

Location Restriction Compliance Demonstrations Phase 2, Modules 10 and 11

Columbia Dry Ash Disposal Facility

Prepared for:

Wisconsin Power and Light Company
Columbia Energy Center
W8375 Murray Road
Pardeeville, Wisconsin 53954

SCS ENGINEERS

25222157.00 | August 22, 2022

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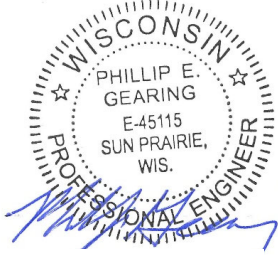
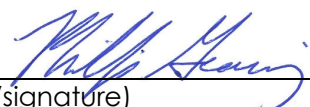
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P.E. CERTIFICATION

 8/22/2022	<p>I, Phillip E. Gearing, hereby certify that the location restriction demonstrations prepared for Phase 2, Modules 10 and 11 at the Columbia Energy Center dry ash disposal facility meet the requirements in 40 CFR 257.60(a), 61(a), 62(a), 63(a), and 64(a). This certification is based on my review of the 2022 Location Restriction Compliance Demonstrations for Phase 2, Modules 10 and 11 prepared by SCS Engineers. I am a duly licensed Professional Engineer under the laws of the State of Wisconsin.</p>	
	 (signature)	8/22/2022 (date)
	Phillip Gearing (printed or typed name)	
	License number <u>E-45115-6</u>	
	My license renewal date is July 31, 2024.	
Pages or sheets covered by this seal: Entire document		

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1.0 INTRODUCTION AND PROJECT SUMMARY

On behalf of Wisconsin Power and Light Company (WPL), SCS Engineers (SCS) has prepared the enclosed Location Restriction Compliance Demonstrations for the Columbia (COL) Dry Ash Disposal Facility Phase 2, Modules 10 and 11 as required by 40 CFR 257.60-64.

The COL facility includes an active coal combustion residual (CCR) landfill which currently consists of Modules 1 through 6, which are contiguous and are managed as a single landfill by the facility and by the Wisconsin Department of Natural Resources (WDNR). Under the federal CCR Rule, Modules 1 through 3 are one existing CCR landfill. Modules 4 through 6 are a new CCR landfill that initiated construction after October 19, 2015, and are therefore managed as a separate CCR unit under the CCR Rule, even though it is contiguous to Modules 1 through 3.

Future proposed CCR modules (Phase 2, Modules 7 through 13) are permitted with the WDNR, but have not been currently developed. When developed, the units will be a lateral expansion of the new CCR landfill, as defined in 40 CFR 257.53. This demonstration addresses Phase 2, Modules 10 and 11. Future Phase 2 CCR modules are not addressed by this demonstration and are not discussed further herein.

Figure 1 shows the site location. **Figure 2** shows the Phase 2, Modules 10 and 11 locations.

2.0 LOCATION RESTRICTIONS

§257.60. *“Placement above the uppermost aquifer.”*

“(a) New CCR landfills, existing and new CCR surface impoundments, and all lateral expansions of CCR units must be constructed with a base that is located no less than 1.52 meters (five feet) above the upper limit of the uppermost aquifer, or must demonstrate that there will not be an intermittent, recurring, or sustained hydraulic connection between any portion of the base of the CCR unit and the uppermost aquifer due to normal fluctuations in groundwater elevations (including the seasonal high water table). The owner or operator must demonstrate by the dates specified in paragraph (c) of this section that the CCR unit meets the minimum requirements for placement above the uppermost aquifer.”

The high water table within the uppermost aquifer below Phase 2, Modules 10 and 11 is at an approximate elevation of 789 feet above mean sea level (amsl), based on a review of water table observation well water levels near Phase 2, Modules 10 and 11, for the period from October 2012 to July 2022; refer to **Appendix A**. The highest water level elevation measured at a well in the area of Phase 2, Modules 10 and 11 was 788.25 feet amsl recorded at MW-1AR, which is located near the Liner Phase/Module Limit between Modules 10 and 11. As shown on **Figure 3**, the lowest subbase grade, which represents the top of subbase soils and bottom of the clay liner, within Phase 2, Modules 10 and 11 is approximately 794 feet amsl. Based on this information, Phase 2, Modules 10 and 11 is located at least 5 feet above the uppermost aquifer.

§257.61 *“Wetlands.”*

“(a) New CCR landfills, existing and new CCR surface impoundments, and all lateral expansions of CCR units must not be located in wetlands, as defined in §232.2 of this chapter, unless the owner or operator demonstrates by the dates specified in paragraph (c) of this section that the CCR unit meets the requirements of paragraphs (a)(1) through (5) of this section.”

Phase 2, Modules 10 and 11 are not located in wetlands. The location of Phase 2, Modules 10 and 11 is shown on **Figure 2**. No federally or state-mapped wetlands are present within the proposed Phase 2, Module 10 and 11 area, and the area is not adjacent to Waters of the United States, which are referenced in 40 CFR 232.2 and defined in 40 CFR 120.2, based on a wetland delineation of undeveloped areas within the ash disposal facility conducted in 2017 (**Appendix B**). In addition, no mapped wetland indicator soils are present in the Phase 2, Module 10 and 11 area. The wetland delineation conducted in 2017 identified one area (“Wetland 1”) within the Phase 2, Module 10 and 11 area that met Wisconsin wetland criteria. However, “Wetland 1” is not located adjacent to jurisdictional waters defined in 40 CFR 120.2 and was exempted from state wetland regulations as artificial by the WDNR.

§257.62 “Fault areas.”

“(a) New CCR landfills, existing and new CCR surface impoundments, and all lateral expansions of CCR units must not be located within 60 meters (200 feet) of the outermost damage zone of a fault that has had displacement in Holocene time unless the owner or operator demonstrates by the dates specified in paragraph (c) of this section that an alternative setback distance of less than 60 meters (200 feet) will prevent damage to the structural integrity of the CCR unit.”

Based on a review of the U.S. Geological Survey (USGS) Quaternary faults database and map as shown in **Appendix C**, Phase 2, Modules 10 and 11 are not located within 200 feet of the outermost damage zone of a fault that has had displacement in Holocene time. In 40 CFR 257.53, Holocene is defined as the most recent epoch of the Quaternary period extending from 11,700 years before present, to present. The USGS map shows that no faults are located in Wisconsin.

§257.63 “Seismic impact zones.”

“(a) New CCR landfills, existing and new CCR surface impoundments, and all lateral expansions of CCR units must not be located in seismic impact zones unless the owner or operator demonstrates by the dates specified in paragraph (c) of this section that all structural components including liners, leachate collection and removal systems, and surface water control systems, are designed to resist the maximum horizontal acceleration in lithified earth material for the site.”

Phase 2, Modules 10 and 11 are not located in seismic impact zones. In 40 CFR 257.53, a seismic impact zone is defined as an area having a 2 percent or greater probability that the maximum expected horizontal acceleration, expressed as a percentage of the earth’s gravitational pull (g), will exceed 0.10 g in 50 years. Based on a review of the USGS 2014 Long-Term Model National Seismic Hazard Map (see **Appendix D**), the maximum expected horizontal acceleration for the majority of Wisconsin, including all of Columbia County, is less than 0.04 g, below the threshold for a seismic impact zone.

257.64 “Unstable areas.”

“(a) An existing or new CCR landfill, existing or new CCR surface impoundment, or any lateral expansion of a CCR unit must not be located in an unstable area unless the owner or operator demonstrates by the dates specified in paragraph (d) of this section that recognized and generally accepted good engineering practices have been incorporated into the design of the CCR unit to ensure that the integrity of the structural components of the CCR unit will not be disrupted.”

“(b) The owner or operator must consider all of the following factors, at a minimum, when determining whether an area is unstable:

“(1) On-site or local soil conditions that may result in significant differential settling;

As discussed in **Appendices E and F**, and as shown by the geologic cross sections from the June 1980 Supplementary Feasibility Study prepared by Warzyn Engineering Inc. (see **Appendix G**), Phase 2, Modules 10 and 11 are not located in on-site or local soil conditions that may result in significant differential settling. The site soils consist primarily of sands of alluvial and glacial origin overlaying sandstone bedrock. Based on the Standard Penetration Test (SPT) blow counts on the geologic cross sections, the soils are typically medium dense to very dense and therefore not susceptible to appreciable differential settlement under the CCR landfill loads.

“(2) On-site or local geologic or geomorphologic features; and

As discussed in **Appendices E, H, and I**, and shown by the geologic cross sections in **Appendix G**, Phase 2, Modules 10 and 11 are not located in on-site or local geologic or geomorphologic features that are unstable. The cross sections show medium dense to very dense sands of alluvial and glacial origin overlaying sandstone bedrock. These geologic features provide a stable foundation for the CCR landfill.

This assessment is confirmed by the slope stability analyses in **Appendix H** that indicate the slope stability safety factors are acceptable. The slope stability analyses in **Appendix H** were performed for Modules 10 and 11 with maximum waste slope heights of 101 feet, and slopes of 3 horizontal to 1 vertical (3H:1V) and 4H:1V. The results in **Appendix H** confirm that the slope stability safety factors for Modules 10 and 11 are acceptable.

“(3) On-site or local human-made features or events (both surface and subsurface).”

As shown by the geologic cross sections in **Appendix G**, Phase 2, Modules 10 and 11 are not located in on-site or local human-made features or events (both surface and subsurface) that are unstable. The predominant native sands are overlain by sand fill in some areas of the site. The sand fill was placed in the landfill area during excavation activities for construction of the generating station. Based on the SPT blow counts for the sand fill on the cross sections, the fill is typically medium dense to very dense and therefore provides a stable base material where present below the landfill.

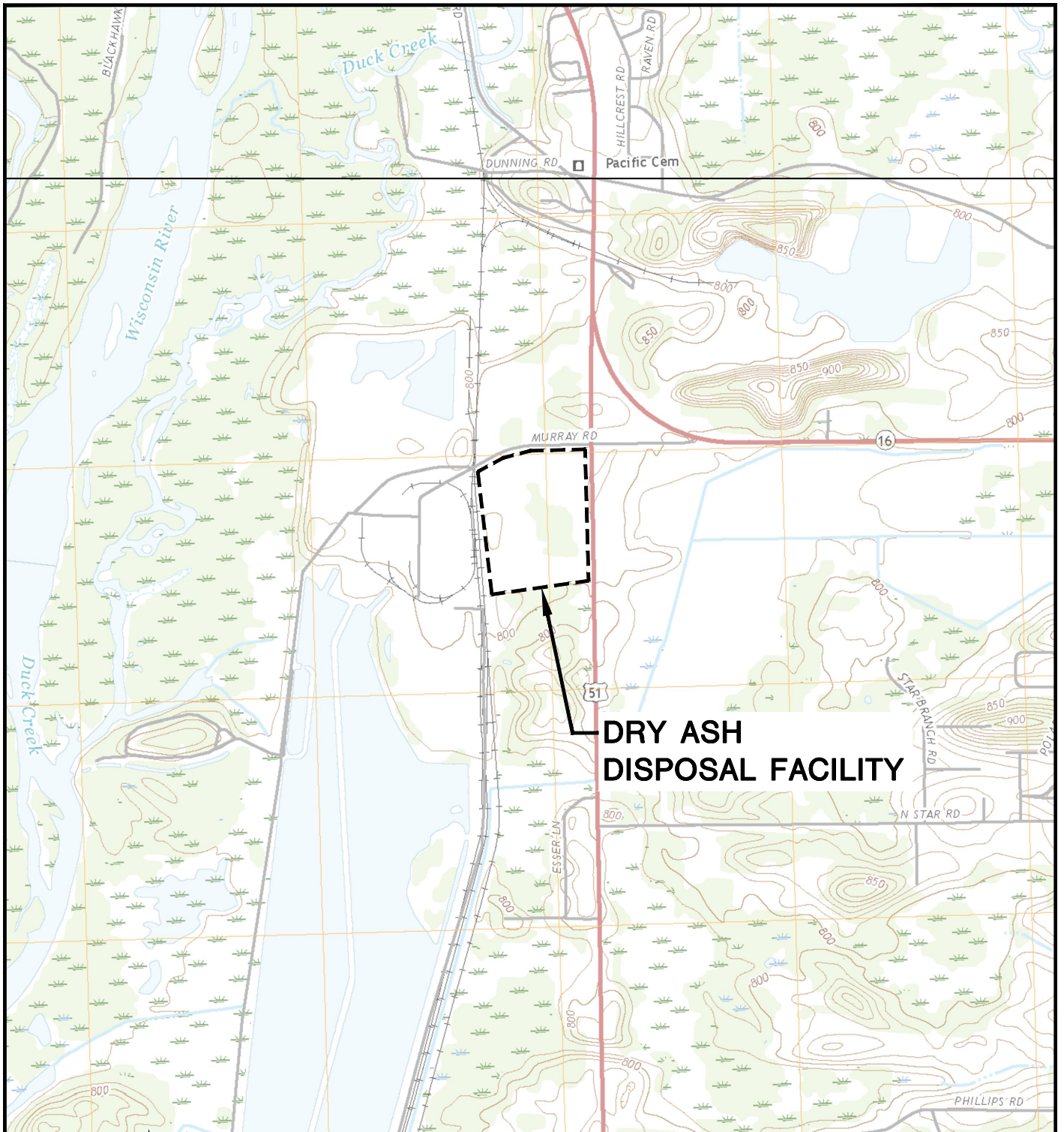
As discussed in **Appendix I**, groundwater or surface water movement is unlikely to cause instability. The facility is designed with adequate run-on and run-off control systems, and is constructed above the water table.

3.0 REFERENCES

- A. Heartland Ecological Group, 2022, Exemption Request for Artificial Wetlands – WPL Columbia Power Plant, Town of Pacifica, Columbia County, Wisconsin
- B. Wisconsin Department of Natural Resources, March 15, 2022, Artificial Wetland Exemption Determination for an area described as Wetlands 1, 2, and active coal combustion residual surface impoundments located at T12N R9E S27 in the Town of Pacific, Columbia County.
- C. Mach IV, 2017, Assured Wetland Delineation Report, Alliant Columbia Energy, Town of Pacific, Columbia County, Wisconsin.
- D. USGS fault map website: https://www.usgs.gov/natural-hazards/earthquake-hazards/faults?qt-science_support_page_related_con=4#qt-science_support_page_related_con
- E. USGS seismic impact zones map reference: Petersen, M.D., Moschetti, M.P., Powers, P.M., Mueller, C.S., Haller, K.M., Frankel, A.D., Zeng, Yuehua, Rezaeian, Sanaz, Harmsen, S.C., Boyd, O.S., Field, E.H., Chen, Rui, Luco, Nicolas, Wheeler, R.L., Williams, R.A., Olsen, A.H., and Rukstales, K.S., 2015, Seismic-hazard maps for the conterminous United States, 2014: U.S. Geological Survey Scientific Investigations Map 3325, 6 sheets, scale 1: 7,000,000, <http://dx.doi.org/10.3133/sim3325>.
- F. Warzyn Engineering Inc., 1980, Supplementary Feasibility Study, Proposed Fly Ash and/or Scrubber Sludge Disposal Facility, Columbia Site – Wisconsin Power & Light Company, Town of Pacific, Columbia County, Wisconsin.

Figures

- 1 Site Location Map
- 2 Module 10 and 11 Locations
- 3 Base Grades and Leachate Collection System



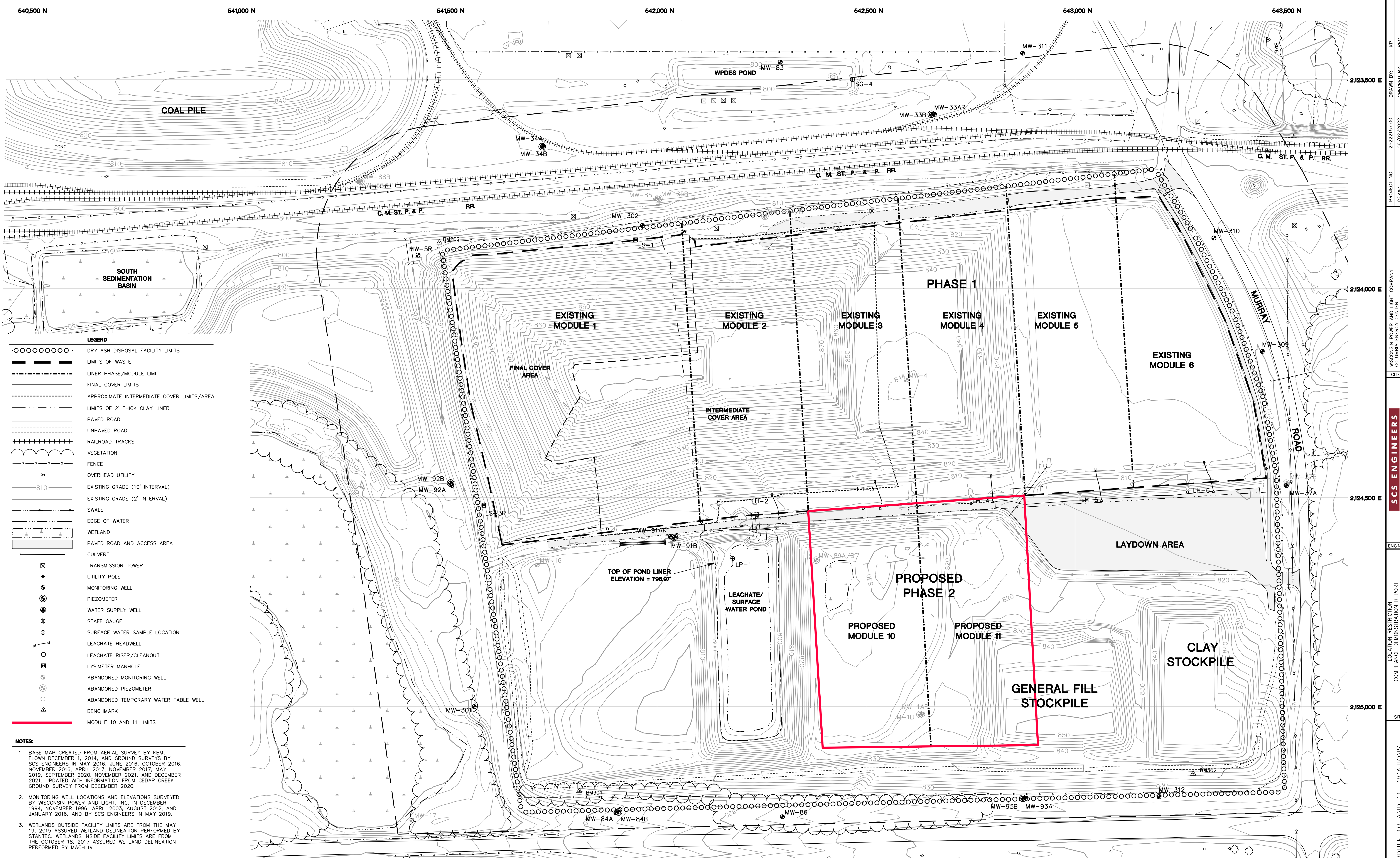
**DRY ASH
DISPOSAL FACILITY**



POYNETTE QUADRANGLE
WISCONSIN-COLUMBIA CO.
7.5 MINUTE SERIES (TOPOGRAPHIC)
2018
SCALE: 1" = 2,000'



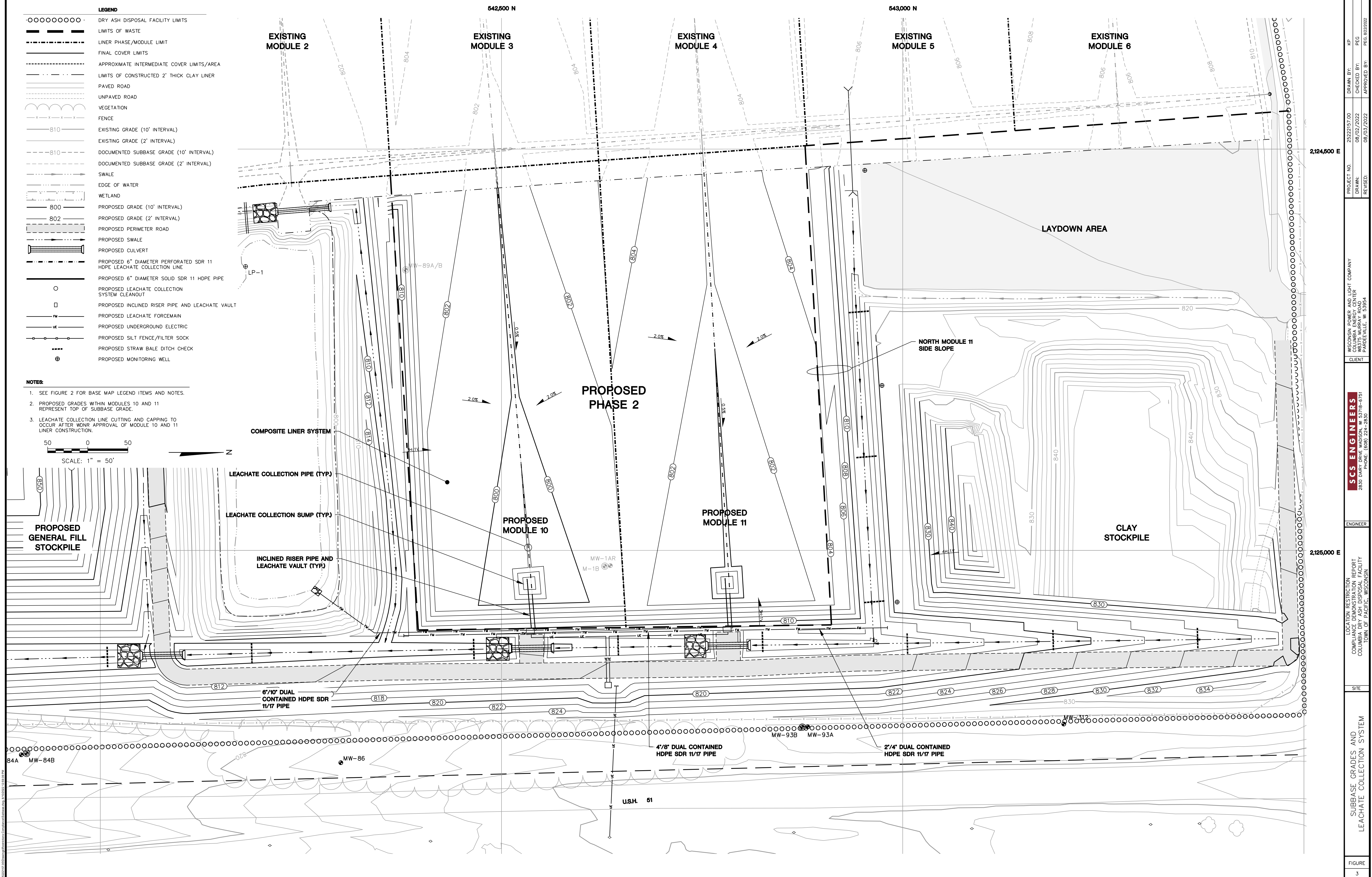
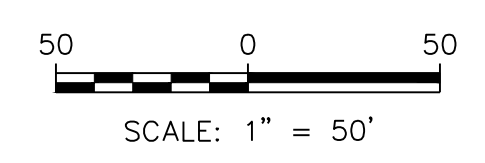
CLIENT	WISCONSIN POWER AND LIGHT COMPANY COLUMBIA ENERGY CENTER W8375 MURRAY ROAD PARDEEVILLE, WI 53954		SITE	LOCATION RESTRICTION COMPLIANCE DEMONSTRATION REPORT COLUMBIA DRY ASH DISPOSAL FACILITY TOWN OF PACIFIC, WISCONSIN		ENGINEER	SITE LOCATION MAP	
	PROJECT NO.	25222157.00		DRAWN BY:	KP		SCS ENGINEERS 2830 DAIRY DRIVE MADISON, WI 53718-6751 PHONE: (608) 224-2830	FIGURE
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PROJECT NO.	25222157.00	DRAWN BY:	KP
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REVISED:	08/03/2022	APPROVED BY:	PEG
CLIENT:	WISCONSIN POWER AND LIGHT COMPANY 8375 MURRAY ROAD PARKEVILLE, WI 53954		
ENGINEER:	SCS ENGINEERS 2830 DARY DRIVE MADISON, WI 53718-6791 PHONE: (608) 224-2830		
SITE:	LOCATION RESTRICTION COMPLIANCE DEMONSTRATION REPORT COLUMBIA DRY ASH DISPOSAL FACILITY TOWN OF PACIFIC, WISCONSIN		
FIGURE:	MODULE 10 AND 11 LOCATIONS		
	2		

- LEGEND**
- DRY ASH DISPOSAL FACILITY LIMITS
 - LIMITS OF WASTE
 - - - - - LINER PHASE/MODULE LIMIT
 - FINAL COVER LIMITS
 - - - - - APPROXIMATE INTERMEDIATE COVER LIMITS/AREA
 - - - - - LIMITS OF CONSTRUCTED 2" THICK CLAY LINER
 - PAVED ROAD
 - UNPAVED ROAD
 - VEGETATION
 - FENCE
 - 810 EXISTING GRADE (10' INTERVAL)
 - 810 EXISTING GRADE (2' INTERVAL)
 - 810 DOCUMENTED SUBBASE GRADE (10' INTERVAL)
 - 810 DOCUMENTED SUBBASE GRADE (2' INTERVAL)
 - SWALE
 - EDGE OF WATER
 - WETLAND
 - 800 PROPOSED GRADE (10' INTERVAL)
 - 802 PROPOSED GRADE (2' INTERVAL)
 - PROPOSED PERMETER ROAD
 - PROPOSED SWALE
 - PROPOSED CULVERT
 - PROPOSED 6" DIAMETER PERFORATED SDR 11 HDPE LEACHATE COLLECTION LINE
 - PROPOSED 6" DIAMETER SOLID SDR 11 HDPE PIPE
 - PROPOSED LEACHATE COLLECTION SYSTEM CLEANOUT
 - PROPOSED INCLINED RISER PIPE AND LEACHATE VAULT
 - PROPOSED LEACHATE FORCEMAIN
 - PROPOSED UNDERGROUND ELECTRIC
 - PROPOSED SILT FENCE/FILTER SOCK
 - PROPOSED STRAW BALE DITCH CHECK
 - ⊕ PROPOSED MONITORING WELL

- NOTES:**
1. SEE FIGURE 2 FOR BASE MAP LEGEND ITEMS AND NOTES.
 2. PROPOSED GRADES WITHIN MODULES 10 AND 11 REPRESENT TOP OF SUBBASE GRADE.
 3. LEACHATE COLLECTION LINE CUTTING AND CAPPING TO OCCUR AFTER WDMR APPROVAL OF MODULE 10 AND 11 LINER CONSTRUCTION.



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ENGINEER:	SCS ENGINEERS 2830 DARY DRIVE MADISON, WI 53718-6791 PHONE: (608) 224-2830
SITE:	LOCATION RESTRICTION COMPLIANCE DEMONSTRATION REPORT COLUMBIA DRY ASH DISPOSAL FACILITY TOWN OF PACIFIC, WISCONSIN
FIGURE:	SUBBASE GRADES AND LEACHATE COLLECTION SYSTEM
	3

Appendix A

Water Levels

**Table 1. Groundwater Elevation - State Monitoring Program and CCR Well Network
Columbia Dry Ash and Ash Pond Disposal Facilities / SCS Engineers Project #25222067.00**

Raw Data	M-3	M-4R	MW-39A	MW-39B	MW-48A	MW-48B	MW-57	MW-59	MW-216R	MW-217	MW-220RR	SG-1	SG-2	SG-3	SG-4
	Measurement Date														
October 2, 2012	8.10	19.34	28.13	28.16	46.83	46.91	5.71	35.60	32.30	10.60	12.35	2.92	1.40	dry	dry
April 15, 2013	3.07	17.71	25.65	25.50	45.09	45.06	1.60	31.82	30.12	6.80	7.88	(1)	NM ⁽²⁾	dry	dry
October 8, 2013	7.01	19.43	NM	NM	45.17	45.26	NM	NM	30.82	9.28	10.54	(3)	3.92	(3)	dry
October 15, 2013	NM	NM	26.68	26.69	NM	NM	3.82	31.99	NM	NM	NM	NM	NM	NM	NM
April 14, 2014	2.19	17.14	26.05	25.82	45.30	45.27	0.78	32.07	30.48	6.30	7.03	788.90	NM	NM	NM
October 1-3, 2014	7.07	18.55	26.20	26.18	44.81	44.90	3.97	31.93	30.42	8.92	9.87	cannot read	dry	dry	dry
April 13-14, 2015	5.15	19.27	26.85	26.82	46.06	46.02	3.48	32.65	31.28	8.21	9.48	(1)	3.55	dry	dry
October 6-7, 2015	7.57	19.98	26.65	26.69	45.76	45.83	4.47	32.23	31.03	9.6	10.64	NM	3.67	dry	dry
April 4-6, 2016	4.02	17.01	24.35	24.23	44.07	44.08	3.08	30.51	28.53	6.53	8.54	From NS	1.85	dry	dry
October 11-13, 2016	6.35	18.22	23.87	23.98	43.13	43.23	3.17	28.97	28.05	7.80	8.81	From NS	2.73	dry	dry
April 10-13, 2017	5.29	18.15	24.18	24.30	43.04	43.15	3.52	29.39	28.26	7.26	8.81	From NS	1.40	dry	dry
October 3-5, 2017	7.30	19.06	26.27	26.32	44.56	44.65	3.92	31.25	30.32	9.07	10.29	From NS	1.8	dry	dry
April 23-25, 2018	5.34	15.67	26.76	26.63	45.72	45.75	3.25	32.46	30.98	8.29	9.45	From NS	above gauge	dry	dry
October 23-25, 2018	5.28	17.63	22.50	22.62	41.74	41.85	2.81	27.75	26.72	6.65	8.38	From NS	2.00	dry	dry
April 1-4, 2019	2.55	16.66	23.34	23.19	42.30	42.39	1.02	28.09	27.68	5.22	7.44	From BC	0.65	dry	dry
October 7-9, 2019	2.90	15.45	22.52	22.48	42.18	42.19	1.00	28.80	27.14	5.54	7.48	From BC	0.05	dry	dry
May 27-29, 2020	6.43	18.37	24.50	24.58	43.12	43.25	3.18	29.59	28.61	8.14	9.01	From BC	above gauge	dry	dry
October 7-8 & 17, 2020	6.81	18.36	24.88	24.86	43.83	43.88	3.46	30.05	29.11	8.49	9.41	From BC	1.93	dry	NM
April 12, 2021	5.93	19.76	25.96	25.85	44.73	44.76	3.50	31.40	30.24	8.40	9.41	From BC	1.80	below gauge	dry
October 11-12, 14, 2021	7.20	19.77	26.68	26.65	45.77	45.81	4.35	32.37	31.17	9.40	10.24	From BC	0.12	dry	dry
April 11-13, 2022	4.28	17.84	26.25	26.16	45.76	45.74	NM	32.49	30.81	7.62	9.07	From BC	0.60	dry	dry
June 3, 2022	NM	NM	NM	NM	NM	NM	4.16	NM	NM	NM	NM	NM	NM	NM	NM
Well Number	M-3	M-4R	MW-39A	MW-39B	MW-48A	MW-48B	MW-57	MW-59	MW-216R	MW-217	MW-220RR	SG-1	SG-2	SG-3	SG-4
Top of Casing Elevation (feet amsl)	788.23	806.10	809.62	809.50	828.86	828.84	786.29	815.48	814.21	791.55	792.90	792.06	795.25	808.60	805.36
Screen Length (ft)															
Total Depth (ft from top of casing)	16.90	25.55	34.80	76.07	51.88	75.80	14.40	38.50	37.85	37.37	18.96	--	--	--	--
Top of Well Screen Elevation (ft)	771.33	780.55	774.82	733.43	776.98	753.04	771.89	776.98	776.36	754.18	773.94	--	--	--	--
Measurement Date															
October 2, 2012	780.13	786.76	781.49	781.34	782.03	781.93	780.58	779.88	781.91	780.95	780.55	789.14	793.85	dry	dry
April 15, 2013	785.16	788.39	783.97	784.00	783.77	783.78	784.69	783.66	784.09	784.75	785.02	789.5 ⁽¹⁾	NM	dry	dry
October 8, 2013	781.22	786.67	NM	NM	783.69	783.58	NM	NM	783.39	782.27	782.36	789.5 ⁽¹⁾	791.33	dry	dry
October 15, 2013	NM	NM	782.94	782.81	NM	NM	782.47	783.49	NM	NM	NM	NM	NM	NM	NM
April 14, 2014	786.04	788.96	783.57	783.68	783.56	783.57	785.51	783.41	783.73	785.25	785.87	788.90	dry	dry	dry
October 1-3, 2014	781.16	787.55	783.42	783.32	784.05	783.94	782.32	783.55	783.79	782.63	783.03	NM	dry	dry	dry
April 13-14, 2015	783.08	786.83	782.77	782.68	782.80	782.82	782.81	782.83	782.93	783.34	783.42	789.3	791.70	dry	dry
October 6-7, 2015	780.66	786.12	782.97	782.81	783.10	783.01	781.82	783.25	783.18	781.95	782.26	788.48	791.58	dry	dry
April 4-6, 2016	784.21	789.09	785.27	785.27	784.79	784.76	783.21	784.97	785.68	785.02	784.36	NM	793.40	dry	dry
October 11-13, 2016	781.88	787.88	785.75	785.52	785.73	785.61	783.12	786.51	786.16	783.75	784.09	788.32	792.52	dry	dry
April 10-13, 2017	782.94	787.95	785.44	785.20	785.82	785.69	782.77	786.09	785.95	784.29	784.09	788.31	793.85	dry	dry
October 3-5, 2017	780.93	787.04	783.35	783.18	784.30	784.19	782.37	784.23	783.89	782.48	782.61	788.3	793.45	dry	dry
April 23-25, 2018	782.89	790.43	782.86	782.87	783.14	783.09	783.04	783.02	783.23	783.26	783.45	788.38	>795.25	dry	dry
October 23-25, 2018	782.95	788.47	787.12	786.88	787.12	786.99	783.48	787.73	787.49	784.90	784.52	787.76	793.25	dry	dry
April 1-4, 2019	785.68	789.44	786.28	786.31	786.56	786.45	785.27	787.39	786.53	786.33	785.46	788.40	794.60	dry	dry
October 7-9, 2019	785.33	790.65	787.10	787.02	786.68	786.65	785.29	786.68	787.07	786.01	785.42	748.48	795.20	dry	dry
May 27-29, 2020	781.80	787.73	785.12	784.92	785.74	785.59	783.11	785.89	785.60	783.41	783.89	748.48	>795.25	dry	dry
October 7-8 & 17, 2020	781.42	787.74	784.74	784.64	785.03	784.96	782.83	785.43	785.10	783.06	783.49	788.34	793.32	dry	NM
April 12, 2021	782.30	786.34	783.66	783.65	784.13	784.08	782.79	784.08	783.97	783.15	783.49	788.03	793.45	below gauge	dry
October 11-12, 14, 2021	781.03	786.33	782.94	782.85	783.09	783.03	781.94	783.11	783.04	782.15	782.66	788.59	795.13	dry	dry
April 11-13, 2022	783.95	788.26	783.37	783.34	783.10	783.10	NM	782.99	783.40	783.93	783.83	788.4	794.65	dry	dry
June 3, 2022	NM	NM	NM	NM	NM	NM	782.13	NM	NM	NM	NM	NM	NM	NM	NM
Bottom of Well Elevation (ft)	771.33	780.55	774.82	733.43	776.98	753.04	771.89	776.98	776.36	754.18	773.94	--	--	--	--

Ash Pond Facility
(Facility ID #02325)

**Table 1. Groundwater Elevation - State Monitoring Program and CCR Well Network
Columbia Dry Ash and Ash Pond Disposal Facilities / SCS Engineers Project #25222067.00**

	Raw Data	MW-301	MW-302	MW-303	MW-304	MW-305	M-4R	MW-33AR	MW-34A	MW-84A	MW-93A	MW-93B	MW-306	MW-307	MW-308	MW-309	MW-310	MW-311
	Measurement Date																	
	December 21-22, 2015	21.33	28.22	27.41	19.29	17.36	18.52	24.52	22.45	28.97	NI	NI	NI	NI	NI	NI	NI	NI
	April 4-5, 2016	20.11	27.19	26.04	17.34	16.71	17.01	23.00	20.32	27.91	NI	NI	NI	NI	NI	NI	NI	NI
	July 7-8, 2016	20.58	26.72	26.92	18.06	17.06	18.67	23.10	20.90	28.39	NI	NI	NI	NI	NI	NI	NI	NI
	July 28, 2016	NM	NM	27.17	NM	NM	NM	NM	21.09	28.67	NI	NI	NI	NI	NI	NI	NI	NI
	October 11-13, 2016	19.25	25.24	25.34	17.24	16.54	18.22	20.93	19.50	27.06	NI	NI	NI	NI	NI	NI	NI	NI
	December 29, 2016	19.52	25.95	NM	NM	NM	NM	22.63	20.23	27.65	NI	NI	NI	NI	NI	NI	NI	NI
	January 25-26, 2017	19.62	26.11	26.24	16.08	16.96	16.46	22.41	19.97	27.58	NI	NI	22.13	21.53	21.17	NI	NI	NI
	April 10 & 11, 2017	19.00	25.45	25.52	17.20	16.75	18.15	21.9	19.65	27.12	NI	NI	21.41	21.25	20.39	NI	NI	NI
	June 6, 2017	18.64	24.63	25.03	16.84	16.53	18.27	21.02	19.29	26.65	NI	NI	20.78	20.82	20.44	NI	NI	NI
	August 7-9, 2017	19.55	25.45	26.10	15.90	17.02	17.56	22.18	20.14	27.60	NI	NI	21.94	21.70	21.53	NI	NI	NI
	October 23-24, 2017	21.00	27.06	27.60	16.45	18.18	18.10	24.16	21.45	28.96	NI	NI	23.66	22.10	22.73	NI	NI	NI
	February 21, 2018	NM	NM	NM	NM	NM	NM	NM	NM	NM	NI	NI	NM	NM	NM	30.08	30.57	26.72
	March 23, 2018	NM	NM	NM	NM	NM	NM	NM	NM	NM	NI	NI	NM	NM	NM	30.17	30.52	26.74
	April 23-25, 2018	21.60	28.63	28.25	15.73	18.65	15.67	25.20	24.18	28.40	NI	NI	24.39	23.24	24.25	30.20	30.65	27.91
	May 24, 2018	NM	NM	NM	NM	NM	NM	NM	NM	NM	NI	NI	21.84	21.80	NM	27.82	27.65	23.63
	June 23, 2018	NM	NM	NM	NM	NM	NM	NM	NM	NM	NI	NI	NM	NM	NM	27.24	26.98	23.27
	July 23, 2018	NM	NM	NM	NM	NM	NM	NM	NM	NM	NI	NI	NM	NM	NM	27.00	27.27	23.19
	August 7, 2018	19.83	NM	26.32	17.17	17.76	18.47	NM	NM	27.73	NI	NI	NM	NM	NM	NM	NM	NM
	August 22, 2018	NM	NM	NM	NM	NM	NM	NM	NM	NM	NI	NI	NM	NM	NM	27.73	28.22	24.28
	September 21, 2018	NM	24.63	25.02	NM	NM	NM	20.39	18.94	NM	NI	NI	NM	NM	NM	26.19	26.38	22.08
	October 22-24, 2018	17.91	23.84	24.01	16.37	16.28	17.63	19.52	18.07	25.96	NI	NI	19.97	20.32	19.09	25.28	25.44	21.10
	April 1-4, 2019	19.85	25.44	25.00	15.70	16.25	16.66	21.66	19.13	26.93	NI	NI	20.91	20.18	19.37	26.97	27.24	23.36
	June 12, 2019	NM	NM	NM	NM	NM	NM	NM	NM	NM	NI	NI	NM	NM	NM	NM	26.37	NM
	June 19, 2019	NM	NM	24.71	NM	NM	NM	NM	NM	NM	NI	NI	NM	NM	NM	NM	NM	NM
	October 7-9, 2019	18.42	24.69	24.50	15.01	15.96	15.45	NM	NM	NM	NI	NI	20.16	19.90	19.72	26.01	25.68	22.10
	December 13, 2019	NM	NM	NM	NM	NM	NM	NM	NM	NM	NI	NI	20.60	21.21	20.47	NM	NM	NM
	December 23, 2019	NM	NM	NM	NM	NM	NM	NM	NM	NM	NI	NI	NM	NM	NM	NM	38.40	NM
	January 17, 2020	NM	NM	25.94	NM	NM	NM	NM	NM	NM	NI	NI	NM	NM	NM	NM	NM	NM
	February 3, 2020	19.65	NM	--	NM	NM	NM	NM	NM	27.78	NI	NI	21.86	21.32	20.42	NM	NM	NM
	May 27-29, 2020	19.12	25.71	25.96	16.12	18.54	18.37	22.28	19.97	27.26	NI	NI	21.86	21.54	20.62	27.29	27.81	23.89
	June 30, 2020	NM	NM	NM	NM	NM	NM	NM	NM	NM	NI	NI	NM	NM	NM	27.09	NM	NM
	August 6, 2020	NM	NM	NM	NM	NM	NM	NM	NM	NM	NI	NI	NM	NM	NM	27.34	NM	NM
	October 7-8, 2020	20.36	26.26	26.36	16.90	18.36	18.36	22.38	20.25	28.18	NI	NI	22.24	22.18	21.22	27.80	28.06	23.91
	December 11, 2020	NM	NM	NM	NM	18.13	NM	NM	NM	NM	NI	NI	NM	NM	NM	28.01	28.36	NM
	February 25, 2021	NM	NM	27.25	NM	17.96	NM	NM	21.20	NM	NI	NI	NM	NM	NM	NM	NM	NM
	April 12, 2021	20.39	27.23	27.45	17.43	18.21	19.76	24.02	21.18	28.44	NI	NI	23.31	22.68	21.35	28.98	29.38	25.59
	June 11, 2021	NM	NM	NM	NM	NM	NM	24.10	21.29	NM	NI	NI	NM	NM	NM	29.07	29.57	NM
	July 20, 2021	NM	NM	27.88	NM	17.93	NM	NM	NM	NM	NI	NI	NM	NM	NM	NM	NM	NM
	October 11-12, 14, 2021	21.61	27.91	28.43	17.64	18.57	19.77	24.56	21.53	29.32	NI	NI	24.70	24.45	23.14	29.62	30.14	26.26
	December 21, 2021	NM	NM	NM	NM	NM	NM	NM	NM	NM	NI	NI	NM	NM	NM	30.34	NM	NM
	February 24, 2022	NM	NM	29.18	NM	19.83	NM	NM	NM	NM	NI	NI	NM	NM	NM	NM	NM	NM
	April 11-13, 2022	21.45	28.58	28.12	17.22	18.45	17.84	25.02	21.65	29.26	43.90	43.74	24.52	23.57	22.71	30.13	30.43	26.70
	July 27, 2022	NM	NM	28.45	NM	19.29	NM	NM	NM	NM	NM	NM	NM	NM	NM	NM	NM	NM

**Table 1. Groundwater Elevation - State Monitoring Program and CCR Well Network
Columbia Dry Ash and Ash Pond Disposal Facilities / SCS Engineers Project #25222067.00**

Well Number	MW-301	MW-302	MW-303	MW-304	MW-305	M-4R	MW-33AR	MW-34A	MW-84A	MW-93A	MW-93B	MW-306	MW-307	MW-308	MW-309	MW-310	MW-311
	Top of Casing Elevation (feet amsl)	806.89	813.00	811.52	805.42	806.32	806.10	808.29	805.95	814.28	827.89	827.71	807.63	806.89	806.9	813.27	813.62
Screen Length (ft)	10	10	10	10	10	10	10	10	10	10	5	10	10	10	10	10	10
Total Depth (ft from top of casing)	29.40	33.6	35.80	25.7	25.6	39.58	31.08	35.43	40.21	50.7	82.5	27	26.5	28	37.67	38.41	36.19
Top of Well Screen Elevation (ft)	787.49	789.40	785.72	789.72	790.72	776.52	787.21	780.52	784.07	787.19	750.21	790.63	790.39	788.90	785.60	785.21	783.55
Measurement Date																	
December 21-22, 2015	NM	784.78	784.11	786.13	788.96	787.58	783.77	783.50	785.31	NI	NI	NI	NI	NI	NI	NI	NI
May 27-29, 2020	787.77	787.29	785.56	789.30	787.78	787.73	786.01	785.98	787.02	NI	NI	785.77	785.35	786.28	785.98	785.81	785.85
June 30, 2020	NM	NM	NM	NM	NM	NM	NM	NM	NM	NI	NI	NM	NM	NM	786.18	NM	NM
August 6, 2020	NM	NM	NM	NM	NM	NM	NM	NM	NM	NI	NI	NM	NM	NM	785.93	NM	NM
October 7-8, 2020	786.53	786.74	785.16	788.52	787.96	787.74	785.91	785.70	786.10	NI	NI	785.39	784.71	785.68	785.47	785.56	785.83
December 11, 2020	NM	NM	NM	NM	788.19	NM	NM	NM	NM	NI	NI	NM	NM	NM	785.26	785.26	NM
February 25, 2021	NM	NM	784.27	NM	788.36	NM	NM	784.75	NM	NI	NI	NM	NM	NM	NM	NM	NM
April 12, 2021	786.50	785.77	784.07	787.99	788.11	786.34	784.27	784.77	785.84	NI	NI	784.32	784.21	785.55	784.29	784.24	784.15
June 11, 2021	NM	NM	NM	NM	NM	NM	784.19	784.66	NM	NI	NI	NM	NM	NM	784.20	784.05	NM
July 20, 2021	NM	NM	783.64	NM	788.39	NM	NM	NM	NM	NI	NI	NM	NM	NM	NM	NM	NM
October 11-12, 14, 2021	785.28	785.09	783.09	787.78	787.75	786.33	783.73	784.42	784.96	NI	NI	782.93	782.44	783.76	783.65	783.48	783.48
December 21, 2021	NM	NM	NM	NM	NM	NM	NM	NM	NM	NI	NI	NM	NM	NM	782.93	NM	NM
February 24, 2022	NM	NM	782.34	NM	786.49	NM	NM	NM	NM	NI	NI	NM	NM	NM	NM	NM	NM
April 11-13, 2022	785.44	784.42	783.40	788.20	787.87	788.26	783.27	784.30	785.02	783.99	783.97	783.11	783.32	784.19	783.14	783.19	783.04
July 27, 2022	NM	NM	783.07	NM	787.03	NM	NM	NM	NM	NM	NM	NM	NM	NM	NM	NM	NM
Bottom of Well Elevation (ft)	777.49	779.40	775.72	779.72	780.72	766.52	777.21	770.52	774.07	777.19	745.21	780.63	780.39	778.90	775.60	775.21	773.55


Notes:

NM = not measured

Created by: MDB Date: 5/6/2013
 Last revision by: MDB Date: 8/2/2022
 Checked by: AJR Date: 8/3/2022

- (1) The elevation for SG-1 is read off of the staff gauge (rather than measured from the top of the gauge).
- (2) SG-2 could not be located during the April 2013 event.
- (3) SG-3 could not be located during the October 2013 event. SG-1 could not be safely accessed during the October 2013 event.
- (4) LH-2 measurements are given as leachate depth, measured by a transducer.
- (5) LH-2 and LH-3 measurements were collected by WPL staff on October 9, 2017.
- (6) The depth to water at MW-84A was not measured prior to purging for sampling during the October 3-5 sampling event. The level was allowed to return to static and was measured on 10/10/2017.
- (7) BC = Brian Clepper; NS = Nate Sievers - Columbia Site employees.

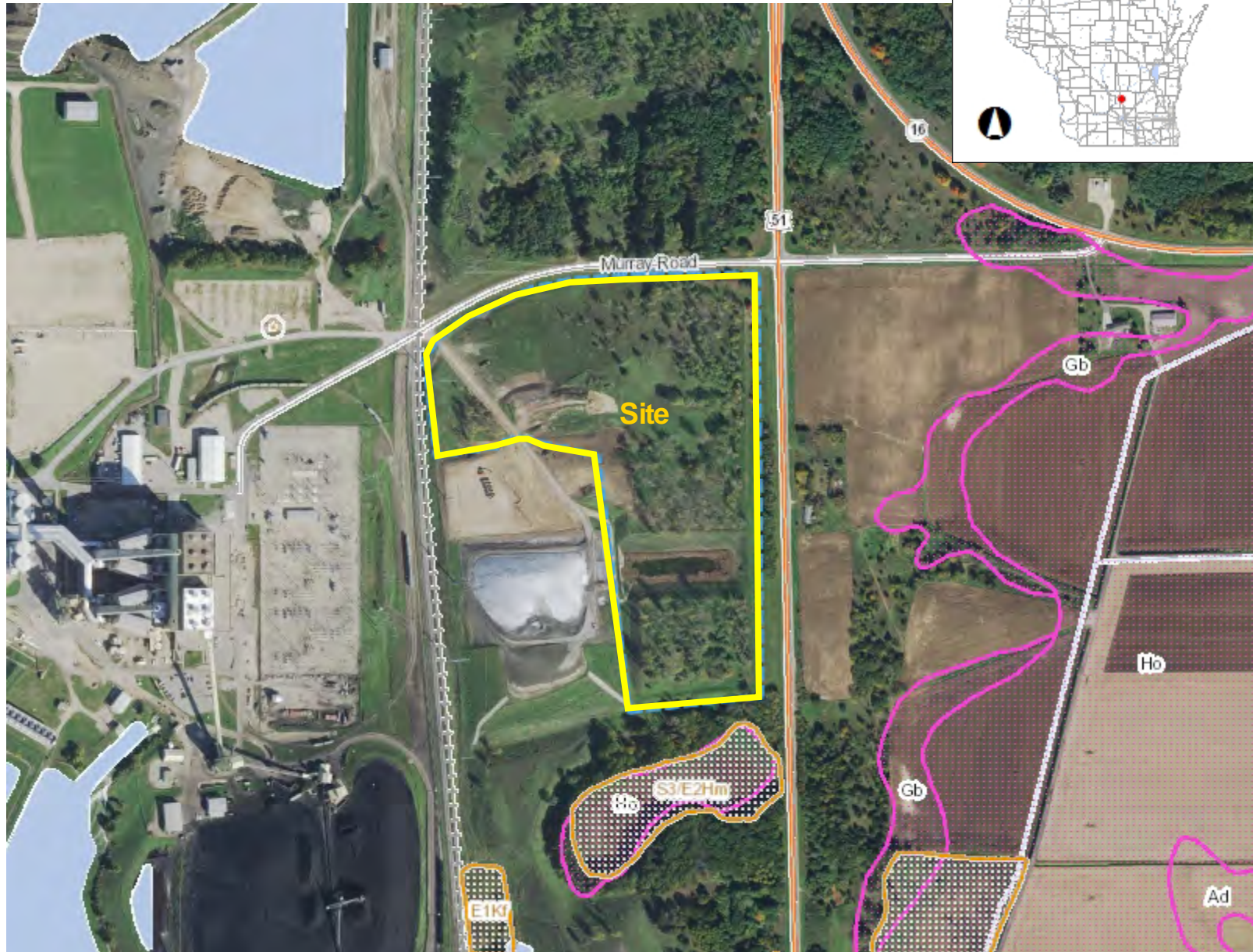
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Appendix B
Wetland Delineation Maps



Surface Water Data Viewer Map



- Legend**
- Wetland Class Points**
 - Dammed pond
 - Excavated pond
 - Filled excavated pond
 - Filled/draind wetland
 - Wetland too small to delineate
 - Filled Points**
 -
 - Wetland Class Areas**
 - Wetland
 - Upland
 - Filled Areas**
 -
 - NRCS Wetspots**
 - Wetland Indicators**
 - Municipality**
 - State Boundaries**
 - County Boundaries**
 - Major Roads**
 - Interstate Highway
 - State Highway
 - US Highway
 - County and Local Roads**
 - County HWY
 - Local Road
 - Railroads**
 - Tribal Lands**
 - Rivers and Streams**
 - Intermittent Streams**
 - Lakes and Open water**



NAD_1983_HARN_Wisconsin_TM

1: 7,920

DISCLAIMER: The information shown on these maps has been obtained from various sources, and are of varying age, reliability and resolution. These maps are not intended to be used for navigation, nor are these maps an authoritative source of information about legal land ownership or public access. No warranty, expressed or implied, is made regarding accuracy, applicability for a particular use, completeness, or legality of the information depicted on this map. For more information, see the DNR Legal Notices web page: <http://dnr.wi.gov/legal/>








Notes



U.S. Fish and Wildlife Service, National Standards and Support Team,
wetlands_team@fws.gov

September 25, 2017

Wetlands

- | | | |
|--|---|--|
|  Estuarine and Marine Deepwater |  Freshwater Emergent Wetland |  Lake |
|  Estuarine and Marine Wetland |  Freshwater Forested/Shrub Wetland |  Other |
| |  Freshwater Pond |  Riverine |

This map is for general reference only. The US Fish and Wildlife Service is not responsible for the accuracy or currentness of the base data shown on this map. All wetlands related data should be used in accordance with the layer metadata found on the Wetlands Mapper web site.



03/15/2022

Jeff Maxted
4902 N Biltmore Lane
Madison, WI 53718

EXE-SC-2022-11-00802

RE: Artificial Wetland Exemption Determination for an area described as Wetlands 1, 2, and active coal combustion residual surface impoundments (purple colored on map) located at T12N R9E S27 in the Town of PACIFIC, Columbia County.

Dear Mr. Maxted:

This letter is in response to your request for an artificial wetland exemption determination for the above mentioned wetlands.

According to 281.36 (4n), State Statutes, a landscape feature where hydrophytic vegetation may be present as a result of human modification to the landscape or hydrology and for which no definitive evidence exists showing a prior wetland or stream history before August 1, 1991, may be exempt from state wetland regulations. The following types of artificial wetlands cannot be exempted from state wetland regulation: 1) a wetland that serves as a fish spawning area or that is passage to a fish spawning area and 2) a wetland created as a result of a wetland mitigation requirement. In addition, DNR must also consider whether the artificial wetland is providing significant flood protection to adjacent or downstream properties and infrastructure, and/or significant water quality functions to adjacent or downstream water bodies.

The Department reviewed the following materials to aid in our exemption determination:

The request narrative.

Historic Maps, including the Original Land Survey Plat, Bordner Survey, the USGS topographic Quad map from 1962 and 1984, and soil mapping.

Aerial photographs, including the 1937/8 era photograph, a pre-construction aerial photograph, and a post-construction photograph.

Site photographs that show different angles and views of the wetland.

Below is a summary of our findings:

Request Narrative

According to the request narrative the basis for a determination of artificial wetlands is that wetland characteristics formed within areas lacking a history of wetland land cover. This is due to the construction of CCRSIs in the CCRSI area, and the excavation/construction of a PVC-lined leachate and stormwater runoff collection basin and grading in the landfill area.

Historic Map Review

Original Land Survey Plat. The original land survey indicates inconclusive maps and notes along the WI River.

The Bordner survey indicates cropland including oak, hickory woodland.

The 1962 and 1984 USGS Quad map indicates no wetlands.

The 1913 soil survey maps indicate no wetlands.

Aerial Photograph Review

The 1937/38 aerial photograph shows farm field.

The 1972-74 aerial photographs show mass grading.

Site Photographs

The site photographs show the ponds and conveyance features.

Conclusion:

Based upon the information provided above, the wetland identified as Wetlands 1, 2 and active coal combustion residual surface impoundments (purple colored on map) lacked a wetland history prior to August 1, 1991, and fulfills all artificial wetland exemption standards. Therefore, Wetlands 1, 2, and active coal combustion residual surface impoundments (purple colored) are exempt from state wetland regulations.

This letter describes DNR's decision regarding the jurisdictional status of Wetlands 1, 2, and active coal combustion residual surface impoundments (purple colored on map) and are only valid for state jurisdictional purposes. For decisions regarding the federal jurisdictional status of Wetlands 1 and 2, you will need to contact the U.S. Army Corps of Engineers.

If you have any questions, please call me at (608) 228-4067 or email Allen.Ramminger@wisconsin.gov

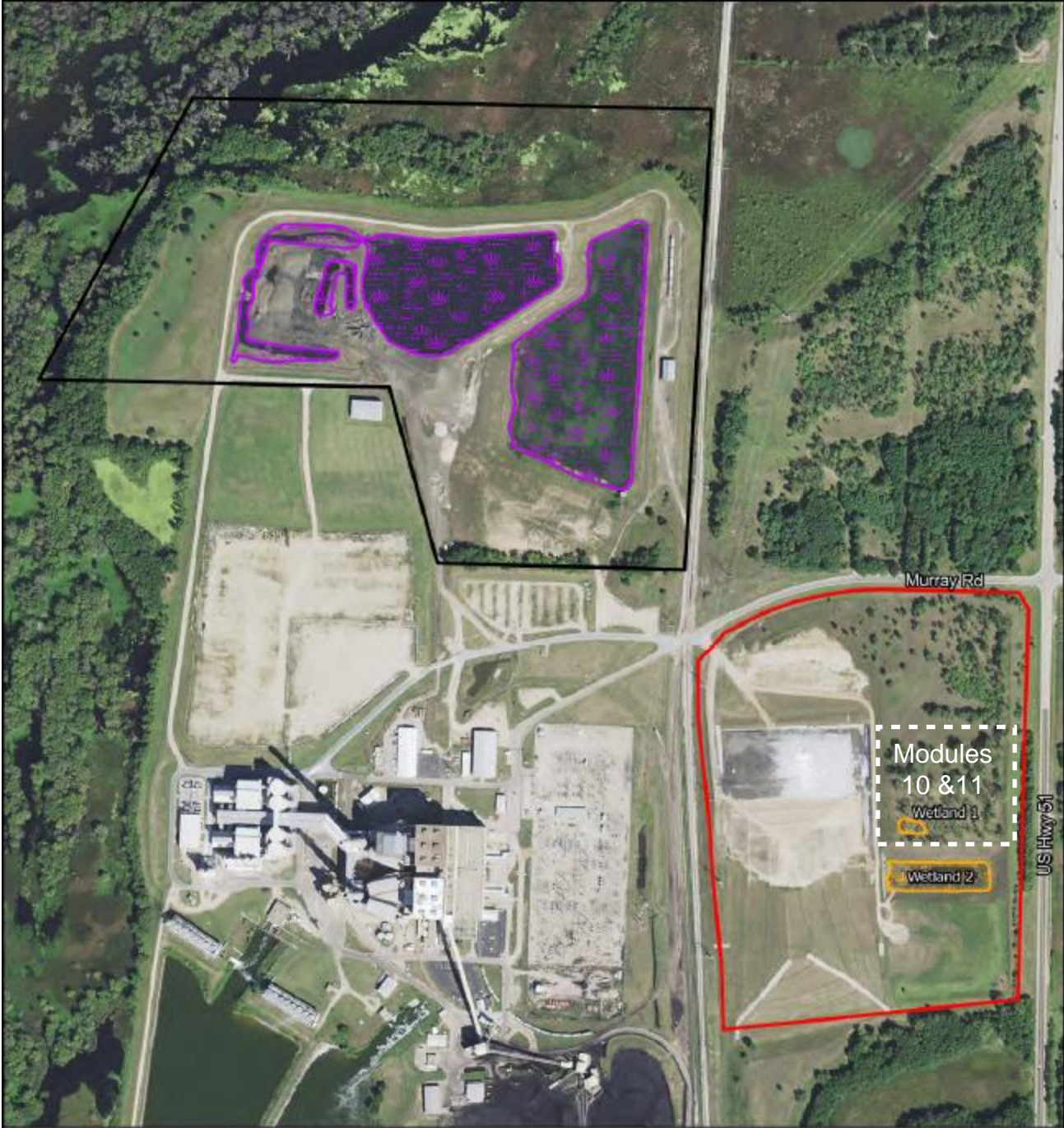
Sincerely,



Allen Ramminger
Water Management Specialist

Copy to:

USACE Project Manager
Water Management Specialist
County Zoning Administrator
Consultant



- CCRSI Review Area (101.47 ac)
- Approximate Landfill Limits (61.26 ac)
- Potentially Artificial Wetlands Documented by Heartland in 2020 (22.22 ac)
- Potentially Artificial Wetlands Delineated by Mach IV in 2017 (1.565 ac)



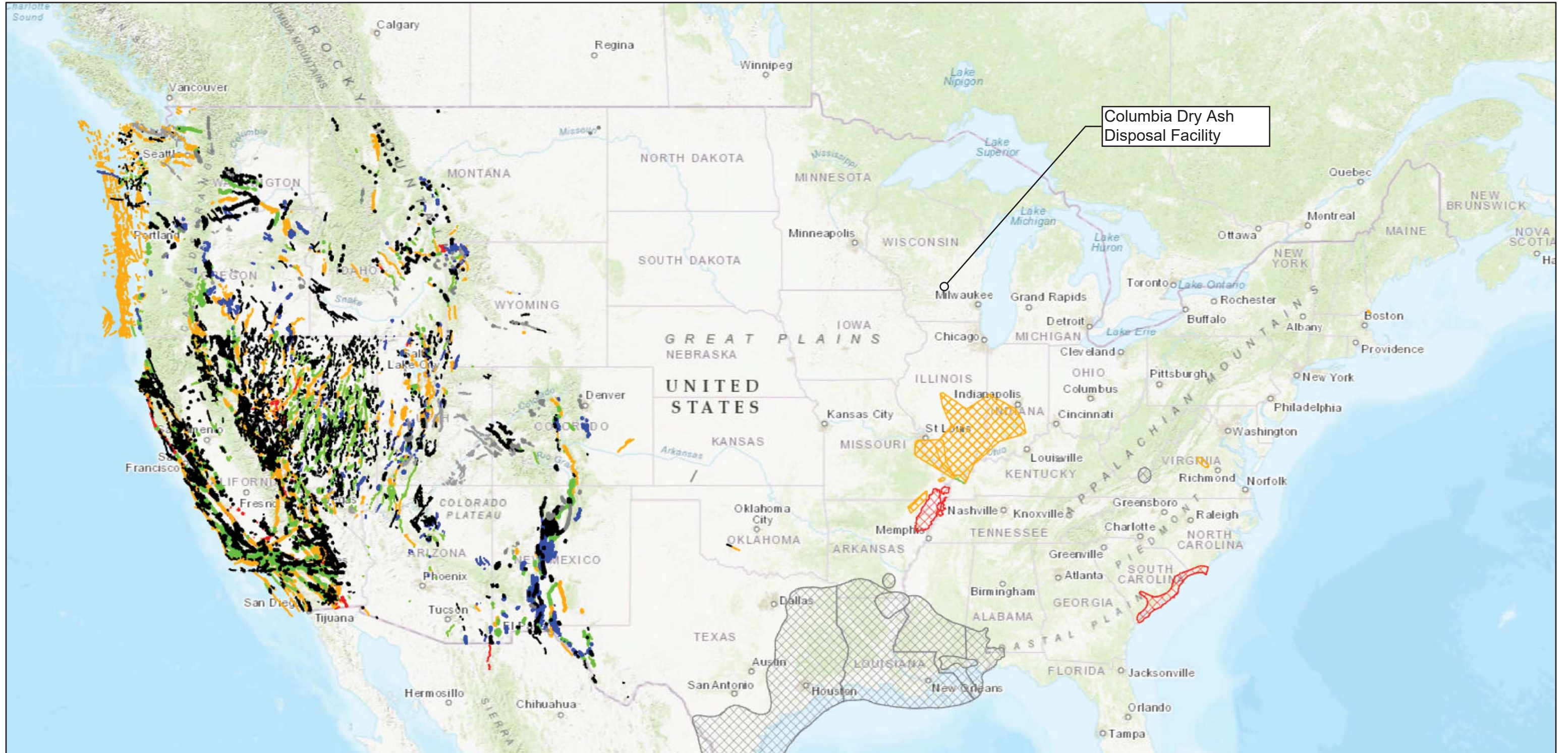
Heartland
 ECOLOGICAL GROUP INC
 WPL Columbia Energy Center Project Limits & Artificial Wetlands
 WPL Columbia Power Plant Project #20200376
 T9N, R12E, S27
 T Pacific, Columbia Co

2020 NAIP
 Columbia Co, HEG

Appendix C

Fault Location Map

U.S. Geological Survey Quaternary Faults



Columbia Dry Ash Disposal Facility

6/4/2021, 2:28:44 PM

Fault Areas

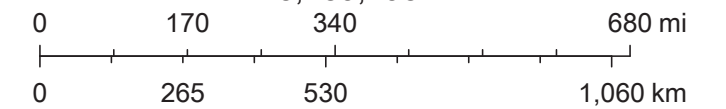
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- historic
- late Quaternary
- latest Quaternary
- middle and late Quaternary

National Database

- Historic (< 150 years), well constrained location

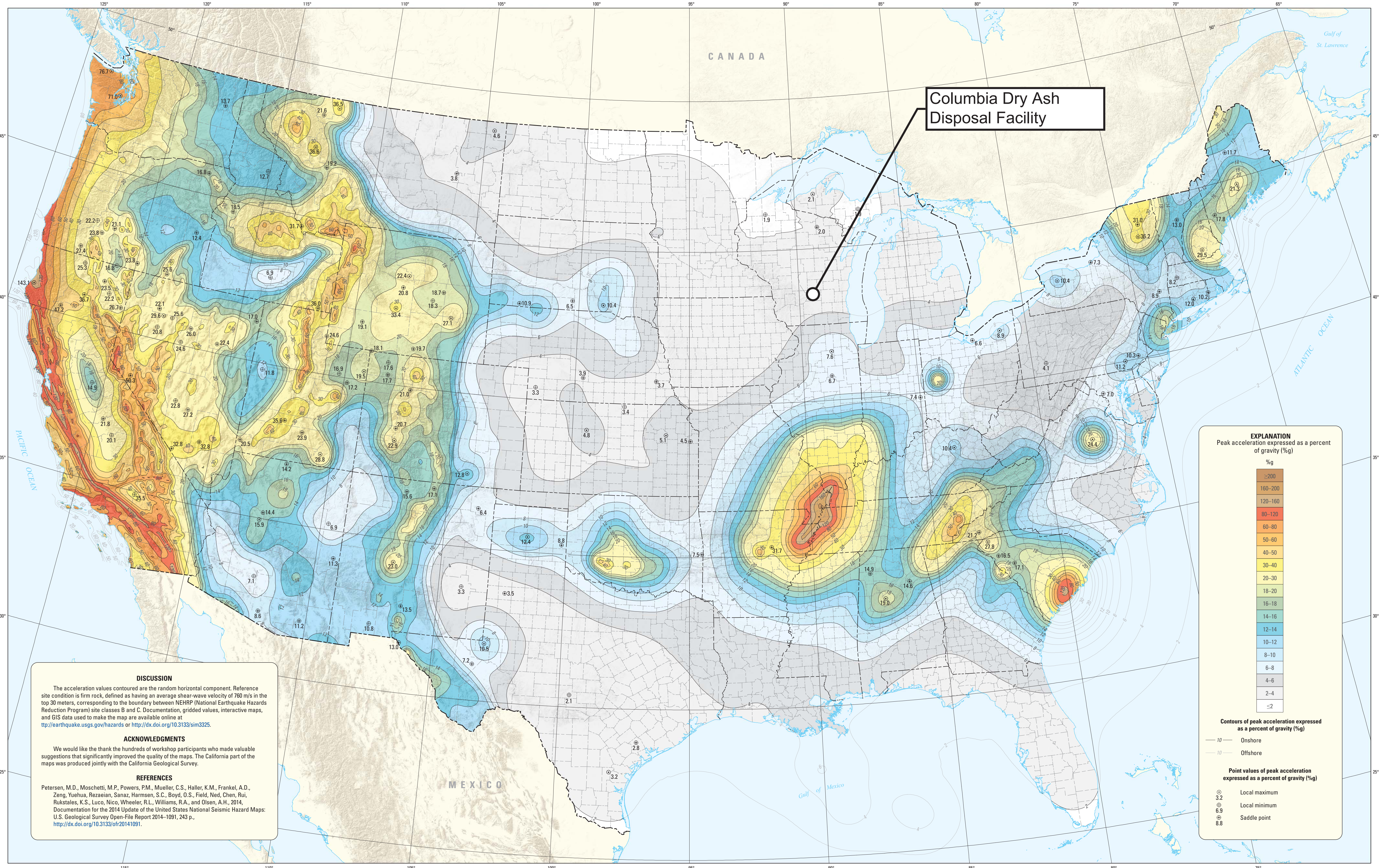
- Historic (< 150 years), moderately constrained location
- Historic (< 150 years), inferred location
- Latest Quaternary (<15,000 years), well constrained location
- Latest Quaternary (<15,000 years), moderately constrained location
- Latest Quaternary (<15,000 years), inferred location
- Late Quaternary (< 130,000 years), well constrained location
- Late Quaternary (< 130,000 years), moderately constrained location
- Late Quaternary (< 130,000 years), inferred location
- Middle and late Quaternary (< 750,000 years), well constrained location
- Middle and late Quaternary (< 750,000 years), moderately constrained location
- Middle and late Quaternary (< 750,000 years), inferred location
- Undifferentiated Quaternary (< 1.6 million years), well constrained location
- Undifferentiated Quaternary (< 1.6 million years), moderately constrained location
- Undifferentiated Quaternary (< 1.6 million years), inferred location

1:18,489,298



Esri, HERE, Garmin, FAO, NOAA, USGS, EPA

Appendix D
Seismic Hazard Map



DISCUSSION
The acceleration values contoured are the random horizontal component. Reference site condition is firm rock, defined as having an average shear-wave velocity of 760 m/s in the top 30 meters, corresponding to the boundary between NEHRP (National Earthquake Hazards Reduction Program) site classes B and C. Documentation, gridded values, interactive maps, and GIS data used to make the map are available online at <http://earthquake.usgs.gov/hazards> or <http://dx.doi.org/10.3133/sim3325>.

ACKNOWLEDGMENTS
We would like to thank the hundreds of workshop participants who made valuable suggestions that significantly improved the quality of the maps. The California part of the maps was produced jointly with the California Geological Survey.

REFERENCES
Petersen, M.D., Moschetti, M.P., Powers, P.M., Mueller, C.S., Haller, K.M., Frankel, A.D., Zeng, Yuehua, Rezaeian, Sanaz, Harmsen, S.C., Boyd, O.S., Field, E.H., Chen, Rui, Rukstales, K.S., Luco, Nico, Wheeler, R.L., Williams, R.A., and Olsen, A.H., 2014. Documentation for the 2014 Update of the United States National Seismic Hazard Maps: U.S. Geological Survey Open-File Report 2014-1091, 243 p., <http://dx.doi.org/10.3133/ofr20141091>.

EXPLANATION
Peak acceleration expressed as a percent of gravity (%g)

>200
160-200
120-160
80-120
60-80
50-60
40-50
30-40
20-30
18-20
16-18
14-16
12-14
10-12
8-10
6-8
4-6
2-4
≤ 2

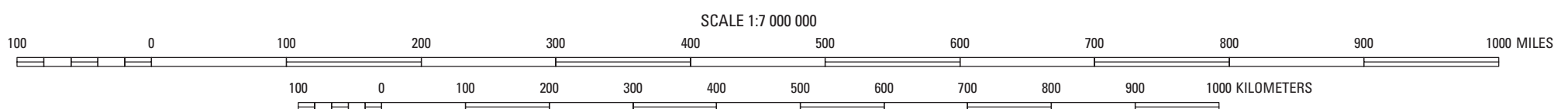
Contours of peak acceleration expressed as a percent of gravity (%g)

- Onshore
- Offshore

Point values of peak acceleration expressed as a percent of gravity (%g)

- ⊙ 3.2 Local maximum
- ⊕ 6.9 Local minimum
- ⊖ 8.8 Saddle point

Shaded relief base from Esri Inc., 2008. Data and Maps
All other base map data from Esri Inc., 1983. Digital Chart of the World
United States County base map from the U.S. Geological Survey National Atlas, available at <http://nationalatlas.gov/>
Projection: Albers equal-area conic
Standard parallels 29.5°N, and 45.5°N, central meridian 95°W



Digital data prepared with ArcGIS 10.1 running under Windows 7

Publishing support provided by:
Denver Publishing Service Center
Edit and digital layout by L.J. Binder
Manuscript approved for publication on April 6, 2015
For more information concerning this publication, contact:
Center Director, USGS Geologic Hazards Science Center
Box 25966, Mail Stop 966
Denver, CO 80225
(303) 273-8579
Or visit the Geologic Hazards Science Center Web site at:
<http://geohazards.cr.usgs.gov/>
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Seismic-Hazard Maps for the Conterminous United States, 2014

Peak Horizontal Acceleration with 2 Percent Probability of Exceedance in 50 Years

By
Mark D. Petersen,¹ Morgan P. Moschetti,¹ Peter M. Powers,¹ Charles S. Mueller,¹ Kathleen M. Haller,¹ Arthur D. Frankel,¹ Yuehua Zeng,¹ Sanaz Rezaeian,¹ Stephen C. Harmsen,¹ Oliver S. Boyd,¹ Edward H. Field,¹ Rui Chen,² Nicolas Luco,¹ Russell L. Wheeler,¹ Robert A. Williams,¹ Anna H. Olsen,¹ and Kenneth S. Rukstales¹
 2015

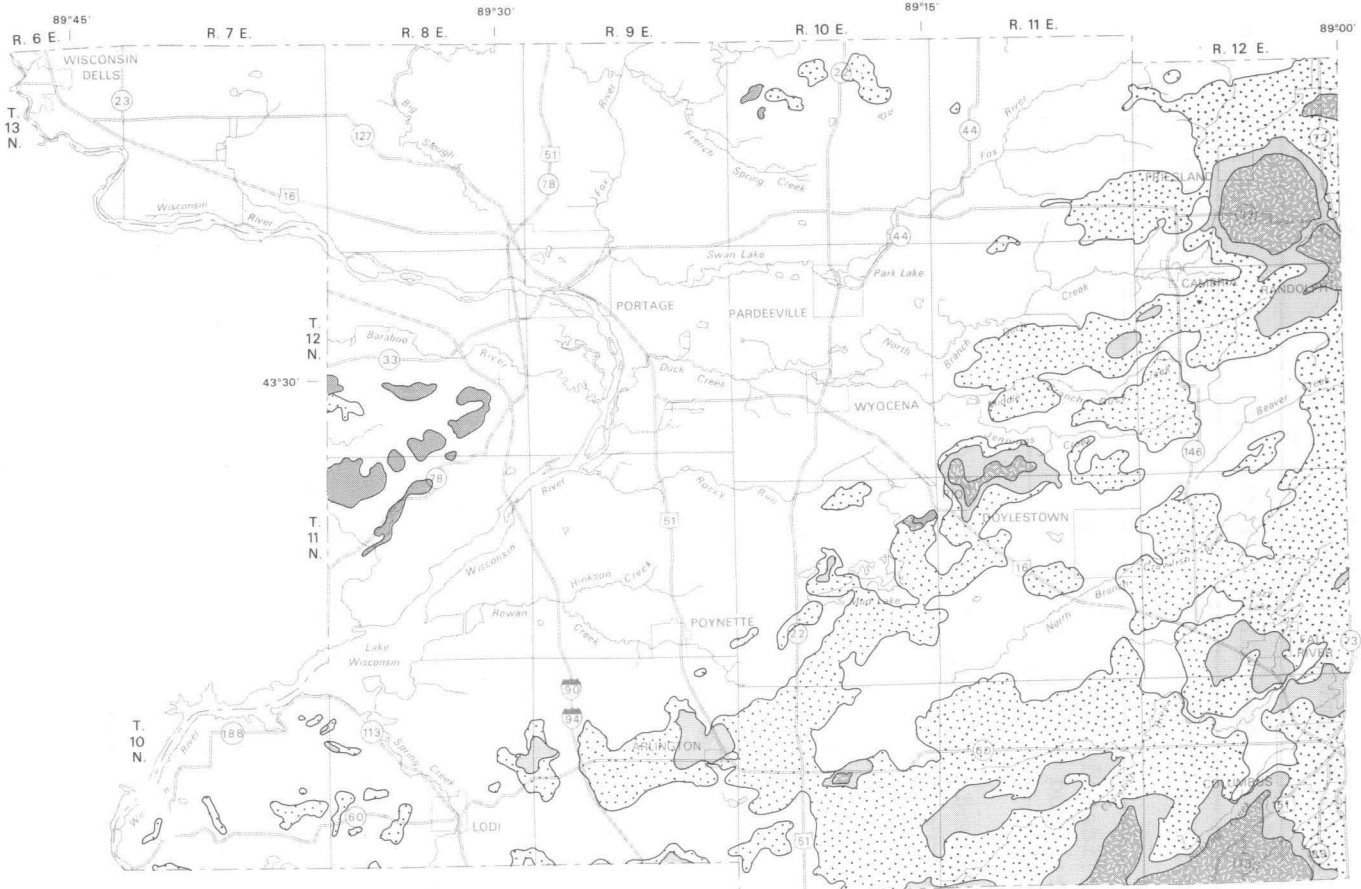
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1-800-ASK-USGS
This report is available at <http://pubs.usgs.gov/sim3325/>
Suggested citation: Petersen, M.D., Moschetti, M.P., Powers, P.M., Mueller, C.S., Haller, K.M., Frankel, A.D., Zeng, Yuehua, Rezaeian, Sanaz, Harmsen, S.C., Boyd, O.S., Field, E.H., Chen, Rui, Luco, Nicolas, Wheeler, R.L., Williams, R.A., Olsen, A.H., and Rukstales, K.S., 2015. Seismic-hazard maps for the conterminous United States, 2014. U.S. Geological Survey Scientific Investigations Map 3325, 6 sheets, scale 1:7,000,000, <http://dx.doi.org/10.3133/sim3325>.
 ISSN 2229-132X (online)
<http://dx.doi.org/10.3133/sim3325>

U.S. Geological Survey
California Geological Survey, Sacramento, Calif.

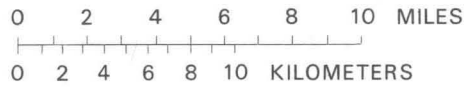


Appendix E
Site Description and Geologic Summary

Attachment E1



Geology by L. C. Trotta (1976)



EXPLANATION

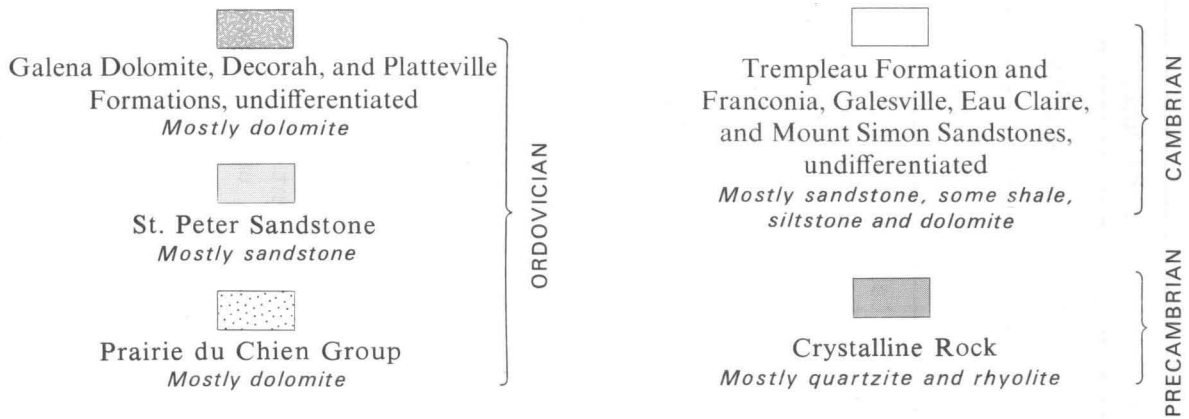


Figure 2. Bedrock geology.

Site Description and Geologic Summary

Site Information

The COL dry ash disposal facility encompasses 62.5 acres, and is located in an industrial and agricultural area with scattered private residences. The site location is Section 27, T12N, R9E, in the town of Pacific, located in Columbia County, Wisconsin. The facility is bounded by U.S. Highway 51 to the east and railroad tracks to the west. Murray Road is located to the north and wetlands are located to the south of the facility.

Regional Geology

Columbia County glacial geology consists mostly of glacial drift. Glacial sediments from the Green Bay Lobe were deposited during the Wisconsin Glaciation (Harr et. al, 1978). Underlying the glacial drift is a mix of dolomite and sandstone from the Ordovician. The Ordovician units: Prairie du Chien Group (mostly dolomite), St. Peter Sandstone, as well as the Platteville and Decorah Formation, and the Galena Dolomite (Galena-Platteville unit) underlay the glacial sediments present in Columbia County (Harr et. al, 1978). In many parts of the county, the Prairie du Chien Group was eroded away and the St. Peter Sandstone overlies Cambrian Sandstone. A bedrock geology map and stratigraphic column are provided in **Attachment E1** and **E2**.

A map of karst and shallow carbonate bedrock in Wisconsin, like the bedrock geology map from Harr et. al, (1978), shows karst structures and shallow carbonate bedrock are found within Columbia County (Bradbury, 2009); however, the karst geology identified is not located at or near the COL dry ash disposal facility (**Attachment E3**).

The COL dry ash disposal facility is located within the area of the county where Ordovician St Peter sandstone bedrock underlies the glacial drift present at the surface (**Appendices G** and **H**). Karst features were not observed in boreholes at COL ADF, and the Wisconsin Geological and Natural History Survey (WGNH) did not identify the site as an area with potential karst structures.

Previous Geologic Investigations

The disposal facility area was investigated by Warzyn Engineering prior to construction by performing approximately 12 borings within and adjacent to the facility footprint. Eleven of the borings were instrumented with groundwater monitoring wells. The borings extended to depths of up to 100 feet. Split spoon samples were collected. Laboratory soil testing included grain size analysis, Atterberg limits, and organic content by loss on ignition. The boring locations and geologic cross sections are shown in **Appendix G**.

Based on the results of the subsurface investigations performed prior to disposal facility construction, the soils below the liner system within the facility footprint consist primarily of medium dense to very dense sands underlain by sandstone bedrock.

References

Harr, C.A., L.C. Trotta, and R.G. Borman, 1978, "Ground-Water Resources and Geology of Columbia County, Wisconsin," University of Wisconsin-Extension Geological and Natural History Survey Information Circular Number 37, 1978.

Bradbury, K. R., "Karst and Shallow Carbonate Bedrock in Wisconsin." University of Wisconsin-Extension Geological and Natural History Survey, Factsheet 02, 2009.

Warzyn Engineering, Inc., 1978, Feasibility Study, Proposed Fly Ash and/or Scrubber Sludge Disposal Facility - Columbia Site, Wisconsin Power and Light Company, Town of Pacific, Columbia County, WI, January 1978.

I:\25222157.00\Deliverables\Locational Restrictions Compliance\Appendices\E-Site Description and Geologic Summary\E1_Site and Geologic Summary.docx

Attachment E2

Table 1.--Stratigraphy of Columbia County

System	Rock unit	Predominant lithology
QUATERNARY	Holocene deposits	Unconsolidated clay, silt, sand, gravel, and organic matter.
	Pleistocene deposits	Unconsolidated clay, silt, sand, gravel, cobbles, boulders, and organic matter.
ORDOVICIAN	Galena Dolomite, Decorah Formation, and Platteville Formation, undifferentiated	Dolomite and some slightly shaly dolomite, light-gray to blue-gray.
	St. Peter Sandstone	Sandstone, dolomitic in some places, shaly at base in some places, white, light-gray, or pink, fine- to medium-grained.
	Prairie du Chien Group	Dolomite, tan, gray, or white; some sandstone and sandy dolomite.
CAMBRIAN	Trempealeau Formation	Sandstone, dolomitic, very fine- to medium-grained; dolomite interbedded with siltstone, light-gray.
	Franconia Sandstone	Sandstone, dolomitic, very fine- to medium-grained; siltstone, dolomitic.
	Galesville, Eau Claire, and Mount Simon Sandstones, undifferentiated	Sandstone, light-gray, fine- to coarse-grained, mostly medium grained.
PRECAMBRIAN	Precambrian rocks, undifferentiated	Crystalline rocks, mostly quartzite and rhyolite.

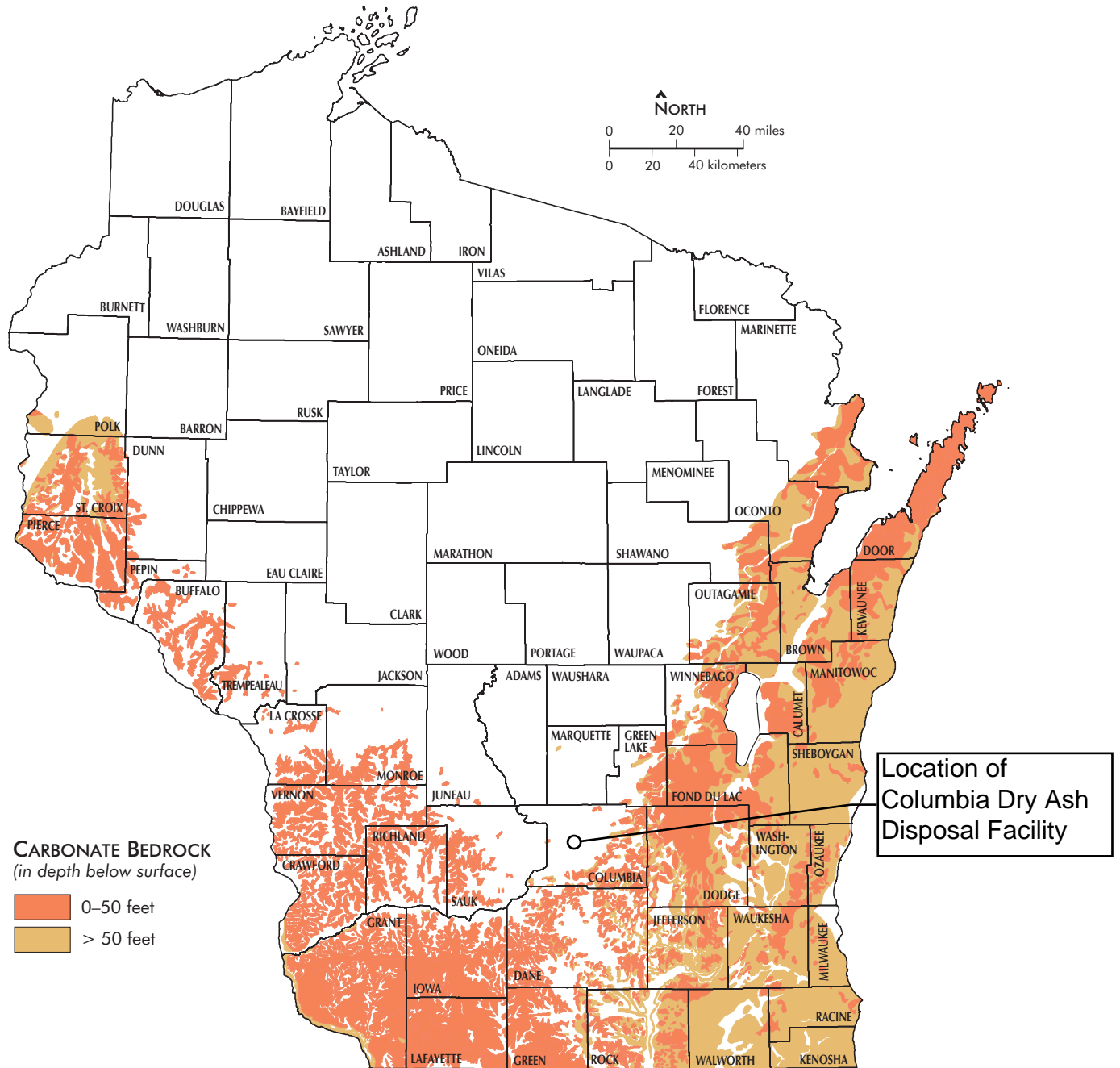
Attachment E3

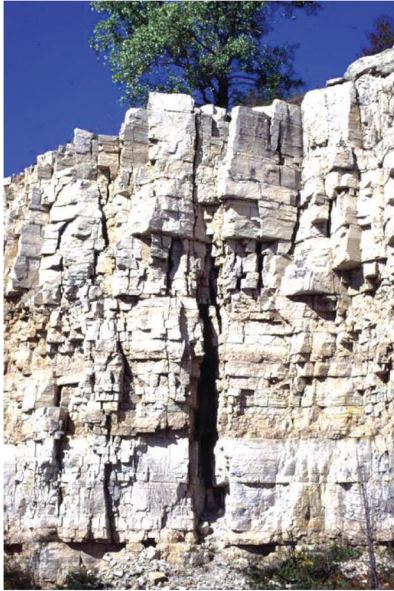
Karst and shallow carbonate bedrock in Wisconsin

Wisconsin Geological and Natural History Survey

Factsheet 02 | 2009

Areas with carbonate bedrock within 50 feet of the land surface are particularly vulnerable to groundwater contamination.





Fracturing and bedding in an exposure of carbonate bedrock near Sturgeon Bay in Door County.

Karst and shallow carbonate bedrock in Wisconsin

Wisconsin Geological and Natural History Survey

Factsheet 02 | 2009

Carbonate bedrock, rock formations composed primarily of limestone or dolomite, underlie the southern third of Wisconsin in a V-shaped belt (see map on other side). These rocks are commonly fractured, with the fractures providing primary pathways for groundwater movement.

Carbonate rocks are soluble, and percolating surface water can enlarge fractures to form conduits, caves, and sinkholes that are the hallmarks of a **karst** system and its related karst landscape.

In Wisconsin, karst landscapes are direct evidence of underlying shallow, fractured carbonate bedrock. But the lack of classic karst features in a landscape does not mean that shallow fractured carbonate bedrock is absent, or that the groundwater is potentially any less vulnerable to contamination.

Carbonate bedrock and groundwater contamination

Carbonate formations are important aquifers in Wisconsin. These aquifers supply water for homes, farms, cities, industries, and other human uses as well as maintaining water levels in lakes and wetlands and flows in streams and springs.

Carbonate aquifers are exceptionally vulnerable to contamination for two reasons:

- Groundwater flow in fractured rocks and karst systems can be extremely rapid—tens to hundreds of feet per day.
- Carbonate rocks are poor at filtering or otherwise removing contaminants.

Some site-specific questions to ask about carbonate aquifers

Carbonate aquifers are particularly vulnerable where overlying soils are thin or absent. There are numerous examples of groundwater contamination of carbonate aquifers in such settings in Wisconsin. Consequently, land-use activities in areas of carbonate rock must be carefully managed to avoid the release of contaminants to groundwater.

Types of questions to ask:

- Is carbonate bedrock present in the subsurface?
- How deeply is it buried? In other words, what is the thickness of the overlying material?
- What is the nature of the overlying material? For example, what is its origin, composition, grain size, etc?

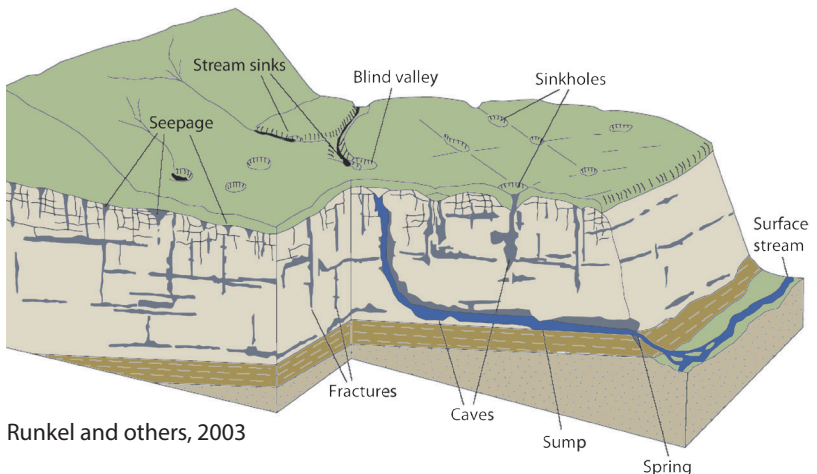
Water- and land-use management plans in areas with carbonate bedrock should always address these sorts of questions as they seek to protect groundwater quantity and quality.

For more information, contact


Kenneth R. Bradbury, Ph.D.
Wisconsin Geological and
Natural History Survey
608.263.7921, krbradbu@wisc.edu



Typical features of a karst system and landscape: Seepages, sinkholes, caves, fractures, springs, and stream sinks.



Runkel and others, 2003



Appendix F
Liquefaction and Settlement Potential Evaluation


Liquefaction and Settlement Potential Evaluation

Based on the results of the site investigation borings and laboratory soil test results, the disposal facility soils are not subject to liquefaction or settlement concerns for the performance of the disposal facility.

Liquefaction is the process by which a saturated, loose, cohesionless soil influenced by external forces can suddenly loses its shear strength and behave as a fluid. The external forces result from ground motion from an earthquake. The disposal facility site soils consist primarily of sand. Borings show that the sands are medium dense to very dense rather than loose so liquefaction is not a concern given the low magnitude of maximum ground accelerations expected in the area; see

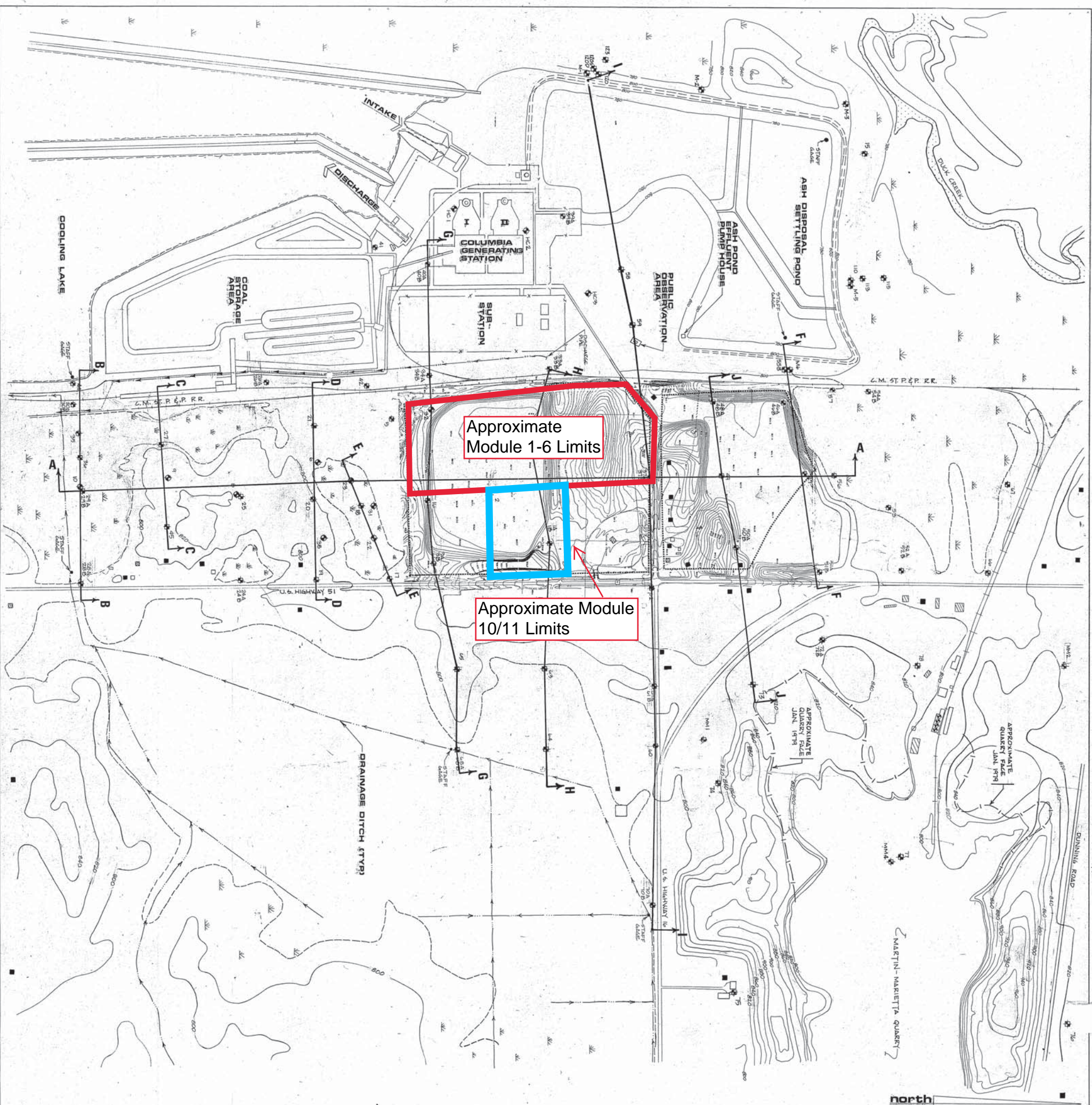
Appendix D.

Settlement below a disposal facility can be a concern if the facility is underlain by extensive soft, fine-grained soils. Soft soils are subject to consolidation settlement depending on the load over the soft soils. The disposal facility soils consist of medium dense to very dense sands that are not subject to consolidation settlement so settlement is not a concern at the disposal facility.



Appendix G

Geologic Cross Sections



Approximate
Module 1-6 Limits

Approximate Module
10/11 Limits

north

- LEGEND**
- PROPOSED PROJECT AREA
 - OBSERVATION WELL LOCATION, NUMBER, AND WATER TABLE ELEVATION
 - BORING LOCATION AND NUMBER
 - WETLANDS
 - TOPOGRAPHIC CONTOURS (CONTOUR INTERVAL: 20 FT)
 - PRIVATE RESIDENCES (ASSUMED LOCATIONS OF PRIVATE WATER SUPPLY WELLS)
 - COMMERCIAL BUILDINGS (ASSUMED LOCATIONS OF POSSIBLE PUBLIC WATER SUPPLY WELLS)
 - SURFACE WATERS (STREAMS OR DRAINAGE DITCHES) ARROWS INDICATE DIRECTION OF FLOW
 - OTHER BUILDINGS (GARAGES, BARN, ETC.)
 - HIGH CAPACITY WELLS

- NOTES**
- 1) TOPOGRAPHIC INFORMATION BASED PRIMARILY ON USGS POLYMETRIC DATA. THE COLUMBIA GENERATING STATION AREA OF DRAINAGE, MARTIN-MARIETTA QUARRY AND THE DISPOSAL AREA HAS BEEN UPDATED, BASED ON VARIOUS MORE RECENT SURVEYS. THE COLUMBIA GENERATING STATION AND FACILITIES ARE SHOWN IN PLANIMETRIC.
 - 2) DETAILS OF THE MARTIN-MARIETTA QUARRY ARE APPROXIMATE. REFER TO DRAWING C7154-F15 AND TEXT FOR MORE DETAILED TOPOGRAPHY AND DISCUSSION.

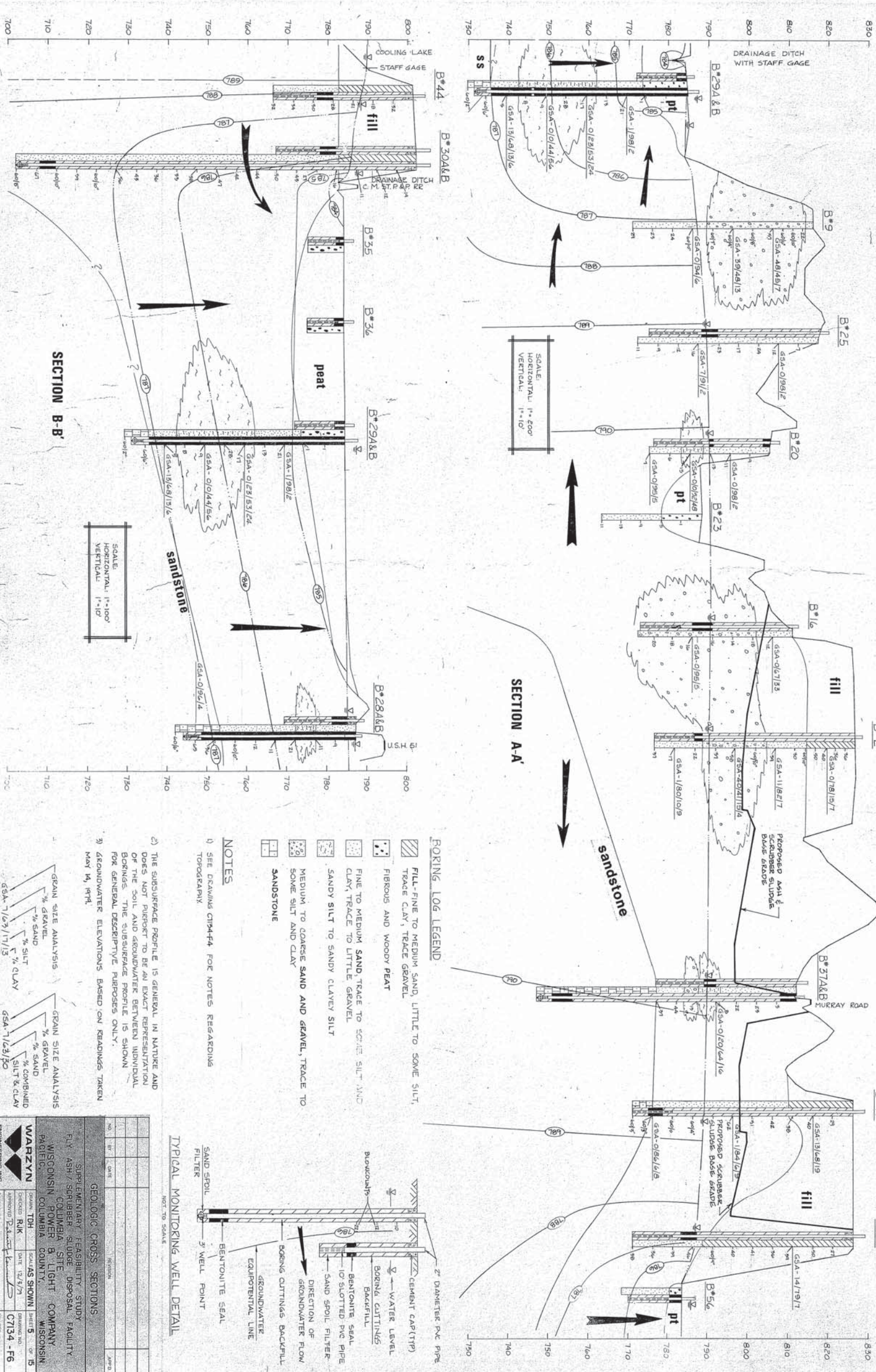
CROSS SECTION LOCATION MAP

NO.	REV.	DATE	REVISION	APP'D.

WARBYN ENGINEERING INC.

SUPPLEMENTARY FEASIBILITY STUDY
 FLY ASH / SLAG / SLUDGE DISPOSAL FACILITY
 WISCONSIN COLUMBIA SITE LIGHT COMPANY
 PACIFIC COLUMBIA COUNTY WISCONSIN

DESIGNER: WARBYN ENGINEERING INC.
 CHECKED: RJK DATE: 12/17/71
 SCALE: 1" = 300'
 SHEET 4 OF 15
 DRAWING NO. C7154-F5
 PRINTED



SCALE
HORIZONTAL: 1" = 200'
VERTICAL: 1" = 10'

SCALE
HORIZONTAL: 1" = 100'
VERTICAL: 1" = 10'

BORING LOG LEGEND:

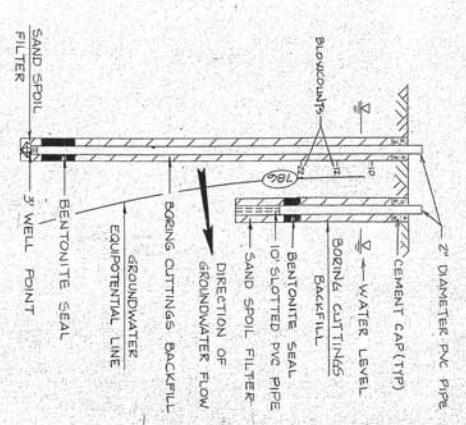
- FILL-FINE TO MEDIUM SAND, LITTLE TO SOME SILT, TRACE CLAY, TRACE GRAVEL
- FIBROUS AND WOODY PEAT
- FINE TO MEDIUM SAND, TRACE TO SOME SILT AND CLAY, TRACE TO LITTLE GRAVEL
- SANDY SILT TO SANDY CLAYEY SILT
- MEDIUM TO COARSE SAND AND GRAVEL, TRACE TO SOME SILT AND CLAY
- SANDSTONE

NOTES

- 1) SEE DRAWING C1734-F4 FOR NOTES REGARDING TOPOGRAPHY
- 2) THE SUBSURFACE PROFILE IS GENERAL IN NATURE AND DOES NOT PURPORT TO BE AN EXACT REPRESENTATION OF THE SOIL AND GROUNDWATER BETWEEN INDIVIDUAL BORINGS. THE SUBSURFACE PROFILE IS SHOWN FOR GENERAL DESCRIPTIVE PURPOSES ONLY.
- 3) GROUNDWATER ELEVATIONS BASED ON READINGS TAKEN MAY 14, 1974.

TYPICAL MONITORING WELL DETAIL

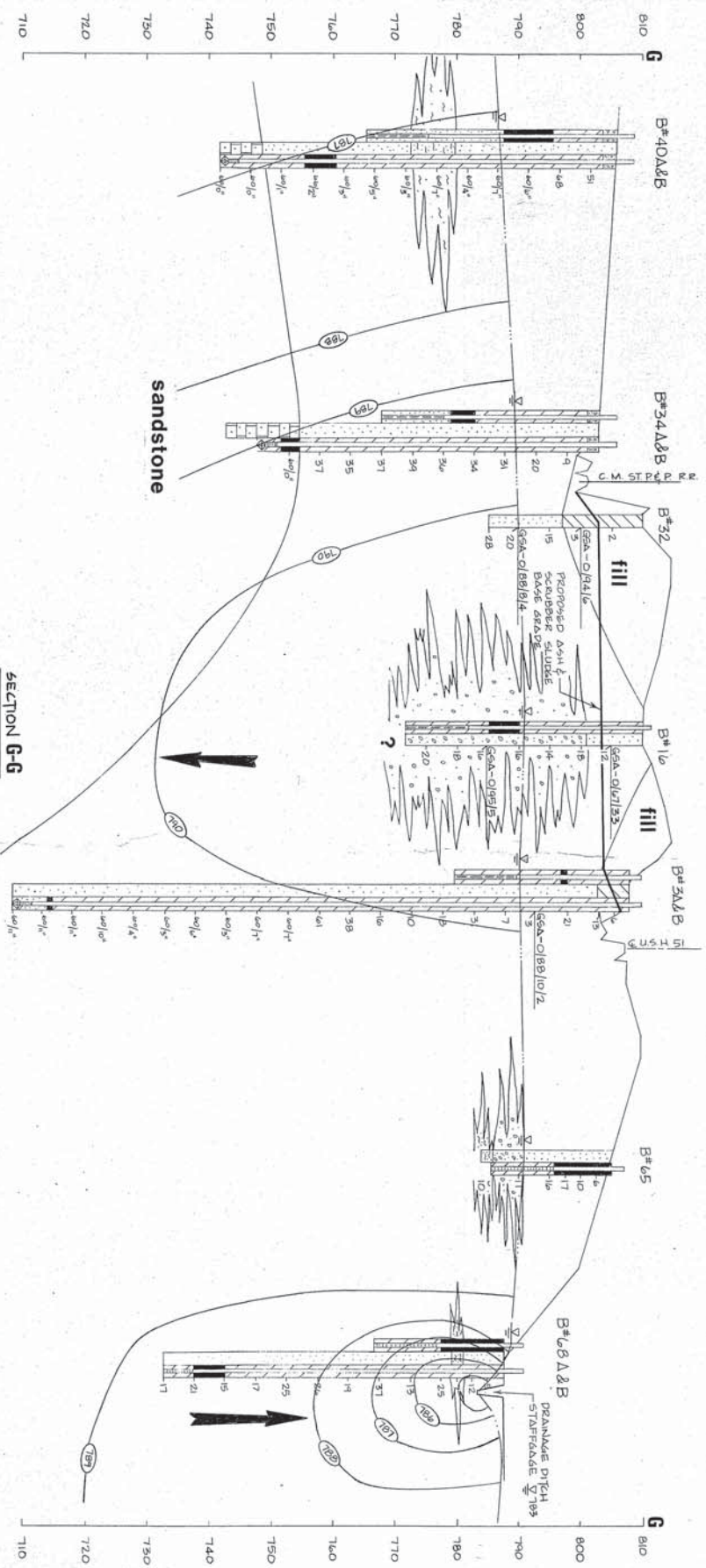
NOT TO SCALE



- GRAIN SIZE ANALYSIS**
- 100% GRAVEL
 - 100% SAND
 - 100% SILT
 - 100% CLAY
- GRAIN SIZE ANALYSIS**
- 100% GRAVEL
 - 100% SAND
 - 100% COMBINED SILT & CLAY

GEOLOGIC CROSS SECTIONS	
NO.	DATE
1	5/14/74
2	5/14/74
3	5/14/74
4	5/14/74
5	5/14/74
6	5/14/74
7	5/14/74
8	5/14/74
9	5/14/74
10	5/14/74

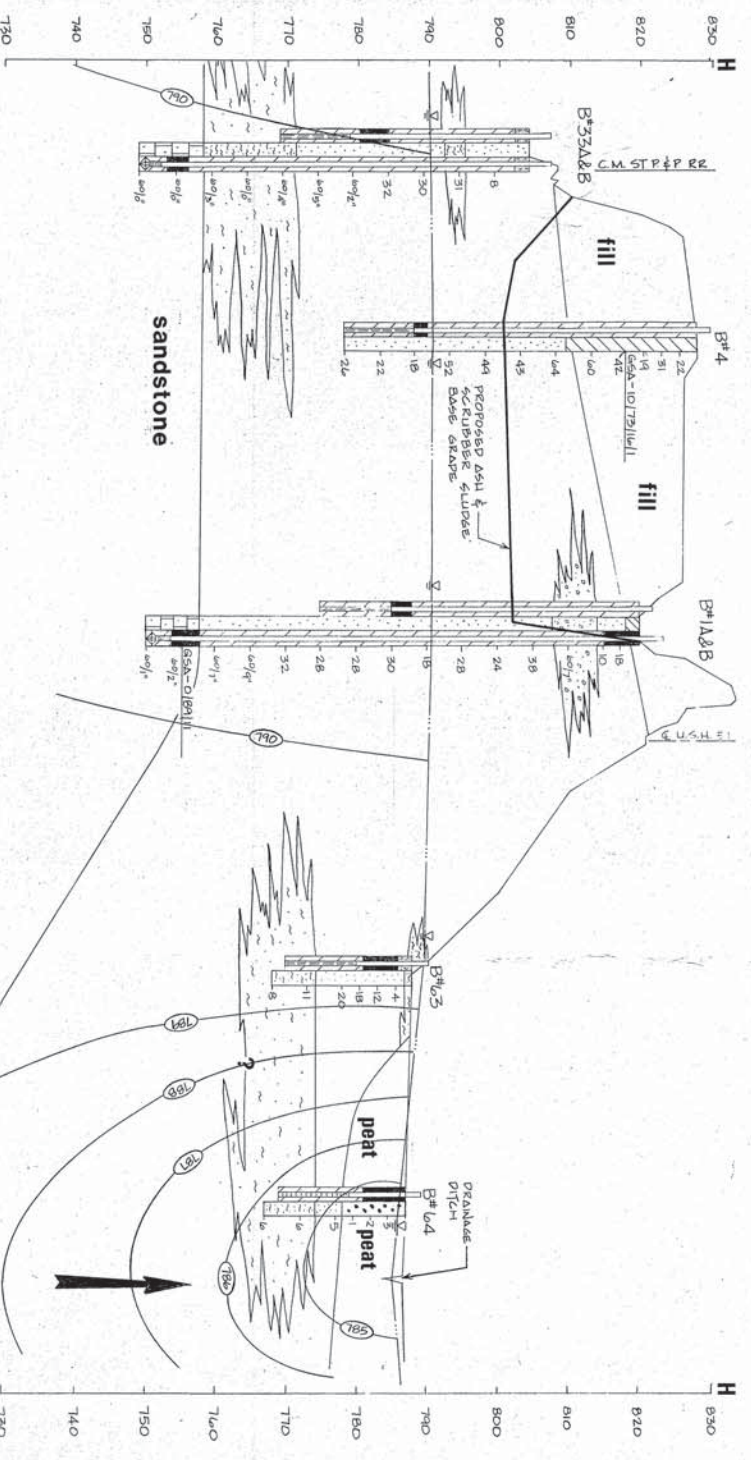
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 SUPPLEMENTARY FEASIBILITY STUDY
 FLY ASH / SPRINGER SLUDGE DISPOSAL FACILITY
 WISCONSIN COLUMBIA SITE
 POWER & LIGHT COMPANY
 COLUMBIA COUNTY, WISCONSIN
 SHEET 5 OF 15
 DRAWING NO. C7134-F6
 DATE 12/17/74
 APPROVED BY [Signature]
 CHECKED BY [Signature]
 DESIGNED BY [Signature]



SECTION G-G

SCALE:
 VERTICAL: 1"=10'
 HORIZONTAL: 1"=200'

NOTES
 1) REFER TO DRAWING C7134-15 FOR NOTES AND LEGEND



SECTION H-H

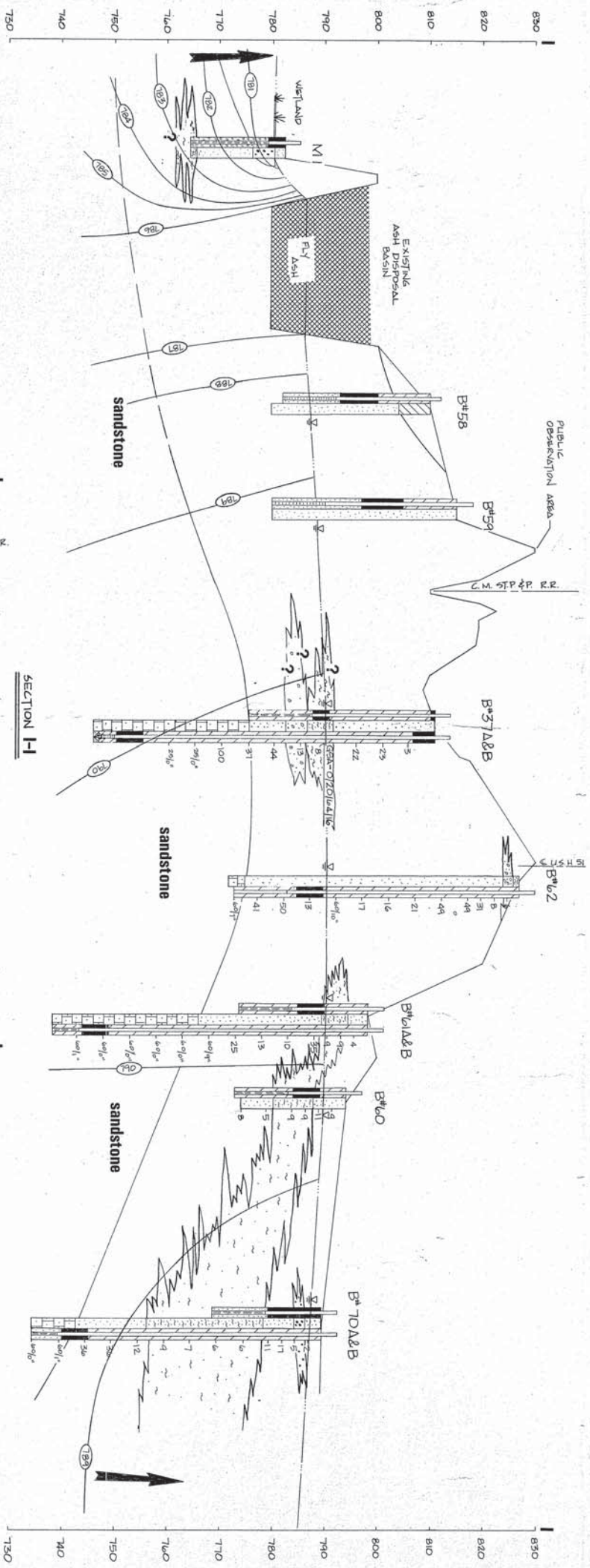
NO.	REV.	DATE	REVISION	APP'D.

GEOLOGIC CROSS SECTIONS

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 FLY ASH / SCRUBBER SLUDGE DISPOSAL FACILITY
 COLUMBIA SITE
 WISCONSIN POWER & LIGHT COMPANY
 PACIFIC COLUMBIA COUNTY WISCONSIN

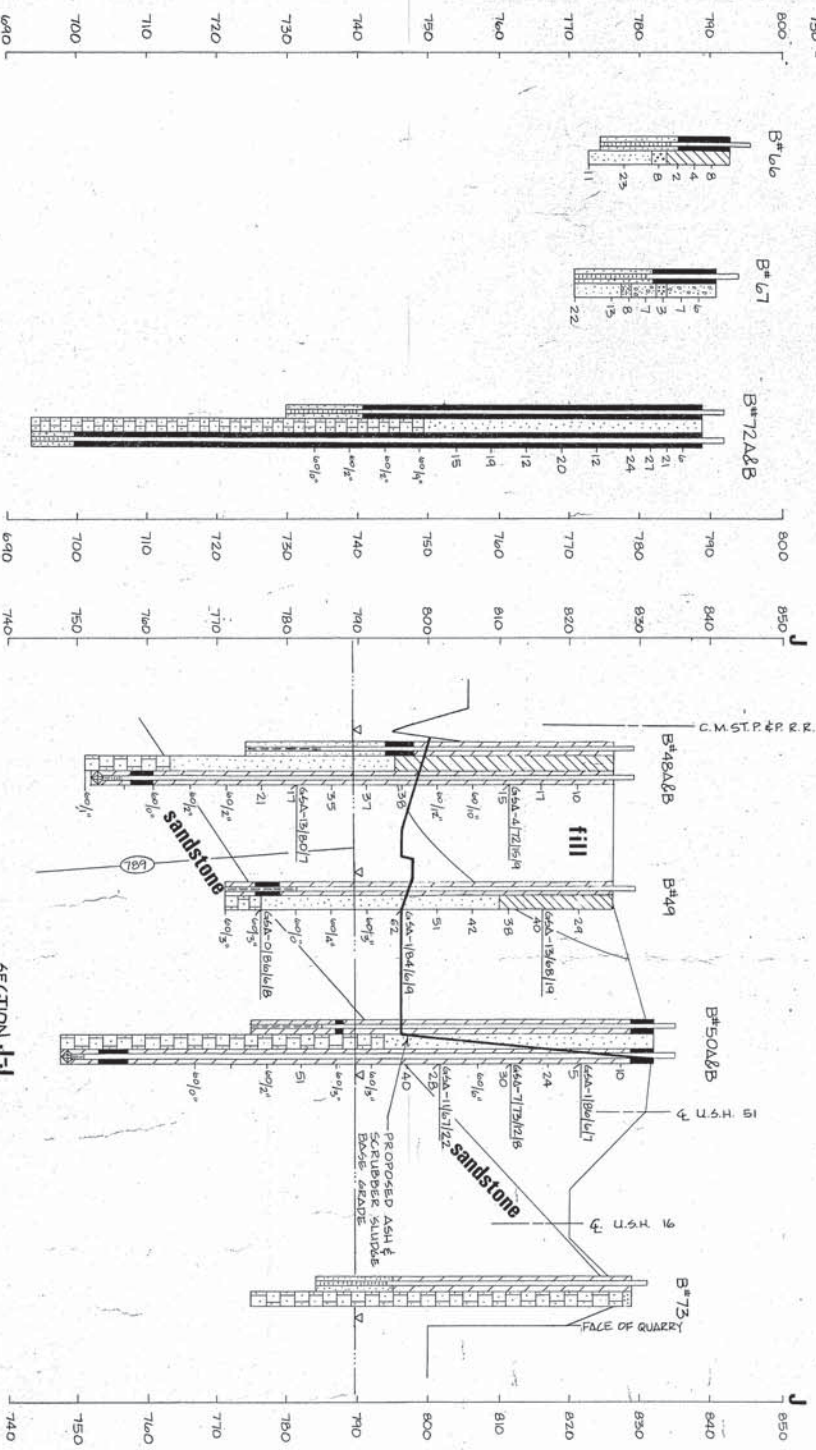
WARZYN
 ENGINEERING INC.

DRAWN: TDH
 CHECKED: RJK
 DATE: 12/1/74
 SHEETS SHOWN: 7 OF 15
 PROJECT: C7134-F8
 PRINTED:



SECTION I-I

NOTES
 1) REFER TO DRAWING C114-15 FOR NOTES AND LEGEND.




SECTION J-J

MISCELLANEOUS BORINGS

NO.	REV.	DATE	REVISION	APP'D.

WARZYN ENGINEERING INC.
 SUPPLEMENTARY FEASIBILITY STUDY
 FLY ASH / SCRUBBER SLUDGE DISPOSAL FACILITY
 COLUMBIA SITE
 WISCONSIN POWER & LIGHT COMPANY
 PACIFIC COLUMBIA COUNTY WISCONSIN
 DRAWN: TDH DATE: 12/1/79 SHEET: 8 OF 15
 CHECKED: RJK SCALE: AS SHOWN
 APPROVED: J.L.H. PROJECT NO.: C7134-F9
 REFERENCE:



Appendix H

Slope Stability Analysis

May 10, 2022
File No. 25220183.00

TECHNICAL MEMORANDUM

ANALYSIS BY: Brandon Suchomel

REVIEWED BY: Deb Nelson
 Phil Gearing

SUBJECT: Slope Stability Analyses
 Plan of Operation 2022 Update
 Columbia Dry Ash Disposal Facility

PURPOSE

The purposes of the slope stability analyses were to evaluate:

- The interim 3H:1V waste slope in Module 5 at the highest waste grade (Interim Waste Filling Stage 2).
- The interim 4H:1V east waste slope in Module 4/Module 11 at the highest waste grade (Interim Waste Filling Stage 3).
- The final 4H:1V final cover slope Module 4/Module 11 at the highest final cover grade.

CONCLUSION

The attached results confirm that the interim waste slopes will be stable during the construction and operation of the disposal facility modules and that the final grade slope will be stable post-closure of the disposal facility.

APPROACH

SCS Engineers (SCS) evaluated the waste mass slope stability of the interim slope of Module 5 during interim waste filling stage 2 and the waste mass slope stability of the interim slope of Module 4/Module 11 during the interim waste filling stage 3 at the most critical/highest waste grade cross-sections. The Module 5 interim 3H:1V waste slope analyzed is the eastern filling face with a maximum waste fill height of approximately 63 feet above the base grade corresponding to a peak elevation of approximately 870 feet above mean sea level. The Module 4/Module 11 interim 4H:1V waste slope analyzed is at the eastern filling face with a maximum waste fill height of approximately 65 feet above the base grade corresponding to a peak elevation of approximately 870 feet above mean sea level. The interim waste slopes were evaluated for block failure and optimized circular failure.



SCS completed analysis for this waste slope by iteratively modifying the coal combustion residual (CCR) friction angle to determine the minimum friction angle required for a safety factor of 1.3. This calculated CCR friction angle was used in the other analyzed sections. The calculated CCR friction angle of 22.7 degrees is still conservative based on assumed published values of stabilized CCR in the range of 35 to 45 degrees (see Reference 7).

SCS evaluated the final grade slope stability of longest final cover slope at the most critical/highest final grade cross-section. The 4H:1V slope of analyzed is through the Module 4/Module 11 waste mass with a maximum waste fill height of approximately 101 feet above base grades corresponding to a peak elevation of approximately 908 feet above mean sea level. The final grade slope was evaluated for block failure and optimized circular failure.

RESULTS

The calculated safety factors for each slope section and failure type are shown in the attached summary table.

SCS recommends a minimum safety factor of 1.3 for the interim waste slopes and 1.5 for the final grade slopes. The results indicate that the interim waste slopes and final grade slopes have acceptable minimum safety factors.

REFERENCES

1. SCS Engineers, Columbia Dry Ash Disposal Facility, Module 3 Liner Construction, 2016, existing composite liner grades and material properties for geosynthetics.
2. SCS Engineers, Columbia Dry Ash Disposal Facility, 2018 Module 4 Liner Construction, 2018, existing composite liner grades and material properties for subbase, clay, and drainage layer.
3. SCS Engineers, Columbia Dry Ash Disposal Facility, Module 5-6 Liner Construction, 2021, existing composite liner grades and material properties for subbase, clay, and drainage layer.
4. SCS Engineers, Columbia Dry Ash Disposal Facility, Plan of Operation 2022 Update, 2022, Module 10-11 composite liner grades, interim waste filling stages, final grades.
5. TRI/Environmental, Interface Friction Test Results, 2016, for 2016 Module 3 Liner Construction.
6. TRI/Environmental, Consolidated-Undrained Triaxial Compression Test Results for FGD Material, 2015, material properties for CCR (SCS Project No. 25214049.00).
7. U.S. Department of Transportation, Federal Highway Administration, Recycled Materials, User Guidelines for Waste and Byproduct Materials in Pavement Construction.
8. Stabilization of FGD By-Products by Using Fly Ash, Cement, and Sialite, 2009 WOCA Conference.
9. Geo-Slope International, Ltd., GeoStudio 2016, Version 8.16.2.14053, Slope/W slope stability software.

ASSUMPTIONS

- Sand drainage layer in each of the existing and future modules have the same properties.
- Geosynthetics installed for each of the module composite liners have the same properties.
- Clay material for each of the module composite liners have the same properties.
- CCR waste material will be the same in each of the existing and future modules.
- A waste fill slope of 3H:1V or 4H:1V is representative of the design interim waste slopes.
- The groundwater elevation will remain below the elevation at the base of the landfill liner system.
- The disposal facility will be operated to prevent development of liquid pressures, or seepage forces within the waste, and there will be no buildup of leachate above the top of the drainage layer.
- The disposal facility will be operated to prevent placement of weak layers of waste within the overall waste mass.
- Optimized circular and sliding block failure stability analyses are appropriate to evaluate the waste interim grade and final grade slope stability.
- Material properties are as shown in the table below, based on the indicated references and assumed values based on experience. Friction angles for soils are conservative assumed values based on soil type, published typical values, and SCS experience. The CCR friction angle is a calculated conservative value that is in line with assumed published values and the CCR unit weight is based on 2015 triaxial compression test results by TRI/Environmental for CCR.

Table 1. Material Properties Summary Table

Material	Unit Weight (pcf)	Friction Angle (degrees)	Cohesion (psf)	Reference
Subbase	120	30	0	1, 2, and 3
Clay	125	28	0	1, 2, and 3
Geosynthetics	58	24.3	0	5
Drainage Layer	115	30	0	2 and 3
CCR	86	22.7 ⁽¹⁾	0	6, 7, 8, and Calculation
Final Cover	120	30	0	1, 2, 3, and 4

Notes: CCR friction angle iteratively calculated for minimum value for a safety factor of 1.3 for Module 5 interim 3H:1V analysis. Calculated CCR friction angle was used in the other analyzed sections.

Waste Slope Stability Analysis

May 10, 2022

Page 4

Attachments: Calculations organized as follows:

- Factor of Safety Summary Table
- Cross Section Locations
- Slope/W Outputs

BSS/DLN/REO/PEG

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Plan of Operation Update - Slope Stability Analysis
Factor of Safety Results Summary
Columbia Dry Ash Disposal Facility / SCS Project No. 25220183.00

Scenario Analyzed	Failure Type	Calculated Safety Factor	Recommended Minimum Safety Factor
Interim Waste Stage 2 (Module 5 Interim 3H:1V Waste Slope)			
2-2_Optimized Circular_Forced Full Slope_FS=1.3	Optimized Circular	1.302 ⁽¹⁾	1.300
3_Block	Block	1.579	1.300
Interim Waste Stage 3 (Module 4/Module 11 Interim 4H:1V Waste Slope)			
2-1_Optimized Circular_Forced Full Slope	Optimized Circular	1.691	1.300
3_Block	Block	2.063	1.300
Final Grade (Module 4/Module 11 4H:1V Final Cover Slope)			
2_Optimized Circular	Optimized Circular	1.715	1.500
3_Block	Block	2.143	1.500

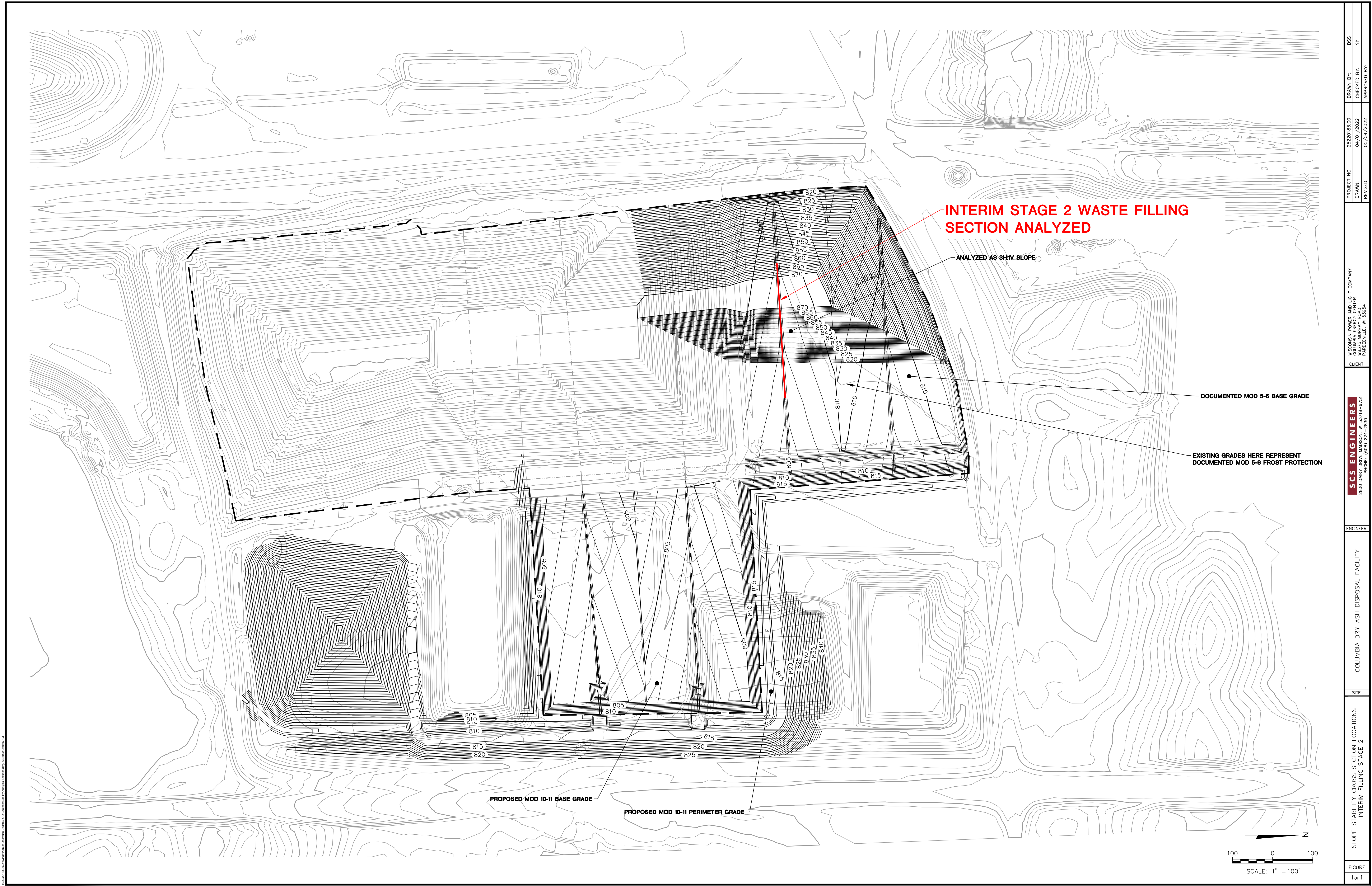
Notes:

1. Coal combustion residual (CCR) friction angle iteratively calculated for minimum value for a safety factor of 1.3.

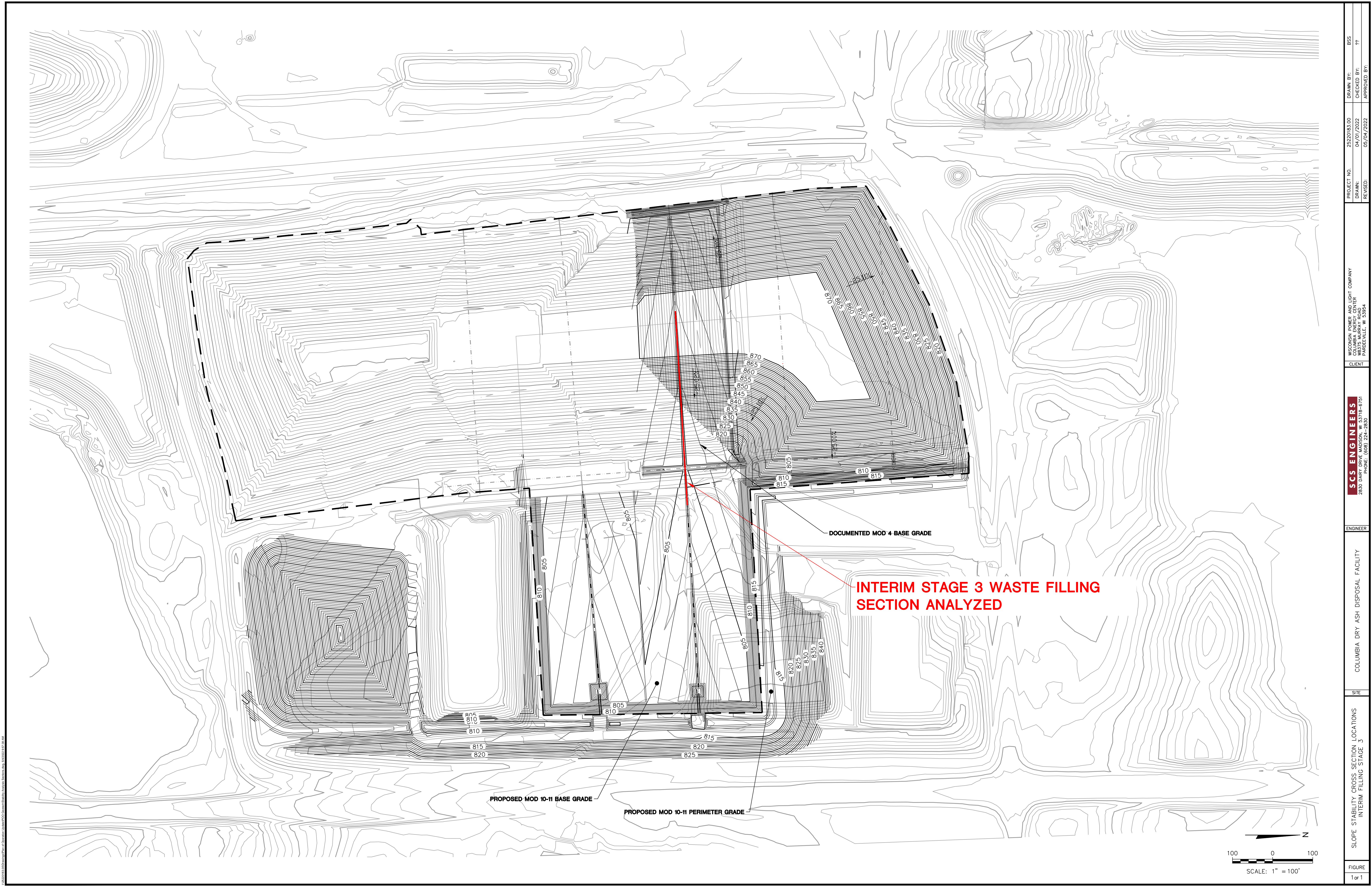
Updated by: BSS, 05/04/2022

Checked by: DLN, 05/05/2022

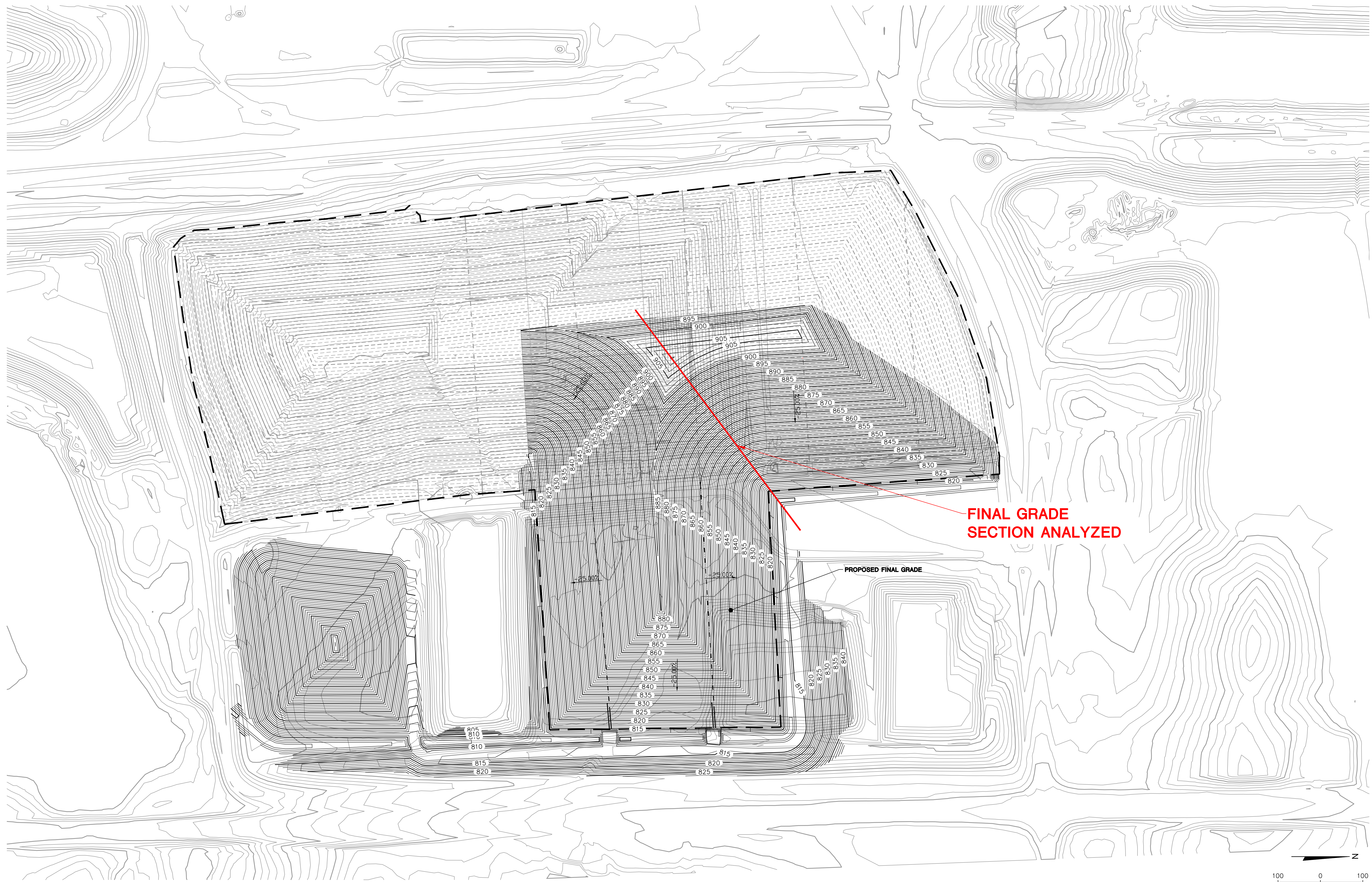
I:\25220183.00\Data and Calculations_Issued for Permitting POO Geotech Calculations\Slope Stability\Tech Memo\[A1_POO Slope Stability_FS Results Summary Table_220504.xlsx]FS Results Summary



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DRAWN:	04/07/2022	CHECKED BY:	PT
REVISED:	05/04/2022	APPROVED BY:	
CLIENT:	WISCONSIN POWER AND LIGHT COMPANY 8375 MURRAY ROAD PARISVILLE, WI 53544		
ENGINEER:	SCS ENGINEERS 2830 DARY DRIVE MADISON, WI 53718-6797 PHONE: (608) 224-2830		
SITE:	COLUMBIA DRY ASH DISPOSAL FACILITY		
FIGURE:	SLOPE STABILITY CROSS SECTION LOCATIONS INTERIM FILLING STAGE 2		
	1 of 1		

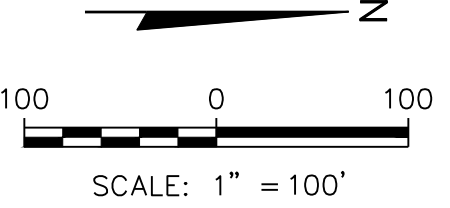


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REVISED:	05/04/2022	APPROVED BY:	
CLIENT:	WISCONSIN POWER AND LIGHT COMPANY COLUMBIA DRY ASH DISPOSAL FACILITY 8375 MURRAY ROAD PARKEVILLE, WI 53554		
ENGINEER:	SCS ENGINEERS 2830 DARY DRIVE MADISON, WI 53718-6797 PHONE: (608) 224-2830		
SITE:	SLOPE STABILITY CROSS SECTION LOCATIONS INTERIM FILLING STAGE 3		
FIGURE:	1 of 1		

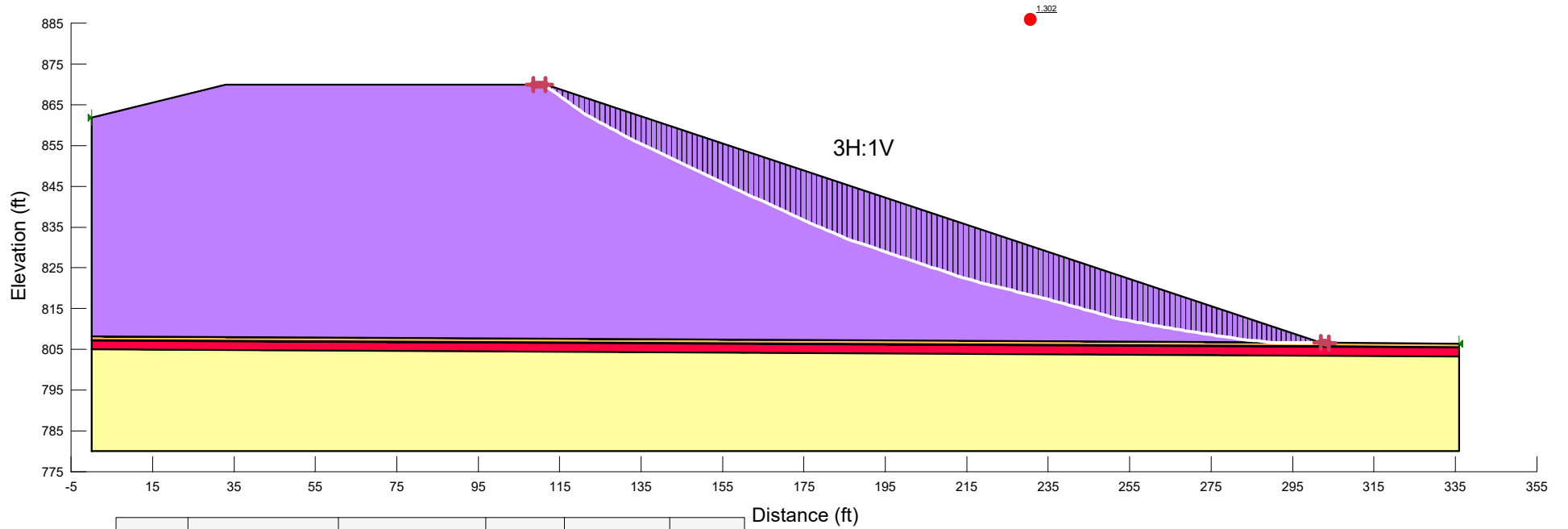


FINAL GRADE SECTION ANALYZED

PROPOSED FINAL GRADE



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DRAWN:	04/07/2022	CHECKED BY:	PT
REVISION:	05/04/2022	APPROVED BY:	
CLIENT	WISCONSIN POWER AND LIGHT COMPANY ATTENTION: PROJECT MANAGER W8375 MURRAY ROAD PARKEVILLE, WI 53554		
ENGINEER	SCS ENGINEERS 2830 DARY DRIVE MADISON, WI 53718-6797 PHONE: (608) 224-2830		
SITE	COLUMBIA DRY ASH DISPOSAL FACILITY		
FIGURE	SLOPE STABILITY CROSS SECTION LOCATIONS FINAL GRADE		
	1 of 1		



Color	Name	Model	Unit Weight (pcf)	Cohesion' (psf)	Phi' (°)
■	CCR (Optimized Circular FS=1.3)	Mohr-Coulomb	86	0	22.7
■	Clay	Mohr-Coulomb	125	0	28
■	Drainage Layer	Mohr-Coulomb	115	0	30
■	Geosynthetics	Mohr-Coulomb	58	0	24.3
■	Subbase	Mohr-Coulomb	120	0	30

Title: Columbia Mod 10-11 Interim Waste Stage 2
Name: 2-2_Optimized Circular_Forced Full Slope_FS=1.3
Method: Bishop
Last Edited By: Suchomel, Brandon

F of S: 1.302, **F of S Rank (Analysis):** 1 of 8,650 slip surfaces
Last Solved Date: 4/7/2022, **Last Solved Time:** 4:36:09 PM

2-2_Optimized Circular_Forced Full Slope_FS=1.3

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File Information

File Version: 8.16
Title: Columbia Mod 10-11 Interim Waste Stage 2
Created By: Suchomel, Brandon
Last Edited By: Suchomel, Brandon
Revision Number: 54
Date: 4/7/2022
Time: 4:35:53 PM
Tool Version: 8.16.3.14580
File Name: Columbia Mod 10-11 Interim Waste Stage 2.gsz
Directory: I:\25220183.00\Data and Calculations_Issued for Permitting POO Geotech Calculations\Slope Stability\
Last Solved Date: 4/7/2022
Last Solved Time: 4:36:08 PM

Project Settings

Length(L) Units: Feet
Time(t) Units: Seconds
Force(F) Units: Pounds
Pressure(p) Units: psf
Strength Units: psf
Unit Weight of Water: 62.4 pcf
View: 2D
Element Thickness: 1

Analysis Settings

2-2_Optimized Circular_Forced Full Slope_FS=1.3

Kind: SLOPE/W
Method: Bishop
Settings
 PWP Conditions Source: (none)
Slip Surface
 Direction of movement: Left to Right
 Use Passive Mode: No
 Slip Surface Option: Entry and Exit
 Critical slip surfaces saved: 10
 Resisting Side Maximum Convex Angle: 1 °
 Driving Side Maximum Convex Angle: 5 °
 Optimize Critical Slip Surface Location: Yes
Critical Slip Surface Optimizations
 Maximum Iterations: 2,000
 Convergence Tolerance: 1e-007

Starting Points: 8

Ending Points: 16

Complete Passes per Insertion: 1

Tension Crack

Tension Crack Option: (none)

F of S Distribution

F of S Calculation Option: Constant

Advanced

Number of Slices: 150

F of S Tolerance: 0.001

Minimum Slip Surface Depth: 0.1 ft

Materials

Clay

Model: Mohr-Coulomb

Unit Weight: 125 pcf

Cohesion': 0 psf

Phi': 28 °

Phi-B: 0 °

Drainage Layer

Model: Mohr-Coulomb

Unit Weight: 115 pcf

Cohesion': 0 psf

Phi': 30 °

Phi-B: 0 °

Geosynthetics

Model: Mohr-Coulomb

Unit Weight: 58 pcf

Cohesion': 0 psf

Phi': 24.3 °

Phi-B: 0 °

Subbase

Model: Mohr-Coulomb

Unit Weight: 120 pcf

Cohesion': 0 psf

Phi': 30 °

Phi-B: 0 °

CCR (Optimized Circular FS=1.3)

Model: Mohr-Coulomb

Unit Weight: 86 pcf

Cohesion': 0 psf

Phi': 22.7 °

Phi-B: 0 °

Slip Surface Entry and Exit

Left Projection: Range

Left-Zone Left Coordinate: (108.48, 870) ft
 Left-Zone Right Coordinate: (111.54, 870) ft
 Left-Zone Increment: 30
 Right Projection: Range
 Right-Zone Left Coordinate: (301.96, 806.59965) ft
 Right-Zone Right Coordinate: (303.97, 806.58782) ft
 Right-Zone Increment: 30
 Radius Increments: 8

Slip Surface Limits

Left Coordinate: (0, 861.8) ft
 Right Coordinate: (335.9, 806.4) ft

Points

	X (ft)	Y (ft)
Point 1	0	780
Point 2	335.9	780
Point 3	0	805
Point 4	335.9	803.3
Point 5	0	807.1
Point 6	335.9	805.4
Point 7	0	808.1
Point 8	335.9	806.4
Point 9	0	861.8
Point 10	33	870
Point 11	111.6	870
Point 12	305	805.6
Point 13	301.9	806.6
Point 14	0	807.2
Point 15	305	805.7
Point 16	335.9	805.5

Regions

	Material	Points	Area (ft ²)
Region 1	Subbase	1,2,4,3	8,112
Region 2	Clay	3,5,12,6,4	712.72
Region 3	CCR (Optimized Ciruclar FS=1.3)	7,9,10,11,13	12,746
Region 4	Geosynthetics	5,14,15,16,6,12	33.59
Region 5	Drainage Layer	14,7,13,8,16,15	299.67

Current Slip Surface

Slip Surface: 8,650
 F of S: 1.302
 Volume: 1,754.0514 ft³
 Weight: 150,848.42 lbs
 Resisting Moment: 15,727,122 lbs-ft

Activating Moment: 12,083,493 lbs-ft
 F of S Rank (Analysis): 1 of 8,650 slip surfaces
 F of S Rank (Query): 1 of 8,650 slip surfaces
 Exit: (301.8996, 806.60013) ft
 Entry: (111.00732, 870) ft
 Radius: 95.822462 ft
 Center: (282.35976, 1,073.0057) ft

Slip Slices

	X (ft)	Y (ft)	PWP (psf)	Base Normal Stress (psf)	Frictional Strength (psf)	Cohesive Strength (psf)
Slice 1	111.30366	869.78663	0	14.901895	6.2335978	0
Slice 2	112.27238	869.08913	0	47.970541	20.066512	0
Slice 3	113.61713	868.12087	0	84.304041	35.265144	0
Slice 4	114.96189	867.15261	0	120.63754	50.463777	0
Slice 5	116.30665	866.18435	0	156.97104	65.662409	0
Slice 6	117.6514	865.21609	0	193.30454	80.861041	0
Slice 7	118.99616	864.24784	0	229.63804	96.059674	0
Slice 8	120.34091	863.27958	0	265.97154	111.25831	0
Slice 9	121.64885	862.45093	0	307.70165	128.71439	0
Slice 10	122.91997	861.76189	0	327.15121	136.85031	0
Slice 11	124.1911	861.07285	0	346.60077	144.98624	0
Slice 12	125.46222	860.38381	0	366.05033	153.12217	0
Slice 13	126.73334	859.69477	0	385.4999	161.2581	0
Slice 14	128.00446	859.00573	0	404.94946	169.39403	0
Slice 15	129.27559	858.31669	0	424.39902	177.52996	0
Slice 16	130.54671	857.62765	0	443.84858	185.66588	0
Slice 17	131.81132	856.98435	0	468.71531	196.06786	0
Slice 18	133.06943	856.38679	0	482.02669	201.63613	0
Slice 19	134.32754	855.78924	0	495.33807	207.2044	0
Slice 20	135.58564	855.19168	0	508.64945	212.77267	0
Slice 21	136.84375	854.59412	0	521.96083	218.34094	0
Slice 22	138.10185	853.99656	0	535.27221	223.90922	0
Slice 23	139.35996	853.39901	0	548.58359	229.47749	0
Slice 24	140.61807	852.80145	0	561.89497	235.04576	0
Slice 25	141.87617	852.20389	0	575.20635	240.61403	0

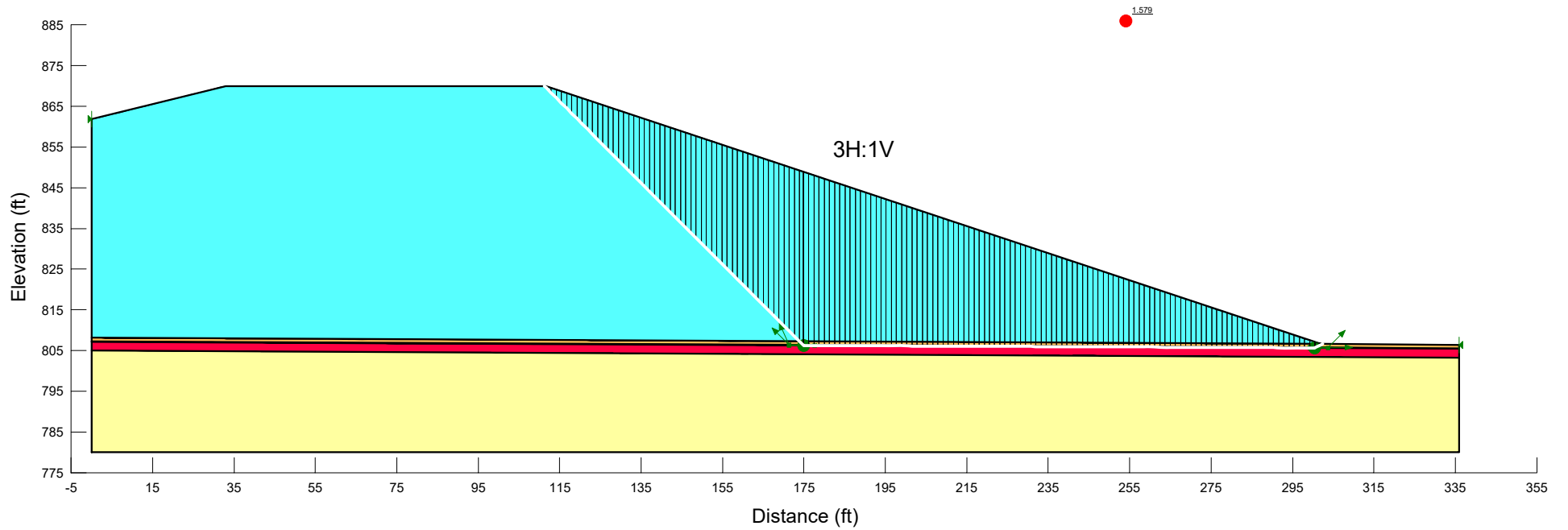
Slice 26	143.13428	851.60633	0	588.51773	246.1823	0
Slice 27	144.39238	851.00878	0	601.82911	251.75057	0
Slice 28	145.65049	850.41122	0	615.14049	257.31884	0
Slice 29	146.90859	849.81366	0	628.45187	262.88711	0
Slice 30	148.1667	849.2161	0	641.76325	268.45538	0
Slice 31	149.42481	848.61854	0	655.07463	274.02365	0
Slice 32	150.68291	848.02099	0	668.38601	279.59192	0
Slice 33	151.94102	847.42343	0	681.69739	285.1602	0
Slice 34	153.19913	846.82587	0	695.00877	290.72847	0
Slice 35	154.45723	846.22831	0	708.32015	296.29674	0
Slice 36	155.71534	845.63076	0	721.63153	301.86501	0
Slice 37	156.97344	845.0332	0	734.94291	307.43328	0
Slice 38	158.23155	844.43564	0	748.25429	313.00155	0
Slice 39	159.48966	843.83808	0	761.56567	318.56982	0
Slice 40	160.74776	843.24053	0	774.87705	324.13809	0
Slice 41	162.00587	842.64297	0	788.18843	329.70636	0
Slice 42	163.28072	842.05115	0	805.41636	336.91296	0
Slice 43	164.57233	841.46506	0	817.1082	341.80376	0
Slice 44	165.86394	840.87897	0	828.80004	346.69457	0
Slice 45	167.15555	840.29289	0	840.49189	351.58537	0
Slice 46	168.44716	839.7068	0	852.18373	356.47618	0
Slice 47	169.73877	839.12071	0	863.87557	361.36698	0
Slice 48	171.03038	838.53463	0	875.56742	366.25778	0
Slice 49	172.32199	837.94854	0	887.25926	371.14859	0
Slice 50	173.6136	837.36245	0	898.9511	376.03939	0
Slice 51	174.90521	836.77636	0	910.64295	380.9302	0
Slice	176.19682	836.19028	0	922.33479	385.821	0

52						
Slice 53	177.48843	835.60419	0	934.02663	390.7118	0
Slice 54	178.78004	835.0181	0	945.71848	395.60261	0
Slice 55	180.04425	834.46978	0	966.36152	404.23778	0
Slice 56	181.28106	833.95921	0	973.84146	407.36671	0
Slice 57	182.51788	833.44863	0	981.32141	410.49564	0
Slice 58	183.7547	832.93807	0	988.80136	413.62457	0
Slice 59	184.99151	832.4275	0	996.2813	416.7535	0
Slice 60	186.28858	831.93574	0	1,019.4282	426.43606	0
Slice 61	187.64588	831.46281	0	1,021.0319	427.10689	0
Slice 62	189.0032	830.98987	0	1,022.6355	427.77771	0
Slice 63	190.3605	830.51694	0	1,024.2392	428.44853	0
Slice 64	191.71782	830.04401	0	1,025.8428	429.11935	0
Slice 65	193.03417	829.5952	0	1,031.2415	431.37765	0
Slice 66	194.30958	829.17051	0	1,031.224	431.37034	0
Slice 67	195.58499	828.74582	0	1,031.2065	431.36302	0
Slice 68	196.8604	828.32113	0	1,031.189	431.35571	0
Slice 69	198.13581	827.89645	0	1,031.1715	431.3484	0
Slice 70	199.41122	827.47176	0	1,031.1541	431.34109	0
Slice 71	200.68662	827.04707	0	1,031.1366	431.33377	0
Slice 72	201.96203	826.62238	0	1,031.1191	431.32646	0
Slice 73	203.23744	826.19769	0	1,031.1016	431.31915	0
Slice 74	204.51285	825.77301	0	1,031.0841	431.31183	0
Slice 75	205.78826	825.34832	0	1,031.0666	431.30452	0
Slice 76	207.06366	824.92363	0	1,031.0492	431.29721	0
Slice 77	208.33907	824.49894	0	1,031.0317	431.2899	0
Slice 78	209.61448	824.07426	0	1,031.0142	431.28258	0

Slice 79	210.88989	823.64957	0	1,030.9967	431.27527	0
Slice 80	212.1653	823.22488	0	1,030.9792	431.26796	0
Slice 81	213.44071	822.80019	0	1,030.9618	431.26065	0
Slice 82	214.78558	822.3828	0	1,041.5881	435.70573	0
Slice 83	216.19992	821.9727	0	1,036.7818	433.69523	0
Slice 84	217.61425	821.56259	0	1,031.9755	431.68472	0
Slice 85	218.96492	821.1995	0	1,038.6881	434.49264	0
Slice 86	220.25192	820.88343	0	1,029.7049	430.73488	0
Slice 87	221.53892	820.56736	0	1,020.7216	426.97711	0
Slice 88	222.82591	820.25128	0	1,011.7384	423.21935	0
Slice 89	224.11291	819.93521	0	1,002.7552	419.46159	0
Slice 90	225.39991	819.61913	0	993.77197	415.70382	0
Slice 91	226.68691	819.30306	0	984.78875	411.94606	0
Slice 92	227.97391	818.98699	0	975.80553	408.18829	0
Slice 93	229.26091	818.67091	0	966.8223	404.43053	0
Slice 94	230.54791	818.35484	0	957.83908	400.67277	0
Slice 95	231.8349	818.03876	0	948.85585	396.915	0
Slice 96	233.1219	817.72269	0	939.87263	393.15724	0
Slice 97	234.4089	817.40662	0	930.88941	389.39947	0
Slice 98	235.68854	817.07255	0	915.05172	382.77443	0
Slice 99	236.96081	816.72049	0	909.38064	380.40216	0
Slice 100	238.23309	816.36842	0	903.70957	378.0299	0
Slice 101	239.50537	816.01636	0	898.03849	375.65764	0
Slice 102	240.77764	815.6643	0	892.36742	373.28538	0
Slice 103	242.04992	815.31224	0	886.69634	370.91311	0
Slice 104	243.32219	814.96018	0	881.02526	368.54085	0

Slice 105	244.59447	814.60811	0	875.35419	366.16859	0
Slice 106	245.86675	814.25605	0	869.68311	363.79633	0
Slice 107	247.13902	813.90399	0	864.01204	361.42406	0
Slice 108	248.4113	813.55193	0	858.34096	359.0518	0
Slice 109	249.68358	813.19986	0	852.66988	356.67954	0
Slice 110	250.95585	812.8478	0	846.99881	354.30728	0
Slice 111	252.25214	812.53777	0	856.00314	358.07387	0
Slice 112	253.57244	812.26977	0	842.12775	352.26967	0
Slice 113	254.89275	812.00176	0	828.25236	346.46547	0
Slice 114	256.2161	811.74951	0	819.12328	342.64669	0
Slice 115	257.54249	811.51301	0	802.41621	335.65797	0
Slice 116	258.86888	811.27652	0	785.70914	328.66925	0
Slice 117	260.19527	811.04002	0	769.00206	321.68053	0
Slice 118	261.52166	810.80352	0	752.29499	314.69181	0
Slice 119	262.84805	810.56702	0	735.58792	307.70309	0
Slice 120	264.17444	810.33052	0	718.88084	300.71437	0
Slice 121	265.50083	810.09403	0	702.17377	293.72565	0
Slice 122	266.82722	809.85753	0	685.4667	286.73693	0
Slice 123	268.1267	809.64225	0	673.0427	281.53986	0
Slice 124	269.39927	809.44819	0	654.19403	273.65529	0
Slice 125	270.67185	809.25414	0	635.34535	265.77072	0
Slice 126	271.94442	809.06008	0	616.49668	257.88615	0
Slice 127	273.217	808.86602	0	597.648	250.00157	0
Slice 128	274.48957	808.67196	0	578.79932	242.117	0
Slice 129	275.76215	808.47791	0	559.95065	234.23243	0
Slice 130	277.03472	808.28385	0	541.10197	226.34786	0
Slice	278.3073	808.08979	0	522.2533	218.46329	0

131						
Slice 132	279.57987	807.89573	0	503.40462	210.57871	0
Slice 133	280.85245	807.70168	0	484.55595	202.69414	0
Slice 134	282.12502	807.50762	0	465.70727	194.80957	0
Slice 135	283.34622	807.34941	0	451.95442	189.05663	0
Slice 136	284.51604	807.22705	0	429.7078	179.75067	0
Slice 137	285.68586	807.10469	0	407.46119	170.44471	0
Slice 138	286.85568	806.98234	0	385.21458	161.13875	0
Slice 139	288.0255	806.85998	0	362.96796	151.83279	0
Slice 140	289.19532	806.73762	0	340.72135	142.52683	0
Slice 141	290.3862	806.67262	0	322.98961	135.10948	0
Slice 142	291.59814	806.66499	0	288.9907	120.88743	0
Slice 143	292.81007	806.65736	0	254.9918	106.66538	0
Slice 144	294.02201	806.64973	0	220.99289	92.443328	0
Slice 145	295.23395	806.6421	0	186.99398	78.221278	0
Slice 146	296.44588	806.63447	0	152.99508	63.999227	0
Slice 147	297.65782	806.62684	0	118.99617	49.777177	0
Slice 148	298.86976	806.61921	0	84.997265	35.555126	0
Slice 149	300.08169	806.61158	0	50.998359	21.333076	0
Slice 150	301.29363	806.60395	0	16.999453	7.1110253	0



Color	Name	Model	Unit Weight (pcf)	Cohesion' (psf)	Phi' (°)
Cyan	CCR	Mohr-Coulomb	86	0	22.7
Red	Clay	Mohr-Coulomb	125	0	28
Orange	Drainage Layer	Mohr-Coulomb	115	0	30
Black	Geosynthetics	Mohr-Coulomb	58	0	24.3
Yellow	Subbase	Mohr-Coulomb	120	0	30

Title: Columbia Mod 10-11 Interim Waste Stage 2
Name: 3_Block
Method: Janbu
Last Edited By: Suchomel, Brandon

F of S: 1.579, F of S Rank (Analysis): 1 of 553,536 slip surfaces
Last Solved Date: 5/4/2022, Last Solved Time: 5:54:25 PM

3_Block

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File Information

File Version: 8.16
Title: Columbia Mod 10-11 Interim Waste Stage 2
Created By: Suchomel, Brandon
Last Edited By: Suchomel, Brandon
Revision Number: 59
Date: 5/4/2022
Time: 5:51:08 PM
Tool Version: 8.16.3.14580
File Name: Columbia Mod 10-11 Interim Waste Stage 2.gsz
Directory: I:\25220183.00\Data and Calculations_Issued for Permitting POO Geotech Calculations\Slope Stability\
Last Solved Date: 5/4/2022
Last Solved Time: 5:54:25 PM

Project Settings

Length(L) Units: Feet
Time(t) Units: Seconds
Force(F) Units: Pounds
Pressure(p) Units: psf
Strength Units: psf
Unit Weight of Water: 62.4 pcf
View: 2D
Element Thickness: 1

Analysis Settings

3_Block

Kind: SLOPE/W
Method: Janbu
Settings
 PWP Conditions Source: (none)
Slip Surface
 Direction of movement: Left to Right
 Use Passive Mode: No
 Slip Surface Option: Block
 Critical slip surfaces saved: 10
 Resisting Side Maximum Convex Angle: 1 °
 Driving Side Maximum Convex Angle: 5 °
 Restrict Block Crossing: No
 Optimize Critical Slip Surface Location: No
 Tension Crack
 Tension Crack Option: (none)
F of S Distribution
 F of S Calculation Option: Constant
Advanced

Number of Slices: 150
F of S Tolerance: 0.001
Minimum Slip Surface Depth: 0.1 ft

Materials

CCR

Model: Mohr-Coulomb
Unit Weight: 86 pcf
Cohesion': 0 psf
Phi': 22.7 °
Phi-B: 0 °

Clay

Model: Mohr-Coulomb
Unit Weight: 125 pcf
Cohesion': 0 psf
Phi': 28 °
Phi-B: 0 °

Drainage Layer

Model: Mohr-Coulomb
Unit Weight: 115 pcf
Cohesion': 0 psf
Phi': 30 °
Phi-B: 0 °

Geosynthetics

Model: Mohr-Coulomb
Unit Weight: 58 pcf
Cohesion': 0 psf
Phi': 24.3 °
Phi-B: 0 °

Subbase

Model: Mohr-Coulomb
Unit Weight: 120 pcf
Cohesion': 0 psf
Phi': 30 °
Phi-B: 0 °

Slip Surface Limits

Left Coordinate: (0, 861.8) ft
Right Coordinate: (335.9, 806.4) ft

Slip Surface Block

Left Grid
Upper Left: (171.41, 806.37) ft
Lower Left: (171.41, 806.24) ft
Lower Right: (177.59, 806.22) ft

X Increments: 30
 Y Increments: 3
 Starting Angle: 115 °
 Ending Angle: 135 °
 Angle Increments: 5

Right Grid

Upper Left: (299.3, 805.73) ft
 Lower Left: (299.3, 805.62) ft
 Lower Right: (303.71, 805.6) ft
 X Increments: 30
 Y Increments: 3
 Starting Angle: 0 °
 Ending Angle: 45 °
 Angle Increments: 5

Points

	X (ft)	Y (ft)
Point 1	0	780
Point 2	335.9	780
Point 3	0	805
Point 4	335.9	803.3
Point 5	0	807.1
Point 6	335.9	805.4
Point 7	0	808.1
Point 8	335.9	806.4
Point 9	0	861.8
Point 10	33	870
Point 11	111.6	870
Point 12	305	805.6
Point 13	301.9	806.6
Point 14	0	807.2
Point 15	305	805.7
Point 16	335.9	805.5

Regions

	Material	Points	Area (ft ²)
Region 1	Subbase	1,2,4,3	8,112
Region 2	Clay	3,5,12,6,4	712.72
Region 3	CCR	7,9,10,11,13	12,746
Region 4	Geosynthetics	5,14,15,16,6,12	33.59
Region 5	Drainage Layer	14,7,13,8,16,15	299.67

Current Slip Surface

Slip Surface: 218,230
 F of S: 1.579
 Volume: 4,130.1925 ft³
 Weight: 358,224.99 lbs

Resisting Force: 147,760.65 lbs
 Activating Force: 93,577.095 lbs
 F of S Rank (Analysis): 1 of 553,536 slip surfaces
 F of S Rank (Query): 1 of 553,536 slip surfaces
 Exit: (302.33287, 806.59745) ft
 Entry: (111.184, 870) ft
 Radius: 102.0734 ft
 Center: (222.53102, 885.85064) ft

Slip Slices

	X (ft)	Y (ft)	PWP (psf)	Base Normal Stress (psf)	Frictional Strength (psf)	Cohesive Strength (psf)
Slice 1	111.392	869.792	0	14.140131	5.9149449	0
Slice 2	112.23621	868.94779	0	57.121324	23.894367	0
Slice 3	113.50862	867.67538	0	114.80345	48.023322	0
Slice 4	114.78103	866.40297	0	172.48557	72.152277	0
Slice 5	116.05345	865.13055	0	230.16769	96.281232	0
Slice 6	117.32586	863.85814	0	287.84982	120.41019	0
Slice 7	118.59827	862.58573	0	345.53194	144.53914	0
Slice 8	119.87069	861.31331	0	403.21406	168.6681	0
Slice 9	121.1431	860.0409	0	460.89619	192.79705	0
Slice 10	122.41552	858.76848	0	518.57831	216.92601	0
Slice 11	123.68793	857.49607	0	576.26043	241.05496	0
Slice 12	124.96034	856.22366	0	633.94256	265.18392	0
Slice 13	126.23276	854.95124	0	691.62468	289.31287	0
Slice 14	127.50517	853.67883	0	749.30681	313.44183	0
Slice 15	128.77758	852.40642	0	806.98893	337.57078	0
Slice 16	130.05	851.134	0	864.67105	361.69974	0
Slice 17	131.32241	849.86159	0	922.35318	385.82869	0
Slice 18	132.59482	848.58918	0	980.0353	409.95765	0
Slice 19	133.86724	847.31676	0	1,037.7174	434.0866	0
Slice 20	135.13965	846.04435	0	1,095.3995	458.21556	0
Slice 21	136.41207	844.77193	0	1,153.0817	482.34451	0
Slice 22	137.68448	843.49952	0	1,210.7638	506.47347	0
Slice 23	138.95689	842.22711	0	1,268.4459	530.60242	0
Slice 24	140.22931	840.95469	0	1,326.128	554.73138	0
Slice	141.50172	839.68228	0	1,383.8102	578.86033	0

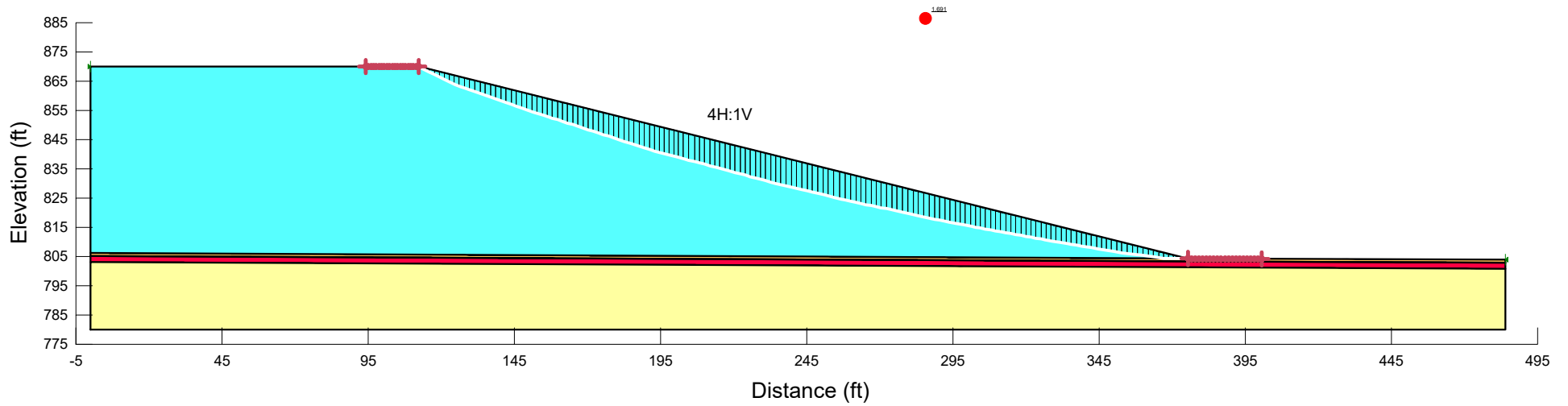
25						
Slice 26	142.77413	838.40987	0	1,441.4923	602.98929	0
Slice 27	144.04655	837.13745	0	1,499.1744	627.11824	0
Slice 28	145.31896	835.86504	0	1,556.8565	651.2472	0
Slice 29	146.59137	834.59263	0	1,614.5387	675.37615	0
Slice 30	147.86379	833.32021	0	1,672.2208	699.50511	0
Slice 31	149.1362	832.0478	0	1,729.9029	723.63406	0
Slice 32	150.40862	830.77538	0	1,787.585	747.76302	0
Slice 33	151.68103	829.50297	0	1,845.2672	771.89197	0
Slice 34	152.95344	828.23056	0	1,902.9493	796.02093	0
Slice 35	154.22586	826.95814	0	1,960.6314	820.14988	0
Slice 36	155.49827	825.68573	0	2,018.3135	844.27884	0
Slice 37	156.77068	824.41332	0	2,075.9956	868.40779	0
Slice 38	158.0431	823.1409	0	2,133.6778	892.53674	0
Slice 39	159.31551	821.86849	0	2,191.3599	916.6657	0
Slice 40	160.58792	820.59608	0	2,249.042	940.79465	0
Slice 41	161.86034	819.32366	0	2,306.7241	964.92361	0
Slice 42	163.13275	818.05125	0	2,364.4063	989.05256	0
Slice 43	164.40517	816.77883	0	2,422.0884	1,013.1815	0
Slice 44	165.67758	815.50642	0	2,479.7705	1,037.3105	0
Slice 45	166.94999	814.23401	0	2,537.4526	1,061.4394	0
Slice 46	168.22241	812.96159	0	2,595.1348	1,085.5684	0
Slice 47	169.49482	811.68918	0	2,652.8169	1,109.6973	0
Slice 48	170.76723	810.41677	0	2,710.499	1,133.8263	0
Slice 49	172.03965	809.14435	0	2,768.1811	1,157.9552	0
Slice 50	173.31206	807.87194	0	2,825.8633	1,182.0842	0
Slice 51	174.39608	806.78792	0	2,672.3431	1,542.878	0

Slice 52	174.87794	806.30606	0	2,868.8112	1,295.3179	0
Slice 53	175.54616	806.26887	0	3,667.4758	1,655.9288	0
Slice 54	176.81448	806.2626	0	3,631.7233	1,639.786	0
Slice 55	178.08281	806.25633	0	3,595.9708	1,623.6431	0
Slice 56	179.35113	806.25006	0	3,560.2183	1,607.5002	0
Slice 57	180.61945	806.24379	0	3,524.4658	1,591.3573	0
Slice 58	181.88778	806.23752	0	3,488.7133	1,575.2144	0
Slice 59	183.1561	806.23125	0	3,452.9608	1,559.0716	0
Slice 60	184.42442	806.22498	0	3,417.2082	1,542.9287	0
Slice 61	185.69275	806.21871	0	3,381.4557	1,526.7858	0
Slice 62	186.96107	806.21244	0	3,345.7032	1,510.6429	0
Slice 63	188.22939	806.20617	0	3,309.9507	1,494.5001	0
Slice 64	189.49772	806.1999	0	3,274.1982	1,478.3572	0
Slice 65	190.76604	806.19363	0	3,238.4457	1,462.2143	0
Slice 66	192.03436	806.18736	0	3,202.6932	1,446.0714	0
Slice 67	193.30269	806.18109	0	3,166.9407	1,429.9285	0
Slice 68	194.57101	806.17482	0	3,131.1881	1,413.7857	0
Slice 69	195.83933	806.16856	0	3,095.4356	1,397.6428	0
Slice 70	197.10766	806.16229	0	3,059.6831	1,381.4999	0
Slice 71	198.37598	806.15602	0	3,023.9306	1,365.357	0
Slice 72	199.6443	806.14975	0	2,988.1781	1,349.2141	0
Slice 73	200.91263	806.14348	0	2,952.4256	1,333.0713	0
Slice 74	202.18095	806.13721	0	2,916.6731	1,316.9284	0
Slice 75	203.44927	806.13094	0	2,880.9205	1,300.7855	0
Slice 76	204.7176	806.12467	0	2,845.168	1,284.6426	0
Slice 77	205.98592	806.1184	0	2,809.4155	1,268.4997	0

Slice 78	207.25424	806.11213	0	2,773.663	1,252.3569	0
Slice 79	208.52257	806.10586	0	2,737.9105	1,236.214	0
Slice 80	209.79089	806.09959	0	2,702.158	1,220.0711	0
Slice 81	211.05921	806.09332	0	2,666.4055	1,203.9282	0
Slice 82	212.32754	806.08705	0	2,630.653	1,187.7854	0
Slice 83	213.59586	806.08078	0	2,594.9004	1,171.6425	0
Slice 84	214.86418	806.07452	0	2,559.1479	1,155.4996	0
Slice 85	216.13251	806.06825	0	2,523.3954	1,139.3567	0
Slice 86	217.40083	806.06198	0	2,487.6429	1,123.2138	0
Slice 87	218.66915	806.05571	0	2,451.8904	1,107.071	0
Slice 88	219.93747	806.04944	0	2,416.1379	1,090.9281	0
Slice 89	221.2058	806.04317	0	2,380.3854	1,074.7852	0
Slice 90	222.47412	806.0369	0	2,344.6328	1,058.6423	0
Slice 91	223.74244	806.03063	0	2,308.8803	1,042.4994	0
Slice 92	225.01077	806.02436	0	2,273.1278	1,026.3566	0
Slice 93	226.27909	806.01809	0	2,237.3753	1,010.2137	0
Slice 94	227.54741	806.01182	0	2,201.6228	994.07081	0
Slice 95	228.81574	806.00555	0	2,165.8703	977.92793	0
Slice 96	230.08406	805.99928	0	2,130.1178	961.78505	0
Slice 97	231.35238	805.99301	0	2,094.3653	945.64217	0
Slice 98	232.62071	805.98674	0	2,058.6127	929.49929	0
Slice 99	233.88903	805.98047	0	2,022.8602	913.35641	0
Slice 100	235.15735	805.97421	0	1,987.1077	897.21353	0
Slice 101	236.42568	805.96794	0	1,951.3552	881.07066	0
Slice 102	237.694	805.96167	0	1,915.6027	864.92778	0
Slice 103	238.96232	805.9554	0	1,879.8502	848.7849	0
Slice	240.23065	805.94913	0	1,844.0977	832.64202	0

104						
Slice 105	241.49897	805.94286	0	1,808.3451	816.49914	0
Slice 106	242.76729	805.93659	0	1,772.5926	800.35626	0
Slice 107	244.03562	805.93032	0	1,736.8401	784.21338	0
Slice 108	245.30394	805.92405	0	1,701.0876	768.0705	0
Slice 109	246.57226	805.91778	0	1,665.3351	751.92762	0
Slice 110	247.84059	805.91151	0	1,629.5826	735.78475	0
Slice 111	249.10891	805.90524	0	1,593.8301	719.64187	0
Slice 112	250.37723	805.89897	0	1,558.0775	703.49899	0
Slice 113	251.64556	805.8927	0	1,522.325	687.35611	0
Slice 114	252.91388	805.88643	0	1,486.5725	671.21323	0
Slice 115	254.1822	805.88017	0	1,450.82	655.07035	0
Slice 116	255.45053	805.8739	0	1,415.0675	638.92747	0
Slice 117	256.71885	805.86763	0	1,379.315	622.78459	0
Slice 118	257.98717	805.86136	0	1,343.5625	606.64172	0
Slice 119	259.25549	805.85509	0	1,307.81	590.49884	0
Slice 120	260.52382	805.84882	0	1,272.0574	574.35596	0
Slice 121	261.79214	805.84255	0	1,236.3049	558.21308	0
Slice 122	263.06046	805.83628	0	1,200.5524	542.0702	0
Slice 123	264.32879	805.83001	0	1,164.7999	525.92732	0
Slice 124	265.59711	805.82374	0	1,129.0474	509.78444	0
Slice 125	266.86543	805.81747	0	1,093.2949	493.64156	0
Slice 126	268.13376	805.8112	0	1,057.5424	477.49868	0
Slice 127	269.40208	805.80493	0	1,021.7898	461.35581	0
Slice 128	270.6704	805.79866	0	986.03733	445.21293	0
Slice 129	271.93873	805.79239	0	950.28482	429.07005	0
Slice 130	273.20705	805.78612	0	914.53231	412.92717	0

Slice 131	274.47537	805.77986	0	878.77979	396.78429	0
Slice 132	275.7437	805.77359	0	843.02728	380.64141	0
Slice 133	277.01202	805.76732	0	807.27476	364.49853	0
Slice 134	278.28034	805.76105	0	771.52225	348.35565	0
Slice 135	279.54867	805.75478	0	735.76974	332.21277	0
Slice 136	280.81699	805.74851	0	700.01722	316.0699	0
Slice 137	282.08531	805.74224	0	664.26471	299.92702	0
Slice 138	283.35364	805.73597	0	628.5122	283.78414	0
Slice 139	284.62196	805.7297	0	592.75968	267.64126	0
Slice 140	285.89028	805.72343	0	557.00717	251.49838	0
Slice 141	287.15861	805.71716	0	521.25466	235.3555	0
Slice 142	288.42693	805.71089	0	485.50214	219.21262	0
Slice 143	289.69525	805.70462	0	449.74963	203.06974	0
Slice 144	290.96358	805.69835	0	413.99712	186.92687	0
Slice 145	292.2319	805.69208	0	378.2446	170.78399	0
Slice 146	293.50022	805.68581	0	342.49209	154.64111	0
Slice 147	294.76855	805.67955	0	306.73958	138.49823	0
Slice 148	296.03687	805.67328	0	270.98706	122.35535	0
Slice 149	297.30519	805.66701	0	235.23455	106.21247	0
Slice 150	298.57352	805.66074	0	199.48204	90.069593	0
Slice 151	299.84184	805.65447	0	163.72952	73.926714	0
Slice 152	300.54492	805.68645	0	166.29893	75.086847	0
Slice 153	301.25692	806.04923	0	100.60907	58.086672	0
Slice 154	302.11643	806.48718	0	15.767383	9.1033026	0



Color	Name	Model	Unit Weight (pcf)	Cohesion' (psf)	Phi' (°)
■	CCR	Mohr-Coulomb	86	0	22.7
■	Clay	Mohr-Coulomb	125	0	28
■	Drainage Layer	Mohr-Coulomb	115	0	30
■	Geosynthetics	Mohr-Coulomb	58	0	24.3
■	Subbase	Mohr-Coulomb	120	0	30

Title: Columbia Mod 10-11 Interim Waste Stage 3
Name: 2-1_Optimized Circular_Forced Full Slope
Method: Bishop
Last Edited By: Suchomel, Brandon

F of S: 1.691, F of S Rank (Analysis): 1 of 3,970 slip surfaces
Last Solved Date: 5/4/2022, Last Solved Time: 5:59:59 PM

2-1_Optimized Circular_Forced Full Slope

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File Information

File Version: 8.16
Title: Columbia Mod 10-11 Interim Waste Stage 3
Created By: Suchomel, Brandon
Last Edited By: Suchomel, Brandon
Revision Number: 50
Date: 5/4/2022
Time: 5:59:45 PM
Tool Version: 8.16.3.14580
File Name: Columbia Mod 10-11 Interim Waste Stage 3.gsz
Directory: I:\25220183.00\Data and Calculations_Issued for Permitting POO Geotech Calculations\Slope Stability\
Last Solved Date: 5/4/2022
Last Solved Time: 5:59:59 PM

Project Settings

Length(L) Units: Feet
Time(t) Units: Seconds
Force(F) Units: Pounds
Pressure(p) Units: psf
Strength Units: psf
Unit Weight of Water: 62.4 pcf
View: 2D
Element Thickness: 1

Analysis Settings

2-1_Optimized Circular_Forced Full Slope

Kind: SLOPE/W
Method: Bishop
Settings
 PWP Conditions Source: (none)
Slip Surface
 Direction of movement: Left to Right
 Use Passive Mode: No
 Slip Surface Option: Entry and Exit
 Critical slip surfaces saved: 10
 Resisting Side Maximum Convex Angle: 1 °
 Driving Side Maximum Convex Angle: 5 °
 Optimize Critical Slip Surface Location: Yes
 Critical Slip Surface Optimizations
 Maximum Iterations: 2,000
 Convergence Tolerance: 1e-007
 Starting Points: 8
 Ending Points: 16
 Complete Passes per Insertion: 1

Tension Crack

Tension Crack Option: (none)

F of S Distribution

F of S Calculation Option: Constant

Advanced

Number of Slices: 150

F of S Tolerance: 0.001

Minimum Slip Surface Depth: 0.1 ft

Materials

CCR

Model: Mohr-Coulomb

Unit Weight: 86 pcf

Cohesion': 0 psf

Phi': 22.7 °

Phi-B: 0 °

Clay

Model: Mohr-Coulomb

Unit Weight: 125 pcf

Cohesion': 0 psf

Phi': 28 °

Phi-B: 0 °

Drainage Layer

Model: Mohr-Coulomb

Unit Weight: 115 pcf

Cohesion': 0 psf

Phi': 30 °

Phi-B: 0 °

Geosynthetics

Model: Mohr-Coulomb

Unit Weight: 58 pcf

Cohesion': 0 psf

Phi': 24.3 °

Phi-B: 0 °

Subbase

Model: Mohr-Coulomb

Unit Weight: 120 pcf

Cohesion': 0 psf

Phi': 30 °

Phi-B: 0 °

Slip Surface Entry and Exit

Left Projection: Range

Left-Zone Left Coordinate: (94.1, 870) ft

Left-Zone Right Coordinate: (112.23, 870) ft

Left-Zone Increment: 20

Right Projection: Range
 Right-Zone Left Coordinate: (375.32, 804.29919) ft
 Right-Zone Right Coordinate: (400.59, 804.20629) ft
 Right-Zone Increment: 20
 Radius Increments: 8

Slip Surface Limits

Left Coordinate: (0, 870) ft
 Right Coordinate: (483.9, 803.9) ft

Points

	X (ft)	Y (ft)
Point 1	0	780
Point 2	483.9	780
Point 3	0	805.2
Point 4	483.9	802.9
Point 5	483.9	800.9
Point 6	0	803.2
Point 7	0	870
Point 8	112.5	870
Point 9	379.2	803.3
Point 10	0	806.2
Point 11	375.1	804.3
Point 12	483.9	803.9
Point 13	0	805.3
Point 14	483.9	803
Point 15	379.2	803.4

Regions

	Material	Points	Area (ft ²)
Region 1	Subbase	1,6,5,2	10,670
Region 2	Clay	6,3,9,4,5	944.17
Region 3	Geosynthetics	3,13,15,14,4,9	48.39
Region 4	Drainage Layer	13,10,11,12,14,15	430.8
Region 5	CCR	10,7,8,11	15,661

Current Slip Surface

Slip Surface: 3,970
 F of S: 1.691
 Volume: 1,735.9578 ft³
 Weight: 149,292.37 lbs
 Resisting Moment: 32,761,608 lbs-ft
 Activating Moment: 19,375,797 lbs-ft
 F of S Rank (Analysis): 1 of 3,970 slip surfaces
 F of S Rank (Query): 1 of 3,970 slip surfaces
 Exit: (375.08152, 804.30462) ft

Entry: (112.07755, 870) ft

Radius: 116.45652 ft

Center: (372.09783, 1,350.7512) ft

Slip Slices

	X (ft)	Y (ft)	PWP (psf)	Base Normal Stress (psf)	Frictional Strength (psf)	Cohesive Strength (psf)
Slice 1	112.28878	869.89648	0	7.9403998	3.3215412	0
Slice 2	113.34107	869.38075	0	31.358062	13.117361	0
Slice 3	115.0232	868.55634	0	62.312587	26.06592	0
Slice 4	116.70533	867.73193	0	93.267112	39.014478	0
Slice 5	118.38746	866.90752	0	124.22164	51.963036	0
Slice 6	120.06959	866.08311	0	155.17616	64.911595	0
Slice 7	121.75172	865.2587	0	186.13069	77.860153	0
Slice 8	123.43385	864.43429	0	217.08521	90.808711	0
Slice 9	125.16346	863.70958	0	247.02114	103.33118	0
Slice 10	126.94057	863.08457	0	261.29339	109.30139	0
Slice 11	128.71767	862.45957	0	275.56565	115.27161	0
Slice 12	130.49477	861.83457	0	289.8379	121.24182	0
Slice 13	132.27188	861.20956	0	304.11016	127.21203	0
Slice 14	134.04898	860.58456	0	318.38241	133.18225	0
Slice 15	135.82609	859.95955	0	332.65466	139.15246	0
Slice 16	137.60319	859.33455	0	346.92692	145.12267	0
Slice 17	139.38029	858.70955	0	361.19917	151.09289	0
Slice 18	141.1574	858.08454	0	375.47143	157.0631	0
Slice 19	142.9345	857.45954	0	389.74368	163.03331	0
Slice 20	144.71161	856.83453	0	404.01594	169.00353	0
Slice 21	146.48871	856.20953	0	418.28819	174.97374	0
Slice 22	148.26581	855.58453	0	432.56045	180.94395	0
Slice 23	150.04292	854.95952	0	446.8327	186.91417	0
Slice 24	151.80489	854.36508	0	462.02398	193.26882	0
Slice 25	153.55174	853.8012	0	472.12555	197.49439	0
Slice 26	155.29858	853.23732	0	482.22711	201.71997	0
Slice 27	157.04543	852.67344	0	492.32868	205.94555	0

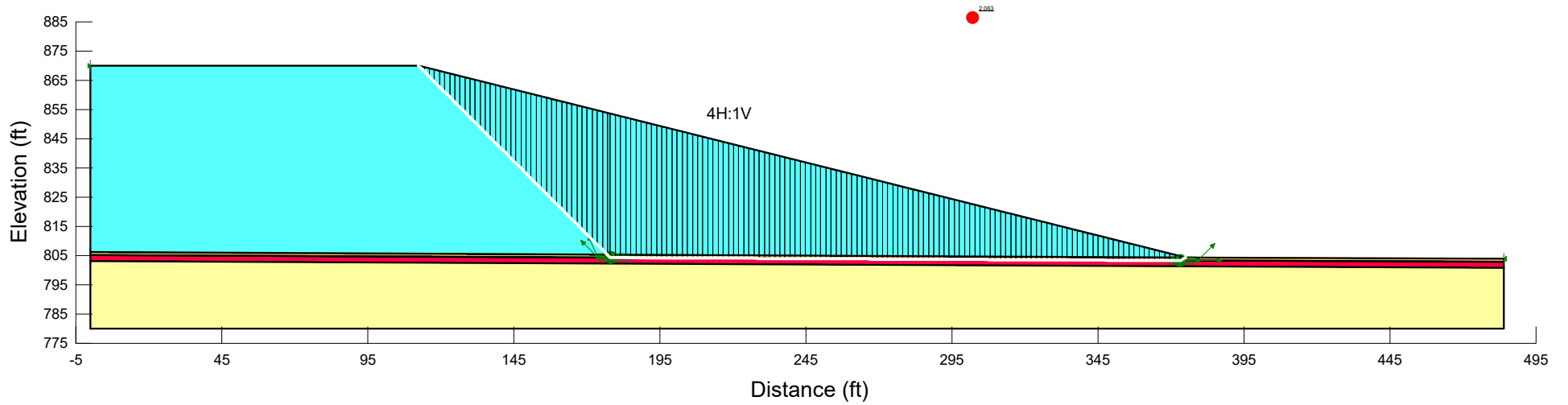
Slice 28	158.79227	852.10956	0	502.43025	210.17112	0
Slice 29	160.53912	851.54568	0	512.53181	214.3967	0
Slice 30	162.28596	850.9818	0	522.63338	218.62228	0
Slice 31	164.03281	850.41792	0	532.73495	222.84786	0
Slice 32	165.77965	849.85404	0	542.83651	227.07343	0
Slice 33	167.5265	849.29016	0	552.93808	231.29901	0
Slice 34	169.27334	848.72628	0	563.03965	235.52459	0
Slice 35	171.02019	848.1624	0	573.14121	239.75016	0
Slice 36	172.76703	847.59852	0	583.24278	243.97574	0
Slice 37	174.51388	847.03464	0	593.34435	248.20132	0
Slice 38	176.26072	846.47076	0	603.44591	252.42689	0
Slice 39	178.00757	845.90688	0	613.54748	256.65247	0
Slice 40	179.75441	845.343	0	623.64905	260.87805	0
Slice 41	181.50126	844.77912	0	633.75061	265.10362	0
Slice 42	183.2481	844.21524	0	643.85218	269.3292	0
Slice 43	184.99495	843.65136	0	653.95374	273.55478	0
Slice 44	186.74179	843.08748	0	664.05531	277.78035	0
Slice 45	188.48864	842.5236	0	674.15688	282.00593	0
Slice 46	190.23548	841.95972	0	684.25844	286.23151	0
Slice 47	191.98233	841.39584	0	694.36001	290.45708	0
Slice 48	193.67524	840.89879	0	710.01929	297.0075	0
Slice 49	195.31421	840.46857	0	711.64781	297.68873	0
Slice 50	196.95319	840.03835	0	713.27633	298.36995	0
Slice 51	198.59217	839.60812	0	714.90485	299.05118	0
Slice 52	200.23115	839.1779	0	716.53337	299.7324	0
Slice 53	201.87012	838.74768	0	718.16189	300.41362	0
Slice	203.64843	838.28605	0	720.41291	301.35525	0

54						
Slice 55	205.56608	837.79301	0	721.48539	301.80388	0
Slice 56	207.39225	837.31305	0	721.33214	301.73977	0
Slice 57	209.12696	836.84616	0	723.98333	302.84879	0
Slice 58	210.86167	836.37927	0	726.63452	303.95781	0
Slice 59	212.59638	835.91239	0	729.28571	305.06682	0
Slice 60	214.33109	835.4455	0	731.9369	306.17584	0
Slice 61	216.0658	834.97861	0	734.5881	307.28486	0
Slice 62	217.80051	834.51172	0	737.23929	308.39387	0
Slice 63	219.53522	834.04484	0	739.89048	309.50289	0
Slice 64	221.26993	833.57795	0	742.54167	310.61191	0
Slice 65	223.00463	833.11106	0	745.19286	311.72093	0
Slice 66	224.73934	832.64418	0	747.84405	312.82994	0
Slice 67	226.47405	832.17729	0	750.49524	313.93896	0
Slice 68	228.20876	831.7104	0	753.14643	315.04798	0
Slice 69	229.94347	831.24351	0	755.79762	316.15699	0
Slice 70	231.67818	830.77663	0	758.44881	317.26601	0
Slice 71	233.41289	830.30974	0	761.1	318.37503	0
Slice 72	235.1476	829.84285	0	763.7512	319.48405	0
Slice 73	236.91982	829.39551	0	769.91705	322.06328	0
Slice 74	238.72955	828.96771	0	767.88747	321.21429	0
Slice 75	240.53929	828.53991	0	765.85789	320.36529	0
Slice 76	242.34902	828.11211	0	763.82831	319.5163	0
Slice 77	244.15876	827.68431	0	761.79873	318.66731	0
Slice 78	245.96849	827.25652	0	759.76915	317.81832	0
Slice 79	247.77822	826.82872	0	757.73957	316.96933	0
Slice 80	249.58796	826.40092	0	755.70999	316.12033	0

Slice 81	251.39769	825.97312	0	753.68041	315.27134	0
Slice 82	253.24754	825.53553	0	751.57388	314.39017	0
Slice 83	255.1375	825.08816	0	749.50415	313.52438	0
Slice 84	257.02745	824.64079	0	747.43443	312.65859	0
Slice 85	258.91741	824.19341	0	745.3647	311.79281	0
Slice 86	260.80737	823.74604	0	743.29497	310.92702	0
Slice 87	262.61573	823.34871	0	745.01303	311.6457	0
Slice 88	264.34249	823.00144	0	738.07047	308.74157	0
Slice 89	266.06925	822.65416	0	731.12791	305.83743	0
Slice 90	267.796	822.30688	0	724.18534	302.93329	0
Slice 91	269.52276	821.95961	0	717.24278	300.02915	0
Slice 92	271.29595	821.58763	0	708.55328	296.39426	0
Slice 93	273.11557	821.19094	0	703.77422	294.39513	0
Slice 94	274.9352	820.79426	0	698.99516	292.39601	0
Slice 95	276.75482	820.39757	0	694.2161	290.39688	0
Slice 96	278.57444	820.00088	0	689.43703	288.39776	0
Slice 97	280.39406	819.6042	0	684.65797	286.39863	0
Slice 98	282.21369	819.20751	0	679.87891	284.39951	0
Slice 99	284.03331	818.81083	0	675.09985	282.40038	0
Slice 100	285.85293	818.41414	0	670.32079	280.40126	0
Slice 101	287.67255	818.01745	0	665.54172	278.40213	0
Slice 102	289.49218	817.62077	0	660.76266	276.40301	0
Slice 103	291.3118	817.22408	0	655.9836	274.40388	0
Slice 104	293.09319	816.86859	0	654.41264	273.74674	0
Slice 105	294.83634	816.5543	0	644.38282	269.55117	0
Slice 106	296.57151	816.23752	0	634.04049	265.22488	0

Slice 107	298.2987	815.91827	0	624.75774	261.34183	0
Slice 108	300.02589	815.59902	0	615.475	257.45877	0
Slice 109	301.75308	815.27976	0	606.19225	253.57571	0
Slice 110	303.48026	814.96051	0	596.9095	249.69265	0
Slice 111	305.20745	814.64126	0	587.62675	245.8096	0
Slice 112	306.93464	814.322	0	578.34401	241.92654	0
Slice 113	308.66183	814.00275	0	569.06126	238.04348	0
Slice 114	310.38901	813.6835	0	559.77851	234.16042	0
Slice 115	312.1162	813.36425	0	550.49577	230.27737	0
Slice 116	313.84339	813.04499	0	541.21302	226.39431	0
Slice 117	315.57058	812.72574	0	531.93027	222.51125	0
Slice 118	317.29776	812.40649	0	522.64752	218.62819	0
Slice 119	319.02495	812.08723	0	513.36478	214.74514	0
Slice 120	320.75214	811.76798	0	504.08203	210.86208	0
Slice 121	322.47933	811.44873	0	494.79928	206.97902	0
Slice 122	324.20393	811.14243	0	486.17056	203.36955	0
Slice 123	325.92595	810.8491	0	474.82366	198.62304	0
Slice 124	327.64797	810.55576	0	463.47676	193.87653	0
Slice 125	329.36999	810.26243	0	452.12985	189.13001	0
Slice 126	331.09201	809.9691	0	440.78295	184.3835	0
Slice 127	332.81403	809.67576	0	429.43605	179.63699	0
Slice 128	334.53605	809.38243	0	418.08915	174.89048	0
Slice 129	336.25807	809.08909	0	406.74225	170.14397	0
Slice 130	337.98009	808.79576	0	395.39534	165.39746	0
Slice 131	339.70211	808.50242	0	384.04844	160.65094	0
Slice 132	341.42413	808.20909	0	372.70154	155.90443	0
Slice	343.14615	807.91575	0	361.35464	151.15792	0

133						
Slice 134	344.86817	807.62242	0	350.00774	146.41141	0
Slice 135	346.59019	807.32909	0	338.66084	141.6649	0
Slice 136	348.31221	807.03575	0	327.31393	136.91838	0
Slice 137	350.03423	806.74242	0	315.96703	132.17187	0
Slice 138	351.79639	806.47788	0	304.26993	127.27887	0
Slice 139	353.5987	806.24214	0	286.34431	119.78042	0
Slice 140	355.40101	806.0064	0	268.4187	112.28197	0
Slice 141	357.20332	805.77066	0	250.49308	104.78352	0
Slice 142	359.00563	805.53491	0	232.56746	97.285077	0
Slice 143	360.80794	805.29917	0	214.64184	89.786628	0
Slice 144	362.61025	805.06343	0	196.71623	82.28818	0
Slice 145	364.41256	804.82769	0	178.79061	74.789732	0
Slice 146	366.21487	804.59195	0	160.86499	67.291283	0
Slice 147	367.91257	804.45713	0	140.3953	58.728628	0
Slice 148	369.50567	804.42324	0	109.19635	45.677822	0
Slice 149	371.09877	804.38935	0	77.997391	32.627016	0
Slice 150	372.69187	804.35546	0	46.798435	19.576209	0
Slice 151	374.28497	804.32157	0	15.599478	6.5254031	0



Color	Name	Model	Unit Weight (pcf)	Cohesion' (psf)	Phi' (°)
Cyan	CCR	Mohr-Coulomb	86	0	22.7
Red	Clay	Mohr-Coulomb	125	0	28
Orange	Drainage Layer	Mohr-Coulomb	115	0	30
Black	Geosynthetics	Mohr-Coulomb	58	0	24.3
Yellow	Subbase	Mohr-Coulomb	120	0	30

Title: Columbia Mod 10-11 Interim Waste Stage 3
 Name: 3_Block
 Method: Janbu
 Last Edited By: Suchomel, Brandon

F of S: 2.063, F of S Rank (Analysis): 1 of 147,456 slip surfaces
 Last Solved Date: 5/4/2022, Last Solved Time: 6:00:41 PM

3_Block

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File Information

File Version: 8.16
Title: Columbia Mod 10-11 Interim Waste Stage 3
Created By: Suchomel, Brandon
Last Edited By: Suchomel, Brandon
Revision Number: 50
Date: 5/4/2022
Time: 5:59:45 PM
Tool Version: 8.16.3.14580
File Name: Columbia Mod 10-11 Interim Waste Stage 3.gsz
Directory: I:\25220183.00\Data and Calculations_Issued for Permitting POO Geotech Calculations\Slope Stability\
Last Solved Date: 5/4/2022
Last Solved Time: 6:00:41 PM

Project Settings

Length(L) Units: Feet
Time(t) Units: Seconds
Force(F) Units: Pounds
Pressure(p) Units: psf
Strength Units: psf
Unit Weight of Water: 62.4 pcf
View: 2D
Element Thickness: 1

Analysis Settings

3_Block

Kind: SLOPE/W
Method: Janbu
Settings
 PWP Conditions Source: (none)
Slip Surface
 Direction of movement: Left to Right
 Use Passive Mode: No
 Slip Surface Option: Block
 Critical slip surfaces saved: 10
 Resisting Side Maximum Convex Angle: 1 °
 Driving Side Maximum Convex Angle: 5 °
 Restrict Block Crossing: No
 Optimize Critical Slip Surface Location: No
 Tension Crack
 Tension Crack Option: (none)
F of S Distribution
 F of S Calculation Option: Constant
Advanced

Number of Slices: 150
F of S Tolerance: 0.001
Minimum Slip Surface Depth: 0.1 ft

Materials

CCR

Model: Mohr-Coulomb
Unit Weight: 86 pcf
Cohesion': 0 psf
Phi': 22.7 °
Phi-B: 0 °

Clay

Model: Mohr-Coulomb
Unit Weight: 125 pcf
Cohesion': 0 psf
Phi': 28 °
Phi-B: 0 °

Drainage Layer

Model: Mohr-Coulomb
Unit Weight: 115 pcf
Cohesion': 0 psf
Phi': 30 °
Phi-B: 0 °

Geosynthetics

Model: Mohr-Coulomb
Unit Weight: 58 pcf
Cohesion': 0 psf
Phi': 24.3 °
Phi-B: 0 °

Subbase

Model: Mohr-Coulomb
Unit Weight: 120 pcf
Cohesion': 0 psf
Phi': 30 °
Phi-B: 0 °

Slip Surface Limits

Left Coordinate: (0, 870) ft
Right Coordinate: (483.9, 803.9) ft

Slip Surface Block

Left Grid

Upper Left: (173.66, 804.44) ft
Lower Left: (173.65, 804.32) ft
Lower Right: (184.43, 804.28) ft

X Increments: 15
 Y Increments: 3
 Starting Angle: 115 °
 Ending Angle: 135 °
 Angle Increments: 5

Right Grid

Upper Left: (369.03, 803.46) ft
 Lower Left: (369.04, 803.34) ft
 Lower Right: (379.14, 803.32) ft
 X Increments: 15
 Y Increments: 3
 Starting Angle: 0 °
 Ending Angle: 45 °
 Angle Increments: 5

Points

	X (ft)	Y (ft)
Point 1	0	780
Point 2	483.9	780
Point 3	0	805.2
Point 4	483.9	802.9
Point 5	483.9	800.9
Point 6	0	803.2
Point 7	0	870
Point 8	112.5	870
Point 9	379.2	803.3
Point 10	0	806.2
Point 11	375.1	804.3
Point 12	483.9	803.9
Point 13	0	805.3
Point 14	483.9	803
Point 15	379.2	803.4

Regions

	Material	Points	Area (ft ²)
Region 1	Subbase	1,6,5,2	10,670
Region 2	Clay	6,3,9,4,5	944.17
Region 3	Geosynthetics	3,13,15,14,4,9	48.39
Region 4	Drainage Layer	13,10,11,12,14,15	430.8
Region 5	CCR	10,7,8,11	15,661

Current Slip Surface

Slip Surface: 52,648
 F of S: 2.063
 Volume: 6,571.6975 ft³
 Weight: 569,769.11 lbs
 Resisting Force: 243,018.44 lbs

Activating Force: 117,793.02 lbs
 F of S Rank (Analysis): 1 of 147,456 slip surfaces
 F of S Rank (Query): 1 of 147,456 slip surfaces
 Exit: (375.01939, 804.32017) ft
 Entry: (112.30933, 870) ft
 Radius: 124.18106 ft
 Center: (255.97976, 886.41996) ft

Slip Slices

	X (ft)	Y (ft)	PWP (psf)	Base Normal Stress (psf)	Frictional Strength (psf)	Cohesive Strength (psf)
Slice 1	112.40467	869.90467	0	6.8170337	2.8516269	0
Slice 2	113.3717	868.93763	0	60.372004	25.254156	0
Slice 3	115.11511	867.19423	0	153.84788	64.355961	0
Slice 4	116.85851	865.45082	0	247.32375	103.45777	0
Slice 5	118.60191	863.70742	0	340.79962	142.55957	0
Slice 6	120.34532	861.96402	0	434.2755	181.66138	0
Slice 7	122.08872	860.22061	0	527.75137	220.76318	0
Slice 8	123.83212	858.47721	0	621.22724	259.86499	0
Slice 9	125.57553	856.73381	0	714.70312	298.96679	0
Slice 10	127.31893	854.9904	0	808.17899	338.0686	0
Slice 11	129.06233	853.247	0	901.65487	377.1704	0
Slice 12	130.80574	851.5036	0	995.13074	416.27221	0
Slice 13	132.54914	849.76019	0	1,088.6066	455.37401	0
Slice 14	134.29254	848.01679	0	1,182.0825	494.47582	0
Slice 15	136.03595	846.27339	0	1,275.5584	533.57762	0
Slice 16	137.77935	844.52998	0	1,369.0342	572.67942	0
Slice 17	139.52275	842.78658	0	1,462.5101	611.78123	0
Slice 18	141.26616	841.04318	0	1,555.986	650.88303	0
Slice 19	143.00956	839.29977	0	1,649.4619	689.98484	0
Slice 20	144.75296	837.55637	0	1,742.9377	729.08664	0
Slice 21	146.49637	835.81297	0	1,836.4136	768.18845	0
Slice 22	148.23977	834.06956	0	1,929.8895	807.29025	0
Slice 23	149.98317	832.32616	0	2,023.3653	846.39206	0
Slice 24	151.72658	830.58276	0	2,116.8412	885.49386	0
Slice 25	153.46998	828.83935	0	2,210.3171	924.59567	0

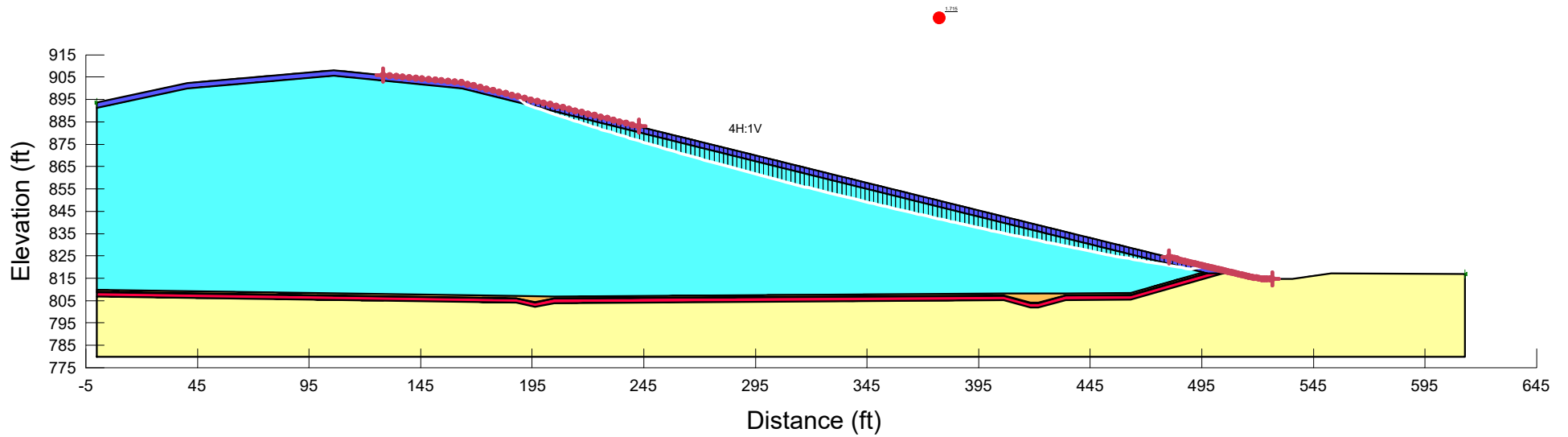
Slice 26	155.21338	827.09595	0	2,303.793	963.69747	0
Slice 27	156.95679	825.35255	0	2,397.2688	1,002.7993	0
Slice 28	158.70019	823.60914	0	2,490.7447	1,041.9011	0
Slice 29	160.44359	821.86574	0	2,584.2206	1,081.0029	0
Slice 30	162.187	820.12234	0	2,677.6965	1,120.1047	0
Slice 31	163.9304	818.37893	0	2,771.1723	1,159.2065	0
Slice 32	165.6738	816.63553	0	2,864.6482	1,198.3083	0
Slice 33	167.41721	814.89213	0	2,958.1241	1,237.4101	0
Slice 34	169.16061	813.14872	0	3,051.6	1,276.5119	0
Slice 35	170.90401	811.40532	0	3,145.0758	1,315.6137	0
Slice 36	172.64742	809.66192	0	3,238.5517	1,354.7155	0
Slice 37	174.39082	807.91851	0	3,332.0276	1,393.8173	0
Slice 38	176.13422	806.17511	0	3,425.5034	1,432.9191	0
Slice 39	177.45332	804.85601	0	3,295.7974	1,902.8295	0
Slice 40	178.81192	804.37175	0	4,204.9245	1,898.5962	0
Slice 41	180.60202	804.33032	0	4,201.5161	1,897.0573	0
Slice 42	182.35981	804.32121	0	4,164.5095	1,880.3481	0
Slice 43	184.1176	804.31209	0	4,127.5028	1,863.639	0
Slice 44	185.87539	804.30297	0	4,090.4962	1,846.9298	0
Slice 45	187.63318	804.29386	0	4,053.4895	1,830.2207	0
Slice 46	189.39097	804.28474	0	4,016.4828	1,813.5115	0
Slice 47	191.14876	804.27562	0	3,979.4762	1,796.8024	0
Slice 48	192.90655	804.2665	0	3,942.4695	1,780.0932	0
Slice 49	194.66434	804.25739	0	3,905.4628	1,763.3841	0
Slice 50	196.42213	804.24827	0	3,868.4562	1,746.6749	0
Slice 51	198.17992	804.23915	0	3,831.4495	1,729.9658	0
Slice	199.93771	804.23004	0	3,794.4429	1,713.2566	0







52						
Slice 53	201.6955	804.22092	0	3,757.4362	1,696.5475	0
Slice 54	203.45329	804.2118	0	3,720.4295	1,679.8383	0
Slice 55	205.21108	804.20268	0	3,683.4229	1,663.1292	0
Slice 56	206.96886	804.19357	0	3,646.4162	1,646.42	0
Slice 57	208.72665	804.18445	0	3,609.4095	1,629.7109	0
Slice 58	210.48444	804.17533	0	3,572.4029	1,613.0017	0
Slice 59	212.24223	804.16622	0	3,535.3962	1,596.2926	0
Slice 60	214.00002	804.1571	0	3,498.3895	1,579.5834	0
Slice 61	215.75781	804.14798	0	3,461.3829	1,562.8743	0
Slice 62	217.5156	804.13886	0	3,424.3762	1,546.1652	0
Slice 63	219.27339	804.12975	0	3,387.3696	1,529.456	0
Slice 64	221.03118	804.12063	0	3,350.3629	1,512.7469	0
Slice 65	222.78897	804.11151	0	3,313.3562	1,496.0377	0
Slice 66	224.54676	804.1024	0	3,276.3496	1,479.3286	0
Slice 67	226.30455	804.09328	0	3,239.3429	1,462.6194	0
Slice 68	228.06234	804.08416	0	3,202.3362	1,445.9103	0
Slice 69	229.82013	804.07505	0	3,165.3296	1,429.2011	0
Slice 70	231.57792	804.06593	0	3,128.3229	1,412.492	0
Slice 71	233.33571	804.05681	0	3,091.3163	1,395.7828	0
Slice 72	235.0935	804.04769	0	3,054.3096	1,379.0737	0
Slice 73	236.85129	804.03858	0	3,017.3029	1,362.3645	0
Slice 74	238.60908	804.02946	0	2,980.2963	1,345.6554	0
Slice 75	240.36687	804.02034	0	2,943.2896	1,328.9462	0
Slice 76	242.12466	804.01123	0	2,906.2829	1,312.2371	0
Slice 77	243.88245	804.00211	0	2,869.2763	1,295.5279	0
Slice 78	245.64024	803.99299	0	2,832.2696	1,278.8188	0

Slice 79	247.39803	803.98387	0	2,795.2629	1,262.1096	0
Slice 80	249.15582	803.97476	0	2,758.2563	1,245.4005	0
Slice 81	250.91361	803.96564	0	2,721.2496	1,228.6913	0
Slice 82	252.6714	803.95652	0	2,684.243	1,211.9822	0
Slice 83	254.42919	803.94741	0	2,647.2363	1,195.273	0
Slice 84	256.18698	803.93829	0	2,610.2296	1,178.5639	0
Slice 85	257.94477	803.92917	0	2,573.223	1,161.8547	0
Slice 86	259.70256	803.92005	0	2,536.2163	1,145.1456	0
Slice 87	261.46035	803.91094	0	2,499.2096	1,128.4364	0
Slice 88	263.21814	803.90182	0	2,462.203	1,111.7273	0
Slice 89	264.97593	803.8927	0	2,425.1963	1,095.0181	0
Slice 90	266.73372	803.88359	0	2,388.1897	1,078.309	0
Slice 91	268.49151	803.87447	0	2,351.183	1,061.5998	0
Slice 92	270.2493	803.86535	0	2,314.1763	1,044.8907	0
Slice 93	272.00709	803.85623	0	2,277.1697	1,028.1815	0
Slice 94	273.76488	803.84712	0	2,240.163	1,011.4724	0
Slice 95	275.52267	803.838	0	2,203.1563	994.76323	0
Slice 96	277.28046	803.82888	0	2,166.1497	978.05408	0
Slice 97	279.03825	803.81977	0	2,129.143	961.34493	0
Slice 98	280.79604	803.81065	0	2,092.1363	944.63578	0
Slice 99	282.55383	803.80153	0	2,055.1297	927.92663	0
Slice 100	284.31162	803.79241	0	2,018.123	911.21749	0
Slice 101	286.06941	803.7833	0	1,981.1164	894.50834	0
Slice 102	287.8272	803.77418	0	1,944.1097	877.79919	0
Slice 103	289.58499	803.76506	0	1,907.103	861.09004	0
Slice 104	291.34277	803.75595	0	1,870.0964	844.38089	0

Slice 105	293.10056	803.74683	0	1,833.0897	827.67174	0
Slice 106	294.85835	803.73771	0	1,796.083	810.96259	0
Slice 107	296.61614	803.72859	0	1,759.0764	794.25344	0
Slice 108	298.37393	803.71948	0	1,722.0697	777.54429	0
Slice 109	300.13172	803.71036	0	1,685.0631	760.83514	0
Slice 110	301.88951	803.70124	0	1,648.0564	744.12599	0
Slice 111	303.6473	803.69213	0	1,611.0497	727.41684	0
Slice 112	305.40509	803.68301	0	1,574.0431	710.7077	0
Slice 113	307.16288	803.67389	0	1,537.0364	693.99855	0
Slice 114	308.92067	803.66477	0	1,500.0297	677.2894	0
Slice 115	310.67846	803.65566	0	1,463.0231	660.58025	0
Slice 116	312.43625	803.64654	0	1,426.0164	643.8711	0
Slice 117	314.19404	803.63742	0	1,389.0097	627.16195	0
Slice 118	315.95183	803.62831	0	1,352.0031	610.4528	0
Slice 119	317.70962	803.61919	0	1,314.9964	593.74365	0
Slice 120	319.46741	803.61007	0	1,277.9898	577.0345	0
Slice 121	321.2252	803.60096	0	1,240.9831	560.32535	0
Slice 122	322.98299	803.59184	0	1,203.9764	543.6162	0
Slice 123	324.74078	803.58272	0	1,166.9698	526.90706	0
Slice 124	326.49857	803.5736	0	1,129.9631	510.19791	0
Slice 125	328.25636	803.56449	0	1,092.9564	493.48876	0
Slice 126	330.01415	803.55537	0	1,055.9498	476.77961	0
Slice 127	331.77194	803.54625	0	1,018.9431	460.07046	0
Slice 128	333.52973	803.53714	0	981.93646	443.36131	0
Slice 129	335.28752	803.52802	0	944.92979	426.65216	0
Slice 130	337.04531	803.5189	0	907.92313	409.94301	0
Slice	338.8031	803.50978	0	870.91647	393.23386	0

131						
Slice 132	340.56089	803.50067	0	833.9098	376.52471	0
Slice 133	342.31868	803.49155	0	796.90314	359.81556	0
Slice 134	344.07647	803.48243	0	759.89648	343.10642	0
Slice 135	345.83426	803.47332	0	722.88981	326.39727	0
Slice 136	347.59205	803.4642	0	685.88315	309.68812	0
Slice 137	349.34984	803.45508	0	648.87649	292.97897	0
Slice 138	351.10763	803.44596	0	611.86982	276.26982	0
Slice 139	352.86542	803.43685	0	574.86316	259.56067	0
Slice 140	354.62321	803.42773	0	537.8565	242.85152	0
Slice 141	356.381	803.41861	0	500.84983	226.14237	0
Slice 142	358.13879	803.4095	0	463.84317	209.43322	0
Slice 143	359.89658	803.40038	0	426.83651	192.72407	0
Slice 144	361.65437	803.39126	0	389.82984	176.01492	0
Slice 145	363.41216	803.38214	0	352.82318	159.30577	0
Slice 146	365.16995	803.37303	0	315.81652	142.59663	0
Slice 147	366.92774	803.36391	0	278.80986	125.88748	0
Slice 148	368.68553	803.35479	0	241.80319	109.17833	0
Slice 149	370.44332	803.34568	0	204.79653	92.469178	0
Slice 150	372.20111	803.33656	0	167.78987	75.760029	0
Slice 151	373.17588	803.38085	0	162.70935	73.466091	0
Slice 152	374.12637	803.86515	0	82.91754	47.872464	0
Slice 153	375.00019	804.31039	0	1.398867	0.58515874	0



Color	Name	Model	Unit Weight (pcf)	Cohesion' (psf)	Phi' (°)
	CCR	Mohr-Coulomb	86	0	22.7
	Clay	Mohr-Coulomb	125	0	28
	Drainage Layer	Mohr-Coulomb	115	0	30
	Final Cover	Mohr-Coulomb	120	0	30
	Geosynthetics	Mohr-Coulomb	58	0	24.3
	Subbase	Mohr-Coulomb	120	0	30

Title: Columbia Mod 10-11 Final Grade
 Name: 2_Optimized Circular
 Method: Bishop
 Last Edited By: Suchomel, Brandon

F of S: 1.715, F of S Rank (Analysis): 1 of 15,130 slip surfaces
 Last Solved Date: 5/4/2022, Last Solved Time: 6:09:49 PM

2_Optimized Circular

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File Information

File Version: 8.16
Title: Columbia Mod 10-11 Final Grade
Created By: Suchomel, Brandon
Last Edited By: Suchomel, Brandon
Revision Number: 76
Date: 5/4/2022
Time: 6:09:17 PM
Tool Version: 8.16.3.14580
File Name: Columbia Mod 10-11 Final Grade.gsz
Directory: I:\25220183.00\Data and Calculations_Issued for Permitting POO Geotech Calculations\Slope Stability\
Last Solved Date: 5/4/2022
Last Solved Time: 6:09:49 PM

Project Settings

Length(L) Units: Feet
Time(t) Units: Seconds
Force(F) Units: Pounds
Pressure(p) Units: psf
Strength Units: psf
Unit Weight of Water: 62.4 pcf
View: 2D
Element Thickness: 1

Analysis Settings

2_Optimized Circular

Kind: SLOPE/W
Method: Bishop
Settings
 PWP Conditions Source: (none)
Slip Surface
 Direction of movement: Left to Right
 Use Passive Mode: No
 Slip Surface Option: Entry and Exit
 Critical slip surfaces saved: 10
 Resisting Side Maximum Convex Angle: 1 °
 Driving Side Maximum Convex Angle: 5 °
 Optimize Critical Slip Surface Location: Yes
 Critical Slip Surface Optimizations
 Maximum Iterations: 2,000
 Convergence Tolerance: 1e-007
 Starting Points: 8
 Ending Points: 16
 Complete Passes per Insertion: 1

Tension Crack

Tension Crack Option: (none)

F of S Distribution

F of S Calculation Option: Constant

Advanced

Number of Slices: 150

F of S Tolerance: 0.001

Minimum Slip Surface Depth: 0.1 ft

Materials

CCR

Model: Mohr-Coulomb

Unit Weight: 86 pcf

Cohesion': 0 psf

Phi': 22.7 °

Phi-B: 0 °

Clay

Model: Mohr-Coulomb

Unit Weight: 125 pcf

Cohesion': 0 psf

Phi': 28 °

Phi-B: 0 °

Drainage Layer

Model: Mohr-Coulomb

Unit Weight: 115 pcf

Cohesion': 0 psf

Phi': 30 °

Phi-B: 0 °

Geosynthetics

Model: Mohr-Coulomb

Unit Weight: 58 pcf

Cohesion': 0 psf

Phi': 24.3 °

Phi-B: 0 °

Subbase

Model: Mohr-Coulomb

Unit Weight: 120 pcf

Cohesion': 0 psf

Phi': 30 °

Phi-B: 0 °

Final Cover

Model: Mohr-Coulomb

Unit Weight: 120 pcf

Cohesion': 0 psf

Phi': 30 °

Phi-B: 0 °

Slip Surface Entry and Exit

Left Projection: Range

Left-Zone Left Coordinate: (128.23053, 906.01) ft

Left-Zone Right Coordinate: (242.77011, 883.007) ft

Left-Zone Increment: 40

Right Projection: Range

Right-Zone Left Coordinate: (480.36, 824.4345) ft

Right-Zone Right Coordinate: (526.61, 814.8) ft

Right-Zone Increment: 40

Radius Increments: 8

Slip Surface Limits

Left Coordinate: (0, 893.8) ft

Right Coordinate: (613, 816.8) ft

Points

	X (ft)	Y (ft)
Point 1	0	808.8
Point 2	187.7	806
Point 3	196.4	804.2
Point 4	205.1	805.9
Point 5	406.3	807.2
Point 6	418.1	803.9
Point 7	421.7	803.9
Point 8	433.9	807.3
Point 9	463	807.5
Point 10	497.4	817.3
Point 11	0	806.8
Point 12	187.7	804
Point 13	196.4	802.2
Point 14	205.1	803.9
Point 15	406.3	805.2
Point 16	418.1	801.9
Point 17	421.7	801.9
Point 18	433.9	805.3
Point 19	463	805.5
Point 20	504.6	817.3
Point 21	0	809.8
Point 22	187.7	807
Point 23	205.1	806.9
Point 24	406.3	808.2
Point 25	433.9	808.3
Point 26	463	808.5
Point 27	494	817.3
Point 28	0	891.3
Point 29	40.4	900
Point 30	106.1	905.7

Point 31	163.7	900
Point 32	0	893.8
Point 33	40.4	902.5
Point 34	106.1	908.2
Point 35	163.7	902.5
Point 36	509.3	817.3
Point 37	521.2	814.8
Point 38	535.6	814.8
Point 39	553.1	817.2
Point 40	613	816.8
Point 41	0	780
Point 42	613	780
Point 43	497	817.3
Point 44	0	808.9
Point 45	187.7	806.1
Point 46	196.4	804.3
Point 47	205.1	806
Point 48	406.3	807.3
Point 49	418.1	804
Point 50	421.7	804
Point 51	433.9	807.4
Point 52	463	807.6

Regions

	Material	Points	Area (ft ²)
Region 1	Subbase	41,11,12,13,14,15,16,17,18,19,20,36,37,38,39,40,42	16,750
Region 2	Clay	11,1,2,3,4,5,6,7,8,9,10,20,19,18,17,16,15,14,13,12	1,002.9
Region 3	Geosynthetics	1,44,45,46,47,48,49,50,51,52,43,10,9,8,7,6,5,4,3,2	49.96
Region 4	Drainage Layer	44,21,22,23,24,25,26,27,43,52,51,50,49,48,47,46,45	512.68
Region 5	CCR	21,28,29,30,31,10,43,27,26,25,24,23,22	31,970
Region 6	Final Cover	28,32,33,34,35,36,20,10,31,30,29	1,333.3

Current Slip Surface

Slip Surface: 15,130

F of S: 1.715

Volume: 2,057.5599 ft³

Weight: 205,107.91 lbs

Resisting Moment: 1.9773823e+008 lbs-ft

Activating Moment: 1.1529957e+008 lbs-ft

F of S Rank (Analysis): 1 of 15,130 slip surfaces

F of S Rank (Query): 1 of 15,130 slip surfaces

Exit: (496.40689, 820.47851) ft

Entry: (187.91178, 896.53112) ft

Radius: 135.32146 ft

Center: (884.20908, 3,149.1166) ft

Slip Slices

	X (ft)	Y (ft)	PWP	Base Normal Stress	Frictional Strength	Cohesive Strength
--	--------	--------	-----	--------------------	---------------------	-------------------

			(psf)	(psf)	(psf)	(psf)
Slice 1	188.94788	895.64148	0	59.043882	34.089001	0
Slice 2	191.02008	893.8622	0	177.13165	102.267	0
Slice 3	192.136	892.90403	0	255.19769	106.75151	0
Slice 4	193.30095	892.46224	0	297.05904	124.26249	0
Slice 5	195.47124	891.71573	0	313.92727	131.31862	0
Slice 6	197.64153	890.96921	0	330.79551	138.37476	0
Slice 7	199.81182	890.2227	0	347.66374	145.43089	0
Slice 8	201.98211	889.47619	0	364.53198	152.48703	0
Slice 9	204.1524	888.72967	0	381.40021	159.54317	0
Slice 10	206.32269	887.98316	0	398.26845	166.5993	0
Slice 11	208.45878	887.27447	0	415.11896	173.64802	0
Slice 12	210.56069	886.60361	0	427.38749	178.78006	0
Slice 13	212.6626	885.93275	0	439.65601	183.91209	0
Slice 14	214.76451	885.2619	0	451.92453	189.04413	0
Slice 15	216.86642	884.59104	0	464.19306	194.17616	0
Slice 16	218.96833	883.92018	0	476.46158	199.3082	0
Slice 17	221.07024	883.24932	0	488.7301	204.44023	0
Slice 18	223.17215	882.57846	0	500.99863	209.57227	0
Slice 19	225.27406	881.9076	0	513.26715	214.7043	0
Slice 20	227.37597	881.23675	0	525.53567	219.83633	0
Slice 21	229.47788	880.56589	0	537.8042	224.96837	0
Slice 22	231.57979	879.89503	0	550.07272	230.1004	0
Slice 23	233.66565	879.251	0	563.18804	235.58666	0
Slice 24	235.73548	878.6338	0	571.84604	239.20838	0
Slice 25	237.8053	878.0166	0	580.50403	242.83009	0
Slice 26	239.87513	877.3994	0	589.16202	246.45181	0
Slice 27	241.94495	876.7822	0	597.82001	250.07353	0
Slice 28	244.01478	876.165	0	606.478	253.69524	0
Slice 29	246.0846	875.5478	0	615.136	257.31696	0
Slice 30	248.15443	874.9306	0	623.79399	260.93868	0

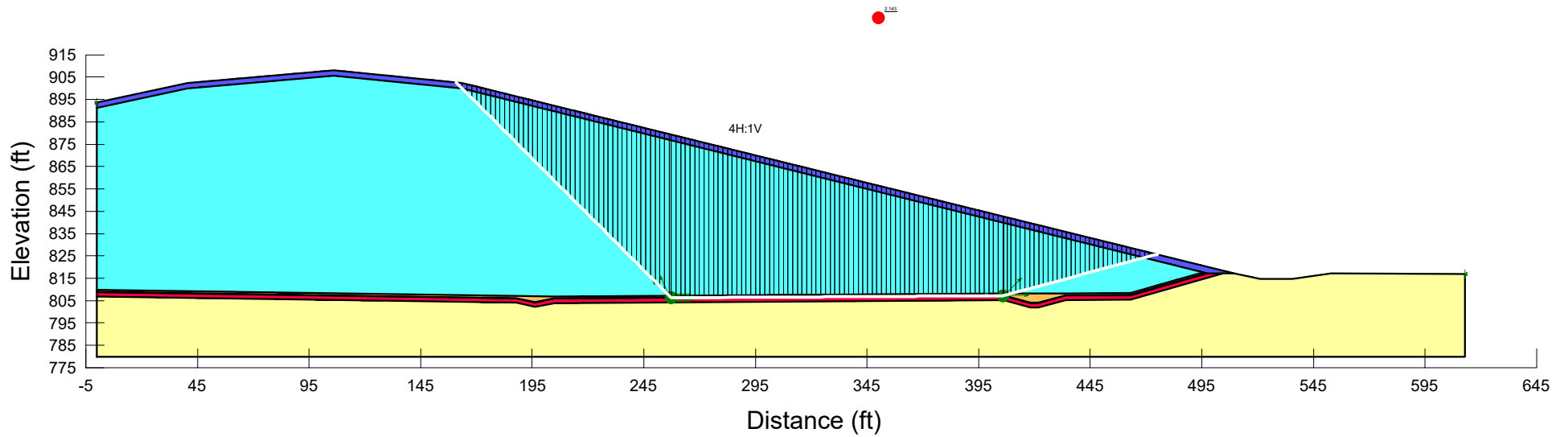
Slice 31	250.22425	874.3134	0	632.45198	264.56039	0
Slice 32	252.29407	873.6962	0	641.10997	268.18211	0
Slice 33	254.3639	873.079	0	649.76797	271.80383	0
Slice 34	256.43372	872.4618	0	658.42596	275.42554	0
Slice 35	258.50355	871.8446	0	667.08395	279.04726	0
Slice 36	260.57337	871.2274	0	675.74194	282.66898	0
Slice 37	262.6432	870.6102	0	684.39994	286.29069	0
Slice 38	264.76104	870.0051	0	694.99471	290.72258	0
Slice 39	266.9269	869.4121	0	699.84528	292.75162	0
Slice 40	269.09277	868.8191	0	704.69585	294.78066	0
Slice 41	271.25863	868.2261	0	709.54641	296.80969	0
Slice 42	273.42449	867.6331	0	714.39698	298.83873	0
Slice 43	275.59036	867.0401	0	719.24755	300.86777	0
Slice 44	277.67848	866.47383	0	724.38225	303.01566	0
Slice 45	279.68887	865.9343	0	728.01062	304.53344	0
Slice 46	281.69926	865.39476	0	731.63899	306.05122	0
Slice 47	283.70965	864.85523	0	735.26736	307.569	0
Slice 48	285.72004	864.31569	0	738.89573	309.08678	0
Slice 49	287.73043	863.77616	0	742.5241	310.60456	0
Slice 50	289.74082	863.23662	0	746.15247	312.12234	0
Slice 51	291.75121	862.69709	0	749.78083	313.64012	0
Slice 52	293.7616	862.15755	0	753.4092	315.1579	0
Slice 53	295.77199	861.61802	0	757.03757	316.67568	0
Slice 54	297.78237	861.07848	0	760.66594	318.19346	0
Slice 55	299.79276	860.53895	0	764.29431	319.71124	0
Slice 56	301.80315	859.99941	0	767.92268	321.22902	0
Slice	303.81354	859.45988	0	771.55105	322.7468	0







57						
Slice 58	305.82393	858.92034	0	775.17942	324.26458	0
Slice 59	307.83432	858.38081	0	778.80779	325.78236	0
Slice 60	309.84471	857.84127	0	782.43616	327.30014	0
Slice 61	311.8551	857.30174	0	786.06453	328.81792	0
Slice 62	313.86549	856.7622	0	789.6929	330.3357	0
Slice 63	315.87588	856.22267	0	793.32127	331.85347	0
Slice 64	317.93207	855.6982	0	799.58807	334.47494	0
Slice 65	320.03408	855.18881	0	798.96026	334.21232	0
Slice 66	322.13609	854.67942	0	798.33244	333.94969	0
Slice 67	324.2381	854.17003	0	797.70462	333.68707	0
Slice 68	326.3401	853.66064	0	797.07681	333.42445	0
Slice 69	328.44211	853.15125	0	796.44899	333.16183	0
Slice 70	330.54412	852.64185	0	795.82117	332.89921	0
Slice 71	332.64613	852.13246	0	795.19336	332.63659	0
Slice 72	334.74813	851.62307	0	794.56554	332.37397	0
Slice 73	336.85014	851.11368	0	793.93772	332.11134	0
Slice 74	338.95215	850.60429	0	793.30991	331.84872	0
Slice 75	341.05416	850.0949	0	792.68209	331.5861	0
Slice 76	343.08943	849.60487	0	792.40744	331.47121	0
Slice 77	345.05798	849.13423	0	791.29902	331.00755	0
Slice 78	347.02653	848.66358	0	790.19061	330.54389	0
Slice 79	348.99507	848.19292	0	789.0822	330.08023	0
Slice 80	350.96362	847.72227	0	787.97378	329.61657	0
Slice 81	352.93216	847.25162	0	786.86537	329.15291	0
Slice 82	354.90071	846.78098	0	785.75696	328.68925	0
Slice 83	356.86926	846.31033	0	784.64854	328.22559	0

Slice 84	358.89006	845.83546	0	784.28138	328.07201	0
Slice 85	360.96313	845.35638	0	781.76363	327.01881	0
Slice 86	363.0362	844.87731	0	779.24588	325.96561	0
Slice 87	365.10927	844.39823	0	776.72813	324.91241	0
Slice 88	367.18234	843.91915	0	774.21037	323.85921	0
Slice 89	369.2554	843.44007	0	771.69262	322.80602	0
Slice 90	371.32847	842.96099	0	769.17487	321.75282	0
Slice 91	373.40154	842.48192	0	766.65712	320.69962	0
Slice 92	375.47461	842.00284	0	764.13936	319.64642	0
Slice 93	377.52585	841.53663	0	762.36799	318.90544	0
Slice 94	379.55527	841.08329	0	758.62269	317.33874	0
Slice 95	381.58468	840.62994	0	754.87739	315.77205	0
Slice 96	383.6141	840.1766	0	751.13208	314.20536	0
Slice 97	385.64352	839.72326	0	747.38678	312.63866	0
Slice 98	387.67293	839.26991	0	743.64148	311.07197	0
Slice 99	389.70235	838.81657	0	739.89618	309.50528	0
Slice 100	391.73177	838.36323	0	736.15088	307.93858	0
Slice 101	393.76119	837.90989	0	732.40558	306.37189	0
Slice 102	395.7906	837.45654	0	728.66028	304.8052	0
Slice 103	397.82002	837.0032	0	724.91498	303.2385	0
Slice 104	399.84944	836.54986	0	721.16968	301.67181	0
Slice 105	401.87885	836.09651	0	717.42438	300.10512	0
Slice 106	403.90827	835.64317	0	713.67908	298.53842	0
Slice 107	405.93372	835.20322	0	710.95565	297.39919	0
Slice 108	407.95521	834.77667	0	705.16772	294.97805	0
Slice 109	409.9767	834.35013	0	699.37979	292.5569	0

Slice 110	411.99819	833.92358	0	693.59187	290.13576	0
Slice 111	414.04037	833.4998	0	688.2659	287.90786	0
Slice 112	416.10325	833.07881	0	681.17935	284.94349	0
Slice 113	418.16613	832.65781	0	674.0928	281.97913	0
Slice 114	420.22901	832.23682	0	667.00625	279.01476	0
Slice 115	422.29189	831.81582	0	659.9197	276.05039	0
Slice 116	424.35477	831.39483	0	652.83315	273.08602	0
Slice 117	426.41765	830.97383	0	645.7466	270.12165	0
Slice 118	428.48053	830.55284	0	638.66005	267.15729	0
Slice 119	430.54341	830.13184	0	631.5735	264.19292	0
Slice 120	432.60629	829.71085	0	624.48695	261.22855	0
Slice 121	434.66916	829.28985	0	617.4004	258.26418	0
Slice 122	436.73204	828.86886	0	610.31385	255.29981	0
Slice 123	438.79492	828.44786	0	603.2273	252.33545	0
Slice 124	440.8578	828.02687	0	596.14075	249.37108	0
Slice 125	442.92068	827.60587	0	589.0542	246.40671	0
Slice 126	444.98356	827.18488	0	581.96765	243.44234	0
Slice 127	447.04644	826.76388	0	574.8811	240.47798	0
Slice 128	449.10932	826.34289	0	567.79455	237.51361	0
Slice 129	451.1722	825.92189	0	560.708	234.54924	0
Slice 130	453.23508	825.5009	0	553.62146	231.58487	0
Slice 131	455.25753	825.11339	0	547.84698	229.16936	0
Slice 132	457.23956	824.75938	0	536.83751	224.56399	0
Slice 133	459.22159	824.40536	0	525.82804	219.95863	0
Slice 134	461.20362	824.05135	0	514.81857	215.35327	0
Slice 135	463.18565	823.69734	0	503.8091	210.74791	0
Slice	465.16768	823.34332	0	492.79962	206.14255	0

136						
Slice 137	467.14971	822.98931	0	481.79015	201.53719	0
Slice 138	469.13453	822.64483	0	471.04949	197.04427	0
Slice 139	471.12216	822.30988	0	458.32507	191.72153	0
Slice 140	473.10978	821.97494	0	445.60064	186.39879	0
Slice 141	475.09741	821.63999	0	432.87622	181.07605	0
Slice 142	477.08503	821.30505	0	420.1518	175.7533	0
Slice 143	479.07266	820.9701	0	407.42737	170.43056	0
Slice 144	481.06028	820.63515	0	394.70295	165.10782	0
Slice 145	483.0479	820.30021	0	381.97853	159.78508	0
Slice 146	485.03553	819.96526	0	369.2541	154.46234	0
Slice 147	487.02315	819.63032	0	356.52968	149.1396	0
Slice 148	489.01078	819.29537	0	343.80526	143.81685	0
Slice 149	491.07519	819.35375	0	315.06893	181.90513	0
Slice 150	493.21107	819.80433	0	188.85259	109.03409	0
Slice 151	495.34162	820.25378	0	62.950863	36.344698	0



Color	Name	Model	Unit Weight (pcf)	Cohesion' (psf)	Phi' (°)
	CCR	Mohr-Coulomb	86	0	22.7
	Clay	Mohr-Coulomb	125	0	28
	Drainage Layer	Mohr-Coulomb	115	0	30
	Final Cover	Mohr-Coulomb	120	0	30
	Geosynthetics	Mohr-Coulomb	58	0	24.3
	Subbase	Mohr-Coulomb	120	0	30

Title: Columbia Mod 10-11 Final Grade
 Name: 3_Block
 Method: Janbu
 Last Edited By: Suchomel, Brandon

F of S: 2.143, F of S Rank (Analysis): 1 of 65,536 slip surfaces
 Last Solved Date: 5/4/2022, Last Solved Time: 6:10:13 PM

3_Block

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File Information

File Version: 8.16
Title: Columbia Mod 10-11 Final Grade
Created By: Suchomel, Brandon
Last Edited By: Suchomel, Brandon
Revision Number: 76
Date: 5/4/2022
Time: 6:09:17 PM
Tool Version: 8.16.3.14580
File Name: Columbia Mod 10-11 Final Grade.gsz
Directory: I:\25220183.00\Data and Calculations_Issued for Permitting POO Geotech Calculations\Slope Stability\
Last Solved Date: 5/4/2022
Last Solved Time: 6:10:13 PM

Project Settings

Length(L) Units: Feet
Time(t) Units: Seconds
Force(F) Units: Pounds
Pressure(p) Units: psf
Strength Units: psf
Unit Weight of Water: 62.4 pcf
View: 2D
Element Thickness: 1

Analysis Settings

3_Block

Kind: SLOPE/W
Method: Janbu
Settings
 PWP Conditions Source: (none)
Slip Surface
 Direction of movement: Left to Right
 Use Passive Mode: No
 Slip Surface Option: Block
 Critical slip surfaces saved: 10
 Resisting Side Maximum Convex Angle: 1 °
 Driving Side Maximum Convex Angle: 5 °
 Restrict Block Crossing: No
 Optimize Critical Slip Surface Location: No
 Tension Crack
 Tension Crack Option: (none)
F of S Distribution
 F of S Calculation Option: Constant
Advanced

Number of Slices: 150
F of S Tolerance: 0.001
Minimum Slip Surface Depth: 0.1 ft

Materials

CCR

Model: Mohr-Coulomb
Unit Weight: 86 pcf
Cohesion': 0 psf
Phi': 22.7 °
Phi-B: 0 °

Clay

Model: Mohr-Coulomb
Unit Weight: 125 pcf
Cohesion': 0 psf
Phi': 28 °
Phi-B: 0 °

Drainage Layer

Model: Mohr-Coulomb
Unit Weight: 115 pcf
Cohesion': 0 psf
Phi': 30 °
Phi-B: 0 °

Geosynthetics

Model: Mohr-Coulomb
Unit Weight: 58 pcf
Cohesion': 0 psf
Phi': 24.3 °
Phi-B: 0 °

Subbase

Model: Mohr-Coulomb
Unit Weight: 120 pcf
Cohesion': 0 psf
Phi': 30 °
Phi-B: 0 °

Final Cover

Model: Mohr-Coulomb
Unit Weight: 120 pcf
Cohesion': 0 psf
Phi': 30 °
Phi-B: 0 °

Slip Surface Limits

Left Coordinate: (0, 893.8) ft
Right Coordinate: (613, 816.8) ft

Slip Surface Block

Left Grid

Upper Left: (256.72, 806.35) ft
Lower Left: (256.72, 806.22) ft
Lower Right: (266.56, 806.28) ft
X Increments: 15
Y Increments: 3
Starting Angle: 115 °
Ending Angle: 135 °
Angle Increments: 3

Right Grid

Upper Left: (398.42, 807.26) ft
Lower Left: (398.42, 807.12) ft
Lower Right: (406.38, 807.17) ft
X Increments: 15
Y Increments: 3
Starting Angle: 0 °
Ending Angle: 45 °
Angle Increments: 3

Points

	X (ft)	Y (ft)
Point 1	0	808.8
Point 2	187.7	806
Point 3	196.4	804.2
Point 4	205.1	805.9
Point 5	406.3	807.2
Point 6	418.1	803.9
Point 7	421.7	803.9
Point 8	433.9	807.3
Point 9	463	807.5
Point 10	497.4	817.3
Point 11	0	806.8
Point 12	187.7	804
Point 13	196.4	802.2
Point 14	205.1	803.9
Point 15	406.3	805.2
Point 16	418.1	801.9
Point 17	421.7	801.9
Point 18	433.9	805.3
Point 19	463	805.5
Point 20	504.6	817.3
Point 21	0	809.8
Point 22	187.7	807
Point 23	205.1	806.9
Point 24	406.3	808.2
Point 25	433.9	808.3
Point 26	463	808.5
Point 27	494	817.3

Point 28	0	891.3
Point 29	40.4	900
Point 30	106.1	905.7
Point 31	163.7	900
Point 32	0	893.8
Point 33	40.4	902.5
Point 34	106.1	908.2
Point 35	163.7	902.5
Point 36	509.3	817.3
Point 37	521.2	814.8
Point 38	535.6	814.8
Point 39	553.1	817.2
Point 40	613	816.8
Point 41	0	780
Point 42	613	780
Point 43	497	817.3
Point 44	0	808.9
Point 45	187.7	806.1
Point 46	196.4	804.3
Point 47	205.1	806
Point 48	406.3	807.3
Point 49	418.1	804
Point 50	421.7	804
Point 51	433.9	807.4
Point 52	463	807.6

Regions

	Material	Points	Area (ft ²)
Region 1	Subbase	41,11,12,13,14,15,16,17,18,19,20,36,37,38,39,40,42	16,750
Region 2	Clay	11,1,2,3,4,5,6,7,8,9,10,20,19,18,17,16,15,14,13,12	1,002.9
Region 3	Geosynthetics	1,44,45,46,47,48,49,50,51,52,43,10,9,8,7,6,5,4,3,2	49.96
Region 4	Drainage Layer	44,21,22,23,24,25,26,27,43,52,51,50,49,48,47,46,45	512.68
Region 5	CCR	21,28,29,30,31,10,43,27,26,25,24,23,22	31,970
Region 6	Final Cover	28,32,33,34,35,36,20,10,31,30,29	1,333.3

Current Slip Surface

Slip Surface: 18,298

F of S: 2.143

Volume: 12,851.682 ft³

Weight: 1,137,317.2 lbs

Resisting Force: 483,744.11 lbs

Activating Force: 225,710.24 lbs

F of S Rank (Analysis): 1 of 65,536 slip surfaces

F of S Rank (Query): 1 of 65,536 slip surfaces

Exit: (475.02664, 825.74934) ft

Entry: (160.86254, 902.78079) ft

Radius: 153.63542 ft

Center: (332.11038, 922.03865) ft

Slip Slices

	X (ft)	Y (ft)	PWP (psf)	Base Normal Stress (psf)	Frictional Strength (psf)	Cohesive Strength (psf)
Slice 1	162.28127	901.36206	0	120.84936	69.772411	0
Slice 2	164.75354	898.88979	0	312.2515	130.61763	0
Slice 3	166.86063	896.7827	0	426.57116	178.43858	0
Slice 4	168.96772	894.67562	0	540.89082	226.25953	0
Slice 5	171.0748	892.56853	0	655.21047	274.08048	0
Slice 6	173.18189	890.46145	0	769.53013	321.90143	0
Slice 7	175.28897	888.35436	0	883.84978	369.72237	0
Slice 8	177.39606	886.24727	0	998.16944	417.54332	0
Slice 9	179.50315	884.14019	0	1,112.4891	465.36427	0
Slice 10	181.61023	882.0331	0	1,226.8088	513.18522	0
Slice 11	183.71732	879.92601	0	1,341.1284	561.00617	0
Slice 12	185.82441	877.81893	0	1,455.4481	608.82711	0
Slice 13	187.93149	875.71184	0	1,569.7677	656.64806	0
Slice 14	190.03858	873.60475	0	1,684.0874	704.46901	0
Slice 15	192.14566	871.49767	0	1,798.407	752.28996	0
Slice 16	194.25275	869.39058	0	1,912.7267	800.11091	0
Slice 17	196.35984	867.2835	0	2,027.0463	847.93185	0
Slice 18	198.46692	865.17641	0	2,141.366	895.7528	0
Slice 19	200.57401	863.06932	0	2,255.6857	943.57375	0
Slice 20	202.6811	860.96224	0	2,370.0053	991.3947	0
Slice 21	204.78818	858.85515	0	2,484.325	1,039.2156	0
Slice 22	206.89527	856.74806	0	2,598.6446	1,087.0366	0
Slice 23	209.00235	854.64098	0	2,712.9643	1,134.8575	0
Slice 24	211.10944	852.53389	0	2,827.2839	1,182.6785	0
Slice 25	213.21653	850.42681	0	2,941.6036	1,230.4994	0
Slice 26	215.32361	848.31972	0	3,055.9232	1,278.3204	0
Slice 27	217.4307	846.21263	0	3,170.2429	1,326.1413	0
Slice 28	219.53779	844.10555	0	3,284.5626	1,373.9623	0
Slice 29	221.64487	841.99846	0	3,398.8822	1,421.7832	0


Slice 30	223.75196	839.89137	0	3,513.2019	1,469.6042	0
Slice 31	225.85905	837.78429	0	3,627.5215	1,517.4251	0
Slice 32	227.96613	835.6772	0	3,741.8412	1,565.2461	0
Slice 33	230.07322	833.57012	0	3,856.1608	1,613.067	0
Slice 34	232.1803	831.46303	0	3,970.4805	1,660.888	0
Slice 35	234.28739	829.35594	0	4,084.8002	1,708.7089	0
Slice 36	236.39448	827.24886	0	4,199.1198	1,756.5299	0
Slice 37	238.50156	825.14177	0	4,313.4395	1,804.3508	0
Slice 38	240.60865	823.03468	0	4,427.7591	1,852.1718	0
Slice 39	242.71574	820.9276	0	4,542.0788	1,899.9927	0
Slice 40	244.82282	818.82051	0	4,656.3984	1,947.8137	0
Slice 41	246.92991	816.71343	0	4,770.7181	1,995.6346	0
Slice 42	249.03699	814.60634	0	4,885.0377	2,043.4556	0
Slice 43	251.14408	812.49925	0	4,999.3574	2,091.2765	0
Slice 44	253.25117	810.39217	0	5,113.6771	2,139.0975	0
Slice 45	255.35825	808.28508	0	5,227.9967	2,186.9184	0
Slice 46	256.85891	806.78443	0	5,009.3458	2,892.1472	0
Slice 47	258.3866	806.30899	0	6,344.487	2,864.6457	0
Slice 48	260.51276	806.28732	0	6,343.6373	2,864.2621	0
Slice 49	262.60393	806.30064	0	6,298.1818	2,843.7381	0
Slice 50	264.69511	806.31397	0	6,252.7263	2,823.2142	0
Slice 51	266.78628	806.32729	0	6,207.2708	2,802.6902	0
Slice 52	268.87746	806.34061	0	6,161.8153	2,782.1663	0
Slice 53	270.96863	806.35394	0	6,116.3598	2,761.6423	0
Slice 54	273.0598	806.36726	0	6,070.9043	2,741.1184	0
Slice 55	275.15098	806.38059	0	6,025.4488	2,720.5945	0

Slice 56	277.24215	806.39391	0	5,979.9933	2,700.0705	0
Slice 57	279.33332	806.40723	0	5,934.5378	2,679.5466	0
Slice 58	281.4245	806.42056	0	5,889.0823	2,659.0226	0
Slice 59	283.51567	806.43388	0	5,843.6268	2,638.4987	0
Slice 60	285.60685	806.44721	0	5,798.1713	2,617.9747	0
Slice 61	287.69802	806.46053	0	5,752.7158	2,597.4508	0
Slice 62	289.78919	806.47385	0	5,707.2603	2,576.9268	0
Slice 63	291.88037	806.48718	0	5,661.8048	2,556.4029	0
Slice 64	293.97154	806.5005	0	5,616.3493	2,535.8789	0
Slice 65	296.06271	806.51383	0	5,570.8938	2,515.355	0
Slice 66	298.15389	806.52715	0	5,525.4383	2,494.831	0
Slice 67	300.24506	806.54047	0	5,479.9827	2,474.3071	0
Slice 68	302.33623	806.5538	0	5,434.5272	2,453.7831	0
Slice 69	304.42741	806.56712	0	5,389.0717	2,433.2592	0
Slice 70	306.51858	806.58045	0	5,343.6162	2,412.7352	0
Slice 71	308.60976	806.59377	0	5,298.1607	2,392.2113	0
Slice 72	310.70093	806.60709	0	5,252.7052	2,371.6874	0
Slice 73	312.7921	806.62042	0	5,207.2497	2,351.1634	0
Slice 74	314.88328	806.63374	0	5,161.7942	2,330.6395	0
Slice 75	316.97445	806.64707	0	5,116.3387	2,310.1155	0
Slice 76	319.06562	806.66039	0	5,070.8832	2,289.5916	0
Slice 77	321.1568	806.67371	0	5,025.4277	2,269.0676	0
Slice 78	323.24797	806.68704	0	4,979.9722	2,248.5437	0
Slice 79	325.33915	806.70036	0	4,934.5167	2,228.0197	0
Slice 80	327.43032	806.71369	0	4,889.0612	2,207.4958	0
Slice 81	329.52149	806.72701	0	4,843.6057	2,186.9718	0
Slice	331.61267	806.74033	0	4,798.1502	2,166.4479	0

82						
Slice 83	333.70384	806.75366	0	4,752.6947	2,145.9239	0
Slice 84	335.79501	806.76698	0	4,707.2392	2,125.4	0
Slice 85	337.88619	806.78031	0	4,661.7837	2,104.876	0
Slice 86	339.97736	806.79363	0	4,616.3282	2,084.3521	0
Slice 87	342.06854	806.80695	0	4,570.8727	2,063.8281	0
Slice 88	344.15971	806.82028	0	4,525.4172	2,043.3042	0
Slice 89	346.25088	806.8336	0	4,479.9617	2,022.7802	0
Slice 90	348.34206	806.84692	0	4,434.5062	2,002.2563	0
Slice 91	350.43323	806.86025	0	4,389.0506	1,981.7324	0
Slice 92	352.5244	806.87357	0	4,343.5951	1,961.2084	0
Slice 93	354.61558	806.8869	0	4,298.1396	1,940.6845	0
Slice 94	356.70675	806.90022	0	4,252.6841	1,920.1605	0
Slice 95	358.79792	806.91354	0	4,207.2286	1,899.6366	0
Slice 96	360.8891	806.92687	0	4,161.7731	1,879.1126	0
Slice 97	362.98027	806.94019	0	4,116.3176	1,858.5887	0
Slice 98	365.07145	806.95352	0	4,070.8621	1,838.0647	0
Slice 99	367.16262	806.96684	0	4,025.4066	1,817.5408	0
Slice 100	369.25379	806.98016	0	3,979.9511	1,797.0168	0
Slice 101	371.34497	806.99349	0	3,934.4956	1,776.4929	0
Slice 102	373.43614	807.00681	0	3,889.0401	1,755.9689	0
Slice 103	375.52731	807.02014	0	3,843.5846	1,735.445	0
Slice 104	377.61849	807.03346	0	3,798.1291	1,714.921	0
Slice 105	379.70966	807.04678	0	3,752.6736	1,694.3971	0
Slice 106	381.80084	807.06011	0	3,707.2181	1,673.8731	0
Slice 107	383.89201	807.07343	0	3,661.7626	1,653.3492	0
Slice 108	385.98318	807.08676	0	3,616.3071	1,632.8253	0

Slice 109	388.07436	807.10008	0	3,570.8516	1,612.3013	0
Slice 110	390.16553	807.1134	0	3,525.3961	1,591.7774	0
Slice 111	392.2567	807.12673	0	3,479.9406	1,571.2534	0
Slice 112	394.34788	807.14005	0	3,434.4851	1,550.7295	0
Slice 113	396.43905	807.15338	0	3,389.0296	1,530.2055	0
Slice 114	398.53023	807.1667	0	3,343.5741	1,509.6816	0
Slice 115	400.6214	807.18002	0	3,298.1185	1,489.1576	0
Slice 116	402.71257	807.19335	0	3,252.663	1,468.6337	0
Slice 117	404.80375	807.20667	0	3,207.2075	1,448.1097	0
Slice 118	406.00948	807.25625	0	3,364.1808	1,518.9859	0
Slice 119	406.23482	807.31662	0	3,411.2113	1,969.4637	0
Slice 120	407.11898	807.55353	0	3,361.7917	1,940.9313	0
Slice 121	408.75694	807.99242	0	3,270.2285	1,888.0673	0
Slice 122	410.60729	808.48822	0	3,108.7021	1,300.3983	0
Slice 123	412.67002	809.04093	0	3,012.497	1,260.1548	0
Slice 124	414.73275	809.59364	0	2,916.292	1,219.9114	0
Slice 125	416.79548	810.14634	0	2,820.0869	1,179.6679	0
Slice 126	418.85821	810.69905	0	2,723.8818	1,139.4244	0
Slice 127	420.92094	811.25176	0	2,627.6767	1,099.181	0
Slice 128	422.98367	811.80447	0	2,531.4717	1,058.9375	0
Slice 129	425.0464	812.35717	0	2,435.2666	1,018.6941	0
Slice 130	427.10913	812.90988	0	2,339.0615	978.45063	0
Slice 131	429.17187	813.46259	0	2,242.8564	938.20717	0
Slice 132	431.2346	814.01529	0	2,146.6514	897.96372	0
Slice 133	433.29733	814.568	0	2,050.4463	857.72026	0
Slice 134	435.36006	815.12071	0	1,954.2412	817.47681	0

Slice 135	437.42279	815.67342	0	1,858.0361	777.23335	0
Slice 136	439.48552	816.22612	0	1,761.8311	736.9899	0
Slice 137	441.54825	816.77883	0	1,665.626	696.74645	0
Slice 138	443.61098	817.33154	0	1,569.4209	656.50299	0
Slice 139	445.67371	817.88424	0	1,473.2158	616.25954	0
Slice 140	447.73645	818.43695	0	1,377.0108	576.01608	0
Slice 141	449.79918	818.98966	0	1,280.8057	535.77263	0
Slice 142	451.86191	819.54237	0	1,184.6006	495.52917	0
Slice 143	453.92464	820.09507	0	1,088.3955	455.28572	0
Slice 144	455.98737	820.64778	0	992.19047	415.04227	0
Slice 145	458.0501	821.20049	0	895.9854	374.79881	0
Slice 146	460.11283	821.75319	0	799.78033	334.55536	0
Slice 147	462.17556	822.3059	0	703.57525	294.3119	0
Slice 148	464.23829	822.85861	0	607.37018	254.06845	0
Slice 149	466.30102	823.41132	0	511.1651	213.82499	0
Slice 150	468.36376	823.96402	0	414.96003	173.58154	0
Slice 151	470.33371	824.49187	0	312.26526	180.28643	0
Slice 152	472.21088	824.99486	0	187.35915	108.17186	0
Slice 153	474.08805	825.49784	0	62.453052	36.057286	0



Appendix I
Seepage Potential and Karst Condition Assessment

Seepage Potential and Karst Condition Assessment

The disposal facility is designed and constructed to include storm water run-on and run-off management and leachate collection systems. The liner system is designed and constructed to be above the high groundwater level. There are currently no concerns that storm water, leachate, or groundwater movement will impact the stability of the landfill.

As noted in **Appendix E**, karst features were not observed in the borings within and adjacent to the disposal facility. The borings encountered sandstone bedrock that is not subject to karst conditions. The Wisconsin map of karst and shallow carbonate bedrock in **Appendix E** indicates that karst structures are not located in or near the disposal facility.

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