Class	SC
Plasticity Index, PI	16
Results Summary	
Design Q (ft <sup>3</sup> /s)	6.1
Calculated Q (ft <sup>3</sup> /s)	6.1
Difference Between Design & Calc. Flow (%)	0.5%
Stable (Yes or No)	YES
Channel Parameters	
Vegetation Height, h (ft)	0.67
Grass Roughness Coefficient, C <sub>n</sub>	0.238
Cover Factor, C <sub>f</sub>	0.90
Noncohesive Soil	
Soil Grain Roughness, n <sub>s</sub>	0.016
Permissible Soil Shear Stress, τ <sub>p</sub> (lb/ft²)	N/A
Cohesive Soil	
Porosity, e	0.35
Soil Coefficient 1, c <sub>1</sub>	1.0700
Soil Coefficient 2, c <sub>2</sub>	14.30
Soil Coefficient 3, c <sub>3</sub>	47.700
Soil Coefficient 4, c <sub>4</sub>	1.42
Soil Coefficient 5, c <sub>5</sub>	-0.61
Soil Coefficient 6, c <sub>6</sub>	0.00010
Permissible Soil Shear Stress, τ <sub>p</sub> (lb/ft²)	0.080
Total Permissible Shear Stress, τ <sub>p</sub> (lb/ft²)	0.080
Cross Sectional Area, A (ft²)	3.000
Wetted Perimeter, P (ft)	6.36
Hydraulic Radius, R (ft)	0.472
Top Width, T (ft)	6.00
Hydraulic Depth, D (ft)	0.500
Froude Number (Q design)	0.505
Channel Shear Stress, $\tau_o$ (lb/ft²)	0.59
Actual Sheer Stress, τ <sub>d</sub> (lb/ft²) Mannings n	1.25 0.063
Average Velocity, V (ft/s)	2.02
	6.1
Calculated Flow, Q (ft³/s) Difference Between Design & Calc. Flow (%)	
Effective Shear on Soil Surface, $\tau_e$ (lb/ft <sup>2</sup> )	0.5%
Total Permissible Shear on Veg., $\tau_{\text{n veg}}$ (lb/ft <sup>2</sup> )	12.42
rotar i cimiosible Onear On Vey., t <sub>o vea</sub> (ID/IL)	14.42

Source: Grass Lined Channel Design WisDOT Spreadsheet, FDM 13-30 Attachment 15.2



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Client: WPL	Subject: Downslope Pipe and Inlet Sizing	Chk'd: MJT	Date: 04/04/22

To size the downslope pipe and inlet to accommodate the 25-year, 24-hour storm event.

#### References:

1. HydroCAD Report\_POO Landfill Closure

#### Approach:

Use the orifice equation to size the downslope pipe inlet. Size the inlet for the largest diversion berm flow rate and apply that inlet size to all downslope pipe inlets. Confirm the head (h) acting on the orifice will not overtop the diversion berm depth of 2.0 ft.

Use Manning's equation to size the downslope pipe based on the largest diversion berm flow rate. Confirm the pipe has capacity for the design flow under open channel flow conditions.

#### Assumptions:

- 1. Orifice coefficient = 0.63
- 2. Assume the orifice head (h) acts on the centerline of the inlet pipe.
- 3. Manning's n = 0.012 (For smooth walled HDPE pipe: http://www.engineeringtoolbox.com/mannings-roughness-d\_799.html)
- 4. Size flumes under the vegetated cover condition.

#### Calculations:

#### Size the downslope pipe inlet:

From the HydroCAD report (Reference #1), the maximum 25-year, 24-hour flow along a diversion berm is in HydroCAD model).

Flume 3 Area 24

6.1 cfs

```
Orifice Equation: Q = C * A * (2 * g * h)^{0.5}
   where: Q = flow rate (cfs) =
                                           6.1 (From above)
            C = orifice coefficient =
                                           0.63 (See assumption #1)
            A = orifice area (sf) =
                                           1.77 (area of 18" diameter pipe) Actual Pipe Diameter =
                                                                                                              18 inches
            g = gravity (ft/sec^2)=
                                           32.2
            h = orifice head acting on centerline (ft)
            h = (Q/(C * A))^2/(2 * g) =
                                             0.5 ft
            Given Assumption #2, depth of flow along diversion berm = h + D/2/12 =
                                                                                                1.21
                                                                                                        ft
```

#### Results:

Based on the inlet sizing calculation, an 18" diameter inlet will convey the stormwater runoff from the largest flow rate to a flume.

Based on the Manning's calculation for flow within the pipe, the 12" diameter downslope pipe will accommodate the design flow under open channel flow conditions. Although the flow for the downslope pipes can be handled by 12" dia. pipes, for ease of construction, all downslope pipes will be 18" dia.

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#### Calculations (Continued):

The diversion swale depth of 2 ft is sufficient to prevent overtopping at the downslope pipe inlet locations. The depth of the diversion berm increases at the entrance of the down slope pipes due to mounding of the soil over the pipe.

#### Size the downslope flume pipe:

Use Manning's equation to size the downslope pipe.

Manning's Equation:  $Q = (1.49/n) \times A \times R^{(2/3)} \times S^{(1/2)}$ 

Q = Flow Rate, cfs where:

n = Manning's Roughness Coefficient

A = Flow Area, sf

R = Hydraulic Radius, ft (= A/P)

S = Channel Slope, ft/ft

From the HydroCAD Report (Reference 1), the peak discharge to each downslope flume resulting from a 25-year, 24-hour storm is as follows:

Flume 1 3.58	3 cfs	Flume 2 4.89 cfs	Flume 3 6.05	cfs	Flume 4 3.66 cfs	Flume 5 4.89	cfs
Area 5	3.58	Area 3 2.13	7 Area 1	4.58	Area 12 0.35	Area 10	3.17
Area 6	2.92	Area 4 3.7	4 Area 2	3.73	Area 13 2.91	Area 11	3.10
Area 20	3.43	Area 22 3.3	5 Area 24	6.05	Area 14 3.66	Area 16	4.89
Area 21	3.35	Area 23 4.8	9 Area 25	5.13	Area 15 1.71	Area 17	4.00
Total =	13.28	14.1	5	19.49	8.63		15.16

#### Flume 6 3.40 cfs Area 8 3.29 Area 9

3.40 Area 18 2.66 Area 19 2.77

Total = 12.12

For flow rates < 20 cfs, assume a 12" diameter downslope flume:

19.49 Use cfs to Flume 3 to check sizing (max flow to a flume that is  $\leq$  20 cfs)

Design Criteria

Pipe Diameter (in) = D =12

Pipe Slope (ft/ft) = S =0.25

Manning's Roughness Coefficient = n =0.012

See Downslope Flume 3 pipe flow calculator on Sheet 3

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### Calculations (Continued):

# Manning Formula Uniform Pipe Flow at Given Slope and Depth

### Inputs:

<u> </u>		
Pipe Diameter, d <sub>o</sub>	12.00	in
Manning Roughness,		
<u>n</u>	0.0120	
Pressure slope		
(possibly equal to		
pipe slope), So	0.2500	slope
Percent of (or ratio		
to) full depth (100%		
or 1 if flowing full)	0.8290	fraction

#### **Results:**

Flow, Q	19.4905	ft^3/s
Velocity, v	27.9991	ft/s
Velocity head, hv	12.1838	ft
Flow Area, A	0.6961	ft^2
Wetted Perimeter, P	2.2890	ft
Hydraulic Radius	0.3041	ft
Top Width, T	0.7530	ft
Froude Number, F	5.21	
Shear Stress (tractive		
force), τ	12.9373	psf

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**HawsEDC Calculators** 

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Calculations (Continued):

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Client: WPL

# Manning Formula Uniform Pipe Flow at Given Slope and Depth

### Inputs:

parto.		
Pipe Diameter, d <sub>o</sub>	18.00	in
Manning Roughness,		
<u>n</u>	0.0120	
Pressure slope		
(possibly equal to		
pipe slope), So	0.2500	slope
Percent of (or ratio		
to) full depth (100%		
or 1 if flowing full)	0.4037	fraction

#### **Results:**

Flow, Q	19.4983	ft^3/s
Velocity, v	29.1783	ft/s
Velocity head, hv	13.2317	ft
Flow Area, A	0.6682	ft^2
Wetted Perimeter, P	2.0655	ft
Hydraulic Radius	0.3235	ft
Top Width, T	1.4719	ft
Froude Number, F	7.75	
Shear Stress (tractive		
force), τ	9.4502	psf

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**HawsEDC Calculators** 

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Client: WPL	Subject: Energy Dissipator Sizing	Chk'd: MJT		Date	: 4/1/22	

To size an energy dissipator structure and riprap apron at the outlet of the downslope flume pipes.

#### References:

- 1. "Hydraulic Design of Energy Dissipators for Culverts and Channels," HEC-14, Third Edition, July 2006, USDOT FHWA.
- 2. Downslope Pipe and Inlet Sizing calculation (for pipe size, flow rate, and pipe velocity).
- 3. HydroCAD Model\_POO Landfill Closure
- 4. Facilities Development Manual Chapter 13, Section 13-30 Rock Riprap Lined Chutes.

#### Approach:

Use the downslope pipe outlet velocity to size an energy dissipator structure (USBR Type VI Impact Basin) following the design approach outlined in Section 9.4 of Reference #1.

Use Rock Chute Data Spreadsheet, FDM 13-30-30 Attachment 30.1 (from Reference #5) to design the rock chute.

For construction purposes use the maximum flow to size all dissipators and riprap apron.

#### Assumptions:

El...... 1 2 50 efe

- 1. Riprap specific gravity = 2.65
- $2. From the \ HydroCAD \ Report, the \ 25-year, \ 24-hour \ peak \ discharge \ to \ each \ downslope \ flume \ is \ as \ follows:$

El., ...... 2 4 0 5 afa

El., ... E 4 90 afa

Flume I 3.58	cts	Flume 2 4.89	cts	Flume 3 6.05	cts	Flume 4 3.00	cts	Flume 5 4.89	cts
Area 5	3.58	Area 3	2.17	Area 1	4.58	Area 12	0.35	Area 10	3.17
Area 6	2.92	Area 4	3.74	Area 2	3.73	Area 13	2.91	Area 11	3.10
Area 20	3.43	Area 22	3.35	Area 24	6.05	Area 14	3.66	Area 16	4.89
Area 21	3.35	_ Area 23	4.89	Area 25	5.13	Area 15	1.71	Area 17	4.00
Total =	13.28		14.15		19.49		8.63		15.16
Flume 6 3.40	cfs								
Area 8	3.29								
Area 9	3.40								
Area 18	2.66								
Area 19	2.77	=							
Total =	12.12								

Using Figure 9.14 (See Sheet 4), enter the Froude Number and the Energy from Step 2 to determine the from the downslope flume pipe and inlet sizing calculation.

#### Results:

The energy dissipator structures for the 18" dia. downslope flume pipes will consist of dissipator structures with widths ( $W_B$ ) of 6 feet, with the remaining dimensions from Table 9.2 on Sheets 5 and 6.

Riprap at the Flume 3, 4, 5 and 6 energy dissipator outlets will consist of WisDOT Light Riprap (D50= 5.5 inches) (See Page 3).

The riprap apron footprint will be based on the energy dissipator width and the outlet swale geometry.

Riprap at Flume 1 and 2 energy dissipator outlets will consist of WisDOT Light Riprap (D50= 5.8 and 3.6 inches). The riprap apron footprint will be 6 feet wide (based on rock chute calcs for RC1 and RC2) and extend down to the existing swale (Swale S4).

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#### Calculations:

#### For 18" dia. downslope flume pipes

From Reference #2:

Flow rate (Q) = 19.5 cfs  
Pipe velocity (V) = 8.9 ft/s  
Flow area (A) = 
$$Q/V = 2.19$$
 sf

Design procedure from pg. 9-40 of Reference #1:

Step 1: Compute the Equivalent Depth of Flow Entering Dissipator:

$$Y_e = (A/2)^{1/2}$$
 where:  $Y_e = Equivalent depth$ 

$$A = Area (from above)$$

$$Y_e = 1.05 ft$$

Step 2: Compute the Froude Number and the energy at the end of the pipe:

#### Step 3: Determine H<sub>a</sub>/W<sub>B</sub> and calculate the required width of the energy dissipator:

Using Figure 9.14 (See Sheet 4), enter the Froude Number and the Energy from Step 2 to determine the width of the energy dissipator.

From Figure 9.14, 
$$H_o/W_B =$$
 0.40 
$$W_B = H_o/(H_o/W_B) \qquad W_B = 5.7 \text{ ft.}$$
 Use  $W_B =$  6.0 ft.

Step 4: Obtain the remaining energy dissipator dimensions from Table 9.2 from Reference #1 (see Sheets 5 and 6)

#### Step 5: Size the riprap at the structure outlet

From Reference #5, use Rock Chute Design spreadsheet (see Sheet 3)

# **Rock Chute Design Data**

(Version WI-April-2005, Based on <u>Design of Rock Chutes</u> by Robinson, Rice, Kadavy, ASAE, 1998) Revised for WisDOT 9/2010

Project: COL - POO Landfill Closure County: Columbia Designer: RJG Checked by: MJT Date: February 23, 2022 Date: 04/05/22 Input Geometry: - Upstream Channel **Downstream Channel** Bottom Width = 6.0 Bottom Width = 6.0 Bottom Width = 6.0 2.0 (m:1) Side slopes = 1.0 (m:1) Factor of safety = 1.20 (SF Side slopes = Side slopes = 2.0 (z:1) Mannings n value = 0.012 Mannings n value = 0.030 2.0:1 max. Bed slope = 0.2500 ft./ft Bed slope = 0.0001 ft./ft 3.0:1 max. Bed slope = 0.0050 ft./ft. Freeboard = 1.0 ft. Note: Use procedures 13-30-15 or 13-30-25 Base flow = 0.0 upstream and downstream Mannings n Outlet apron depth, d = 1.0 ft. cfs Flow and Elevation Data: Apron elev. --- Inlet = 818.0 ft. Outlet 816.0 ft. --- (H<sub>c</sub> Note: The total required capacity is routed Degree of angularity = through the chute (principal spillway) or in combination with an auxiliary spillway. Q<sub>high</sub> = Runoff from design storm 1 --> 50% angular, 50% rounded Q<sub>5</sub> = Runoff from a 5-year,24-hour storm 2 --> 100 % rounded Input tailwater (Tw): Q<sub>high</sub>= 19.5 → Tw (ft.) = Program cfs High flow storm through chute - $Q_{low} = 19.5$ Low flow storm through chute ➤ Tw (ft.) = Program cfs Profile and Cross Section (Output): Starting Station = 3+00.0 Notes:  $h_{pv} = 0.16 \text{ ft.} (0.16 \text{ ft.})$ 1) Output given as High Flow (Low Flow) values.  $H_{pe} = 1.04 \text{ ft.}$  $h_{cv} = 0.27 \text{ ft.} (0.27 \text{ ft.})$ 2) Tailwater depth plus d must be at or above the  $H_{ce} = 0.91 \text{ ft.}$ hydraulic jump height for the chute to function. **Energy Grade Line** 3) Critical depth occurs 2y<sub>c</sub> - 4y<sub>c</sub> upstream of crest.  $0.715y_c = 0.46 \text{ ft.}$ (0.46 ft.)  $H_{\rm p} = 0.88 \, {\rm ft}$ Inlet  $(0.88 \text{ ft.}) \text{ y}_{c} = 0.64 \text{ ft.}$  $d_1 = 0.38 \text{ ft.}$ Hydraulic Jump Channel (0.38 ft.) Height,  $d_2 = 0.99$  ft. (0.99 ft.) Inlet Apron  $1 y_n = 1.75 \text{ ft.}$ Tw+d = 1.9 ft. - Tw o.k.(1.75 ft.) (1.9 ft.) - Tw o.k. 40\*Design  $D_{50} = 21$  ft Velocity<sub>inlet</sub> = 1.43 fps radius Outlet Channel at normal depth Critical Slope check upstream is OK Slope = 0.005 ft./ft.Geotextile <sup>1</sup> Note: When the normal depth (y<sub>n</sub>) in the inlet Outlet Apron channel is less than the weir head (H<sub>n</sub>), ie., the weir capacity is less d = 1 ft. {1 ft. minimum suggested} than the channel capacity, restricted flow or ponding will occur. This  $15(D_{50})(F_s)$ reduces velocity and prevents erosion upstream of the inlet apron. 2.77 fps Velocity<sub>outlet</sub> = at normal depth **Profile Along Centerline of Chute Typical Cross Section** Equivalent unit discharge SF = Factor of safety (multiplier) Freeboard = 1 ft  $d_1 =$ 0.38 ft Normal depth in chute Geotextile n-value = Manning's roughness coefficient  $D_{50}(SF) =$ Minimum Design D<sub>50</sub>\*  $2(D_{50})(SF) =$ Rock chute thickness Tw + d =Tailwater above outlet apron Rock thickness = 15.3 in.  $d_2 =$ 0.99 ft. Hydraulic jump height Use H<sub>p</sub> along chute \*\*\* The outlet function adequately but not less than d2. B' = 6.8 ft**High Flow Storm Information** 

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 By: RJG
 Date: 2/23/22

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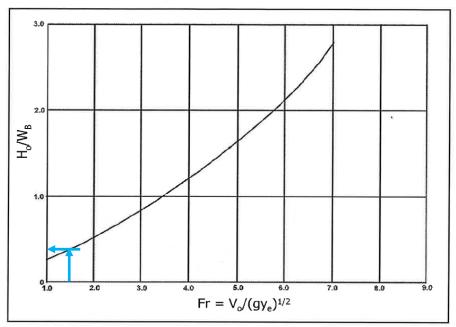


Figure 9.14. Design Curve for USBR Type VI Impact Basin

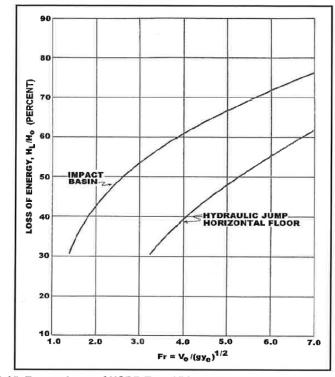


Figure 9.15. Energy Loss of USBR Type VI Impact Basin versus Hydraulic Jump

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#### Table 9.2 (CU). USBR Type VI Impact Basin Dimensions (ft) (AASHTO, 2005)

Table 9.2 (CO). OSBR Type VI impact Basin Dimensions (it) (AASHTO, 2005)							
W <sub>B</sub>	h <sub>1</sub>	h <sub>2</sub>	h <sub>3</sub>	h <sub>4</sub>	L	L <sub>1</sub>	L <sub>2</sub>
4.	3.08	1.50	0.67	1.67	5.42	2.33	3.08
5.	3.83	1.92	0.83	2.08	6.67	2.92	3.83
6.	4.58	2.25	1.00	2.50	8.00	3.42	4.58
7.	5.42	2.58	1.17	2.92	9.42	4.00	5.42
8.	6.17	3.00	1.33	3.33	10.67	4.58	6.17
9.	6.92	3.42	1.50	3.75	12.00	5.17	6.92
10.	7.58	3.75	1.67	4.17	13.42	5.75	7.67
11.	8.42	4.17	1.83	4.58	14.58	6.33	8.42
12.	9.17	4.50	2.00	5.00	16.00	6.83	9.17
13.	10.17	4.92	2.17	5.42	17.33	7.42	10.00
14.	10.75	5.25	2.33	5.83	18.67	8.00	10.75
15.	11.50	5.58	2.50	6.25	20.00	8.50	11.50
16.	12.25	6.00	2.67	6.67	21.33	9.08	12.25
17.	13.00	6.33	2.83	7.08	21.50	9.67	13.00
18.	13.75	6.67	3.00	7.50	23.92	10.25	13.75
19.	14.58	7.08	3.17	7.92	25.33	10.83	14.58
20.	15.33	7.50	3.33	8.33	26.58	11.42	15.33
20.	15.33	7.50	3.33	8.33	26.58	11.42	15.33
20. W <sub>B</sub>	15.33 W <sub>1</sub>	7.50 W <sub>2</sub>	3.33 t <sub>1</sub>	8.33 t <sub>2</sub>	26.58 t <sub>3</sub>	11.42 t <sub>4</sub>	15.33 t <sub>s</sub>
W <sub>B</sub>							_
W <sub>B</sub>	W <sub>1</sub>	W <sub>2</sub>	t <sub>1</sub>	t <sub>2</sub>	t <sub>3</sub>	t,	ts
W <sub>B</sub> 4. 5.	W <sub>1</sub>	W <sub>2</sub>	t <sub>1</sub>	t <sub>2</sub>	t <sub>3</sub>	t <sub>4</sub>	t <sub>s</sub> 0.25
W <sub>B</sub> 4. 5.	W <sub>1</sub> 0.33 0.42	W <sub>2</sub> 1.08 1.42	t <sub>1</sub> 0.50 0.50	t <sub>2</sub> 0.50 0.50	t <sub>3</sub> 0.50 0.50	t <sub>4</sub> 0.50 0.50	t <sub>s</sub> 0.25 0.25
W <sub>B</sub> 4. 5.	W <sub>1</sub> 0.33 0.42 0.50	W <sub>2</sub> 1.08 1.42 1.67 1.92 2.17	t <sub>1</sub> 0.50 0.50 0.50	t <sub>2</sub> 0.50 0.50 0.50	t <sub>3</sub> 0.50 0.50 0.50	t <sub>4</sub> 0.50 0.50 0.50	t <sub>s</sub> 0.25 0.25 0.25
W <sub>B</sub> 4. 5. 6.	W <sub>1</sub> 0.33 0.42 0.50 0.50	W <sub>2</sub> 1.08 1.42 1.67 1.92	t <sub>1</sub> 0.50 0.50 0.50 0.50 0.50	t <sub>2</sub> 0.50 0.50 0.50 0.50 0.50	t <sub>3</sub> 0.50 0.50 0.50 0.50 0.50	t <sub>4</sub> 0.50 0.50 0.50 0.50 0.50	t <sub>5</sub> 0.25 0.25 0.25 0.25 0.25
W <sub>B</sub> 4. 5. 6. 7.	W <sub>1</sub> 0.33 0.42 0.50 0.50 0.58	W <sub>2</sub> 1.08 1.42 1.67 1.92 2.17	t <sub>1</sub> 0.50 0.50 0.50 0.50 0.50 0.50	t <sub>2</sub> 0.50 0.50 0.50 0.50 0.50 0.50	t <sub>3</sub> 0.50 0.50 0.50 0.50 0.50 0.50	t <sub>4</sub> 0.50 0.50 0.50 0.50 0.50 0.50	t <sub>s</sub> 0.25 0.25 0.25 0.25 0.25 0.25
W <sub>B</sub> 4. 5. 6. 7. 8. 9. 10.	W <sub>1</sub> 0.33 0.42 0.50 0.50 0.58 0.67 0.75 0.83	W <sub>2</sub> 1.08 1.42 1.67 1.92 2.17 2.50 2.75 3.00	t <sub>1</sub> 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.67 0.67	t <sub>2</sub> 0.50 0.50 0.50 0.50 0.50 0.58 0.58 0.67 0.75	t <sub>3</sub> 0.50 0.50 0.50 0.50 0.50 0.58 0.67 0.75	0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.67 0.67	t <sub>5</sub> 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25
W <sub>B</sub> 4. 5. 6. 7. 8. 9. 10. 11.	W <sub>1</sub> 0.33 0.42 0.50 0.50 0.58 0.67 0.75 0.83 0.92	W <sub>2</sub> 1.08 1.42 1.67 1.92 2.17 2.50 2.75 3.00 3.00	t <sub>1</sub> 0.50 0.50 0.50 0.50 0.50 0.50 0.67 0.67 0.67	t <sub>2</sub> 0.50 0.50 0.50 0.50 0.58 0.58 0.67 0.75 0.83	t <sub>3</sub> 0.50 0.50 0.50 0.50 0.50 0.58 0.67 0.75 0.75 0.83	0.50 0.50 0.50 0.50 0.50 0.50 0.58 0.67 0.67 0.75	t <sub>5</sub> 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25
W <sub>B</sub> 4. 5. 6. 7. 8. 9. 10. 11. 12.	W <sub>1</sub> 0.33 0.42 0.50 0.50 0.58 0.67 0.75 0.83	W <sub>2</sub> 1.08 1.42 1.67 1.92 2.17 2.50 2.75 3.00 3.00 3.00	t <sub>1</sub> 0.50 0.50 0.50 0.50 0.50 0.50 0.67 0.67 0.67 0.67	t <sub>2</sub> 0.50 0.50 0.50 0.50 0.50 0.58 0.58 0.67 0.75	t <sub>3</sub> 0.50 0.50 0.50 0.50 0.58 0.67 0.75 0.75 0.83 0.83	t <sub>4</sub> 0.50 0.50 0.50 0.50 0.50 0.50 0.67 0.67 0.75 0.83	t <sub>s</sub> 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25
W <sub>B</sub> 4. 5. 6. 7. 8. 9. 10. 11.	W <sub>1</sub> 0.33 0.42 0.50 0.50 0.58 0.67 0.75 0.83 0.92	W <sub>2</sub> 1.08 1.42 1.67 1.92 2.17 2.50 2.75 3.00 3.00	t <sub>1</sub> 0.50 0.50 0.50 0.50 0.50 0.50 0.67 0.67 0.67	t <sub>2</sub> 0.50 0.50 0.50 0.50 0.58 0.58 0.67 0.75 0.83	t <sub>3</sub> 0.50 0.50 0.50 0.50 0.50 0.58 0.67 0.75 0.75 0.83	0.50 0.50 0.50 0.50 0.50 0.50 0.58 0.67 0.67 0.75	t <sub>5</sub> 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25
W <sub>B</sub> 4. 5. 6. 7. 8. 9. 10. 11. 12.	W <sub>1</sub> 0.33 0.42 0.50 0.50 0.58 0.67 0.75 0.83 0.92 1.00	W <sub>2</sub> 1.08 1.42 1.67 1.92 2.17 2.50 2.75 3.00 3.00 3.00	t <sub>1</sub> 0.50 0.50 0.50 0.50 0.50 0.50 0.67 0.67 0.67 0.67	t <sub>2</sub> 0.50 0.50 0.50 0.50 0.50 0.58 0.58 0.67 0.75 0.83 0.92	t <sub>3</sub> 0.50 0.50 0.50 0.50 0.58 0.67 0.75 0.75 0.83 0.83	t <sub>4</sub> 0.50 0.50 0.50 0.50 0.50 0.50 0.67 0.67 0.75 0.83	t <sub>s</sub> 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25
W <sub>B</sub> 4. 5. 6. 7. 8. 9. 10. 11. 12. 13.	W <sub>1</sub> 0.33 0.42 0.50 0.50 0.58 0.67 0.75 0.83 0.92 1.00 1.08	W <sub>2</sub> 1.08 1.42 1.67 1.92 2.17 2.50 2.75 3.00 3.00 3.00 3.00	t <sub>1</sub> 0.50 0.50 0.50 0.50 0.50 0.50 0.67 0.67 0.67 0.67	t <sub>2</sub> 0.50 0.50 0.50 0.50 0.58 0.58 0.67 0.75 0.83 0.92 1.00	t <sub>3</sub> 0.50 0.50 0.50 0.50 0.50 0.58 0.67 0.75 0.75 0.83 0.83 0.92	0.50 0.50 0.50 0.50 0.50 0.50 0.58 0.67 0.67 0.75 0.83	t <sub>s</sub> 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25
W <sub>B</sub> 4. 5. 6. 7. 8. 9. 10. 11. 12. 13. 14.	W <sub>1</sub> 0.33 0.42 0.50 0.50 0.58 0.67 0.75 0.83 0.92 1.00 1.08 1.17	W <sub>2</sub> 1.08 1.42 1.67 1.92 2.17 2.50 2.75 3.00 3.00 3.00 3.00 3.00	t <sub>1</sub> 0.50 0.50 0.50 0.50 0.50 0.50 0.67 0.67 0.67 0.67 0.67 0.67	t <sub>2</sub> 0.50 0.50 0.50 0.50 0.50 0.58 0.58 0.67 0.75 0.83 0.92 1.00 1.00	t <sub>3</sub> 0.50 0.50 0.50 0.50 0.50 0.75 0.75 0.75	0.50 0.50 0.50 0.50 0.50 0.50 0.58 0.67 0.67 0.75 0.83 0.92	t <sub>s</sub> 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25
W <sub>B</sub> 4. 5. 6. 7. 8. 9. 10. 11. 12. 13. 14. 15.	W <sub>1</sub> 0.33 0.42 0.50 0.50 0.58 0.67 0.75 0.83 0.92 1.00 1.08 1.17 1.25	W <sub>2</sub> 1.08 1.42 1.67 1.92 2.17 2.50 2.75 3.00 3.00 3.00 3.00 3.00 3.00	t <sub>1</sub> 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.67 0.67 0.67 0.67 0.67 0.67 0.75	t <sub>2</sub> 0.50 0.50 0.50 0.50 0.50 0.58 0.58 0.67 0.75 0.83 0.92 1.00 1.00	t <sub>3</sub> 0.50 0.50 0.50 0.50 0.50 0.58 0.67 0.75 0.75 0.83 0.83 0.92 1.00 1.00	0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.67 0.67 0.75 0.83 0.92 1.00 1.00	t <sub>s</sub> 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25
W <sub>B</sub> 4. 5. 6. 7. 8. 9. 10. 11. 12. 13. 14. 15. 16.	W <sub>1</sub> 0.33 0.42 0.50 0.50 0.58 0.67 0.75 0.83 0.92 1.00 1.08 1.17 1.25 1.33	W <sub>2</sub> 1.08 1.42 1.67 1.92 2.17 2.50 2.75 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.0	t <sub>1</sub> 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.67 0.67 0.67 0.67 0.67 0.67 0.75	t <sub>2</sub> 0.50 0.50 0.50 0.50 0.50 0.58 0.58 0.67 0.75 0.83 0.92 1.00 1.00 1.08	t <sub>3</sub> 0.50 0.50 0.50 0.50 0.50 0.58 0.67 0.75 0.75 0.83 0.83 0.92 1.00 1.00	0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.67 0.67 0.75 0.83 0.92 1.00 1.00	t <sub>s</sub> 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25

Job No. 25220183.00

Client: WPL

EERS	Sheet No.	6 of	7
	Calc. No.		
	Rev. No.		
Job: Columbia Energy Center POO Landfill Closure	By: RJG	Date:	2/23/22
Subject: Energy Dissipator Sizing	Chk'd: MJT	Date:	4/1/22

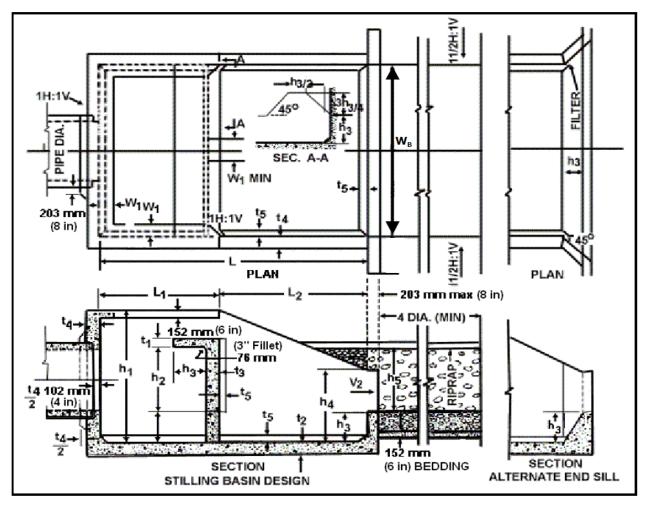


Figure 9.13. USBR Type VI Impact Basin



RSRS	Sheet No:	7 of 7
	Calc. No.	_
	Rev. No.	
Job: Columbia Energy Center POO Landfill Clos	uri By: RJG	Date: 2/4/21
Subject: Energy Dissipator Sizing	Chk'd: MJT	Date: 4/1/22

Calculations (Continued):

Job No. 25220183.00

Client: WPL

# **Downslope Flume 3 - Velocity Calculator (Q = 19.49 cfs)**

## Manning Formula Uniform Pipe Flow at Given Slope and Depth

### Inputs:

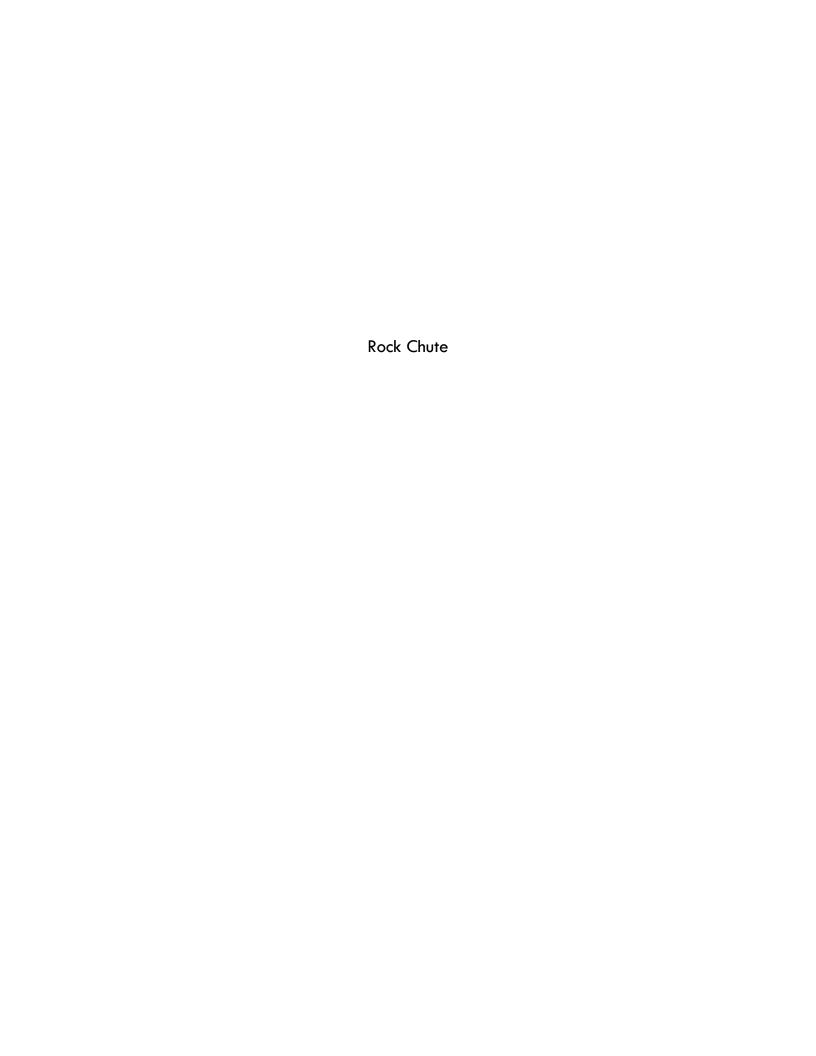
Pipe Diameter, d₀	18	in
Manning Roughness,		
<u>n</u>	0.0120	
Pressure slope	0.2500	slope
Percent of (or ratio		
to) full depth (100%		
or 1 if flowing full)	0.4037	fraction

#### **Results:**

Flow, Q	19.4983	ft^3/s
Velocity, v	8.8936	m/s
Velocity head, hv	4.0330	m
Flow Area, A	0.0621	m^2
Wetted Perimeter, P	0.6296	m
Hydraulic Radius	0.0986	m
Top Width, T	0.4486	m
Froude Number, F	7.75	
Shear Stress (tractive		
force), т	452.4774	N/m^2

Version 2.0 (20 June 2017)

**HawsEDC Calculators** 



SCS ENGI	Sheet No: 1 of 4		
		Calc. No.	
		Rev. No.	
Job No. 25220183.00	Job: COL - POO	By: RJG	Date: 4/11/22
Client: WPL	Subject: Rock Chute Sizing & Riprap Size	Chk'd: MJT	Date: 4/13/22

To size the rock chutes to accommodate the 25-year, 24-hour storm event.

#### References:

- 1. Rock Chute Design Data spreadsheet Version WI-April-2005, Based on Design of Rock Chutes by Robinson, Rice, Kadavy, ASAE, 1998.
- 2. HydroCAD Report\_Post Construction
- 3. Figure 1 Storm Water Post Construction
- 4. Stable 25.1 Typical Particle Sizes of Native Sands at 75 Percent Passing (D75) from WisDOT Facilities. Development Manual (FDM).

#### Approach:

- 1. Enter Inlet Channel data based on culvert apron or swale geometry Reference #2 and #3.
- 2. Enter Chute data based on slope from Reference #3, start the width, Bw equal to inlet channel Bw.
- 3. Enter Outlet Channel data based on Reference #3, start the width, Bw equal to inlet channel Bw.
- 4. Enter drainage area, apron elevations, flow (Q), and rainfall.
- 5. Adjust Bw for Chute and Outlet Channel until spreadsheet shows the rock chute "will" function adequately.
- 6. Determine rip rap classification based on D50 weight per Reference #4.

#### **Assumptions:**

- 1. Assume side slopes of chute and outlet channel are 2:1.
- 2. Assume Factor of Safey is 1.2.
- 3. n-value is based on proposed conditions at the channel.
- 4. Assume Outlet apron depth, d is 1.0 ft.
- 5. Freeboard is 1.0 ft.
- 6. Use 25-year, 24-hour storm event flow (Reference #2) for  $Q_{high}$  and  $Q_{low}$
- 7. Classification of riprap is based on weight (Reference #4).

#### Calculations:

See attached spreadsheet calcs for each rock chute.

### Results:

The rock chutes are adequately designed to accommodate the flows from the 25-year, 24-hour storm event.

Rock Chute	Width (ft)	Thickness (in)	Apron Width (ft)	Apron Length (ft)	D <sub>50</sub> (in)	WisDOT Rip Rap Classification
RC1	6	12	6	7	5.8	Light Riprap Type R
RC2	6	8	6	5	3.6	Light Riprap Type R

## **Rock Chute Design Data**

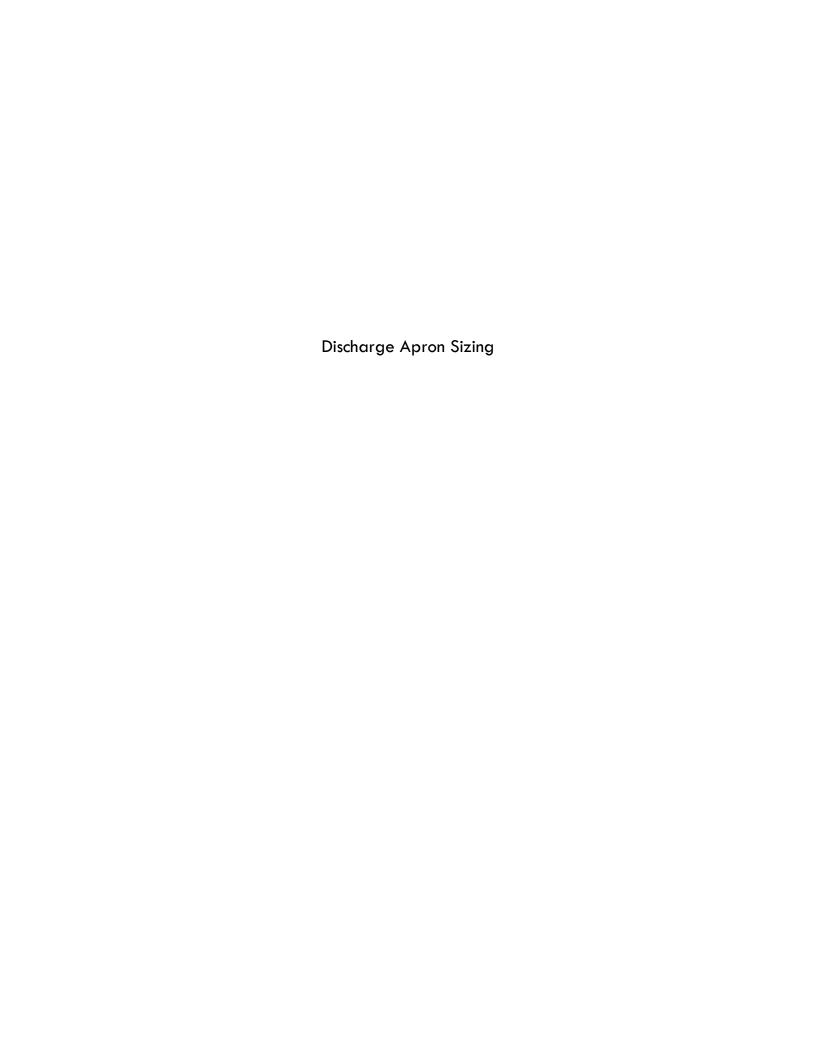
(Version WI-April-2005, Based on <u>Design of Rock Chutes</u> by Robinson, Rice, Kadavy, ASAE, 1998) Revised for WisDOT 9/2010

Project: COL - POO Landfill Closure RC1 County: Columbia Designer: RJG Checked by: MJT Date: April 11, 2022 Date: 04/13/22 Input Geometry: Upstream Channel **Downstream Channel** Bottom Width = 6.0 Bottom Width = 6.0 Bottom Width = 6.0 2.0 (m:1) Side slopes = 1.0 (m:1) Factor of safety = 1.20 (SF Side slopes = Side slopes = 2.0 (z:1) Mannings n value = 0.012 Mannings n value = 0.030 2.0:1 max. Bed slope = 0.1967 ft./ft Bed slope = 0.0001 ft./ft 3.0:1 max. Bed slope = 0.0050 ft./ft. Freeboard = 1.0 ft. Note: Use procedures 13-30-15 or 13-30-25 Base flow = 0.0 upstream and downstream Mannings n Outlet apron depth, d = 1.0 ft. cfs Flow and Elevation Data: Apron elev. --- Inlet = 822.8 ft. Outlet 802.4 ft. --- (H Note: The total required capacity is routed Degree of angularity = through the chute (principal spillway) or in combination with an auxiliary spillway. Q<sub>high</sub> = Runoff from design storm 1 --> 50% angular, 50% rounded Q<sub>5</sub> = Runoff from a 5-year,24-hour storm 2 --> 100 % rounded Input tailwater (Tw): Q<sub>high</sub>= **13.2** → Tw (ft.) = Program cfs High flow storm through chute - $Q_{low} = 13.2$ Low flow storm through chute ➤ Tw (ft.) = Program cfs Profile and Cross Section (Output): Starting Station = 3+00.0 Notes:  $h_{pv} = 0.13 \text{ ft.} (0.13 \text{ ft.})$ 1) Output given as High Flow (Low Flow) values.  $H_{pe} = 0.81 \text{ ft.}$  $h_{cv} = 0.22 \text{ ft.} (0.22 \text{ ft.})$ 2) Tailwater depth plus d must be at or above the  $H_{ce} = 0.72 \text{ ft.}$ hydraulic jump height for the chute to function. **Energy Grade Line** 3) Critical depth occurs 2y<sub>c</sub> - 4y<sub>c</sub> upstream of crest.  $0.715y_c = 0.36 \text{ ft.}$ (0.36 ft.)  $H_{\rm p} = 0.68 \, {\rm ft}$ Inlet  $(0.68 \text{ ft.}) \text{ y}_c = 0.5 \text{ ft.}$  $d_1 = 0.31 \text{ ft.}$ Hydraulic Jump Channel (0.31 ft.)Height,  $d_2 = 0.75$  ft. (0.75 ft.) Inlet Apron  $1 y_n = 1.4 \text{ ft.}$ Tw+d = 1.72 ft. - Tw o.k.(1.4 ft.)(1.72 ft.) - Tw o.k. 40\*Design  $D_{50} = 16$  ft Velocity<sub>inlet</sub> = 1.27 fps radius Channel at normal depth Critical Slope check upstream is OK Slope = 0.005 ft./ft.Geotextile <sup>1</sup> Note: When the normal depth (y<sub>n</sub>) in the inlet Outlet Apron channel is less than the weir head (H<sub>n</sub>), ie., the weir capacity is less d = 1 ft. {1 ft. minimum suggested} than the channel capacity, restricted flow or ponding will occur. This  $15(D_{50})(F_s)$ reduces velocity and prevents erosion upstream of the inlet apron. 2.45 fps Velocity<sub>outlet</sub> = at normal depth **Profile Along Centerline of Chute Typical Cross Section** Equivalent unit discharge SF = Factor of safety (multiplier) Freeboard = 1 ft  $d_1 =$ 0.31 ft Normal depth in chute Geotextile n-value = Manning's roughness coefficient  $D_{50}(SF) =$ Minimum Design D<sub>50</sub>\*  $2(D_{50})(SF) =$ Rock chute thickness Tw + d =Tailwater above outlet apron Rock thickness = 11.7 in.  $d_2 =$ Hydraulic jump height Use H<sub>p</sub> along chute \*\*\* The outlet function adequately but not less than d2. B' = 6.8 ft**High Flow Storm Information** 

## **Rock Chute Design Data**

(Version WI-April-2005, Based on <u>Design of Rock Chutes</u> by Robinson, Rice, Kadavy, ASAE, 1998) Revised for WisDOT 9/2010

Project: COL - POO Landfill Closure RC2 County: Columbia Designer: RJG Checked by: MJT Date: April 11, 2022 Date: 04/13/22 Input Geometry: Upstream Channel **Downstream Channel** Bottom Width = 6.0 Bottom Width = 6.0 Bottom Width = 6.0 2.0 (m:1) Side slopes = 1.0 (m:1) Factor of safety = 1.20 (SF Side slopes = Side slopes = 2.0 (z:1) Mannings n value = 0.012 Mannings n value = 0.030 2.0:1 max. Bed slope = 0.0690 ft./ft Bed slope = 0.0001 ft./ft 3.0:1 max. Bed slope = 0.0050 ft./ft. Freeboard = 1.0 ft. Note: Use procedures 13-30-15 or 13-30-25 Base flow = 0.0 upstream and downstream Mannings n Outlet apron depth, d = 1.0 ft. cfs Flow and Elevation Data: Apron elev. --- Inlet = 815.8 ft. Outlet 808.4 ft. --- (H Note: The total required capacity is routed Degree of angularity = through the chute (principal spillway) or in combination with an auxiliary spillway. Q<sub>high</sub> = Runoff from design storm 1 --> 50% angular, 50% rounded Q<sub>5</sub> = Runoff from a 5-year,24-hour storm 2 --> 100 % rounded Input tailwater (Tw): Q<sub>high</sub>= **14.0** cfs → Tw (ft.) = Program High flow storm through chute - $Q_{low} = 14.0$ Low flow storm through chute ➤ Tw (ft.) = Program cfs Profile and Cross Section (Output): Starting Station = 3+00.0 Notes:  $h_{pv} = 0.14 \text{ ft.} (0.14 \text{ ft.})$ 1) Output given as High Flow (Low Flow) values.  $H_{pe} = 0.84 \text{ ft.}$  $h_{cv} = 0.23 \text{ ft.} (0.23 \text{ ft.})$ 2) Tailwater depth plus d must be at or above the  $H_{ce} = 0.75 \text{ ft.}$ hydraulic jump height for the chute to function. **Energy Grade Line** 3) Critical depth occurs 2y<sub>c</sub> - 4y<sub>c</sub> upstream of crest.  $0.715y_c = 0.37 \text{ ft.}$ (0.37 ft.)  $H_p = 0.71 \text{ ft}$ Inlet  $(0.71 \text{ ft.}) \text{ y}_c = 0.52 \text{ ft.}$  $d_1 = 0.39 \text{ ft.}$ Hydraulic Jump Channel (0.39 ft.) Height,  $d_2 = 0.68$  ft. (0.68 ft.) Inlet Apron  $1 \dot{y}_n = 1.45 \text{ ft.}$ Tw+d = 1.75 ft. - Tw o.k.(1.45 ft.) (1.75 ft.) - Tw o.k. 40\*Design  $D_{50} = 10$  ft Velocity<sub>inlet</sub> = 1.3 fps radius Channel at normal depth Critical Slope check upstream is OK Slope = 0.005 ft./ft.Geotextile <sup>1</sup> Note: When the normal depth (y<sub>n</sub>) in the inlet Outlet Apron channel is less than the weir head (H<sub>n</sub>), ie., the weir capacity is less d = 1 ft. {1 ft. minimum suggested} than the channel capacity, restricted flow or ponding will occur. This  $15(D_{50})(F_s)$ reduces velocity and prevents erosion upstream of the inlet apron. 2.5 fps Velocity<sub>outlet</sub> = at normal depth **Profile Along Centerline of Chute Typical Cross Section** Equivalent unit discharge SF = Factor of safety (multiplier) Freeboard = 1 ft  $d_1 =$ 0 30 ft Normal depth in chute Geotextile n-value = Manning's roughness coefficient  $D_{50}(SF) =$ Minimum Design D<sub>50</sub>\*  $2(D_{50})(SF) =$ Rock chute thickness Tw + d =Tailwater above outlet apron Rock thickness = 7.3 in.  $d_2 =$ 0.68 ft. Hydraulic jump height Use H<sub>p</sub> along chute \*\*\* The outlet function adequately but not less than d2. B' = 6.8 ft**High Flow Storm Information** 





Sheet No.	1 of 2
Calc. No.	
Rev. No.	
By: RJG	Date: 2/21/22

 Job No. 25220183.00
 Job: Columbia Energy Center POO Landfill Closure
 By: RJG
 Date: 2/21/22

 Client: WPL
 Subject: Riprap Sizing at Culvert Outlet
 Chk'd: MJT
 Date: 4/5/22

#### Purpose:

To size the riprap apron dimensions at culvert C2, C3, C4, and C5 based on a 25-year, 24 hour storm event:

#### References:

- 1. "Energy Dissipators," Wisconsin Department of Transportation (WisDOT), Facilities Development Manual (FDM) 13-35-5.
- 2. Post Construction Condition HydroCAD Model.
- 3. "Rock Riprap Lined Channels," WisDOT FDM 13-30-25.
- 4. Culvert Sizing Calculation.
- 5. WisDOT FDM Chapter 13, Section 30 Rock Riprap Lined Chutes

#### Approach:

Use the equations in Section 5.2 - Riprap Blanket of WisDOT FDM 13-35-5 (Energy Dissipators) to determine the average size of stone ( $d_{50}$ ) and riprap apron length. Round up the calculated  $d_{50}$  to the nearest WisDOT standard riprap size.

Use WisDOT FDM 13-35 Attachment 5.2 to determine the width of the riprap apron for discharges to a flat area. For discharges to channels, extend riprap across the channel bottom and up the sides.

#### Assumptions:

Assume riprap apron thickness (T) is  $2*d_{50}$  to protect against washout and undercutting of the riprap.

Assume tailwater depth, TW =  $0.40 * D_o$ 

Assume max TW conditions for the riprap apron width.

Assume that when there are multiple culverts, the total discharge to the culverts is distributed evenly through each barrel.

#### Calculation:

From WisDOT Section 5.2 - Riprap Blanket:

$$d_{50}/D_o = 0.020 (D_o/TW) (Q/D_o^{5/2})^{4/3}$$
  
 $L_{sp}/D_o = 1.7 (Q/D_o^{5/2}) + 8$ 

Or

$$d_{50} = 0.02 \times (D_o/TW) \times (Q/D_o^{5/2})^{4/3} \times D_o$$
  
 $L_{sp} = (1.7 (Q/D_o^{5/2}) + 8) \times D_o$ 

 $L_{sp} = (1.7 (Q/D_0)^{-1} + 0) \times D_0$ where:  $D_0 = \text{Diameter or width of culvert (ft)}$ 

Q = Flow rate (cfs) (discharge rate through culvert, from Worst Case Condition HydroCAD Model (Reference #2))

TW = Tail water depth (ft) d<sub>50</sub> = Average size of stone (ft)

 $L_{sp}$  = Length of stone protection (Apron Length) (ft)

Location	Total Flow (Q, cfs)	Number of Pipes	D <sub>o</sub> (ft)	Q (cfs)	TW (ft)	d <sub>50 calculated</sub>	d <sub>50 Design</sub>	$L_{sp}$
Culvert C2	9.68	2	1.5	4.8	0.60	0.16	0.83	16
Culvert C3	27.38	2	2.5	13.7	1.00	0.19	0.83	26
Culvert C4	35.39	2	2.5	17.7	1.00	0.27	0.83	28
Culvert C5	35.21	2	2.5	17.6	1.00	0.27	0.83	28

#### Results:

Below is a summary of the d<sub>50</sub>, thickness (T), and configuration of the riprap apron. Also refer to WisDOT FDM Attachment 5.2 (Sheet 2) for details on apron layout. Use WisDOT Light Riprap at culvert discharge.

Location	d <sub>50</sub> (in)*	T (in)	L <sub>sp</sub> (ft)	W <sub>sp</sub> (ft)
Culvert C2	10.0	20	16	See Note 1
Culvert C3	10.0	20	26	See Note 1
Culvert C4	10.0	20	28	See Note 1
Culvert C5	10.0	20	28	See Note 1

<sup>1.</sup> For discharges to channels, place riprap along channel bottom and up side of channel.

<sup>\*</sup>Per Table 25.1 on Sheet 2 for standard WisDOT riprap sizes use Light Riprap.

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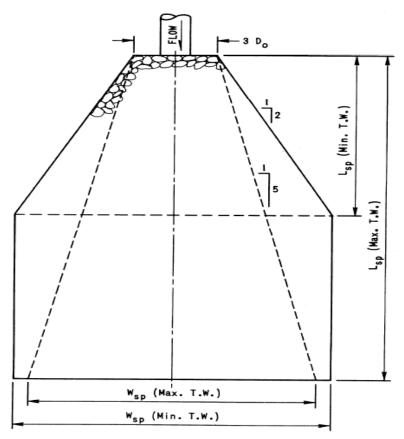
Client: WPL

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Calc. No.	
Rev. No.	
By: RJG	Date: 2/21/22
Chk'd: MJT	Date: 4/5/22

FDM 13-35 Attachment 5.2 Recommended Configuration of Riprap Blanket Subject to Maximum and Minimum Tail Waters

Job: Columbia Energy Center POO Landfill Closure

Subject: Riprap Sizing at Culvert Outlet



# RECOMMENDED CONFIGURATION OF RIPRAP BLANKET SUBJECT TO MAXIMUM AND MINIMUM TAILWATERS

Source: Miscellaneous paper H-72-5, "Practical Guidance for Estimating and Controlling Erosion at Culvert Outlets", U.S. Army Engineer Waterways Experiment Station, May, 1972.

Table 25.1 Typical Particle Sizes of Native Sands at 75 Percent Passing (D75)

Riprap Type	D50 (inches)	D50 (feet)	Riprap Thickness (in)	Geotextile Type
Select Crushed Material	2.2	0.18	5	Type R
Light Riprap	10	0.83	12	Type R
Medium Riprap	12.5	1.04	18	Type HR
Heavy Riprap	16	1.33	24	Type HR
Extra-Heavy Riprap	20	1.67	30	Type HR

Source: Table 25.1 from WisDOT FDM.